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Title: Module 4 - Part 2 - Hand Calculation Methods

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Module 4 – Part 2 Hand Calculation Methods

Section 1 - Array Methods

Presented by: Mark Mitchell



Array Methods

- Limiting surface density method, NB_{N^2}
 - Calculate the critical c-t-c spacing of units of a given mass in a cubic array
 - Accounts for up to 200 mm of water reflection
- Surface density method
 - Calculate the subcritical c-t-c spacing of units of a given mass in an array that is limited in one dimension
 - Accounts for up to 155 mm of water reflection
- Density analog method
 - Calculate the subcritical c-t-c spacing of units of a given mass in a cubic array
 - Accounts for up to 200 mm of water reflection



Array Methods

- Solid angle method
 - Developed as a quick, empirical means of evaluating interaction between small numbers of fissile units
 - In terms of total solid angle, Ω
 - -Maximum acceptable $k_{\it eff}$ of individual units a function of Ω
 - Accounts for thick water reflection



Applicability

- Useful for determining the critical center-to-center spacing for fissile materials stored or staged in array configurations of any shape (>64 units)
- Useful for irregular shapes such as equipment stored on the floor

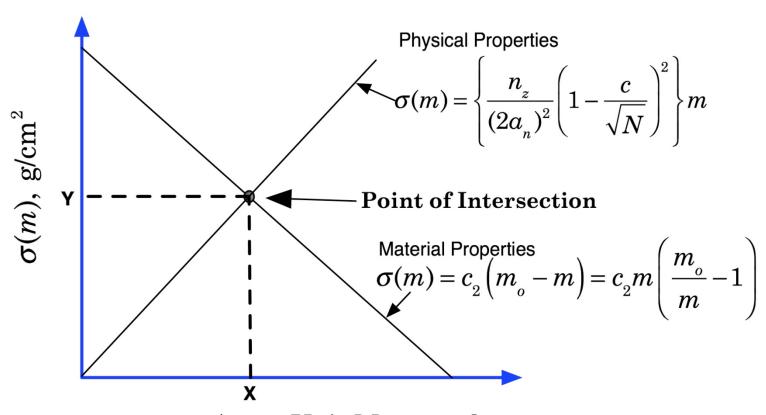
Need to know:

- Fissile unit stack height
- A characteristic constant (c₂) that is a function of the material properties of the array
- Critical mass of an unreflected sphere of the fissile material in the array
- Mass of the fissile material in each array unit

Method Details

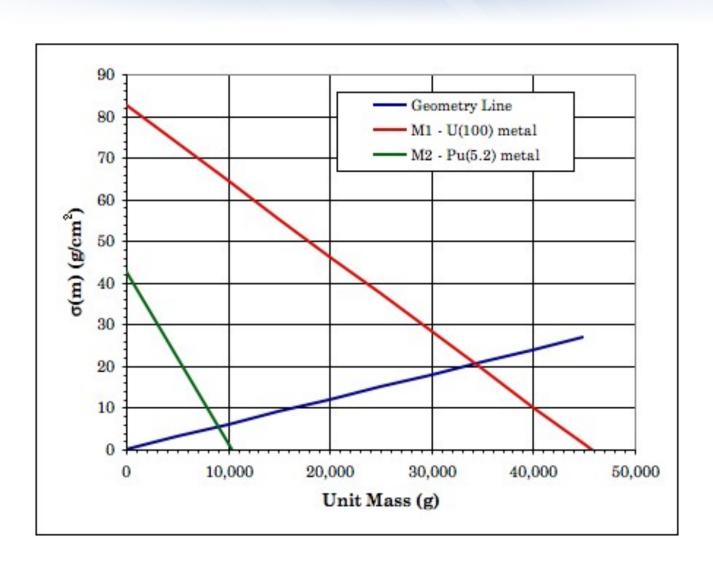
- Developed for U(93.2) spherical metal units can be modified for all fissile materials that have Thomas data
- Considers 20 cm of water reflection surrounding the array





Array Unit Mass, m, kg Required for criticality







$$\frac{\sigma(m)}{m} = \frac{n_z}{(2a_n)^2} \left(1 - \frac{c}{\sqrt{N}}\right)^2 = c_2 \left(\frac{m_o}{m} - 1\right)$$

The array unit mass, *m*, is required for a critical array:

$$m = m_o \left[\frac{n_z}{c_2 (2a_n)^2} \left(1 - \frac{c}{\sqrt{N}} \right)^2 + 1 \right]^{-1}$$

The array unit center-to-center spacing, $2a_n$, is required for a critical array:

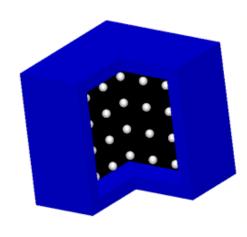
$$d = (2a_n) = \left[\frac{n_z \left(1 - \frac{c}{\sqrt{N}}\right)^2}{c_2 \left(\frac{m_o}{m} - 1\right)}\right]^{\frac{1}{2}}.$$



- c₂ a constant that depends on all of the material properties of the arrays except for the mass, m, and is also equal to the slope of the "material-line" (cm⁻²)
 - the Primer provides Thomas' values for this constant for various fissile systems,
- c an empirically determined constant equal to 0.55 ± 0.18 for the range of fissile materials and arrays studied by Thomas.
 - tends toward zero in a thermal system (i.e., moderated units in the array)



Graphical LSD Example:



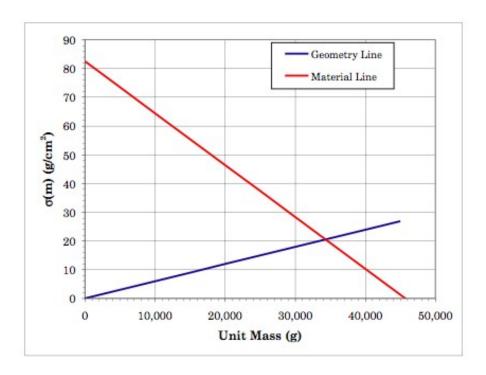
- 4x4x4 Array
- 76.2 cm (30" c-to-c spacing between units)
- •U (100) metal units
- •Determine unit mass for array criticality

Geometry Line:
$$\sigma(m) = \frac{n_z m}{(2a_n)^2} \left(1 - \frac{c}{\sqrt{N}}\right)^2 = \frac{4m}{(2 \times 38.1 \text{ cm})^2} \left(1 - \frac{0.55}{\sqrt{64}}\right)^2$$

$$\sigma(m) = 5.974 \times 10^{-4} m$$
 or $\frac{\sigma(m)}{m} = 5.974 \times 10^{-4}$

Material Line: $\sigma(m) = c_2(m_0 - m)$

$$\sigma(m) = 1.806 \times 10^{-3} \left(45.68 - m \right)$$
 or $\frac{\sigma(m)}{m} = 1.806 \times 10^{-3} \left(\frac{45.68}{m} - 1 \right)$





- Applicability
 - Useful for determining the subcritical center-to-center spacing for fissile materials stored or staged in finite array configurations where the size of the array is controlled in one direction
 - Useful for irregular shapes such as equipment stored on the floor
- Need to know:
 - Fissile unit stack height
 - Critical dimensions for an infinite water-reflected critical slab
 - Critical mass of an unreflected sphere of the fissile material in the array
 - Mass of the fissile material in each array unit
- Method Details
 - Infinite planar array, finite height
 - Derived from limiting surface density relationships
 - Maximum k_{eff} for an individual array unit cannot be larger than 0.9 (~73% of the critical mass)
 - Provides a center-to-center spacing result that is subcritical

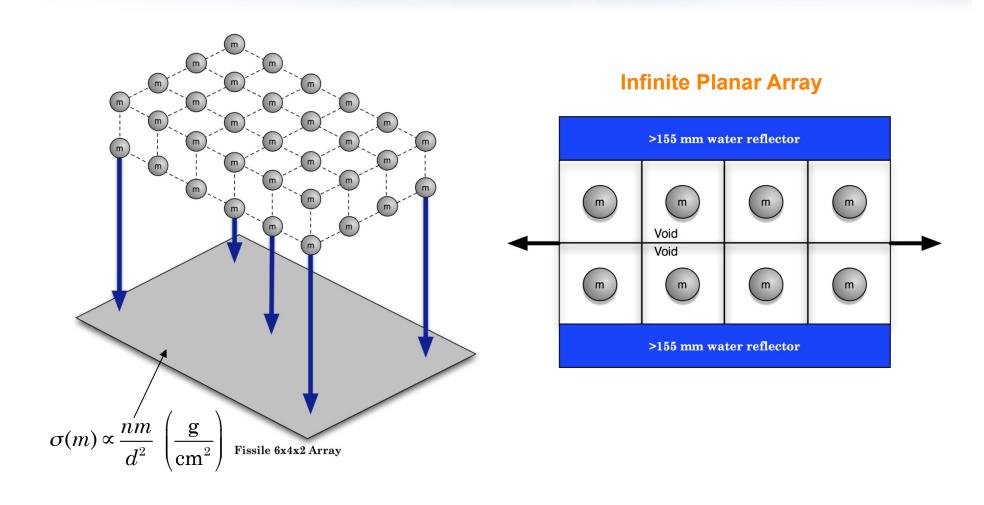


From the limiting surface density technique:

Geometry Line:
$$\sigma(m) = \frac{n_z m}{(2a_n)^2} \left(1 - \frac{c}{\sqrt{N}}\right)^2 = \frac{nm}{d^2} c_3$$

$$\sigma(m) \propto \frac{nm}{d^2}$$







From the limiting surface density technique:

Material Line:
$$\sigma(m) = c_2(m_o - m) = c_2 m_o \left(1 - \frac{m}{m_o}\right) = c_4 \sigma_o \left(1 - f\right)$$

$$\sigma(m) \propto \sigma_0 \left(1-f\right)$$

• Therefore:

$$d = \left[\frac{c_3 nm}{c_4 \sigma_o (1-f)}\right]^{\frac{1}{2}} = \left|\frac{nm}{\frac{c_4}{c_3} \sigma_o (1-f)}\right|^2$$

Note: d approaches infinity as f approaches 1



Remember:

$$k_{\text{eff}} = (f)^{\frac{1}{3}}$$

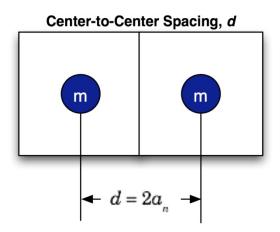
• If we want to limit k_{eff} of each array unit to a maximum of 0.90:

$$f = (k_{eff})^3 = (0.90)^3 = 0.73$$

We must limit f to a maximum of 0.73:

$$d = \left[\frac{nm}{\frac{c_4}{c_3} \sigma_o \left(1 - \frac{f}{0.73} \right)} \right]^{\frac{1}{2}} = c_5 \left[\frac{nm}{\sigma_o \left(1 - 1.37f \right)} \right]^{\frac{1}{2}}$$





$$d = \left[\frac{nm}{0.54\sigma_0 \left(1 - 1.37f\right)}\right]^{\frac{1}{2}} \cong 1.37 \left[\frac{nm}{\sigma_0 \left(1 - 1.37\frac{m}{m_0}\right)}\right]^{\frac{1}{2}}$$

- The coefficient 0.54 represents the product of two factors
 - Array shape
 - Array reflecting materials
 - Concrete vs. water reflected arrays
- The coefficient σ_o is the surface density of the critical water-reflected infinite slab (g/cm²)
- Provides a subcritical result for the center-to-center spacing
- Individual units with a k_{eff}>0.9 (73% of the critical mass) results in an infinite center-to-center spacing result
- May require an administrative control on the array height

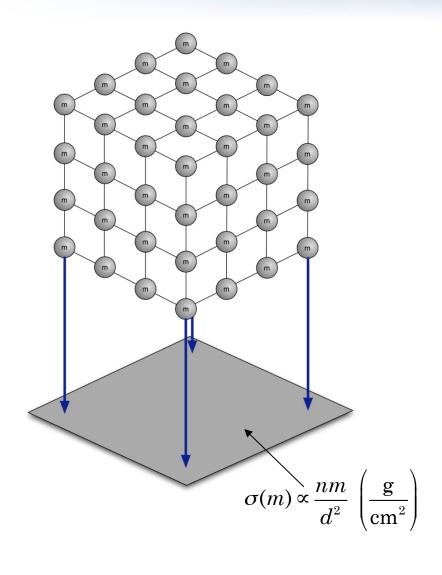


Density Analog Method

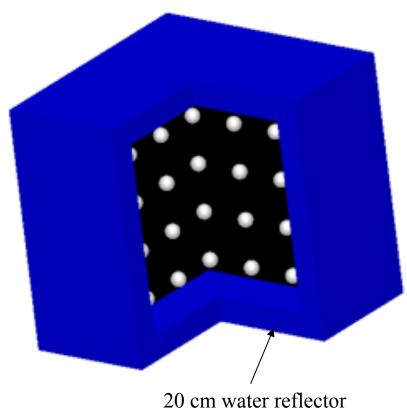
- Applicability
 - Useful for determining the subcritical center-to-center spacing for fissile materials stored or staged in array configurations of any shape
 - Useful for irregular shapes such as equipment stored on the floor
- Need to know:
 - Fissile unit stack height
 - Critical dimensions for an infinite water-reflected critical slab
 - Critical mass of an unreflected sphere of the fissile material in the array
 - Mass of the fissile material in each array unit
- Method Details
 - Cubic array configuration
 - Considers 20 cm of water reflection surrounding the cubic array



Density Analog Method

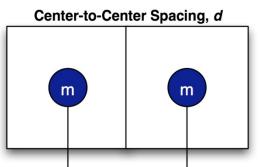


Finite Cubic Array





Density Analog Method



 $-d = 2a_n -$

$$d = \left[\frac{nm}{2.1\sigma_0\left(1-1.37f\right)}\right]^{\frac{1}{2}} \cong 0.69 \left[\frac{nm}{\sigma_0\left(1-1.37\frac{m}{m_0}\right)}\right]^{\frac{1}{2}}$$
 the critical mass) results in an infinite center-to-center spacing result • Can be used for arrays of any shape

- The coefficient 2.1 represents experimental and calculational data for cubic arrangements of fissile materials
- σ_0 is the surface density of the critical water-reflected infinite slab (g/cm²)
- Provides a subcritical result for the center-to-center spacing
- Individual units with a k_{eff}>0.9 (73% of the critical mass) results in an infinite

Array Methods Example Results/Comparison

 What is the minimum center-to-center spacing of an array of 4,500 g Pu(5) metal ingots?

Case	SD	DA	LSD	Code Result
2x2x2		26 cm	Not applicable	15 cm
10x10x10		57 cm	42 cm	41.7 cm
100x100x100		182 cm	136 cm	137 cm
Infinite Planar Array (1 unit high)	36 cm			25 cm



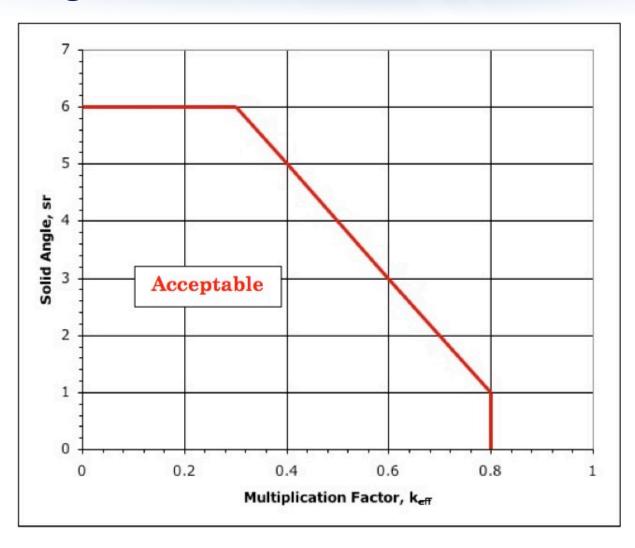
- The basic idea behind this method is that the subcriticality of an array configuration depends on
 - The k_{eff} of a single representative unit in the array, and
 - The probability that a neutron leaking out of this unit will interact with (cause fission in) another unit in the array
- The probability that a leaking neutron will interact with another unit in the array is dependent upon total solid angle, Ω, at the most central unit, or at the most reactive unit, by all other units in the array



- The following conditions must be satisfied in order to apply the method:
 - The k_{eff} of any bare unit shall not exceed 0.8
 - Each unit shall be subcritical when completely reflected by water
 - The minimum surface-to-surface separation between units shall be 0.3 m, and
 - The allowed solid angle, Ω , shall not exceed 6 sr

$$- \Omega_{allowed} = 9 - 10 k_{eff}$$



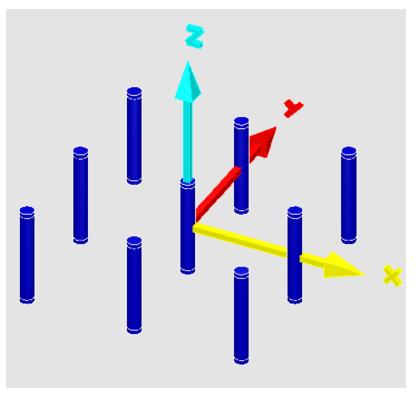




Point-to-Sphere	Point-to-Cylinder	Point-to-Plane	Point-to-Disk
Р H — R	P H	P H B	P H → R
$\Omega=2\pi\left(1-\frac{1}{\sqrt{1+\left(R/H\right)^2}}\right)$ where $R=Radius\ of\ the\ sphere.$ H=Distance from the point to the surface of the sphere.	$\Omega = \frac{LD}{H\sqrt{\left(L/2\right)^2 + H^2}}$ where	$\Omega = \sin^{-1}\left(\frac{AB}{\sqrt{A^2 + H^2}\sqrt{B^2 + H^2}}\right)$ where $A = \text{Length of one side of the plane}$ $B = \text{Length of the other side of the plane}$ $H = \text{Perpendicular distance from the}$ point to the plane. If the point, P , is directly above the center of the plane (not directly over a corner as shown in the figure) with dimensions $2A \times 2B$, multiply Ω by 4 to obtain the solid angle.	$\Omega = 2\pi \left(1 - \frac{1}{\sqrt{1 + \left(R/H\right)^2}}\right) \leq \frac{\pi R^2}{H^3}$ where $R = \text{Radius of the disk}$ $H = \text{Distance from the point P to the surface of the disk}.$



- Problem: We want to store nine "safe"-bottles of fissile solution in a 3-by-3 array with 2-foot edge-to-edge spacing
- Question: What is the highest k_{eff} that each bottle can have as a single unit and still be subcritical in the array?
 - Each bottle is 4-feet tall
 - Each bottle diameter ½foot

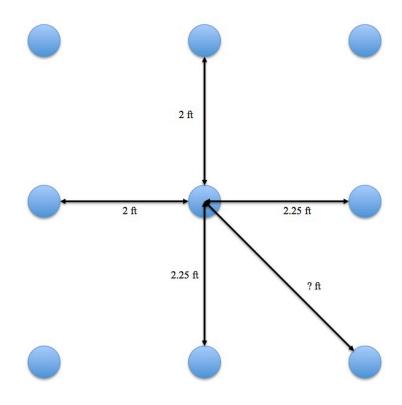




Question: What unit is the most reactive unit? Why?

$$- H_n = ?$$

$$-H_{f} = ?$$

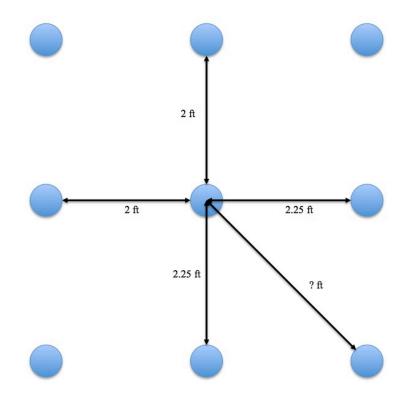




Question: What unit is the most reactive unit? Why?

$$- H_n = 2 ft + \left[\frac{\frac{1}{2} ft}{2} \right] = 2.25 ft$$

$$-H_{f} = ?$$





Question: What unit is the most reactive unit? Why?

$$-H_{n} = 2 ft + \left[\frac{1}{2} \frac{ft}{2}\right] = 2.25 ft$$

$$-\left[H_{f} + \left(\frac{1}{2} \frac{ft}{2}\right)\right]^{2} = \left[2.5 ft\right]^{2} + \left[2.5 ft\right]^{2}$$

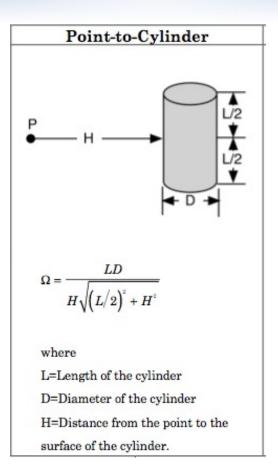
$$H_{f} = 3.29 ft$$



$$-\Omega_n=?$$

$$-\Omega_f=?$$

$$-\Omega_{total}=?$$

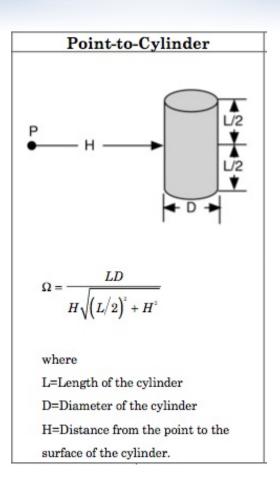




$$-\Omega_{n} = \frac{\left(4 \text{ ft}\right)\left(\frac{1}{2} \text{ ft}\right)}{2.25 \text{ ft}\left[\left(\frac{4 \text{ ft}}{2}\right)^{2} + \left(2.25 \text{ ft}\right)^{2}\right]^{\frac{1}{2}}} = 0.30 \text{ SR}$$

$$\Omega_f = ?$$

$$-\Omega_{total}=?$$

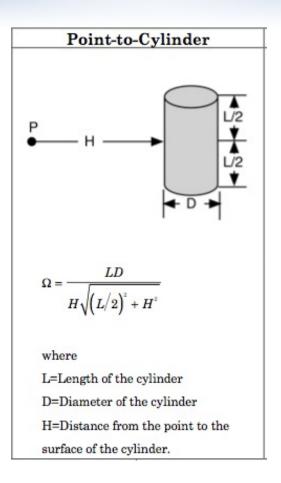




$$-\Omega_{n} = \frac{\left(4 \text{ ft}\right)\left(\frac{1}{2} \text{ ft}\right)}{2.25 \text{ ft}\left[\left(\frac{4 \text{ ft}}{2}\right)^{2} + \left(2.25 \text{ ft}\right)^{2}\right]^{\frac{1}{2}}} = 0.30 \text{ SR}$$

$$-\Omega_{f} = \frac{\left(4 \text{ ft}\right)\left(\frac{1}{2} \text{ ft}\right)}{3.29 \text{ ft}\left[\left(\frac{4 \text{ ft}}{2}\right)^{2} + \left(3.29 \text{ ft}\right)^{2}\right]^{\frac{1}{2}}} = 0.16 \text{ SR}$$

$$-\Omega_{total}=?$$

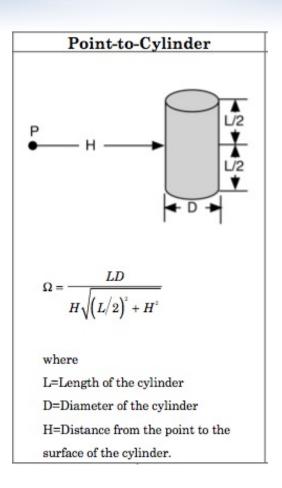




$$-\Omega_{n} = \frac{\left(4 \text{ ft}\right)\left(\frac{1}{2} \text{ ft}\right)}{2.25 \text{ ft}\left[\left(\frac{4 \text{ ft}}{2}\right)^{2} + \left(2.25 \text{ ft}\right)^{2}\right]^{\frac{1}{2}}} = 0.30 \text{ SR}$$

$$-\Omega_{f} = \frac{\left(4 \text{ ft}\right)\left(\frac{1}{2} \text{ ft}\right)}{3.29 \text{ ft}\left[\left(\frac{4 \text{ ft}}{2}\right)^{2} + \left(3.29 \text{ ft}\right)^{2}\right]^{\frac{1}{2}}} = 0.16 \text{ SR}$$

$$-\Omega_{total} = 4\Omega_n + 4\Omega_f = 1.84 SR$$

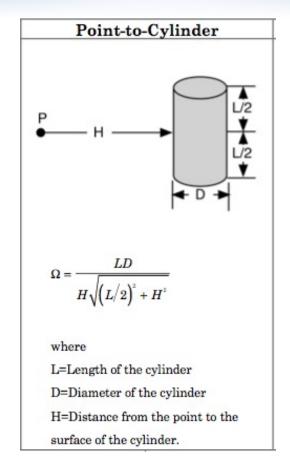




$$-\Omega_{n} = \frac{\left(4 \text{ ft}\right)\left(\frac{1}{2} \text{ ft}\right)}{2.25 \text{ ft}\left[\left(\frac{4 \text{ ft}}{2}\right)^{2} + \left(2.25 \text{ ft}\right)^{2}\right]^{\frac{1}{2}}} = 0.30 \text{ SR}$$

$$-\Omega_{f} = \frac{\left(4 \text{ ft}\right)\left(\frac{1}{2} \text{ ft}\right)}{3.29 \text{ ft}\left[\left(\frac{4 \text{ ft}}{2}\right)^{2} + \left(3.29 \text{ ft}\right)^{2}\right]^{\frac{1}{2}}} = 0.16 \text{ SR}$$

$$\Omega_{total} = 4\Omega_n + 4\Omega_f = 1.84 SR$$

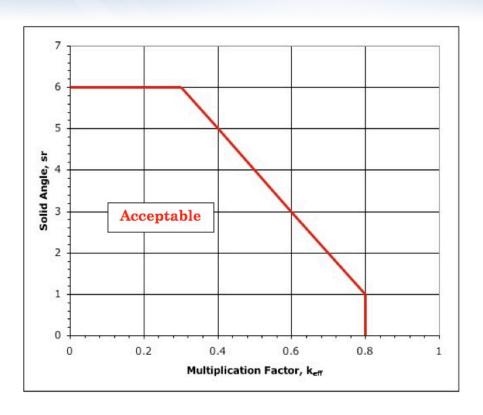


Question: What is the highest allowed k_{eff}?



$$-\Omega_{total} = 1.84 SR$$

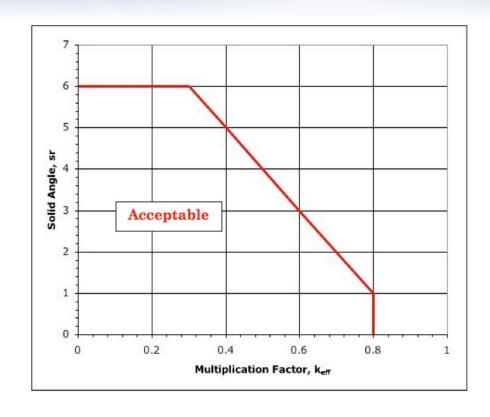
$$- k_{eff} = ?$$





$$-1.84 = 9 - 10k_{eff}$$

$$- k_{eff} = ?$$





$$-1.84 = 9 - 10k_{eff}$$

$$- k_{eff} = \left[\frac{9 - 1.84}{10} \right] = 0.72$$

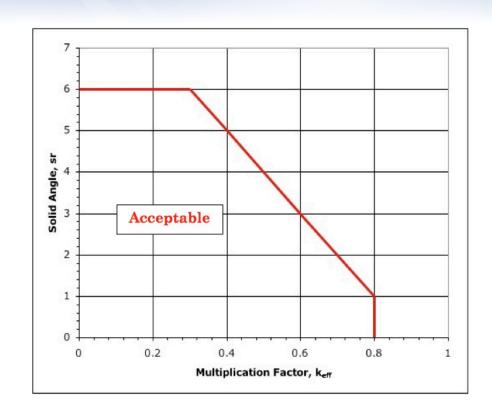




$$-\Omega_{total} = 1.84 SR$$

$$-1.84 = 9 - 10k_{eff}$$

$$- k_{eff} = \left[\frac{9 - 1.84}{10} \right] = 0.72$$



– What else is required?



$$-\Omega_{total} = 1.84 SR$$

$$-1.84 = 9 - 10k_{eff}$$

$$- k_{eff} = \left[\frac{9 - 1.84}{10} \right] = 0.72$$

– What happens if we move the bottles closer together?

