Intro to Robot Control - Spring 2023

Problem Set #3 Solutions: Drive Train and Motor Dynamics

- 1. For the planar 2-DOF robot from PS#2:
 - a. Derive the transmission Jacobian as a compounding of gear and pulley effects:

Derive a gear Jacobian:

$$\dot{\Phi} = J_g \dot{\Phi}_m$$

$$\mathbf{J_g} = \begin{bmatrix} \frac{1}{N_1} & 0\\ 0 & \frac{1}{N_2} \end{bmatrix}$$

Derive a pulley Jacobian:

$$\theta_1 = \phi_1$$

$$\theta_2 = -\frac{r_1}{r_2}\phi_1 + \frac{r_1}{r_2}\phi_2$$

$$\dot{\Theta} = J_n \dot{\Phi}$$

$$\mathbf{J}_{\mathbf{p}} = \begin{bmatrix} 1 & 0 \\ -\frac{r_1}{r_2} & \frac{r_1}{r_2} \end{bmatrix}$$

Combine the Jacobians to get the compound transmission Jacobian to go from $\dot{\Phi}_m$ to $\dot{\Theta}$:

$$\dot{\Theta} = J_p \dot{\Phi} = J_p J_g \dot{\Phi}_m$$

$$J_t = J_p J_g$$

$$\mathbf{J_t} = \begin{bmatrix} \frac{1}{N_1} & 0\\ -\frac{r_1}{N_1} & \frac{r_1}{N_2} & \frac{r_1}{N_2} \end{bmatrix}$$

b. When the pulley radii are equal:

$$\mathbf{J_t} = \begin{bmatrix} \frac{1}{N_1} & 0\\ -\frac{r_1}{N_1} & \frac{r_1}{N_2} & \frac{r_1}{N_2} \end{bmatrix} = \begin{bmatrix} \frac{1}{N_1} & 0\\ -\frac{1}{N_1} & \frac{1}{N_2} \end{bmatrix}$$

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c. To map from motor velocities to end-effector velocities:

$$\dot{d}_{02} = J\dot{\Theta} = JJ_t\dot{\Phi}_m$$

where J is the manipulator Jacobian from PS#1.

$$\begin{aligned} \mathbf{J}\mathbf{J_{t}} &= \begin{bmatrix} -a_{1}\sin\theta_{1} - a_{2}\sin(\theta_{1} + \theta_{2}) & -a_{2}\sin(\theta_{1} + \theta_{2}) \\ a_{1}\cos\theta_{1} + a_{2}\cos(\theta_{1} + \theta_{2}) & a_{2}\cos(\theta_{1} + \theta_{2}) \end{bmatrix} \begin{bmatrix} \frac{1}{N_{1}} & 0 \\ -\frac{1}{N_{1}} & \frac{1}{N_{2}} \end{bmatrix} \\ &= \begin{bmatrix} -\frac{a_{1}\sin\theta_{1}}{N_{1}} & -\frac{a_{2}\sin(\theta_{1} + \theta_{2})}{N_{2}} \\ \frac{a_{1}\cos\theta_{1}}{N_{1}} & \frac{a_{2}\cos(\theta_{1} + \theta_{2})}{N_{2}} \end{bmatrix} = \begin{bmatrix} -\frac{a_{1}}{N_{1}}\sin\left(\frac{\phi_{m1}}{N_{1}}\right) & -\frac{a_{2}}{N_{2}}\sin\left(\frac{\phi_{m2}}{N_{2}}\right) \\ \frac{a_{1}}{N_{1}}\cos\left(\frac{\phi_{m1}}{N_{1}}\right) & \frac{a_{2}}{N_{2}}\cos\left(\frac{\phi_{m2}}{N_{2}}\right) \end{bmatrix} \end{aligned}$$

d. Use duality to write a matrix equation relating motor torques to end-effector forces:

$$\tau_m = \mathbf{J}_t^{\mathrm{T}} \mathbf{J}^{\mathrm{T}} F = (\mathbf{J} \mathbf{J}_t)^T F$$

$$(\mathbf{J}\mathbf{J}_{\mathbf{t}})^{T} = \begin{bmatrix} -\frac{a_1}{N_1} \sin\left(\frac{\phi_{m1}}{N_1}\right) & \frac{a_1}{N_1} \cos\left(\frac{\phi_{m1}}{N_1}\right) \\ -\frac{a_2}{N_2} \sin\left(\frac{\phi_{m2}}{N_2}\right) & \frac{a_2}{N_2} \cos\left(\frac{\phi_{m2}}{N_2}\right) \end{bmatrix}$$

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2. For the 2-DOF Quanser Robot from PS#2, combine arm and transmission dynamics a. Combine the dynamics in motor space:

$$\begin{split} \dot{\mathbf{\Theta}} &= \mathbf{J}_{\mathbf{t}}^{\mathbf{\Phi}_{\mathbf{m}}} \\ \boldsymbol{\tau}_{\mathbf{m}} &= \mathbf{J}_{\mathbf{t}}^{\mathbf{T}} \boldsymbol{\tau}_{foint} \\ \boldsymbol{\tau}_{\mathbf{m}} &= \begin{bmatrix} J_{1} & 0 \\ 0 & J_{2} \end{bmatrix} \begin{bmatrix} \ddot{\boldsymbol{\varphi}}_{m1} \\ \ddot{\boldsymbol{\varphi}}_{m2} \end{bmatrix} + \mathbf{J}_{\mathbf{t}}^{\mathbf{T}} \boldsymbol{H}(\boldsymbol{\Theta}) \mathbf{J}_{\mathbf{t}} \begin{bmatrix} \ddot{\boldsymbol{\varphi}}_{m1} \\ \ddot{\boldsymbol{\varphi}}_{m2} \end{bmatrix} + \mathbf{J}_{\mathbf{t}}^{\mathbf{T}} \boldsymbol{V}(\boldsymbol{\Theta}, \dot{\boldsymbol{\Theta}}) + \mathbf{J}_{\mathbf{t}}^{\mathbf{T}} \boldsymbol{G}(\boldsymbol{\Theta}) + \boldsymbol{F}(\dot{\boldsymbol{\Phi}}_{\mathbf{m}}) \\ \boldsymbol{\tau}_{m} &= \boldsymbol{H}'(\boldsymbol{\Phi}_{\mathbf{m}}) \ddot{\boldsymbol{\Phi}}_{\mathbf{m}} + \mathbf{V}(\boldsymbol{\Phi}_{\mathbf{m}}, \dot{\boldsymbol{\Phi}}_{\mathbf{m}}) + \boldsymbol{G}(\boldsymbol{\Phi}_{\mathbf{m}}) + \boldsymbol{F}(\dot{\boldsymbol{\Phi}}_{\mathbf{m}}) \\ \boldsymbol{H}'(\boldsymbol{\Phi}_{\mathbf{m}}) &= \begin{bmatrix} J_{1} & 0 \\ 0 & J_{2} \end{bmatrix} + \begin{bmatrix} J_{1} & -\frac{1}{N_{1}} \\ 0 & \frac{1}{N_{2}} \end{bmatrix} \begin{bmatrix} H_{11} & H_{12} \\ H_{12} & H_{22} \end{bmatrix} \begin{bmatrix} \frac{1}{N_{1}} & 0 \\ -\frac{1}{N_{1}} & \frac{1}{N_{2}} \end{bmatrix} \\ &= \begin{bmatrix} J_{1} & 0 \\ 0 & J_{2} \end{bmatrix} + \begin{bmatrix} \frac{H_{11}}{N_{1}} - \frac{H_{12}}{N_{1}} & \frac{H_{12}}{N_{1}} - \frac{H_{22}}{N_{1}} \\ \frac{H_{12}}{N_{2}} & \frac{H_{22}}{N_{2}} \end{bmatrix} \begin{bmatrix} \frac{1}{N_{1}} & 0 \\ -\frac{1}{N_{1}} & \frac{1}{N_{2}} \end{bmatrix} \\ &= \begin{bmatrix} J_{1} + \frac{H_{11} - 2H_{12} + H_{22}}{N_{1}^{2}} & \frac{H_{12} - H_{22}}{N_{1}N_{2}} \\ \frac{H_{12} - H_{22}}{N_{1}N_{2}} & J_{2} + \frac{H_{22}}{N_{2}^{2}} \end{bmatrix} \\ \boldsymbol{H}'(\boldsymbol{\Phi}_{\mathbf{m}}) &= \begin{bmatrix} J_{1} + \frac{I_{1} + m_{2}\alpha_{1}^{2}}{N_{1}} & \frac{a_{1}r_{12}m_{2}}{N_{1}} \cos \left(\frac{\boldsymbol{\Phi}_{m2}}{N_{2}} - \frac{\boldsymbol{\Phi}_{m1}}{N_{1}}\right) \\ J_{2} + \frac{I_{2}}{N_{2}^{2}} \end{bmatrix} \end{bmatrix} \\ \boldsymbol{V}(\boldsymbol{\Phi}_{\mathbf{m}}, \boldsymbol{\Phi}_{\mathbf{m}}) &= \begin{bmatrix} \frac{1}{N_{1}} & -\frac{1}{N_{1}} \\ 0 & \frac{1}{N_{1}} \end{bmatrix} \begin{bmatrix} 0 & -2h & -h \\ h & 0 & 0 \end{bmatrix} \begin{bmatrix} \dot{\theta}_{1}^{2} \\ \dot{\theta}_{1} \dot{\theta}_{2} \\ \dot{\theta}_{2}^{2} \end{bmatrix}} \end{aligned}$$

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$$= \begin{bmatrix} -\frac{h}{N_{1}} & -\frac{2h}{N_{1}} & -\frac{h}{N_{1}} \\ \frac{h}{N_{2}} & 0 & 0 \end{bmatrix} \begin{bmatrix} \frac{\dot{\phi}_{m1}}{N_{1}} \begin{pmatrix} \dot{\phi}_{m2} \\ \frac{\dot{\phi}_{m1}}{N_{1}} \begin{pmatrix} \dot{\phi}_{m2} - \dot{\phi}_{m1} \\ \frac{\dot{\phi}_{m2}}{N_{2}} - \frac{\dot{\phi}_{m1}}{N_{1}} \end{pmatrix} \\ \frac{\dot{\phi}_{m1}}{N_{2}} \begin{pmatrix} \frac{\dot{\phi}_{m2}}{N_{2}} - \frac{\dot{\phi}_{m1}}{N_{1}} \\ \frac{\dot{\phi}_{m1}}{N_{2}} \begin{pmatrix} \frac{\dot{\phi}_{m2}}{N_{2}} - \frac{\dot{\phi}_{m1}}{N_{1}} \\ \frac{\dot{\phi}_{m1}}{N_{1}} \begin{pmatrix} \frac{\dot{\phi}_{m2}}{N_{2}} - \frac{\dot{\phi}_{m1}}{N_{1}} \\ \frac{\dot{\phi}_{m2}}{N_{2}} - \frac{\dot{\phi}_{m1}}{N_{1}} \end{pmatrix}^{2} \end{bmatrix}$$

$$= \begin{bmatrix} -\frac{h}{\dot{\phi}_{m1}^{2}} - \frac{2h}{N_{1}^{2}N_{2}} \dot{\phi}_{m1} \dot{\phi}_{m2} + \frac{2h}{N_{1}^{2}N_{2}} \dot{\phi}_{m1} \dot{\phi}_{m2} - \frac{h}{N_{1}^{2}} \dot{\phi}_{m1}^{2} \\ \frac{\dot{\phi}_{m1}}{N_{1}^{2}N_{2}} \end{bmatrix}$$

$$V(\mathbf{\Phi}_{\mathbf{m}}, \dot{\mathbf{\Phi}}_{\mathbf{m}}) = \begin{bmatrix} 0 & -\frac{h}{N_{1}N_{2}^{2}} \\ \frac{h}{N_{2}^{2}N_{2}} & 0 \end{bmatrix} \begin{bmatrix} \dot{\phi}_{m1}^{2} \\ \dot{\phi}_{m2}^{2} \end{bmatrix}$$

Where:

$$h = a_1 r_{12} m_2 sin(\theta_2) = a_1 r_{12} m_2 sin(\frac{\phi_{m2}}{N_2} - \frac{\phi_{m1}}{N_1})$$

$$\mathbf{G}(\mathbf{\Phi_m}) = \begin{bmatrix} \frac{1}{N_1} & -\frac{1}{N_1} \\ 0 & \frac{1}{N_2} \end{bmatrix} \begin{bmatrix} G_1 \\ G_2 \end{bmatrix} = \begin{bmatrix} \frac{G_1 - G_2}{N_1} \\ \frac{G_2}{N_2} \end{bmatrix} = \begin{bmatrix} (r_{01}m_1 + a_1m_2) \frac{g}{N_1} \cos\left(\frac{\phi_{m1}}{N_1}\right) \\ r_{12} m_2 \frac{g}{N_2} \cos\left(\frac{\phi_{m2}}{N_2}\right) \end{bmatrix}$$

$$\mathbf{F}(\dot{\mathbf{\Phi}}_{\mathbf{m}}) = \begin{bmatrix} b_1 \dot{\phi}_{m1} + c_1 * sgn(\dot{\phi}_{m1}) \\ b_2 \dot{\phi}_{m2} + c_2 * sgn(\dot{\phi}_{m2}) \end{bmatrix}$$

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b. Combine the dynamics in joint space:

$$\begin{split} \boldsymbol{\tau_{joint}} &= \mathbf{J_t^{-T}} \boldsymbol{\tau_m} \\ \dot{\boldsymbol{\Phi}_m} &= \mathbf{J_t^{-T}} \boldsymbol{\Theta} \\ \\ \mathbf{J_t^{-1}} &= \begin{bmatrix} \frac{1}{N_1} & 0 \\ -\frac{1}{N_1} & \frac{1}{N_2} \end{bmatrix}^{-1} = \begin{bmatrix} N_1 & 0 \\ N_2 & N_2 \end{bmatrix} \\ \\ \boldsymbol{\tau_{joint}} &= \mathbf{J_t^{-T}} \begin{bmatrix} J_1 & 0 \\ 0 & J_2 \end{bmatrix} \mathbf{J_t^{-1}} \begin{bmatrix} \ddot{\theta}_1 \\ \ddot{\theta}_2 \end{bmatrix} + \mathbf{J_t^{-T}} F(\dot{\boldsymbol{\Phi}_m}) + \mathbf{H}(\boldsymbol{\Theta}) \ddot{\boldsymbol{\Theta}} + \mathbf{V}(\boldsymbol{\Theta}, \dot{\boldsymbol{\Theta}}) + \mathbf{G}(\boldsymbol{\Theta}) \\ \\ \boldsymbol{\tau_{joint}} &= \boldsymbol{H'}(\boldsymbol{\Theta}) \ddot{\boldsymbol{\Theta}} + \mathbf{V}(\boldsymbol{\Theta}, \dot{\boldsymbol{\Theta}}) + \boldsymbol{G}(\boldsymbol{\Theta}) + F(\dot{\boldsymbol{\Theta}}) \\ \\ \boldsymbol{H'}(\boldsymbol{\Theta}) &= \mathbf{J_t^{-T}} \boldsymbol{\tau_{J}} \mathbf{J_t^{-1}} + \boldsymbol{H}(\boldsymbol{\Theta}) \\ &= \begin{bmatrix} N_1 & N_2 \\ 0 & N_2 \end{bmatrix} \begin{bmatrix} J_1 & 0 \\ 0 & J_2 \end{bmatrix} \begin{bmatrix} N_1 & 0 \\ N_2 & N_2 \end{bmatrix} + \begin{bmatrix} H_{11} & H_{12} \\ H_{12} & H_{22} \end{bmatrix} \\ &= \begin{bmatrix} N_1^2 J_1 + N_2^2 J_2 & N_2^2 J_2 \\ N_2^2 J_2 & N_2^2 J_2 \end{bmatrix} + \begin{bmatrix} H_{11} & H_{12} \\ H_{12} & H_{22} \end{bmatrix} \\ &= \begin{bmatrix} H_{11} + N_1^2 J_1 + N_2^2 J_2 & H_{12} + N_2^2 J_2 \\ H_{12} + N_2^2 J_2 & H_{22} + N_2^2 J_2 \end{bmatrix} \\ F(\dot{\boldsymbol{\Theta}}) &= \mathbf{J_t^{-T}} F(\dot{\boldsymbol{\Phi}_m}) = \begin{bmatrix} N_1 & N_2 \\ 0 & N_2 \end{bmatrix} \begin{bmatrix} b_1 N_1 \dot{\theta}_1 + c_1 * sgn(N_1 \dot{\theta}_1) \\ b_2 (N_2 \dot{\theta}_1 + N_2 \dot{\theta}_2) + c_2 * sgn(N_2 \dot{\theta}_1 + N_2 \dot{\theta}_2) \end{bmatrix} \\ &= \begin{bmatrix} b_1 N_1^2 \dot{\theta}_1 + b_1 N_2^2 (\dot{\theta}_1 + \dot{\theta}_2) + c_1 N_1 sgn(\dot{\theta}_1) + c_2 N_2 sgn(\dot{\theta}_1 + \dot{\theta}_2) \\ b_2 N_2^2 (\dot{\theta}_1 + \dot{\theta}_2) + c_2 N_2 sgn(\dot{\theta}_1 + \dot{\theta}_2) \end{bmatrix} \end{split}$$

V and G are same as originally derived in PS#2 because they are already in joint space.

$$\mathbf{V}(\mathbf{\Theta}, \dot{\mathbf{\Theta}}) = \begin{bmatrix} 0 & -2h & -h \\ h & 0 & 0 \end{bmatrix} \begin{bmatrix} \dot{\theta}_1^2 \\ \dot{\theta}_1 \dot{\theta}_2 \\ \dot{\theta}_2^2 \end{bmatrix}$$

$$\mathbf{G}(\mathbf{\Theta}) = \begin{bmatrix} (r_{01}m_1 + a_1m_2)g\cos(\theta_1) + r_{12}m_2g\cos(\theta_1 + \theta_2) \\ r_{12}m_2g\cos(\theta_1 + \theta_2) \end{bmatrix}$$

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c. Use gear Jacobian to reflect dynamics to encoder space

$$\begin{split} \boldsymbol{\tau}_{m} &= \boldsymbol{H}'(\boldsymbol{\Phi}_{m}) \ddot{\boldsymbol{\Phi}}_{m} + \boldsymbol{V}(\boldsymbol{\Phi}_{m}, \dot{\boldsymbol{\Phi}}_{m}) + \boldsymbol{G}(\boldsymbol{\Phi}_{m}) + \boldsymbol{F}(\dot{\boldsymbol{\Phi}}_{m}) \\ \dot{\boldsymbol{\Phi}}_{m} &= \mathbf{J}_{g}^{-1} \dot{\boldsymbol{\Phi}} \quad \text{where} \quad \mathbf{J}_{g}^{-1} = \begin{bmatrix} N_{1} & 0 \\ 0 & N_{2} \end{bmatrix} \\ \boldsymbol{\tau}_{e} &= \mathbf{J}_{g}^{-T} \boldsymbol{\tau}_{m} = \mathbf{J}_{g}^{-T} \boldsymbol{H}'(\boldsymbol{\Phi}_{m}) \mathbf{J}_{g}^{-1} \dot{\boldsymbol{\Phi}} + \mathbf{J}_{g}^{-T} \boldsymbol{V}(\boldsymbol{\Phi}_{m}, \dot{\boldsymbol{\Phi}}_{m}) + \mathbf{J}_{g}^{-T} \boldsymbol{G}(\boldsymbol{\Phi}_{m}) + \mathbf{J}_{g}^{-T} \boldsymbol{F}(\dot{\boldsymbol{\Phi}}_{m}) \\ \boldsymbol{\tau}_{e} &= \boldsymbol{H}'(\boldsymbol{\Phi}) \ddot{\boldsymbol{\Phi}} + \boldsymbol{V}(\boldsymbol{\Phi}, \dot{\boldsymbol{\Phi}}) + \boldsymbol{G}(\boldsymbol{\Phi}) + \boldsymbol{F}(\dot{\boldsymbol{\Phi}}) \\ \boldsymbol{H}'(\boldsymbol{\Phi}) &= \begin{bmatrix} N_{1} & 0 \\ 0 & N_{2} \end{bmatrix} \begin{bmatrix} J_{1} + \frac{I_{1} + m_{2}a_{1}^{2}}{N_{1}^{2}} & \frac{a_{1}r_{12}m_{2}}{N_{1}N_{2}} \cos\left(\frac{\phi_{m2}}{N_{2}} - \frac{\phi_{m1}}{N_{1}}\right) \\ \frac{a_{1}r_{12}m_{2}}{N_{1}N_{2}} \cos\left(\frac{\phi_{m2}}{N_{2}} - \frac{\phi_{m1}}{N_{1}}\right) & J_{2} + \frac{I_{2}}{N_{2}^{2}} \end{bmatrix} \begin{bmatrix} N_{1} & 0 \\ 0 & N_{2} \end{bmatrix} \\ &= \begin{bmatrix} N_{1}^{2} J_{1} + I_{1} + m_{2}a_{1}^{2} & a_{1}r_{12}m_{2}\cos(\phi_{2} - \phi_{1}) \\ a_{1}r_{12}m_{2}\cos(\phi_{2} - \phi_{1}) & N_{2}^{2} J_{2} + I_{2} \end{bmatrix} \\ \boldsymbol{V}(\boldsymbol{\Phi}, \dot{\boldsymbol{\Phi}}) &= \begin{bmatrix} N_{1} & 0 \\ 0 & N_{2} \end{bmatrix} \begin{bmatrix} 0 & -\frac{h}{N_{1}N_{2}^{2}} \\ \frac{h}{N_{1}^{2}N_{2}} & 0 \end{bmatrix} \begin{bmatrix} \dot{\phi}_{1m}^{2} \\ \dot{\phi}_{2m}^{2} \end{bmatrix} = \begin{bmatrix} 0 & -\frac{h}{N_{2}^{2}} \\ \frac{h}{N_{2}^{2}} \dot{\phi}_{2}^{2} \end{bmatrix} = \begin{bmatrix} 0 & -h \\ h & 0 \end{bmatrix} \begin{bmatrix} \dot{\phi}_{1}^{2} \\ \dot{\phi}_{2}^{2} \end{bmatrix} \end{aligned}$$

where

$$h = a_1 r_{12} m_2 \sin(\phi_2 - \phi_1)$$

$$\boldsymbol{G}(\boldsymbol{\Phi}) = \begin{bmatrix} N_1 & 0 \\ 0 & N_2 \end{bmatrix} \begin{bmatrix} (r_{01}m_1 + a_1m_2) \frac{g}{N_1} \cos\left(\frac{\phi_{m1}}{N_1}\right) \\ \frac{r_{12} m_2 g}{N_2} \cos\left(\frac{\phi_{m2}}{N_2}\right) \end{bmatrix} = \begin{bmatrix} (r_{01}m_1 + a_1m_2) g \cos(\phi_1) \\ r_{12} m_2 g \cos(\phi_2) \end{bmatrix}$$

$$\begin{aligned} \boldsymbol{F}(\boldsymbol{\Phi}) &= \begin{bmatrix} N_1 & 0 \\ 0 & N_2 \end{bmatrix} \begin{bmatrix} b_1 & 0 \\ 0 & b_2 \end{bmatrix} \begin{bmatrix} N_1 & 0 \\ 0 & N_2 \end{bmatrix} \begin{bmatrix} \dot{\phi}_1 \\ \dot{\phi}_2 \end{bmatrix} + \begin{bmatrix} N_1 & 0 \\ 0 & N_2 \end{bmatrix} \begin{bmatrix} c_1 & 0 \\ 0 & c_2 \end{bmatrix} sgn\left(\begin{bmatrix} N_1 & 0 \\ 0 & N_2 \end{bmatrix} \begin{bmatrix} \dot{\phi}_1 \\ \dot{\phi}_2 \end{bmatrix} \right) \\ &= \begin{bmatrix} N_1^2 b_1 & 0 \\ 0 & N_2^2 b_2 \end{bmatrix} \begin{bmatrix} \dot{\phi}_1 \\ \dot{\phi}_2 \end{bmatrix} + \begin{bmatrix} N_1 c_1 * sgn(\dot{\phi}_1) \\ N_2 c_2 * sgn(\dot{\phi}_2) \end{bmatrix} \end{aligned}$$

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- 3. Include motor dynamics:
 - a. Current control:

$$\mathbf{J}_{\mathbf{g}}^{\mathsf{T}}\boldsymbol{\tau}_{m} = \boldsymbol{H}'(\boldsymbol{\Phi})\ddot{\boldsymbol{\Phi}} + \mathbf{V}(\boldsymbol{\Phi},\dot{\boldsymbol{\Phi}}) + \boldsymbol{G}(\boldsymbol{\Phi}) + \boldsymbol{F}(\dot{\boldsymbol{\Phi}})$$

$$\boldsymbol{\tau}_{mi} = k_{ti}\,i_{i}(t)$$

$$\begin{bmatrix} N_{1} & 0 \\ 0 & N_{2} \end{bmatrix} \begin{bmatrix} k_{t_{1}}i_{1}(t) \\ k_{t_{2}}i_{2}(t) \end{bmatrix} = \boldsymbol{H}'(\boldsymbol{\Phi})\ddot{\boldsymbol{\Phi}} + \mathbf{V}(\boldsymbol{\Phi},\dot{\boldsymbol{\Phi}}) + \boldsymbol{G}(\boldsymbol{\Phi}) + \boldsymbol{F}(\dot{\boldsymbol{\Phi}})$$
So
$$\begin{bmatrix} A_{1}i_{1}(t) \\ A_{2}i_{2}(t) \end{bmatrix} = \boldsymbol{H}'(\boldsymbol{\Phi})\ddot{\boldsymbol{\Phi}} + \mathbf{V}(\boldsymbol{\Phi},\dot{\boldsymbol{\Phi}}) + \boldsymbol{G}(\boldsymbol{\Phi}) + \boldsymbol{F}(\dot{\boldsymbol{\Phi}})$$
Where
$$\begin{bmatrix} A_{1} \\ A_{2} \end{bmatrix} = \begin{bmatrix} N_{1}k_{t_{1}} \\ N_{2}k_{t_{2}} \end{bmatrix}$$

b. Voltage control:

Voltage control.
$$\mathbf{J}_{\mathbf{g}}^{\mathbf{T}}\boldsymbol{\tau}_{m} = \boldsymbol{H}'(\boldsymbol{\Phi})\ddot{\boldsymbol{\Phi}} + \mathbf{V}(\boldsymbol{\Phi},\dot{\boldsymbol{\Phi}}) + \boldsymbol{G}(\boldsymbol{\Phi}) + \boldsymbol{F}(\dot{\boldsymbol{\Phi}})$$

$$V_{i}(t) = R_{i} \frac{\tau_{mi}}{k_{ti}} + k_{ti} \dot{\phi}_{mi}$$

$$\tau_{mi} = \frac{k_{ti}}{R_{i}} V_{i}(t) - \frac{k_{ti}^{2}}{R_{i}} N_{i} \dot{\phi}_{i}$$

$$\begin{bmatrix} N_{1} & 0 \\ 0 & N_{2} \end{bmatrix} \begin{bmatrix} \frac{k_{t_{1}}}{R_{1}} V_{1}(t) - \frac{k_{t_{1}}^{2}}{R_{1}} N_{1} \dot{\phi}_{1} \\ \frac{k_{t_{2}}}{R_{2}} V_{2}(t) - \frac{k_{t_{2}}^{2}}{R_{2}} N_{2} \dot{\phi}_{2} \end{bmatrix} = \boldsymbol{H}'(\boldsymbol{\Phi}) \ddot{\boldsymbol{\Phi}} + \mathbf{V}(\boldsymbol{\Phi},\dot{\boldsymbol{\Phi}}) + \boldsymbol{G}(\boldsymbol{\Phi}) + \boldsymbol{F}(\dot{\boldsymbol{\Phi}})$$
 So
$$\begin{bmatrix} A_{1}V_{1}(t) \\ A_{2}V_{2}(t) \end{bmatrix} = \boldsymbol{H}'(\boldsymbol{\Phi}) \ddot{\boldsymbol{\Phi}} + \mathbf{V}(\boldsymbol{\Phi},\dot{\boldsymbol{\Phi}}) + \boldsymbol{G}(\boldsymbol{\Phi}) + \boldsymbol{F}'(\dot{\boldsymbol{\Phi}})$$

where

$$\begin{bmatrix} A_1 \\ A_2 \end{bmatrix} = \begin{bmatrix} N_1 \frac{k_{t_1}}{R_1} \\ N_2 \frac{k_{t_2}}{R_2} \end{bmatrix}$$

and
$$F'(\dot{\Phi}) = \begin{bmatrix} N_1^2 \left(b_1 + \frac{k_{t_1}^2}{R_1} \right) & 0 \\ 0 & N_2^2 \left(b_2 + \frac{k_{t_2}^2}{R_2} \right) \end{bmatrix} \begin{bmatrix} \dot{\phi}_1 \\ \dot{\phi}_2 \end{bmatrix} + \begin{bmatrix} N_1 c_1 * sgn(\dot{\phi}_1) \\ N_2 c_2 * sgn(\dot{\phi}_2) \end{bmatrix}$$

Note that with voltage control, the back EMF adds to the viscous damping terms