

Optimal Control of Active Nematics using COMSOL and MATLAB

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I. INTRODUCTION

This document describes how to configure and run the MATLAB scripts that perform the optimal control calculation presented in <https://arxiv.org/abs/2007.14837>. The code utilizes the numerical technique “direct adjoint looping” [2] to iteratively converge on a spatio-temporal field for either activity strength α or applied vorticity g , through consecutive finite element simulations consisting of forward, backward (adjoint), and update (gradient descent) steps, Fig. 1.

All files are described in 1; variables and parameters in tables 2,3 and 4. For those users interested in modifying the code to suit their own PDE systems, tables 5 and 6 describe all COMSOL PDE entries and how they are enabled/disabled during the adjoint loop.

All scripts are run within MATLAB. While the final output is a COMSOL *.mph file, there is largely no need to access the COMSOL gui to perform any calculations.

The code will be maintained at: GitHub: https://github.com/wearefor/activenematic_oc and OSF: <https://osf.io/qyk9t/>.

II. SOFTWARE REQUIREMENTS

- MATLAB[®], written with 2019a, compatibility with other versions is untested
- COMSOL Multiphysics[®] with MATLAB LiveLink module, code written for v5.2, compatibility with other versions is untested
- matlab-ascii-plot, free download from MATLAB Central [1]

III. RUNNING THE CODE

1. **Initializing:** The script `AN_adjointloop_setup.m` serves two functions. Firstly, it creates a COMSOL model with the necessary equations to model nematohydrodynamics and adjoint dynamics, as well as to perform gradient descent on the control fields. Secondly, it generates target solutions for the clockwise (CW) and counterclockwise (CCW) circulating states.

The output of this script will be saved in a data file appended with the date and time: `LimitCycles_yyyymmdd_HHMM.mph`. Note this file name, and define the string variable `params.limitcyclestr` in the file `AN_adjointloop.m` accordingly.

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2. **Running the Adjoint Loop:** The primary execution script is `AN_adjointloop.m`. The beginning of the script defines parameters in lines ~1-115; the adjoint loop starts on 289. When executed, the script will load the previously generated `*.mph` file (define `params.limitcyclestr`) and proceed to configure and execute forward, adjoint, and update steps through several auxiliary functions. All of the computational heavy lifting is done in COMSOL, the sole purpose of the scripts are to configure the “studies” in COMSOL.

All simulation and numerical parameters (with the exception of the base level of active stress `alpha0`, domain size `DomRad`, flow alignment `lam1`, and perhaps a few other parameters) are defined in the beginning of this file, details are below in tables 2,3,4.

While running, the script outputs simulation details into the terminal that I’ve found most useful for monitoring the progress. These include notifications when COMSOL has been asked to do a potentially time-intensive task, a breakdown of all contributions to the cost J of the current control solution, the circulation, and ascii time plots of control effort. Two `*.mat` files `debug.mat` and `params_.mat` are also generated that save the parameter structure `params` and some additional diagnostic variables.

Direct adjoint looping can be a memory-intensive process [2]. The small computational domain and short control windows considered for the problem described in the manuscript partially alleviate this concern, but this will not be the case for all problems of interest. To avoid large data files and clear up memory, the code alternates between saving the control field in `A` and `B` datasets (in other words there are always two control solutions in memory, the current iteration and the previous), Fig. 1 illustrates the process. By contrast, forward and adjoint solutions are overwritten at each iteration since there is never a need to simultaneously use dynamics from different iterations. However, for debugging purposes it can be helpful to access intermediate steps, this can be done by setting `params.save=1`, this will perform calculations as usual but save an `*.mph` file to the disk. Because of the need to flip between different datasets, odd and even iterations require slightly different setups so that solvers for the forward and adjoint steps are using the correct control solution. See table 5 for a summary of the PDE equations and table 6 for how these PDEs are activated/deactivated. The flow chart Fig. 1 illustrates the concept.

3. **Modifying the Control Target:** By default, the scripts are configured to use either CW or CCW solutions, which are saved in the `LimitCycles...mph` file, as the target solution for \mathbf{Q}^* in a tracking problem (i.e., there is a penalty incurred at all times for not matching the target trajectory). A different solution (or function) can be used instead by modifying the file `func_config_adjoint.m`; this reference field can be time varying or stationary. There are several references to these solutions to cover the different cases of the adjoint loop. A quick way to identify them all is to search for all instances of `sol_isolate_...` and edit as needed.
4. **Modifying the Physics:** Modifying the governing equations will necessitate re-deriving the adjoint equations and changing the code accordingly. When new physics involve the control field or if a new control field is introduced, the gradient of the cost function with respect to the control field will also need to be updated. The validity of the adjoint equations in the paper was numerically verified using finite differences. If changes are made, the new equations can be checked in the following way: First, we note that applying point perturbations in space/time to the control solution for the purposes of computing a numerical derivative in COMSOL is not possible. Instead, one can consider an auxiliary problem that introduces a smooth perturbation, such as a Gaussian bump, to the control field of interest, and assess the sensitivity of the cost function to the amplitude of the perturbation A by both adjoint and finite difference methods. We note that since the “control variable” A is a constant in this example, the gradient will now also be a single, scalar value rather than a function of time and space as it was in the paper (eqns. 6 and 7). More detail on the adjoint method for PDEs can be found in the following tutorial [3].

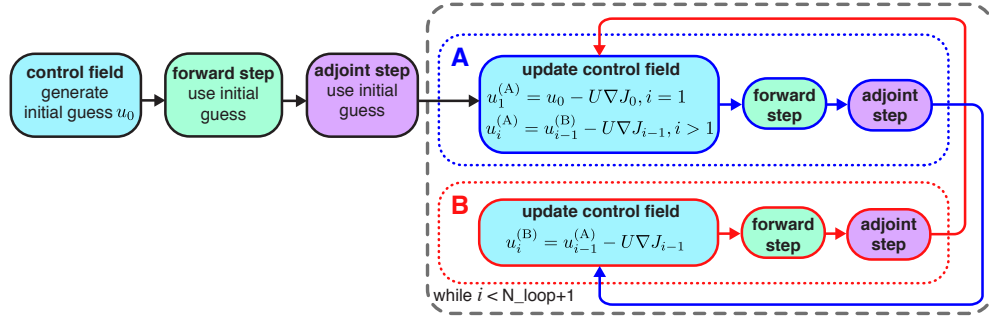


FIG. 1. A visual representation of the adjoint loop as it is implemented in the provided scripts. In the diagram, u refers to either control field (α or g) and U is the gradient step size. For more detail on how equations are enabled/disabled at various stages of the loop see table 6.

file/function name	description
AN_adjointloop_setup.m	configuration script that defines physics, geometry, and boundary conditions, and generates reference solutions (i.e. cw and ccw attractors).
AN_adjointloop.m	defines control parameters (such as weights) and numerical parameters, and runs adjoint loop
AN_plots.m	imports data and generates field plots
func_armijo.m	armijo line search for determining gradient descent step size [4]
func_config_adjoint.m	configures adjoint physics for current
func_config_forward.m	configures forward
func_config_update.m	configures control field update
func_cost.m	calculate value of cost function
func_mphsave.m	saves comsol mph file
func_plot_controlfield.m	plots control field
func_plot_director.m	plot director field and degree of order
func_plot_flowfield.m	plots flow field and vorticity
func_plotcontrol.m	plots the spatial maximum of either α or g as a function of time in a command line asciipLOT
asciipLOT.m	generates command line ascii plots, the width and height may need to be modified to suit your window size[1]

TABLE 1. A list of all scripts and their usage.

IV. NOMENCLATURE AND QUICK REFERENCE GUIDE

symbol	COMSOL variable name	description
forward dynamics		
$\mathbf{Q} = \begin{pmatrix} Q_{xx} & Q_{xy} \\ Q_{xy} & -Q_{xx} \end{pmatrix}$	Qxx, Qxy	components of nematic order tensor
$\mathbf{u} = \{u_x, u_y\}$	ux, uy	components of velocity field
p	p	pressure field
adjoint dynamics		
$\boldsymbol{\psi} = \begin{pmatrix} \psi_{xx} & \psi_{xy} \\ \psi_{xy} & -\psi_{xx} \end{pmatrix}$	psixx, psixy	components of adjoint nematic order tensor field
$\boldsymbol{\nu} = \{\nu_x, \nu_y\}$	nux, nuy	components of adjoint velocity field
ϕ	phi	adjoint pressure field
gradient descent update		
α	Anew	active stress field
$\frac{\partial J}{\partial \alpha}$	Agrad	gradient of cost function w.r.t. active stress control field
g	Gnew	applied vorticity field
$\frac{\partial J}{\partial g}$	Ggrad	gradient of cost function w.r.t. applied vorticity control field

TABLE 2. All field variables as they appear in the manuscript and their variable name in COMSOL.

symbol	MATLAB variable	COMSOL variable	value	description
constants defined in AN_adjointloop_setup.m				
α_0	-	alpha0	fixed: 5	base level of activity
λ	-	lam1	fixed: 1	flow alignment
R	-	DomRad	fixed: 6.5	domain radius
ρ_0	-	rho0	fixed: 1.6	nematic density
-	-	tLCmax	15	duration of reference solution (note that the period of the limit cycle solution used in the paper is ~ 5)
penalty weights for control				
-	params.A_Q_weight	A_Q_weight	-	terminal penalty weight on $\Delta \mathbf{Q}$
-	params.B_Q_weight	B_Q_weight	-	terminal penalty weight on $\Delta \mathbf{u}$
W	params.C_Q_weight	C_Q_weight	$\sim 100-1000$	stage penalty weight on $\Delta \mathbf{Q}$
-	params.D_Q_weight	D_Q_weight	-	stage penalty weight on $\Delta \mathbf{u}$
Γ_α	-	Gamma_alpha	0.1	penalty on active stress gradients
Γ_g	-	Gamma_g	0.1	penalty on applied vorticity gradients
initial conditions, initial control guesses, control window, etc.				
t_f	params.Tf	-	2	control window duration
-	params.dt	-	0.05	time step for saving
-	params.tlist	-	[0:dt:Tf]	list of times
-	-	A(t)	alpha0	naive initial guess for $\alpha(\mathbf{x}, t)$
-	params.G0	G0	-0.75	strength of initial guess value for applied vorticity
-	-	G(t)	$G_0 (1 - \Theta(t - t_f/2))$	uniform time-varying initial guess for applied vorticity
-	params.thetastart	-	3	phase of initial conditions used in paper (units of time)
θ	params.theta	theta	$\in [\mathbf{tLCmax} - t_f, \mathbf{tLCmax}]$	target phase (units of time): following the convention in the paper, the code shifts the lookup of the target solution such that at $t = t_f$, $\mathbf{Q}^*(\theta)$, similarly, at the beginning of the control window, the control target is $\mathbf{Q}^*(\theta - t_f)$. The range on admissible values for θ is set by the duration of the reference solution tLCmax

TABLE 3. List of parameters controlling the optimal control problem. If the field is empty, then the variable may not be defined in the paper and/or may only exist in MATLAB or COMSOL. For example, no penalty was assigned to the velocity field \mathbf{u} , but code exists to support this. Some parameters have both MATLAB and COMSOL names because they are first defined in MATLAB and then passed into COMSOL.

parameter name	value	description
<code>params.armijoskipfirst</code>	0 or 1	option to skip armijo step size optimization
<code>params.armijoskipcutoff</code>	integer	specifies number of adjoint loop steps to skip Armijo backtracking
<code>gradstep</code> (COMSOL parameter)	-	gradient step size, determined by either: 1) the list <code>params.gradstep</code> list or 2) Armijo backtracking note: <code>gradstep</code> multiples gradient ∇J not $\nabla J/ \nabla J $
<code>params.gradstep</code>	$10^{-7} - 10^{-4}$	sequence of gradient step sizes to use in place of backtracking
<code>params.armijo_gammaMax</code>	1	maximum gradient step size scaling factor to consider, $u_{i+1} = u_i - \gamma \nabla J/ \nabla J $
<code>params.armijo_gradstepMin</code>	10^{-11}	minimum gradient step size
<code>params.armijo_beta</code>	1	step size rescaling
<code>params.armijo_mu</code>	1	search region size
<code>params.armijo_mreduce</code>	0.6	If the search region is too large a a negative cost function goal can result, this scaling factor is used to iteratively reduce the Armijo search region
<code>params.costtol</code>	10^{-6}	stop condition, relative tolerance on cost function
<code>params.Q_err_tol</code>	0	alternative stop condition, relative tolerance on $\Delta \mathbf{Q}(t = t_f)$
<code>params.Nloop</code>	~ 50	If tolerances are not met, the maximum number of adjoint loops to perform

TABLE 4. List of numerical tuning parameters. These are variables for controlling various aspects of adjoint looping and Armijo backtracking. These are all Matlab parameters except for **gradstep**, which exists as a Comsol parameter.

physics name	description
	Forward Dynamics:
w	Nematic Dynamics, WeakFormPDE for $\{Q_{xx}, Q_{xy}\}$
w/wfeq1	time derivative
w/wfeq3	material derivative: velocity contribution
w/wfeq4	material derivative: vorticity contribution
w/wfeq5	flow alignment
w/wfeq7	distortion relaxation
w/wfeq15	order/disorder dynamics
w/wfeq16	applied vorticity \mathbf{g}
w2	Stokes flow, WeakFormPDE for $\{u_x, u_y\}$
w2/wfeq1	viscous forces, pressure gradient
w2/wfeq2	uniform and steady active stress
w2/wfeq4	active stress defined during adjoint looping
w2/wfeq5	time-varying, spatially uniform initial guess for α , defined by comsol function A(t)
w2/wfeq6	time-derivative, not utilized, $Re=0$
w3	WeakFormPDE for p
w3/wfeq1	continuity equation
	Backward/Adjoint Dynamics:
w4	WeakFormPDE for $\{ps_{ixx}, ps_{ixy}\}$ (adjoint variables of nematic order tensor)
w4/wfeq1	adjoint dynamics, all contributions except those arising from control fields and stage penalties
w4/wfeq2	time-varying, spatially uniform initial guess for α , defined by comsol function A(t)
w4/wfeq3	active stress defined during adjoint looping
w4/wfeq4	stage penalty on $\Delta \mathbf{Q}$
w4/wfeq5	applied vorticity defined during adjoint looping
w4/wfeq6	uniform and steady active stress
w4/wfeq7	time-varying, spatially uniform initial guess for active vorticity g , defined by comsol function G(t)
w5	WeakFormPDE for $\{n_{ux}, n_{uy}\}$ (adjoint variables of velocity)
w5/wfeq1	adjoint dynamics, all contributions except those arising from stage penalties
w5/wfeq2	stage penalty on $\Delta \mathbf{u}$ (unused in paper)
w6	WeakFormPDE for ϕ (adjoint variable of pressure p)
w6/wfeq1	continuity equation
	Control Field Update:
w7	Active Stress Update
w7/wfeq1	gradient descent update
w7/wfeq2	define gradient, update A
w7/wfeq3	define gradient, update B
w8	Applied Vorticity Update
w8/wfeq1	gradient descent update
w8/wfeq2	define gradient, update A
w8/wfeq3	define gradient, update B

TABLE 5. Comsol physics configured in **AN_matlab_adjointloop_setup.m**. Most of the PDEs are defined symbolically in their weak form in this initial setup file. The exceptions are those that depend on solutions that are only created once the adjoint loop has begun (they will either be commented out in this this setup script or absent altogether). These will be created/enabled as needed in the files **func_config_forward.m**, **func_config_adjoint.m**, and **func_config_update.m**.

	initialization		in adjoint loop, i=1			in adjoint loop, even (B)			in adjoint loop, odd (A)		
physics/PDE	forward	adjoint	control	forward	adjoint	control	forward	adjoint	control	forward	adjoint
w	on	off	off	on	off	off	on	off	off	on	off
w/wfreq1	on	-	-	on	-	-	on	-	-	on	-
w/wfreq3	on	-	-	on	-	-	on	-	-	on	-
w/wfreq4	on	-	-	on	-	-	on	-	-	on	-
w/wfreq5	on	-	-	on	-	-	on	-	-	on	-
w/wfreq7	on	-	-	on	-	-	on	-	-	on	-
w/wfreq15	on	-	-	on	-	-	on	-	-	on	-
w/wfreq16	g^*	-	-	g^*	-	-	*	-	-	g^*	-
w2	on	off	off	on	off	off	on	off	off	on	off
w2/wfreq1	on	-	-	on	-	-	on	-	-	on	-
w2/wfreq2	g^*	-	-	g^*	-	-	g^*	-	-	g^*	-
w2/wfreq4	off	-	-	α^*	-	-	α^*	-	-	α^*	-
w2/wfreq5	α^*	-	-	-	-	-	-	-	-	-	-
w2/wfreq6	off	-	-	off	-	-	off	-	-	off	-
w3	on	off	off	on	off	off	on	off	off	on	off
w3/wfreq1	on	-	-	on	-	-	on	-	-	on	-
w4	off	on	off	off	on	off	off	on	off	off	on
w4/wfreq1	-	on	-	-	on	-	-	on	-	-	on
w4/wfreq2	-	α^*	-	-	off	-	-	off	-	-	off
w4/wfreq3	-	off	-	-	α^*	-	-	α^*	-	-	α^*
w4/wfreq4	-	on	-	-	on	-	-	on	-	-	on
w4/wfreq5	-	off	-	-	g^*	-	-	g^*	-	-	g^*
w4/wfreq6	-	g^*	-	-	g^*	-	-	g^*	-	-	g^*
w4/wfreq7	-	g^*	-	-	off	-	-	off	-	-	off
w5	off	on	off	off	on	off	off	on	off	off	on
w5/wfreq1	-	on	-	-	on	-	-	on	-	-	on
w5/wfreq2	-	on	-	-	on	-	-	on	-	-	on
w6	off	on	off	off	on	off	off	on	off	off	on
w6/wfreq1	-	on	-	-	on	-	-	on	-	-	on
w7	off	off	α^*	off	off	α^*	off	off	α^*	off	off
w7/wfreq1	-	-	α^*	-	-	off	-	-	off	-	-
w7/wfreq2	-	-	off	-	-	off	-	-	α^*	-	-
w7/wfreq3	-	-	off	-	-	α^*	-	-	off	-	-
w8	off	off	g^*	off	off	g^*	off	off	g^*	off	off
w8/wfreq1	-	-	g^*	-	-	off	-	-	off	-	-
w8/wfreq2	-	-	off	-	-	off	-	-	g^*	-	-
w8/wfreq3	-	-	off	-	-	g^*	-	-	off	-	-

TABLE 6. **Enabled/Disabled physics lookup table.** If the field needs to be solved at a given step the "parent" entry (w,w2,etc.) will be listed as "on", however some contributions to the dynamics need are iteration-dependent and need to be disabled. Alternatively, if the parent entry is listed as "off" then all dependent contributions are automatically disabled and listed as "-". The "*" indicates dynamics conditional on the choice of control field (g^* : on if using applied vorticity control OR α^* : on if using active stress control). All enabling/disabling of physics is handled in the functions: **func_config_forward.m**, **func_config_adjoining.m**, **func_config_update.m**, and **func_config_cost.m**.

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