Homework 3

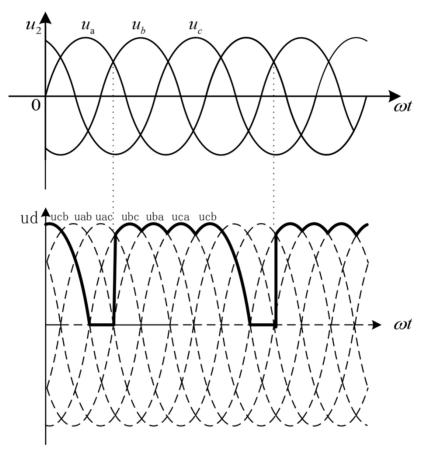
Page 95, Chinese textbook

Question 12

Considering a three-phase bridge fully-controlled rectifier circuit under a resistive load, if one thyristor cannot be conducted, what does the rectifier voltage waveform u_d look like? If one thyristor has been broken down and is a short circuit now, what is the influence on the other thyristors?

Solution:

Assuming that VT1 could not be conducted, and the firing angle $\alpha = 0$, then the waveform of u_d would look like:



If VT1 is broken down and is a short circuit now. When VT3 and VT5 is conducting, a short circuit can be formed between phase a and b or phase a and c. The increasing voltage may cause damage to VT3 and VT5.

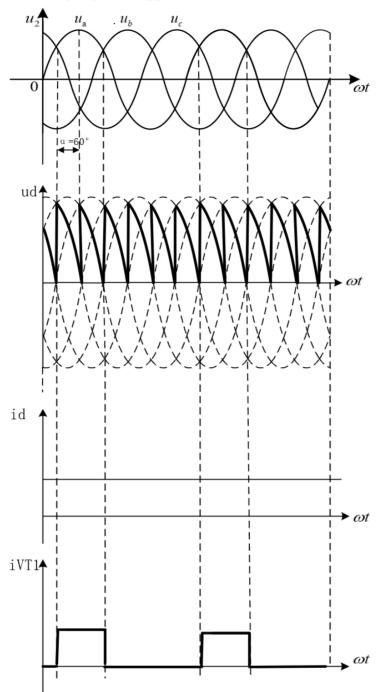
Question 13

Considering a three-phase bridge fully-controlled rectifier circuit with $U_2 = 100V$, under a resistive and inductive load with $R = 5\Omega$ and very large inductance, when $\alpha = 60^{\circ}$:

- 1) Draw the waveform of u_d , i_d and i_{VT1} ;
- 2) Calculate $U_d I_d I_{dVT} I_{VT}$.

Solution:

1) The waveform of u_d , i_d and i_{VT1} is shown as below:



2)
$$U_{d} = \frac{3}{\pi} \int_{\alpha + \frac{2\pi}{3}}^{\alpha + \frac{2\pi}{3}} \sqrt{6} U_{2} \sin \omega t \, d\omega t = 2.34 U_{2} \cos \alpha = 117(V)$$

$$I_{d} = \frac{U_{d}}{R} = 23.4(A)$$

$$I_{dVT} = \frac{1}{3} I_{d} = 7.8(A)$$

$$I_{VT} = \frac{1}{\sqrt{3}} I_{d} \approx 13.51(A)$$

Question 15

Considering a three-phase half-wave controlled rectifier circuit connected to a EMF load with resistor and inductor, when $U_2 = 100V$, $R = 1\Omega$, $L = \infty$, $L_B = 1 \text{mH}$, $\alpha = 30^\circ$, E = 50V,

calculate the value of U_d $\ I_d$ $\ \gamma$ $\$ and draw the waveform of $\ u_d, \ i_{V\!T1}$ $\$ and $\ i_{V\!T2}$

Solution:

Since this is a three-phase half-wave controlled rectifier, we can see ${}^{\Delta U_d}$:

$$\Delta U_d = rac{3 X_B I_d}{2 \pi}$$

$$X_B = 2\pi f L_B \ (f = 50 Hz)$$

Meanwhile.

$$U_d = 1.17 U_2 \cos lpha - \Delta U_d$$

$$I_d = \frac{U_d - E}{R}$$

Solve these equations:

$$egin{align} U_d &= rac{3 X_B E + \pi R imes 1.17 U_2 \cos lpha}{3 X_B + 2 \pi R} pprox 94.63 (V) \ &\Delta U_d = 1.17 U_2 \cos lpha - U_d pprox 6.7 (V) \ &I_d = 44.63 (A) \end{gathered}$$

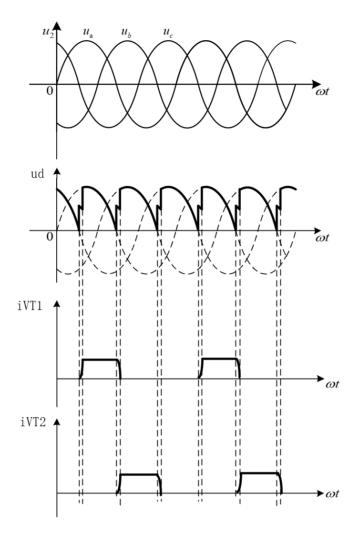
On account of:

$$\cos lpha - \cos \left(lpha + \gamma
ight) = rac{2 I_d X_B}{\sqrt{6} U_2}$$

We can solve γ :

$$\gamma = \arccos(0.752) - 30^{\circ} \approx 11.24^{\circ}$$

The waveform of u_d , i_{VT1} and i_{VT2} is shown as below:



Question 16

Considering a three-phase bridge uncontrolled rectifier circuit connected to a resistive and inductive load, with $R=2\Omega$, $L=\infty$, $U_2=100V$, $X_B=0.1\Omega$, calculate the value of $U_d~I_d~I_{VD}$, I_2 , and γ , and draw the waveform of $u_d~i_{Vd}~i_{2\,2}$.

Solution:

Three-phase bridge uncontrolled rectifier circuit is equal to three-phase bridge fully-controlled rectifier with α being 0.

$$egin{align} U_d = 2.34 U_2 \cos lpha - \Delta U_d \ \Delta U_d = rac{3 X_B I_d}{\pi} \ I_d = rac{U_d}{R} \ \end{split}$$

We can see:

$$egin{align} U_{d} = rac{2.34 U_{2} {\cos lpha}}{1 + 3 X_{B}/\pi R} pprox 223.37(V) \ I_{d} = 111.685(A) \end{gathered}$$

$$I_{\rm VD} = I_{
m d}/3 \approx 37.23 \, ({
m A})$$

$${
m I}_2\!=\!\sqrt{rac{2}{3}}\,{
m I}_{
m d}\!pprox\!91.19\,{
m (A)}$$

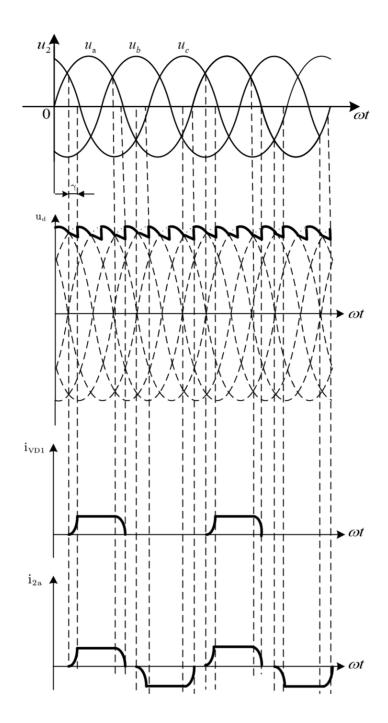
Since:

$$\coslpha-\cos{(lpha+\gamma)}\!=\!rac{2I_dX_B}{\sqrt{6}U_2}$$

We can solve the commutation angle:

$$\gamma = rccosigg(1-rac{2I_dX_B}{\sqrt{6}\,U_2}igg) pprox 24.67^{\circ}$$

The waveform of $\ u_d\ i_{Vd}\ i_{2\,2}.$ is shown as below:



Question 17

Considering a three-phase fully controlled bridge with back electromotive force resistive inductive load, when $E=200V,\,R=1_\Omega,\,L=\infty,\,U=220V,\,\alpha=60^\circ.$

① $L_B=0$; ② $L_B=1$ Mh.

In both cases, calculate the values of $~U_d~and~I_d~$ (also calculate γ). Draw the waveforms of $~u_d~and~i_{VT\,r}$.

Solution:

1) When $L_B=0$:

$$I_d = 2.34 U_2 \cos \alpha = 257.4 (V)$$
 $I_d = \frac{U_d - E}{R} = 57.4 (A)$

2) When $L_B=1Mh$:

$$egin{aligned} U_d = 2.34 U_2 \cos lpha - \Delta U_d \ \Delta U_d = rac{3 X_B I_d}{\pi} \ I_d = rac{U_d - \mathrm{E}}{R} \end{aligned}$$

We can see:

$$egin{align} U_d = rac{3 X_B E + \pi R imes 2.34 U_2 \cos lpha}{3 X_B + \pi R} pprox 244.15(V) \ & ext{I}_{ ext{d}} = 44.15(ext{A}) \ & ext{\Delta} ext{U}_{ ext{d}} = 13.25(ext{V}) \ \end{gathered}$$

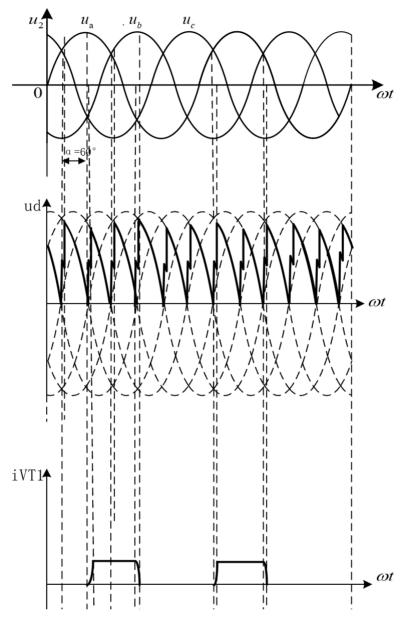
Since:

$$\coslpha-\cos{(lpha+\gamma)}\!=\!rac{2I_dX_B}{\sqrt{6}\,U_2}$$

We can solve the commutation angle:

$$\gamma = \arccos\!\left(\!\cos\!lpha - rac{2I_dX_B}{\sqrt{6}\,U_2}\!
ight)\!-lpha pprox 3.35^{\circ}$$

The waveform is shown as below:



From VT1 to VT6, the latter one's phase is lagged 60° to the former, and the shape of the waveform is totally the same.