

For zero thrust:

For flat earth: $\dot{h} = V \sin \chi$

$$\dot{x} = V \cos \chi \cos \sigma$$

$$\dot{y} = V \sin \chi \cos \sigma$$

$$\dot{V} = -\frac{D}{m} - g \sin \chi$$

$$\dot{\chi} = \frac{1}{mV} (L \cos \sigma + C \sin \sigma) - \frac{g}{V} \cos \chi$$

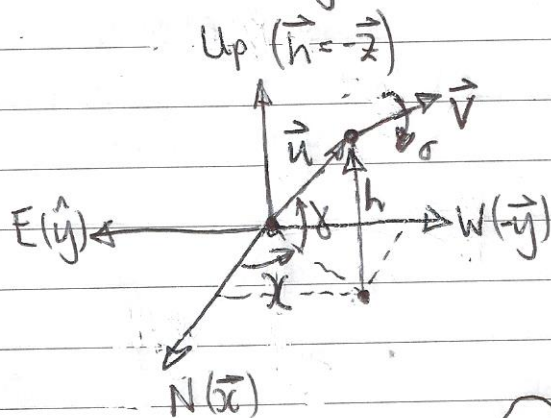
$$\dot{\sigma} = \frac{1}{mV \cos \chi} (L \sin \sigma - C \cos \sigma)$$

$$\begin{cases} V = \|\vec{V}\| \\ h = -z \\ \chi = \text{elevation angle} \\ \sigma = \text{bank angle} \end{cases}$$

D, C, L is the aerodynamic forces

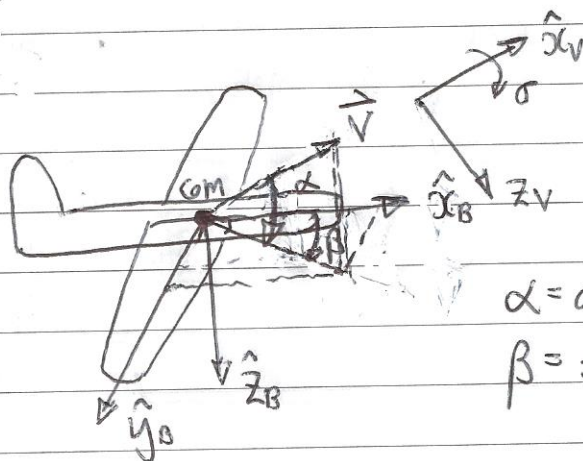
$$\vec{V} = [\dot{x} \ \dot{y} \ \dot{z}]^T$$

$$\vec{u} = \begin{cases} \hat{x} = \text{North direction} \\ \hat{y} = \text{East direction} \\ \hat{z} = \text{Down direction} \end{cases}$$



$$\begin{aligned} \vec{u}_v &= R_{vI}(\chi, \sigma) \vec{u} \\ &= [\hat{x}_v \ \hat{y}_v \ \hat{z}_v]^T \end{aligned}$$

Velocity Frame axis



$\alpha = \text{angle of attack}$
 $\beta = \text{sideslip angle}$

Aerodynamic force vector:

$$\vec{F} = -D \hat{x}_v - C \hat{y}_v - L \hat{z}_v$$

$$\vec{u}_b = [\hat{x}_b \ \hat{y}_b \ \hat{z}_b]^T = R_{bv}(-\beta, \alpha, 0) \vec{u}_v$$

$$(0.0254 \text{ m} = 1'')$$

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$$\begin{aligned} D &= \bar{q} S C_D(\alpha, \beta) & (\text{Drag Force}) \\ C &= \bar{q} S C_C(\beta) & (\text{Side Force}) \\ L &= \bar{q} S C_L(\alpha) & (\text{Lift Force}) \end{aligned}$$

$$\bar{q} = \frac{1}{2} \rho V^2$$

Estimation of aerodynamic coeff:

$$l = \text{wingspan} = 102.4'' (2.6 \text{ m})$$

$$AR = \frac{l}{\bar{c}} = 11.08$$

\Rightarrow

$$S = 946.45 \text{ inch}^2 (61.06 \text{ dm}^2)$$

$$W = 5 \text{ lb} (2.254 \text{ kg})$$

\therefore

$$S_F = \text{Fuselage area} \approx 221 \text{ inch}^2 (\text{for } 102.4'' \text{ wingspan})$$

$$\begin{cases} \text{Measured} \\ l_h = 0.86 \text{ m} \\ l_v = 0.93 \text{ m} \end{cases}$$

$$l_t = \text{Fuselage moment arm} = 0.28 l = 28.7'' (0.73 \text{ m})$$

$$V_H = 0.56 \text{ Horizontal tail volume ratio}$$

$$\left\{ \begin{aligned} 0.56 &= \frac{S_H l_h}{S \bar{c}} = \frac{0.096 \times 0.86}{0.61 \times 0.24} \end{aligned} \right.$$

$$V_V = 0.037 \text{ Vertical tail volume ratio}$$

$$\left\{ \begin{aligned} 0.037 &= \frac{S_V l_v}{S \bar{c}} = \frac{0.063 \times 0.93}{0.61 \times 2.6} \end{aligned} \right.$$

$$\bar{c} = 1.02 l / AR (\text{inch}) = 9.43'' (0.24 \text{ m}) = \text{mean chord}$$

$$e = \text{Oswald efficiency factor} = 0.95$$

Infinite-span wing with aerodynamic characteristics (Reynolds No 150,000):

$$a_0 = 0.1 \frac{180}{\pi} = 5.73 \text{ rad}^{-1} (\text{lift curve slope})$$

$$\alpha_0 = -2.5 \frac{180}{180} = -0.0436 \text{ rad} (\text{zero point})$$

$$C_{d_i} = \text{wing profile drag} = 0.01 + 0.05(C_L - 0.4)^2$$

$$C_{d_f} = 0.008 = \text{Fuselage drag coeff}$$

$$C_{d_T} = 0.01 = \text{tail drag coeff}$$

$$C_{d_E} = 0.002 = \text{misc extra drag}$$

$$S = l^2 / AR = \text{Wing surface area} = 946.45 \text{ inch}^2 (0.6105 \text{ m}^2)$$

$$0.096 \text{ m}^2 = S_T = V_H \bar{c} S / l_t = 124.4 \text{ inch}^2 (0.0803 \text{ m}^2) \text{ Horizontal tail surface area}$$

$$0.063 \text{ m}^2 = S_V = V_V \bar{c} S / l_t = 67.5 \text{ inch}^2 (0.0435 \text{ m}^2) \text{ Vertical tail surface area}$$

$$C_{L\alpha} = \frac{a_0}{1 + a_0 / (\pi e AR)} (\text{Finite wing slope}) = 4.883$$

$$\Rightarrow C_L(\alpha) = C_{L\alpha}(\alpha - \alpha_0) (\text{Glider lift coeff})$$

Drag coeff $C_D(\alpha)$:

$$C_{D0} = C_{DF} \frac{S_F}{S} + C_{DT} \frac{S_T + S_V}{S} + C_{DE} + C_{D0}$$

$$= 0.008 \frac{221}{946.45} + 0.01 \frac{124.4 + 67.5}{946.45} + 0.002 + 0.01 = 0.016$$

Fuselage tail wings extra wing
(0.096 + 0.063)
0.61

$$\Rightarrow C_D(\alpha) = C_{D0} + C_{DL} (C_L(\alpha) - C_{Lmin})^2 + C_L^2(\alpha) / (\pi e AR)$$

$$= 0.016 + 0.05 (C_L(\alpha) - 0.4)^2 + C_L^2(\alpha) / 33.05$$

Drag due to sideslip β : (Assume $AR_V = 0.5 AR = 5.54$)

$$C_{C\beta} = \frac{a_0}{1 + a_0 / (\pi e AR_V)} \left(\frac{\beta_V}{S} \right) = 0.303 \quad (0.44)$$

$$\Rightarrow C_C(\beta) = C_{C\beta} \cdot \beta = 0.303 \beta$$

$$\therefore C_D(\beta) = C_C^2(\beta) \frac{1}{\pi e AR_V} \left(\frac{S}{S_V} \right) = C_C^2(\beta) \cdot 0.8485 \quad (0.59)$$

$$\Rightarrow \therefore C_D(\alpha, \beta) = 0.016 + 0.05 (C_L(\alpha) - 0.4)^2 + C_L^2(\alpha) / 33.05 + C_C^2(\beta) \cdot 0.8485$$

Alt(m) V_{trim} α_{trim} ($m = 2.5 \text{ kg}$)

1000	11.25 m/s	4.2°
2000	11.8 m/s	4.2°
3000	12.5 m/s	4.2°
4000	13.4 m/s	4.2°
5000	14.5 m/s	4.2°
6000	16.0 m/s	4.2°
7000	18.0 m/s	4.2°
8000	21.0 m/s	4.2°
9000	26.2 m/s	4.2°
10000	38.2 m/s	4.2°
500	10.97 m/s	4.2°

$$V_{trim} = 2e-4x^4 - 3e-10x^3 + 1e-6x^2 - 0.0023x$$

412.046

\Rightarrow Lookup table

Subject :

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Input to simulation:

m	glider mass
α, β, σ	angles (assume constant)
$\vec{u}(0)$	initial position
$\chi(0), \gamma(0)$	initial heading and elevation
$\vec{V}(0)$	initial velocity vector

 $t = 0$ to end:

Calculate from $\alpha, \beta \Rightarrow L, D, C$

Integrate $\dot{V}, \dot{\gamma}, \dot{\chi}$

Integrate $\dot{x}, \dot{y}, \dot{z}$

Output $\vec{u}(t), V(t), \gamma(t), \chi(t)$

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Positional Dynamics of Glider

Subject:

Date:

XYZ = Forces ^{coordinates} in glider body axis
 UVW = Linear velocity vector coordinates in body axis
 PQR = Angular velocity coordinates in body axis

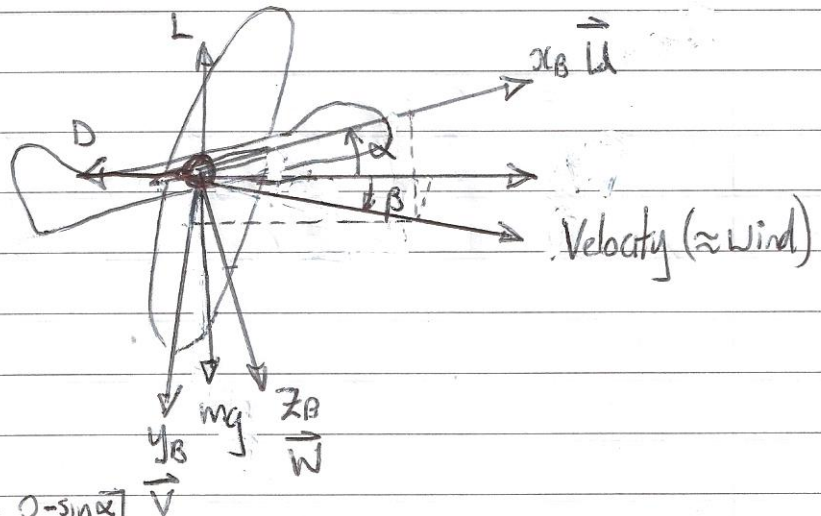
$$\begin{aligned} X &= m(\ddot{u} - v\dot{r} + w\dot{q}) \\ Y &= m(\ddot{v} + u\dot{r} - w\dot{p}) \\ Z &= m(\ddot{w} - u\dot{q} + v\dot{p}) \end{aligned}$$

$$\begin{bmatrix} P \\ Q \\ R \end{bmatrix} = \begin{bmatrix} U\dot{x}_i \\ W\dot{y}_i \\ W\dot{z}_i \end{bmatrix}$$

$$\begin{bmatrix} \ddot{N} \\ \ddot{E} \\ \ddot{D} \end{bmatrix} = \begin{bmatrix} V_N \\ V_E \\ V_D \end{bmatrix} = A_{B/I}(\psi, \theta, \phi) \begin{bmatrix} u \\ v \\ w \end{bmatrix} \quad \begin{cases} \psi = \text{Yaw} \\ \theta = \text{Pitch} \\ \phi = \text{Roll} \end{cases}$$

$$\alpha = \tan^{-1}\left(\frac{W}{U}\right), \quad \beta = \tan^{-1}\left(\frac{V}{U}\right), \quad \bar{V} = \sqrt{U^2 + V^2 + W^2}$$

$$\begin{bmatrix} X^G \\ Y^G \\ Z^G \end{bmatrix} = \begin{bmatrix} -\sin\theta \\ \cos\theta \sin\phi \\ \cos\theta \cos\phi \end{bmatrix} mg$$



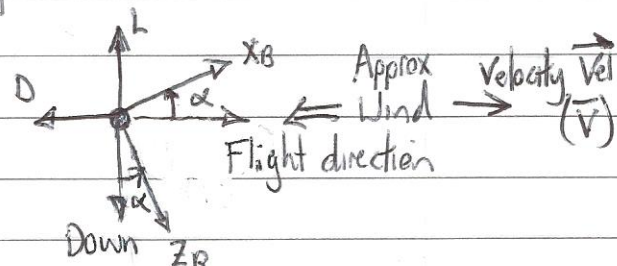
$$\begin{bmatrix} X^A \\ Y^A \\ Z^A \end{bmatrix} = qS \begin{bmatrix} C_x \\ C_y \\ C_z \end{bmatrix} = \frac{W}{B} A(-\beta, \alpha, 0) \begin{bmatrix} -C_D \\ -C_L \\ C_L \end{bmatrix} qS \quad \{q = \frac{1}{2} \rho \bar{V}^2\}$$

Approx small angles:

$$\Rightarrow C_x = -C_D \cos\alpha + C_L \sin\alpha$$

$$C_y = -C_e$$

$$C_z = -C_L \cos\alpha - C_D \sin\alpha$$



\Rightarrow Calculate C_L, C_D, C_e according to glider model in NASA Paper
 $\{C_L(\alpha), C_D(\alpha, \beta), C_e(\beta)\}$

Rotational Dynamics of Glider

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Subject :

Date:

LMN = Moment vector coordinates in body axis (RPY)
 UVW = ^{Linear} Velocity vector coordinates in body axis (X_B, Y_B, Z_B)
 PQR = Angular velocity coordinates in body axis
 δ_E, δ_R = Elevator and rudder deflections

$$\bar{V} = \sqrt{u^2 + v^2 + w^2} \quad \begin{cases} u = \bar{V} \cos \alpha \cos \beta \\ v = \bar{V} \sin \beta \\ w = \bar{V} \sin \alpha \cos \beta \end{cases} \quad \begin{aligned} \alpha &= \text{AoA} \\ \beta &= \text{Sideslip} \end{aligned}$$

$$\begin{aligned} L &= \dot{P} I_{xx} + QR(I_{zz} - I_{yy}) \\ M &= \dot{Q} I_{yy} + PR(I_{xx} - I_{zz}) \\ N &= \dot{R} I_{zz} + PQ(I_{yy} - I_{xx}) \end{aligned} \quad \begin{cases} P \\ Q \\ R \end{cases} = \begin{bmatrix} W_{xi} \\ W_{yi} \\ W_{zi} \end{bmatrix} \quad \begin{aligned} I_{xx} &= 0.2 \text{ kgm}^2 \\ I_{yy} &= 0.36 \text{ kgm}^2 \\ I_{zz} &= 0.525 \text{ kgm}^2 \end{aligned}$$

Aerodynamic Moments: $q = \frac{1}{2} \rho \bar{V}^2$

$$\begin{aligned} L^A &= q S b C_l \\ M^A &= q S \bar{c} C_m \\ N^A &= q S b C_n \end{aligned} \quad \begin{cases} C_l = C_{lp} \beta + \frac{b}{2\bar{V}} C_{lp} P + \frac{b}{2\bar{V}} C_{lr} R + C_{lsr} \delta_R \\ C_m = C_{m0} + C_{m\alpha} \alpha + \frac{\bar{c}}{2\bar{V}} C_{mq} Q + C_{mse} \delta_E \\ C_n = C_{np} \beta + \frac{b}{2\bar{V}} C_{np} P + \frac{b}{2\bar{V}} C_{nr} R + C_{nsr} \delta_R \end{cases}$$

Typically

$$\begin{aligned} C_{m0} &= \text{Static pitch moment coeff} = 0.0 \\ C_{m\alpha} &= -0.2954 = \text{Pitch stiffness coeff} \\ C_{mq} &= -10.281 = \text{Pitch damping coeff} \\ C_{mse} &= -1.5852 = \text{Elevator moment coeff on pitch} \end{aligned}$$

$$\begin{aligned} C_{lp} &= -0.0331 = \text{Roll lateral coeff} \\ C_{l\dot{p}} &= -0.4248 = \text{Roll damping coeff} \\ C_{lr} &= 0.0450 = \text{Roll moment coeff} \\ C_{lsr} &= 0.9080 = \text{Rudder moment coeff on roll} \end{aligned}$$

$$\begin{aligned} C_{np} &= 0.086 = \text{Yaw stiffness coeff} \\ C_{nr} &= -0.0251 = \text{Yaw moment due to roll} \\ C_{n\dot{r}} &= -0.125 = \text{Yaw damping coeff} \\ C_{nsr} &= -0.1129 = \text{Rudder moment coeff on yaw} \end{aligned}$$