

$$I_{ij} = \int d^3 \bar{r} \, \rho(\bar{r}) \left(r^2 \delta_{ij} - \alpha_i x_j \right)$$

$$= \sum_{k} m_k \left(r_k^2 \delta_{ij} - r_{ki} r_{kj} \right)$$

=
$$\sum_{k} w_{k} (\bar{R} + \bar{n}'_{k}) \times (\bar{V} + \bar{\omega} \times \bar{n}'_{k})$$

For rolation around 2 oxis:
$$\bar{\omega} = (0,0,\omega)$$

In general for I:

$$L : I \cdot \tilde{\omega} = (I_{13}\omega, I_{23}\omega, I_{33}\omega)$$

* Parallel-axis theorem

We calculate I in the reference frame attached to the rigid loody and centered on the center of man. This is not a unique choice. If there is a physical fixed point, that is not the center of man, that might be a better choice.

Example: inertia tensor for cube around center of mass

$$T_{ii}^{(cn)} = \int d^3\bar{\tau} \, \rho \left(x_2^2 + x_3^2 \right) = \rho \ell^2 \left[\frac{x_2^3}{3} + \frac{x_3^3}{3} \right] \ell_2^2$$
instead of $T_{ii}^{(conner)} = \frac{2}{3} M \ell^2$ for wortin tensor in home centered on one of the corners

$$=) I_{ii}^{(corner)} = I_{ii}^{(CM)} + \frac{1}{2}M\ell^2$$

$$I_{12}^{(cm)} = \int d^3\tau \, \rho(-x_1x_2) = -\rho l \left[\frac{x_1}{2}\right] - l_2 \left[\frac{x_2^2}{2}\right] - l_2 = 0$$
instead of $I_{ij}^{(conner)} = -\frac{1}{4}Ml^2$ around one of the corners
$$T(conner) = T(cm) = -\frac{1}{4}Ml^2$$

$$=) I_{ij}^{(conner)} = I_{ij}^{(cm)} - \frac{1}{4} Me^{2}$$

Example: inertia tensor for disk around center of man

$$I_{33} = \begin{cases} d^{3} \bar{n} \rho (x_{1}^{2} + x_{2}^{2}) \\ R & d/2 \end{cases}$$

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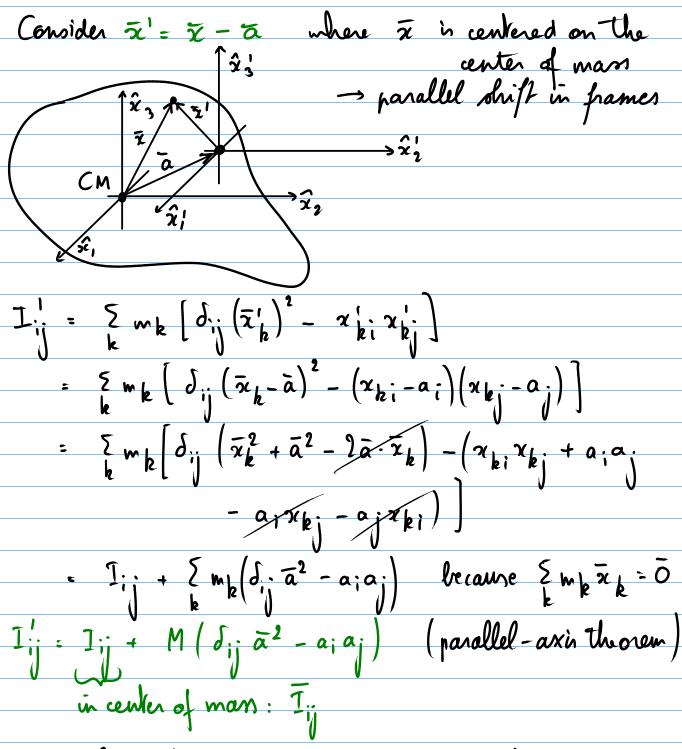
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Note: for I; and I; the difference is the transverse distance between the i-axis.

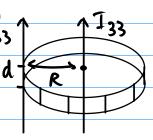
$$T_{11}^{1} = T_{11} + M(x_{1}^{2} + x_{2}^{2} + x_{3}^{2} - x_{1}^{2}) = I_{11} + M(x_{2}^{2} + x_{3}^{2})$$

$$= -\frac{\ell}{2}(1,1,1)$$

$$I_{ij} = I_{ii} + M(J_{ij} \frac{3\ell^2}{4} - \frac{\ell^2}{4}) \quad \hat{x}_{i}$$

$$I''_{12} = I_{12} + \frac{1}{4}M\ell^{2}$$
 as found earlier $I'_{12} = I_{12} - \frac{1}{4}M\ell^{2}$

Example: circular disk with radius R



(c) calculate inertia tensor around point on the edge - hard calculate inertia tensor around center of mass - easy!

hansverse distance is R -> I'z = I33 + MR2

$$I_{33} = \frac{1}{2} M R^2 \Rightarrow I_{33}^1 = \frac{2}{3} M R^2$$

$$I_{ij} = 1_{i} \rightarrow real$$
, symmetric
$$\frac{1}{2} \omega^{T} I \omega = T_{rot} > 0 \quad \text{and} \quad \frac{1}{2} \omega^{T} I \omega = 0 \Leftrightarrow \omega = 0$$

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$$\frac{1}{1} = \frac{1}{1} \cdot \delta_{ij} = \begin{pmatrix} 1 & 1 \\ 1 & 1 \end{pmatrix}$$

$$I_{ij}^{i} = I_{i} \delta_{ij} = \begin{bmatrix} I_{2} & I_{2} \\ I_{3} & I_{4} \end{bmatrix}$$
with I_{ij}^{i} the eigenvalues of I_{ij}^{i} det $I_{ij}^{i} - I_{ij}^{i}$ = 0

Transformation from I to I':

$$\frac{\overline{\xi}}{\overline{\xi}} = \begin{pmatrix} \overline{\xi}_{1} \cdot \overline{\omega} \\ \overline{\xi}_{2} \cdot \overline{\omega} \\ \overline{\xi}_{3} \cdot \overline{\omega} \end{pmatrix} = \begin{pmatrix} \overline{\ell}_{1} \cdot \overline{\omega} \\ \overline{\ell}_{2} \cdot \overline{\omega} \\ \overline{\ell}_{3} \cdot \overline{\omega} \end{pmatrix} = 0^{T} \overline{\omega}$$

$$T = \frac{1}{2}\omega^T I \omega = \frac{1}{2}\xi^T U^T I U \xi = \frac{1}{2}\xi I_i \xi_i^2$$

kinetic energy becomes just sum of 1 I 02-like terms

angular momentum expressed in principal axes coordinates ir now just sum of IO-like terms

Clampication of rigid Rodies:

-
$$I$$
, $\neq I_2 \neq I_3$ \rightarrow asymmetrical top

-
$$I_1 = I_2 \neq I_3$$
 -> symmetrical top

degenerate eigenvalues ê, 2 in a plane perpendicular eigenvalue ê,

Co any three oxes can be chosen as principal oxes

Interpretation of products of mertia I; , i + j no real interpretation necessary - can always transform into diagonal system of principal axes with Tij, i = 0 if I; 10 - not in principal aces system Symmetry: - plane of symmetry -> (center of mass in plane two principal axes in plane example: collection of particles with x3=0 $I_1 = \sum_{k=1}^{\infty} m_k x_{k2}^2$, $I_2 = \sum_{k=1}^{\infty} m_k x_{k1}^2$ $I_3 = \frac{5}{6} m_k (x_{k1}^2 + x_{k2}^2) = I_1 + I_2$ - axis of symmetry -> center of mass on acis principal axis is symmetry acis example: line of particles with x,= xz = 0 $I_1 = \sum_{k=1}^{\infty} m_k x_{k3}^2 = I_2$ 7, = 0 -> special case lecourse of sero eigenvalue S no meaningful notion of relation around the sez arcis for point particles

Physical	meaning	of a	princ	ipal	ain	-
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- object robating around principal axis: e.g.
$$\bar{\omega} = \omega \hat{e}_3$$

- if
$$\dot{\bar{w}} = \dot{\omega} \hat{e}_3 = 0$$
 (uniform rotation) then $\dot{L} = 0$

- => no torque is exerted by uniform rotation around principal arcis
- · if \bar{u} is not along a principal axis, $\bar{I}\bar{u}$ will be a continuously changing linear combination of the $\bar{I}_1,\bar{I}_2,\bar{I}_3$ periodically minimal axis

 balanced (1) unbalanced \bar{I}_1 \bar{I}_2 \bar{I}_3

torque excelled/required

* Euler's Equations of Rigid Body dynamics

Newton's law:
$$\left(\frac{dL}{dt}\right) = \overline{\Gamma}^{(e)} = \text{external torque}$$

Angular momentum:
$$\bar{L} = I\bar{\omega} \Rightarrow \left(\frac{d\bar{L}}{d\bar{f}}\right) = I\frac{d\bar{\omega}}{d\bar{f}}$$

constants in rigid body frame remember that:

In principal occs basis of rigid body:

$$I \bar{\omega} = \begin{pmatrix} I_1 \omega_1 \\ I_2 \omega_2 \\ I_3 \omega_3 \end{pmatrix} \Rightarrow \bar{\omega} \times (I \bar{\omega}) = \begin{pmatrix} \omega_2 I_3 \omega_3 - \omega_3 I_2 \omega_2 \\ \omega_3 I_1 \omega_1 - \omega_1 I_3 \omega_3 \\ \omega_1 I_2 \omega_2 - \omega_2 I_1 \omega_1 \end{pmatrix}$$

$$= \begin{cases} \Gamma_{1}^{(e)} = I_{1}\dot{\omega}_{1} - \omega_{2}\omega_{3}(I_{2} - I_{3}) \\ \Gamma_{2}^{(e)} = I_{2}\dot{\omega}_{2} - \omega_{1}\omega_{3}(I_{3} - I_{1}) \\ \Gamma_{3}^{(e)} = I_{3}\dot{\omega}_{3} - \omega_{1}\omega_{2}(I_{1} - I_{2}) \end{cases}$$