ABSTRACT

DAWN, WILLIAM C. Sodium Cooled Fast Reactor Simulations with the Finite Element Method. (Under the direction of Scott P. Palmtag and David J. Kropaczek.)

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by William C. Dawn

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Nuclear Engineering

Raleigh, North Carolina

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DEDICATION

To the future of clean energy.

BIOGRAPHY

The author was born in a small town ...

ACKNOWLEDGEMENTS

I would like to thank my advisor for his help.

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LIST OF FIGURES

INTRODUCTION

Let's start with a few paragraph basics, here is how to make **bold**, and *italics*, and *emphasized*. Let's say you need to cite something in your references, simply type \cite{key}, which produces [ER35]. Some other references are [GVL96] and [LK74]. Some PTEX compilers require a second compilation for citations and references to be sorted and matched properly in the resulting document.

Here is a quotation:

Alice, Bob and Carol are boring. Who would even want to know their secret?

Let's say we need to make a list, try this on for size

- 1. NCSU is great
- 2. I like NCSU
- 3. I really hope I can find a job when I graduate!

1.1 Math environments

1.1.1 Equations

There are many different ways to write equations, for example we could put $a^2 + b^2 = c^2$ directly into a sentence. Or we could use the equation environment and do

$$a^2 + b^2 = c^2. (1.1)$$

And from here we can later reference it by simply doing typing \ref{label}, which gives 1.1. However, defining and using equation and figure reference macros will ensure that the equation references are consistent, instead of having Eq. (1), Equation 3, Eqn 4 scattered through the thesis. This template file defines \eref and \fref for this purpose. You can modify the macros to your liking in the YourName-thesis.tex file. For example, the command \eref{label} gives Eq. 1.1.

If you don't need to reference an equation you may simply do this

$$a^2 + b^2 = c^2$$
.

For Greek letters you must go to the math environments, for example α , β , and γ . Let's look at equations that cover multiple lines, none of these equations may be true or mean anything, but so that the reader can get some ideas. In addition I will use some other useful notations like subscripts, superscripts, fractions, etc. One important item of note is that one uses the "ampersand" symbol to line up equations (also look at how I used quotations).

$$\gamma_1 = \alpha^{\beta} + \psi_0 \frac{\psi_1}{\psi_2 + \psi_3}
= \beta_1 + \beta_2 + \dots + \beta_k
\rightarrow E(\gamma_2)$$
(1.2)

Alternatively, one can specify a slightly different environment if none of the equations need to be numbered. Remember that if you are planning on referring to them later on, you must use a "label" statement.

$$\gamma_1 = n^{-1/2} \sum_{i=1}^n \left[h(X_i, \beta_0) - E\{h(X_i, \beta_0)\} \right]$$

$$\rightarrow \hat{q} \pm \frac{\partial \gamma_2}{\partial \beta}.$$

Lastly there may be times in which you want to use a non-italicized word your formula, such as an indicator function that may look like this $I\{\mu_i(1,\beta) > \mu_i(0,\beta)\}$, if so just use the "mbox" statement.

You could use a multiline equation for long equations. The environment is multline. Insert \\ for line breaks.

$$\vec{\cdot} \cdot \vec{\nabla} \psi(\vec{r}, \dot{\cdot}, E) + \Sigma_t(\vec{r}, E) \psi(\vec{r}, \dot{\cdot}, E) =$$

$$\int_{4\pi} d^{\prime\prime} \int_0^{\infty} dE' \Sigma_s(\vec{r}, \dot{\cdot}' \to \dot{\cdot}, E' \to E) \psi(\vec{r}, \dot{\cdot}', E') + Q(\vec{r}, \dot{\cdot}, E),$$

we operate with $\int_0^\infty (\cdot) dE$ to obtain

$$\vec{\cdot} \cdot \vec{\nabla} \tilde{\psi}(\vec{r}, \vec{\cdot}) + \Sigma_t(\vec{r}) \tilde{\psi}(\vec{r}, \vec{\cdot}) =$$

$$\int_{4\pi} d \vec{\cdot}' \int_0^{\infty} dE' \psi(\vec{r}, \vec{\cdot}', E') \left[\int_0^{\infty} dE \Sigma_s(\vec{r}, \vec{\cdot}' \to \vec{\cdot}, E' \to E) \right] + \tilde{Q}(\vec{r}, \vec{\cdot}),$$

FINITE ELEMENT NEUTRON DIFFUSION

2.1 Introduction

For typical nuclear reactor applications, diffusion theory well approximates the neutron distribution within the reactor. The neutron diffusion equation is a second order partial differential equation in space and energy.

$$\nabla \cdot (D(\mathbf{r}, E) \nabla \phi(\mathbf{r}, E)) + \Sigma_r(\mathbf{r}, E) \phi(\mathbf{r}, E) = \frac{\chi(\mathbf{r}, E)}{k_{eff}} \int_0^\infty \Sigma_f(\mathbf{r}, E') \phi(\mathbf{r}, E') dE' + \int_0^\infty \Sigma_s(\mathbf{r}, E' \to E) \phi(\mathbf{r}, E') dE'$$
(2.1)

2.2 Formulation

- 2.2.1 Derivation
- 2.2.2 Matrix Quantities
- 2.2.2.1 Linear Triangles
- 2.2.2.2 Linear Wedges

2.3 Implementation

2.4 Reference Results

- 2.4.1 Triangular Element Manufactured Solutions
- 2.4.1.1 One Dimension, One-Group, Fixed Source
- 2.4.1.2 One Dimension, One-Group, Criticality
- 2.4.1.3 One Dimension, Two-Group, Criticality
- 2.4.1.4 One Dimension, One-Group, Two-Region, Criticality
- 2.4.1.5 Two Dimension, One-Group, Criticality
- 2.4.2 Two Dimension Reactors
- 2.4.2.1 VVER440
- 2.4.2.2 SNR
- 2.4.2.3 HWR
- 2.4.2.4 IAEA
- 2.4.3 Wedge Element Manufactured Solution Finite Cylinder
- 2.4.4 Three Dimension Reactors
- 2.4.4.1 MONJU
- 2.4.4.2 KNK

THERMAL HYDRAULICS

- 3.1 Axial Convection Model
- 3.2 Radial Conduction Model
- 3.2.1 Derivation
- 3.2.2 Relations
- 3.3 Cross Section Treatment
- 3.4 Results

THERMAL EXPANSION

- 4.1 Necessity of Modeling
- 4.2 Model Details
- 4.3 Implementation
- 4.4 Results

CONCLUSIONS

- **5.1** Results Discussion
- **5.2** Code Enhancements
- **5.3** Further Investigations

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APPENDIX

APPENDIX A

LOREM IPSUM

A.1 A First Section

A.1.0.0.1 Filler Text

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Table A.1 A table in the appendix.

System	Author
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E TEX	Leslie Lamport

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A.2 A Second Section

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