$$\frac{1}{2} \left(\frac{1}{2} \right)^{\frac{1}{2}} \left(\frac{1}{2} \right)^{\frac{1}$$

| i | ai | di | 1 di | Oi |
|---|----|----|------|-----|
| 1 | a, | 0 | 0 | 0,* |
| 2 | az | 0 | 0 | Oz* |

2.
$$T_{1} = \begin{bmatrix} co_{1} - so_{1} & o \mid a_{1}co_{2} \\ so_{1} & co_{1} & o \mid a_{1}so_{1} \end{bmatrix} \quad T_{2} = \begin{bmatrix} co_{2} - so_{2} & o \mid a_{2}co_{2} \\ so_{2} & co_{2} & o \mid a_{2}so_{2} \end{bmatrix} \quad so_{2} \quad co_{2} \quad o \mid a_{2}so_{2} \quad co_{3} \quad co_{4}so_{5} \quad co_{5} \quad co_{$$

$$|T_2 = \begin{bmatrix}
 cO_2 & -SO_2 & 0 & 1 & 0 \\
 sO_2 & cO_2 & 0 & 1 & 0 \\
 cO_2 & 0 & 0 & 1 & 0 \\
 cO_2 & 0 & 0 & 1
 cO_2
 cO_2$$

$${}^{\circ} T_{2} = \begin{bmatrix} C_{1}C_{2} - S_{1}S_{2} & -C_{1}S_{2} - S_{1}C_{2} & 0 & | & a_{2}C_{1}C_{2} - a_{2}S_{1}S_{2} + a_{1}C_{1} \\ S_{1}C_{2} + C_{1}S_{2} & -S_{1}S_{2} + C_{1}C_{2} & 0 & | & a_{2}S_{1}C_{2} + a_{2}C_{1}S_{2} + a_{1}S_{1} \\ 0 & 0 & 0 & | & 0 \end{bmatrix}$$

$$0 | a_{2}C_{1}C_{2} - a_{2}S_{1}S_{2} + a_{1}C_{1}$$

$$0 | a_{2}S_{1}C_{2} + a_{2}C_{1}S_{2} + a_{1}S_{1}$$

$$0 | 0 | 0$$

$${}^{\circ} T_{2} = \begin{bmatrix} C_{12} & -S_{12} & 0 & 1 & Q_{1}C_{1} + Q_{2}C_{12} \\ S_{12} & C_{12} & 0 & Q_{1}S_{1} + Q_{2}S_{12} \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

where
$$C_{12} = \cos(\theta_1 + \theta_2)$$

$$S_{12} = \sin(\theta_1 + \theta_2)$$

$${}^{\circ}\mathbb{R}_{2} = \begin{bmatrix} C_{12} & -S_{12} & 0 \\ S_{12} & C_{12} & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

$${}^{\circ}\mathbb{R}_{2} = \begin{bmatrix} C_{12} & -S_{12} & 0 \\ S_{12} & C_{12} & 0 \\ 0 & 0 & 1 \end{bmatrix} \qquad {}^{\circ}\mathcal{A}_{02} = \begin{bmatrix} a_{1}C_{1} + a_{2}C_{12} \\ a_{1}S_{1} + a_{2}S_{12} \\ 0 \end{bmatrix} = \begin{bmatrix} X \\ Y \\ Z \end{bmatrix}$$

$$\overset{\circ}{\partial}_{0} = \begin{bmatrix} \dot{x} \\ \dot{y} \end{bmatrix} = \begin{bmatrix} \frac{\partial x}{\partial \theta_{1}} & \frac{\partial x}{\partial \theta_{2}} \\ \frac{\partial y}{\partial \theta_{1}} & \frac{\partial y}{\partial \theta_{2}} \end{bmatrix} \begin{bmatrix} \dot{\theta}_{1} \\ \dot{\theta}_{2} \end{bmatrix} \\
= \begin{bmatrix} -a_{1}S_{1} - a_{2}S_{12} & -a_{2}S_{12} \\ a_{1}C_{1} + a_{2}C_{12} & a_{2}C_{12} \end{bmatrix} \begin{bmatrix} \dot{\theta}_{1} \\ \dot{\theta}_{2} \end{bmatrix} \\
= \begin{bmatrix} \frac{\partial x}{\partial \theta_{1}} & \frac{\partial x}{\partial \theta_{2}} & \frac{\partial x}{\partial \theta_{2}} \\ \frac{\partial y}{\partial \theta_{2}} & \frac{\partial x}{\partial \theta_{2}} & \frac{\partial x}{\partial \theta_{2}} \end{bmatrix} \begin{bmatrix} \dot{\theta}_{1} \\ \dot{\theta}_{2} \end{bmatrix}$$

Then in polar tor Jacobian

$$\begin{vmatrix} -a_1 S_1 - a_2 S_{12} & -a_2 S_{12} \\ a_1 C_1 + a_2 C_{12} & a_2 C_{12} \end{vmatrix} = a_2 C_{12} (-a_1 S_1 - a_2 S_{12}) \\ + a_2 C_{12} (a_1 C_1 + a_2 C_{12}) = 0$$

$$\alpha_{1}(C_{1}S_{12} - S_{1}C_{12}) + \alpha_{2}(S_{12}C_{12} - S_{12}C_{12}) = 0$$

$$C_{1}S_{12} - S_{1}C_{12} = 0$$

$$Sin(\phi_{1} + \phi_{2} - \phi_{1}) = 0$$

$$Sin \phi_{2} = 0$$

$$\phi_{2} = 0, \pi$$

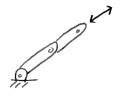
Trig Identifies

Sin A cos B ± sin B cos A

= sin (A ± B)

cos A cos B ± sin A sin B

= cos (A ∓ B)



velocities are limited: and-effector can't move in direction showing

$$\begin{bmatrix} \dot{x} \\ \dot{z} \\ \dot{z} \\ \dot{w}_{1} \\ \dot{w}_{2} \end{bmatrix} = \begin{bmatrix} {}^{\circ}Z_{\circ} \times d_{\circ 2} & {}^{\circ}Z_{i} \times d_{i2} \\ {}^{\circ}Z_{\circ} & {}^{\circ}Z_{i} \end{bmatrix} \begin{bmatrix} \dot{o}_{1} \\ \dot{o}_{2} \end{bmatrix}$$

$$= \begin{bmatrix} {}^{\circ}Q_{\circ} \times d_{\circ 2} & {}^{\circ}Z_{i} \times d_{i2} \\ {}^{\circ}Q_{\circ} & {}^{\circ}Z_{i} \end{bmatrix} \begin{bmatrix} \dot{o}_{1} \\ \dot{o}_{2} \end{bmatrix}$$

$$= \begin{bmatrix} {}^{\circ}Q_{\circ} \times d_{\circ 2} & {}^{\circ}Z_{i} \\ {}^{\circ}Q_{\circ} & {}^{\circ}Z_{i} \end{bmatrix} \begin{bmatrix} \dot{o}_{1} \\ \dot{o}_{2} \end{bmatrix}$$

$$= \begin{bmatrix} {}^{\circ}Q_{\circ} \times d_{\circ 2} \times d_{i2} \\ {}^{\circ}Q_{\circ} & {}^{\circ}Z_{\circ} \end{bmatrix} \begin{bmatrix} \dot{o}_{1} \\ \dot{o}_{2} \end{bmatrix} \begin{bmatrix} \dot{o}_{1} \\ \dot{o}_{2} \end{bmatrix}$$

$$= \begin{bmatrix} {}^{\circ}Q_{\circ} \times d_{\circ} \times d_{\circ} \times d_{\circ} \\ {}^{\circ}Q_{\circ} & {}^{\circ}Z_{\circ} \end{bmatrix} \begin{bmatrix} \dot{o}_{1} \\ \dot{o}_{2} \end{bmatrix} \begin{bmatrix} \dot{o}_{1} \\ \dot{o}_{2} \end{bmatrix}$$

$$= \begin{bmatrix} {}^{\circ}Q_{\circ} \times d_{\circ} \times d_{\circ} \times d_{\circ} \\ {}^{\circ}Q_{\circ} & {}^{\circ}Z_{\circ} \end{bmatrix} \begin{bmatrix} \dot{o}_{1} \\ \dot{o}_{2} \end{bmatrix} \begin{bmatrix} \dot{o}_{1} \\ \dot{o}_{2} \end{bmatrix}$$

$$= \begin{bmatrix} {}^{\circ}Q_{\circ} \times d_{\circ} \times d_{\circ} \times d_{\circ} \\ {}^{\circ}Q_{\circ} \times d_{\circ} \times d_{\circ} \times d_{\circ} \end{bmatrix} \begin{bmatrix} \dot{o}_{1} \\ \dot{o}_{2} \end{bmatrix} \begin{bmatrix} \dot{o}_{1} \\ \dot{o}_{2} \end{bmatrix}$$

$$= \begin{bmatrix} {}^{\circ}Q_{\circ} \times d_{\circ} \times d_{\circ} \times d_{\circ} \\ {}^{\circ}Q_{\circ} \times d_{\circ} \times d_{\circ} \times d_{\circ} \end{bmatrix} \begin{bmatrix} \dot{o}_{1} \\ \dot{o}_{2} \end{bmatrix} \begin{bmatrix} \dot{o}_{1} \\ \dot{o}_{2} \end{bmatrix}$$

$$= \begin{bmatrix} {}^{\circ}Q_{\circ} \times d_{\circ} \times d_{\circ$$

ssociate Professor, University of Utah Velocity Jacobian

1st 2 rows are same as J Since July 15 not square, we can't invert it.

Since robot is only 2-DOF, can't independently specify 3 end-effector velocities.

We can only specify & and y and use July to solve for 0, and 02

Principle of virtual work (or power in = power out) 5. $T_1 \dot{O}_1 + T_2 \dot{O}_2 = F_{\chi} \dot{\chi} + F_{y} \dot{y}$ $\begin{bmatrix} Z_1 \\ Z_2 \end{bmatrix} \begin{bmatrix} \dot{o}_1 \\ \dot{o}_2 \end{bmatrix} = \begin{bmatrix} F_x \\ F_y \end{bmatrix} \begin{bmatrix} \dot{x} \\ \dot{y} \end{bmatrix}$ $\begin{bmatrix} \mathcal{I}_{1} \\ \mathcal{I}_{2} \end{bmatrix} \begin{bmatrix} \dot{o}_{1} \\ \dot{o}_{2} \end{bmatrix} = \begin{bmatrix} \mathcal{F}_{x} \\ \mathcal{F}_{y} \end{bmatrix}^{T} \mathcal{J} \begin{bmatrix} \dot{o}_{1} \\ \dot{o}_{2} \end{bmatrix}$ $\begin{bmatrix} \overline{z}_i \\ \overline{z}_i \end{bmatrix}^T = \begin{bmatrix} \overline{k}_i \\ \overline{k}_j \end{bmatrix}^T \overline{J}$ $\begin{bmatrix} \overline{Z_i} \\ \overline{Z_i} \end{bmatrix} = \int_{-\overline{Z_i}}^{T} \left[\frac{F_X}{F_Y} \right]$ If robot is at singularity, force exerted on the end-effector in direction shown will result in zero joint tarque. (Force born entirely by structure)

$$\begin{bmatrix}
T_1 & O_1 + T_2 & O_2 = F_X & X + F_y & Y + T_z & \omega_z \\
T_1 & T_y & O_1 & F_y & T_z & \omega_z
\end{bmatrix} = \begin{bmatrix}
F_X & T_y & Y & T_z & \omega_z \\
F_y & T_z & U_z
\end{bmatrix} = \begin{bmatrix}
F_X & T_y & U_z & U_z
\end{bmatrix} = \begin{bmatrix}
F_X & T_z & U_z & U_z
\end{bmatrix}$$

$$\begin{bmatrix} T_1 \\ T_2 \end{bmatrix} = J_v \begin{bmatrix} F_x \\ F_y \\ T_z \end{bmatrix}$$

Since Jr is not square, we can't invert Jr.

In this case, this means that given a set of joint turques, there is not a unique solution for the end-effector wrench.

i.e. there are multiple combinations of end-effector forces/turque that result in the same joint torques,