

C R I T I C A L I T Y H A N D B O O K

Volume II

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GENERAL CONTENTS

III. HOMOGENEOUS DATA, PARTS A AND B

PREFACE

The use of the loose-leaf form for ARH-600 has permitted easy addition and modification of data. A loose-leaf notebook, however, can only be filled to the point at which ring holes begin to tear out because of restricted movement. The amount of data accumulated in the first volume of ARH-600 and new data expected to be added in the near future has required the expansion to two volumes, and the re-distribution of data between the two. The expansion into two volumes without overloading one has temporarily required division of data at a somewhat awkward location, the middle of Section III. However, completion of the U-233 part of Section III and the addition of data to Sections IV, V and VI as time permits, will probably require the addition of a third volume. At that time, it is hoped that the data can be redistributed more artistically.

III. HOMOGENEOUS SYSTEMS

- A. PLUTONIUM SYSTEMS
- B. URANIUM-235 SYSTEMS
- C. URANIUM-233 SYSTEMS (SEE VOLUME III)
- D. MIXED AND MISCELLANEOUS SYSTEMS (SEE VOLUME III)

III. HOMOGENEOUS DATA

A. PLUTONIUM SYSTEMS

1. Correlation Between Calculation and Experiment
2. H/Pu versus Plutonium g/l Relationship
3. Critical Sphere Dimensions

Earlier graphs within this and following divisions have the percentage by weight of the major fissile atom (Pu-239) as the fourth identification number (e.g., III.A.3.97-2 would signify the second graph showing data for plutonium containing 97 weight percent Pu-239). Later graphs have been modified to set off the weight percent by parentheses, III.A.3(97)-2, in the interest of clarity.

4. Critical Cylinder Dimensions
5. Critical Slab Dimensions
6. Critical Mass - Sphere
7. Critical Mass per Unit Height - Cylinder
8. Critical Mass per Unit Area - Slab
9. Critical Volume
10. Material Bucklings and Infinite Multiplication Factor

BASIC PLUTONIUM CRITICAL PARAMETERS

<u>Metal</u> ⁽²⁾	<u>Full Reflection*</u>	<u>Bare</u>
Minimum critical mass, kgs ^{239}Pu	$5.425 \pm .027$ ⁽¹⁾	10.2
Infinite cylinder, diameter inches	1.7	2.4
Infinite slab thickness, inches	0.28	1.1
Minimum spherical volume, liters	0.28	0.51
<u>Homogeneous Solutions</u> ⁽³⁾	<u>Full Reflection</u>	<u>Bare</u> ^{**}
Minimum critical mass, g ^{239}Pu		
$^{239}\text{Pu} - \text{H}_2\text{O}$	531	
$^{239}\text{Pu}(\text{NO}_3)_4 - \text{H}_2\text{O}$	547	905
Infinite cylinders diameter, inches		
$^{239}\text{Pu} - \text{H}_2\text{O}$	***	***
$^{239}\text{Pu}(\text{NO}_3)_4 - \text{H}_2\text{O}$	6.41	9.15
Infinite Slab thickness, inches		
$^{239}\text{Pu} - \text{H}_2\text{O}$	***	***
$^{239}\text{Pu}(\text{NO}_3)_4 - \text{H}_2\text{O}$	2.44	5.30
Minimum spherical volume, liters		
$^{239}\text{Pu} - \text{H}_2\text{O}$	***	***
$^{239}\text{Pu}(\text{NO}_3)_4 - \text{H}_2\text{O}$	8.3	16.9
Minimum critical aqueous concentration, g/l ^{239}Pu	7.8 ± 0.3	(H/Pu = 3392 ± 100)

* Reflector is water unless specified otherwise.

** 0.125 inch thick stainless steel container shell.

*** There is no minimum value for theoretical $\text{Pu} - \text{H}_2\text{O}$ solutions unless a maximum concentration is assumed, see pages III.A.4.100-3, III.A.5.100-3 and III.A.9.100-3.

(1) W. U. Geer, D. R. Smith, Measurement of the Critical Mass of a Water - Reflected Plutonium Sphere, ANS Transactions Vol. II No. 1, 1968.

(2) H. C. Paxton, J. T. Thomas, Dixon Callihan, E. B. Johnson, Critical Dimensions of Systems Containing ^{235}U , ^{239}Pu and ^{233}U , TID-7028, 1964.

(3) C. R. Richey, Theoretical Analyses of Homogeneous Plutonium Critical Experiments, Nuclear Science and Engineering: 31, 32-39, 1968.

III.A.1 Correlations Between Calculation and Experiment

The primary means of producing the data in this section has been with the combination of the GAMTEC-II and HFN computer codes. The GAMTEC-II code was used to produce 18 neutron energy group cross-section sets which were then used in the HFN multigroup one-dimensional diffusion theory code to calculate critical sizes, extrapolation distances and material bucklings. A thorough analysis has been made by C. R. Richey⁽¹⁾ using this method to calculate the effective multiplication factor for critical experiments. A selection of these are produced below:

<u>Geom.</u>	<u>Reflector</u>	<u>Pu g/l</u>	<u>% 240</u>	<u>Molarity</u>	<u>Calc. K_{eff}</u>	<u>Remarks</u>
Sphere	Water	33.0	4.6	2.061	0.999	14 in. dia.
"	"	47.9	4.6	6.698	1.005	14 in. dia.
"	Bare	39.0	4.6	0.376	0.997	15.2 in. dia.
"	"	172.8	4.6	4.898	0.993	15.2 in. dia.
"	Water	26.33	0.54	0.806	0.998	14 in. dia.
"	"	28.63	0.54	2.553	0.997	14 in. dia.
"	"	73.0	4.6	0.165	1.001	11.2 in. dia.
"	"	140.0	4.6	2.238	1.001	11.2 in. dia.
"	"	268.0	4.6	1.084	1.001	11.2 in. dia.
Cyl.	"	44.7	1.5	2.058	0.9846	11.6 in. dia., ht.=12.28
"	"	45.45	1.5	2.094	0.9739	12.8 in. dia., ht.=10.34

(1) C. R. Richey, "Theoretical Analysis of Homogeneous Plutonium Critical Experiments," Nuclear Science and Engineering, January, 1968.

Richey found that as the height of the cylinders increased the agreement between theory and experiment became better, approaching a least-squares-fitted value of k_{eff} equal to 1.0086 for infinite cylinders.

The dimensions shown in Section III.A have been calculated with the GAMTEC II - HFN combination for k_{eff} equal to 1.00. The comparison with experiment shows that this can sometimes be slightly non-conservative. Dimensions which are less than critical with some degree of confidence can be obtained by reducing the calculated critical values to values equivalent to k_{eff} equal to 0.986 for spheres and 0.980 for infinite slabs and cylinders. (See page II.B.1-6) Critically favorable values can be obtained by adjusting the critical values by the appropriate safety factor given in Section I.C.

The buckling and extrapolation distance curves (Section A.10) are derived from GAMTEC II - HFN calculations and can be used for calculating general geometries other than those represented by the curves for the simple sphere, infinite cylinder and infinite slab. It might be noted that the use of the buckling and extrapolation distance curves for these simple geometries may give a somewhat smaller critical dimension than the geometry data shows. Since each geometry has a slightly different extrapolation distance for the same plutonium concentration, the graphing of all data would result in an unreadable mess of lines. Therefore, only the most limiting extrapolation distances were used in Section A.10 for each particular solution.

III.A.2. H/Pu versus Pu g/l Relationships

The following relationships were used for the adjoining graph.

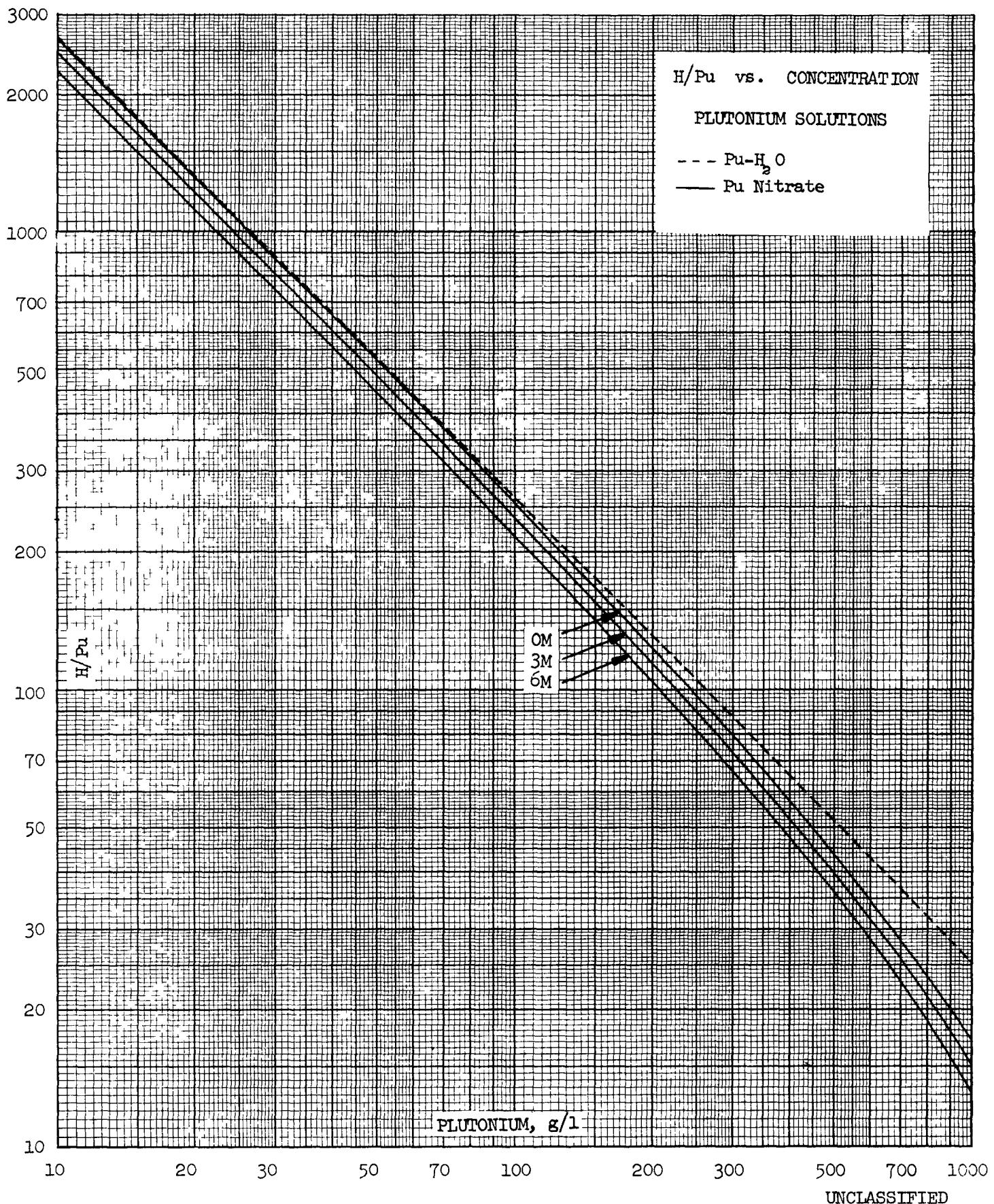
For Pu nitrate solutions:

$$\text{H/Pu} = \left[\frac{26,539 - 638.7 \times \text{Molarity of Excess Nitric Acid}}{\text{Pu g/l}} \right] - 9.606$$

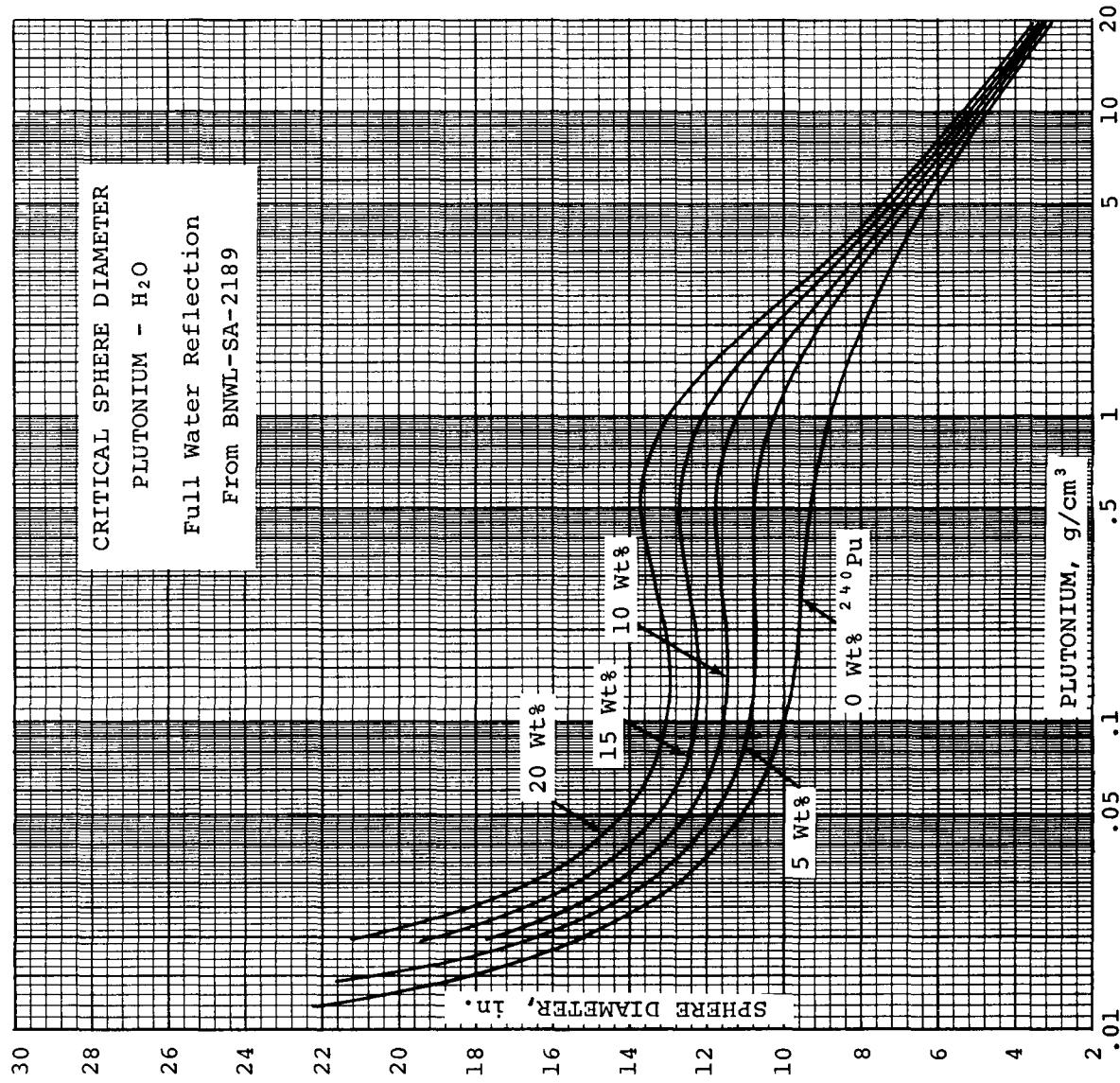
This equation was derived from work performed by C. R. Richey and G. M. Hess.

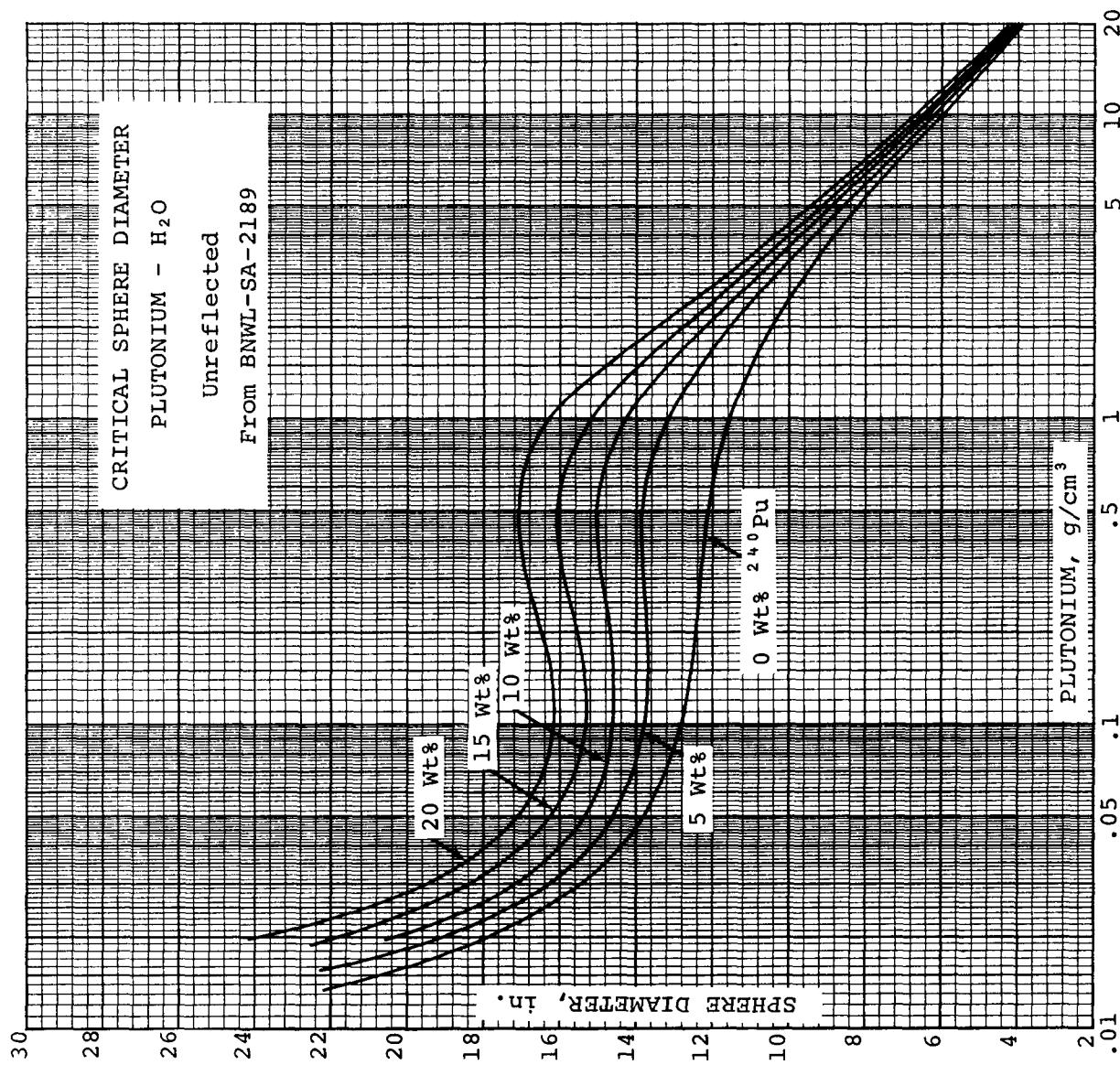
For Pu-H₂O solutions:

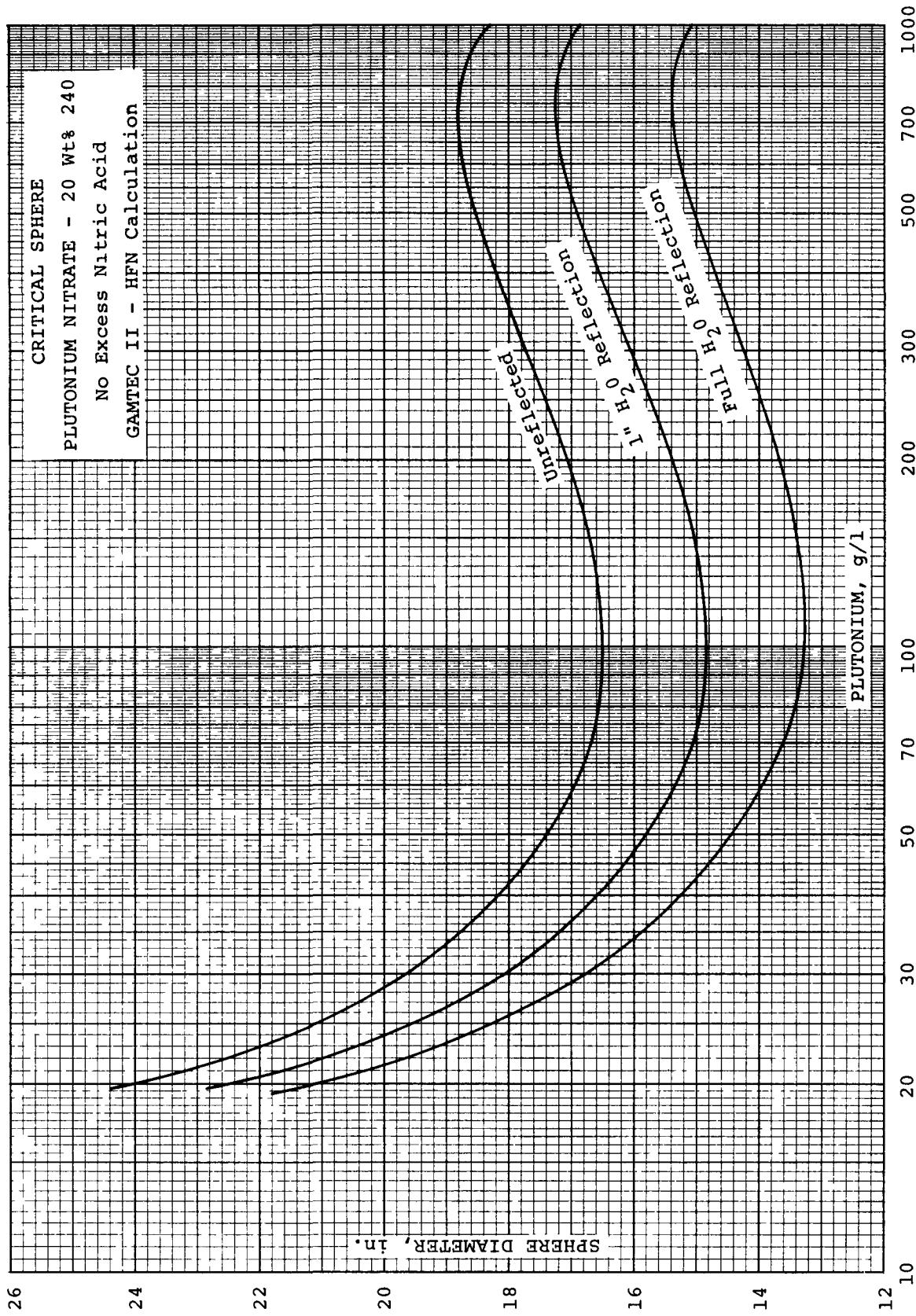
$$\text{H/Pu} = \left[\frac{26,530}{\text{Pu g/l}} \right] - 1.35$$



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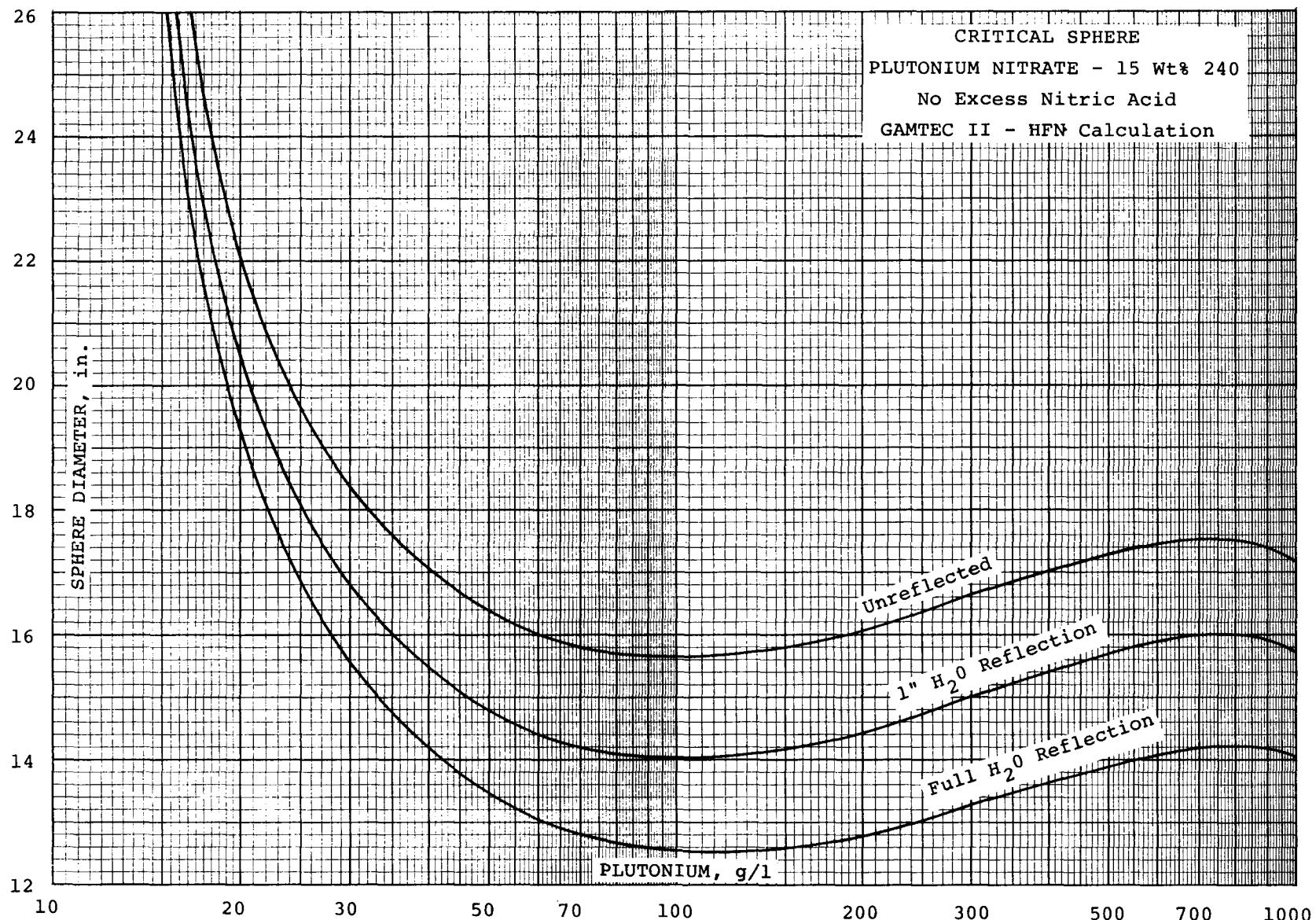
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SPHERE DIAMETER, in.

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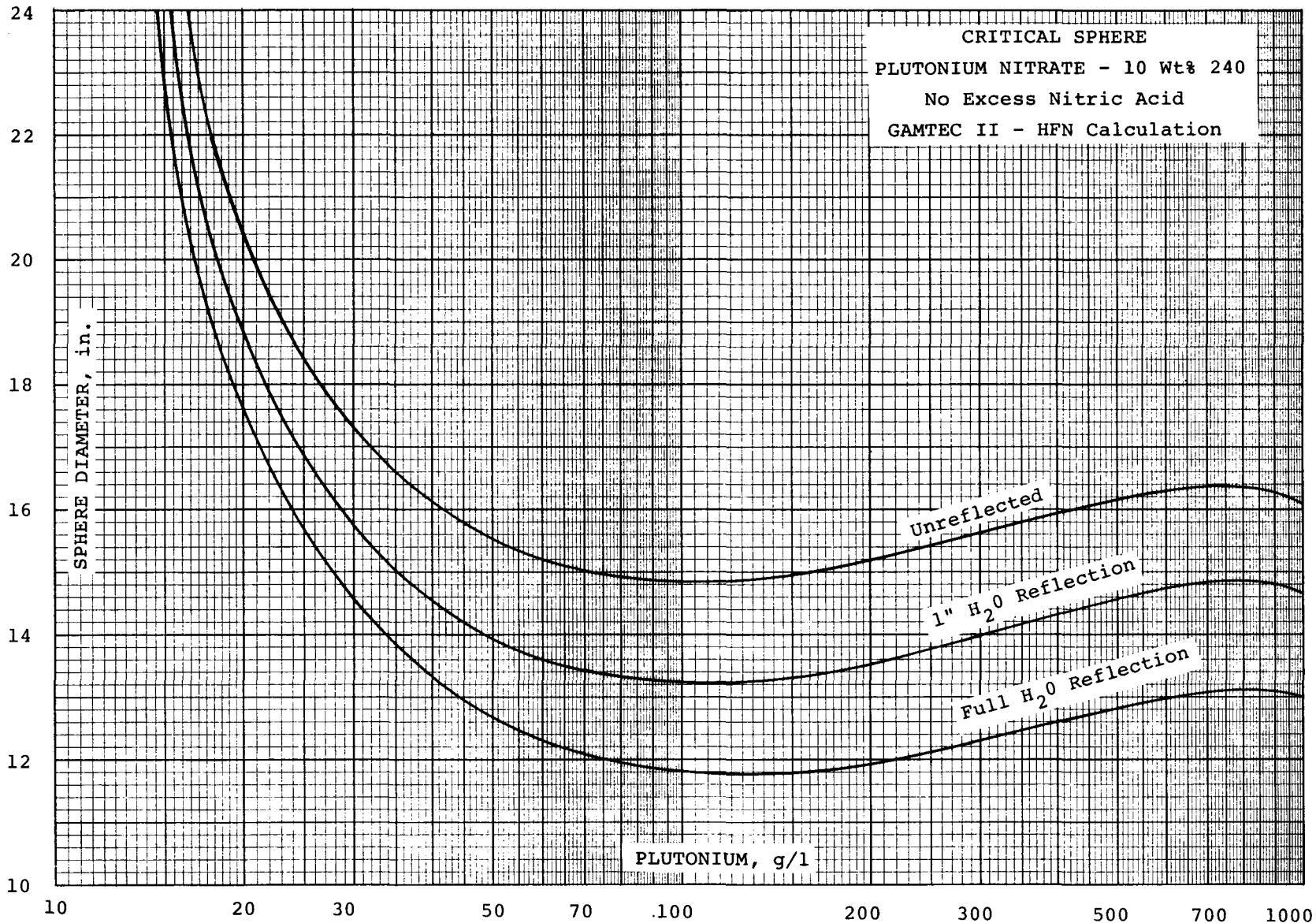


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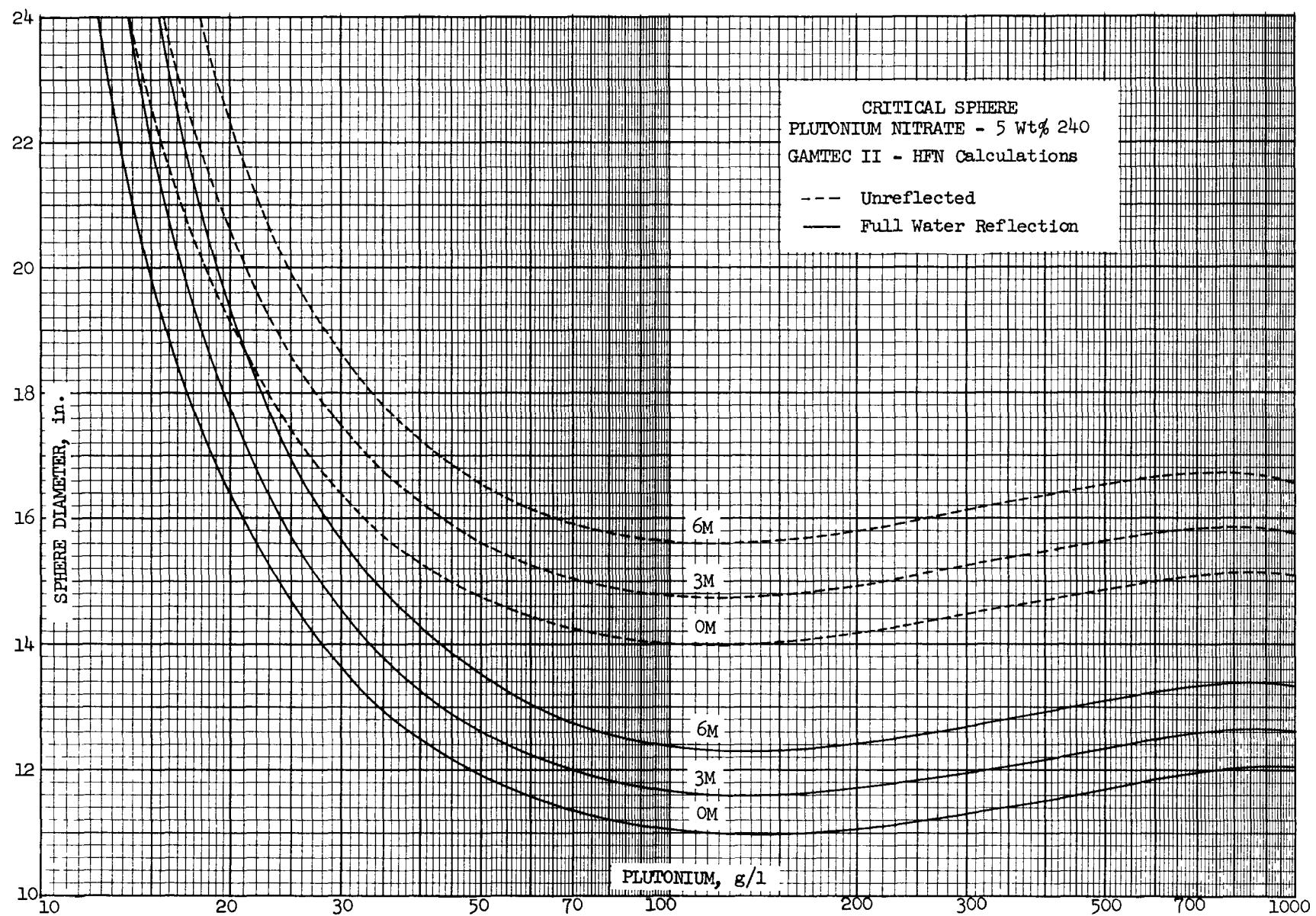


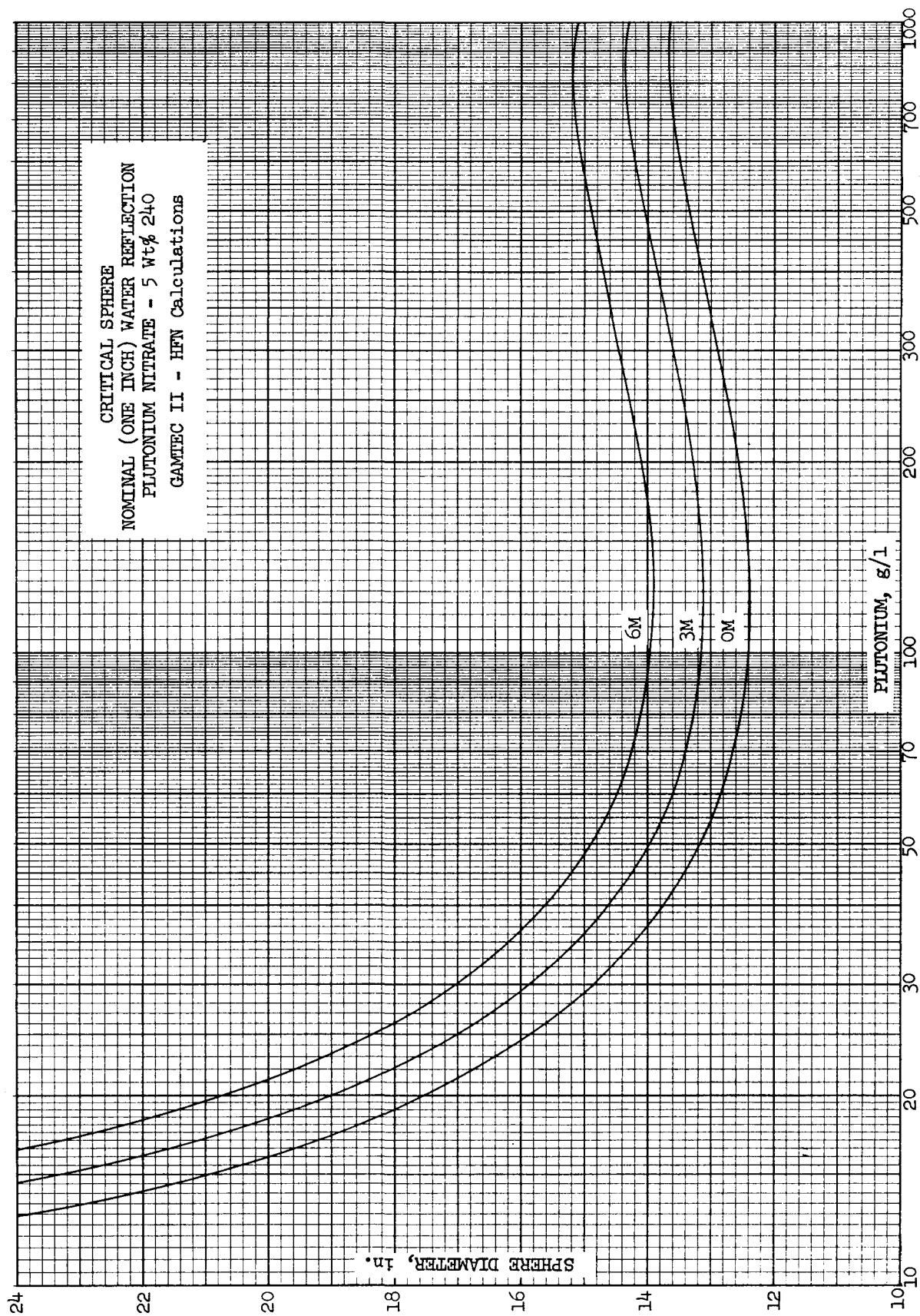
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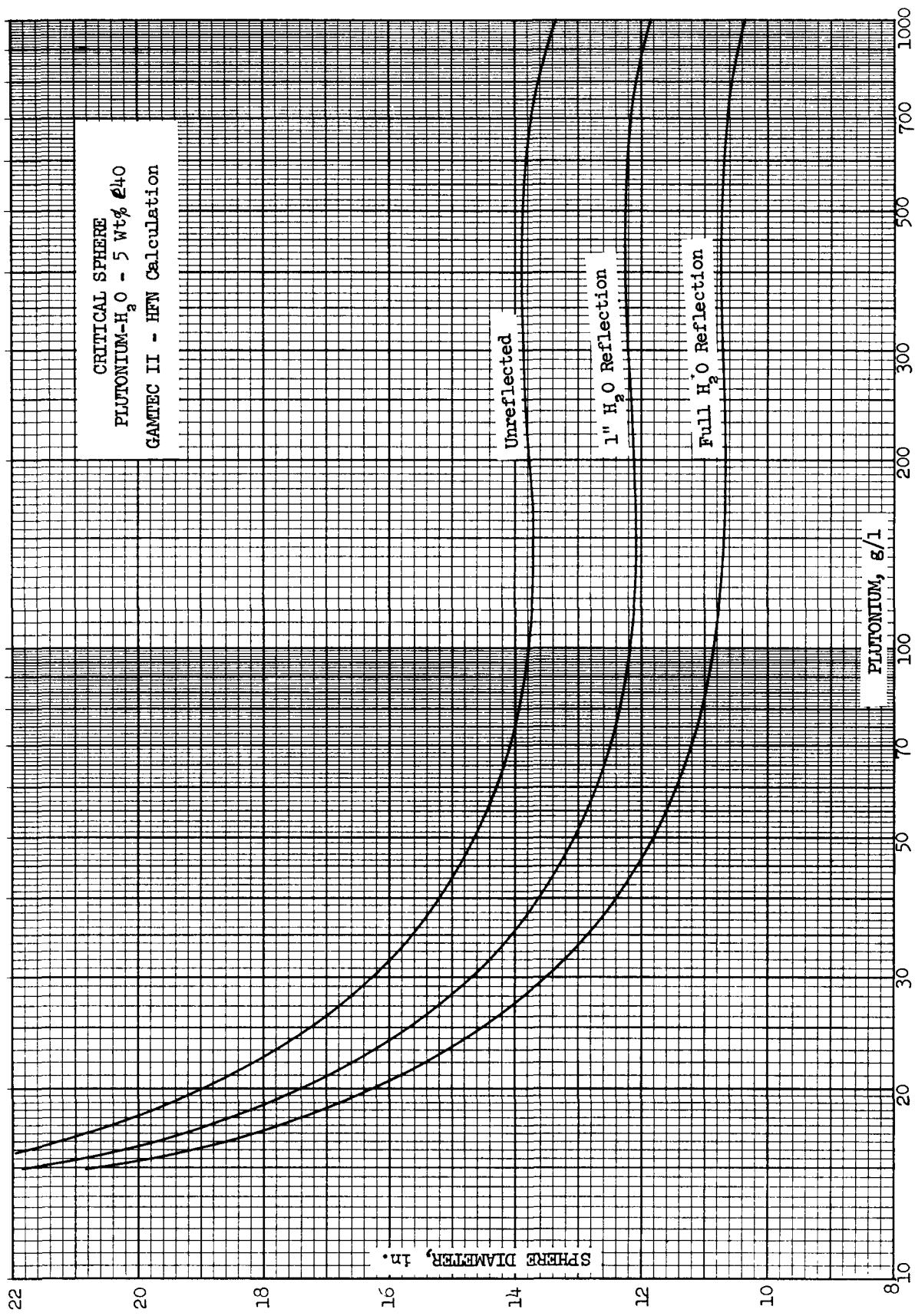
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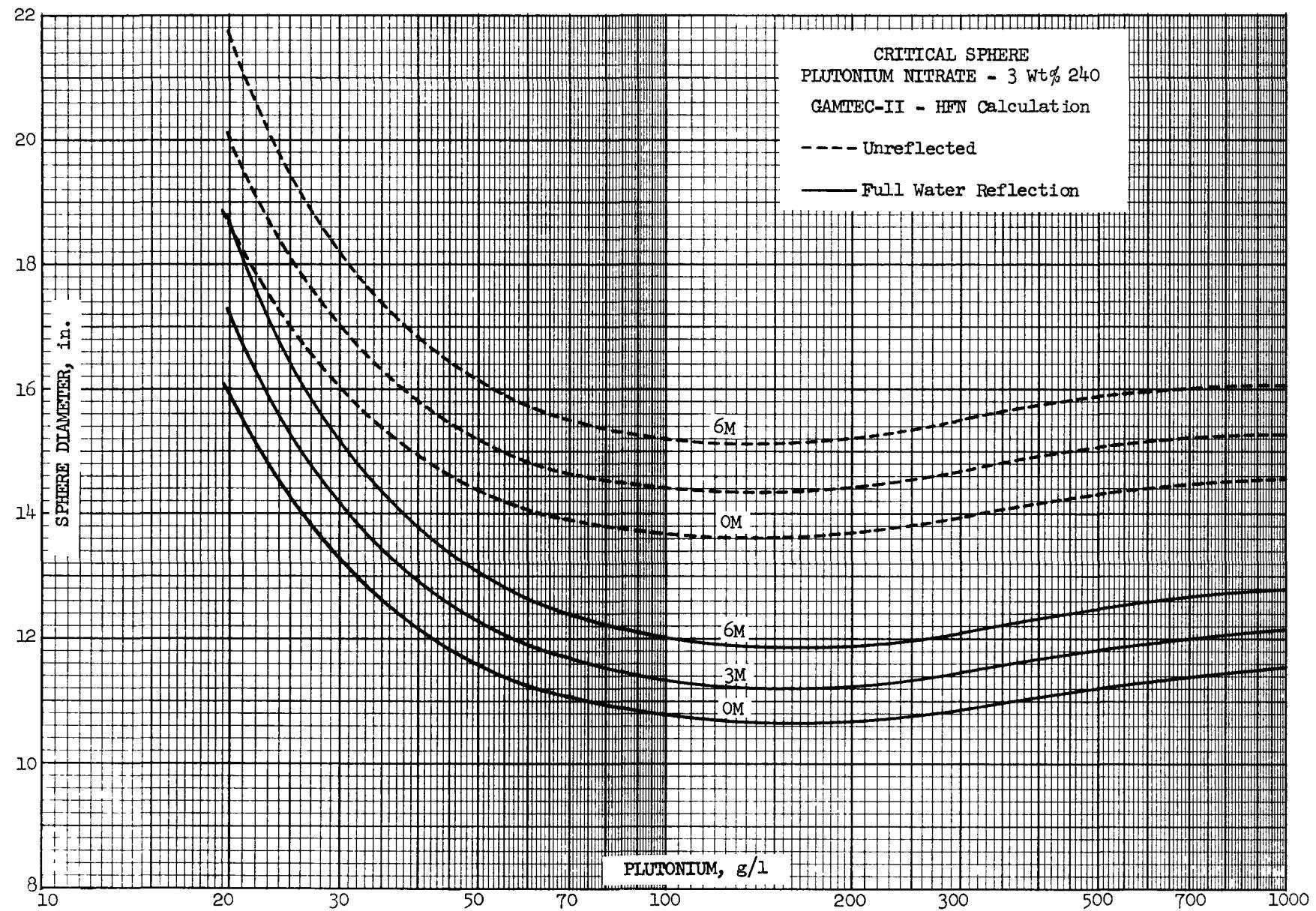




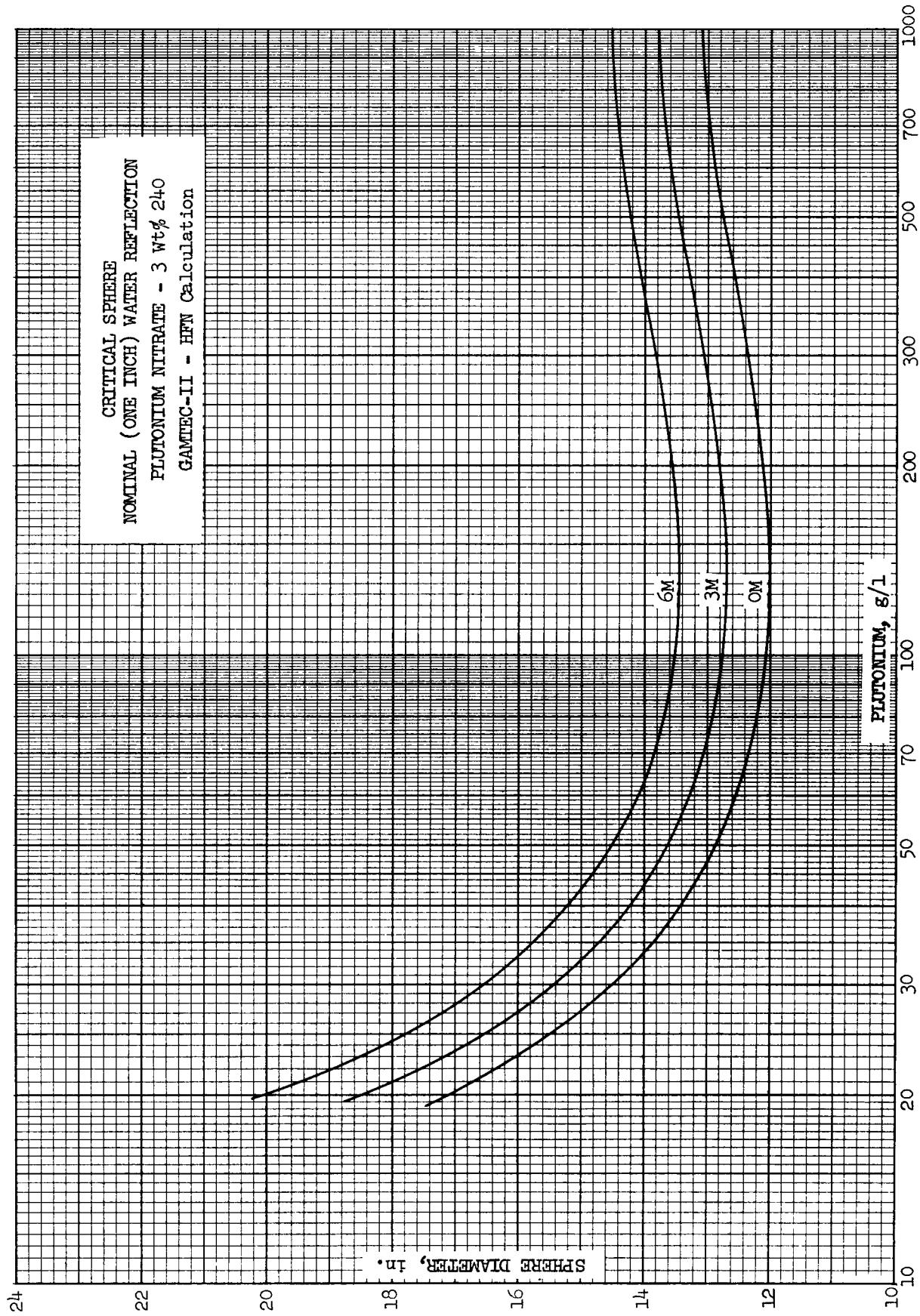
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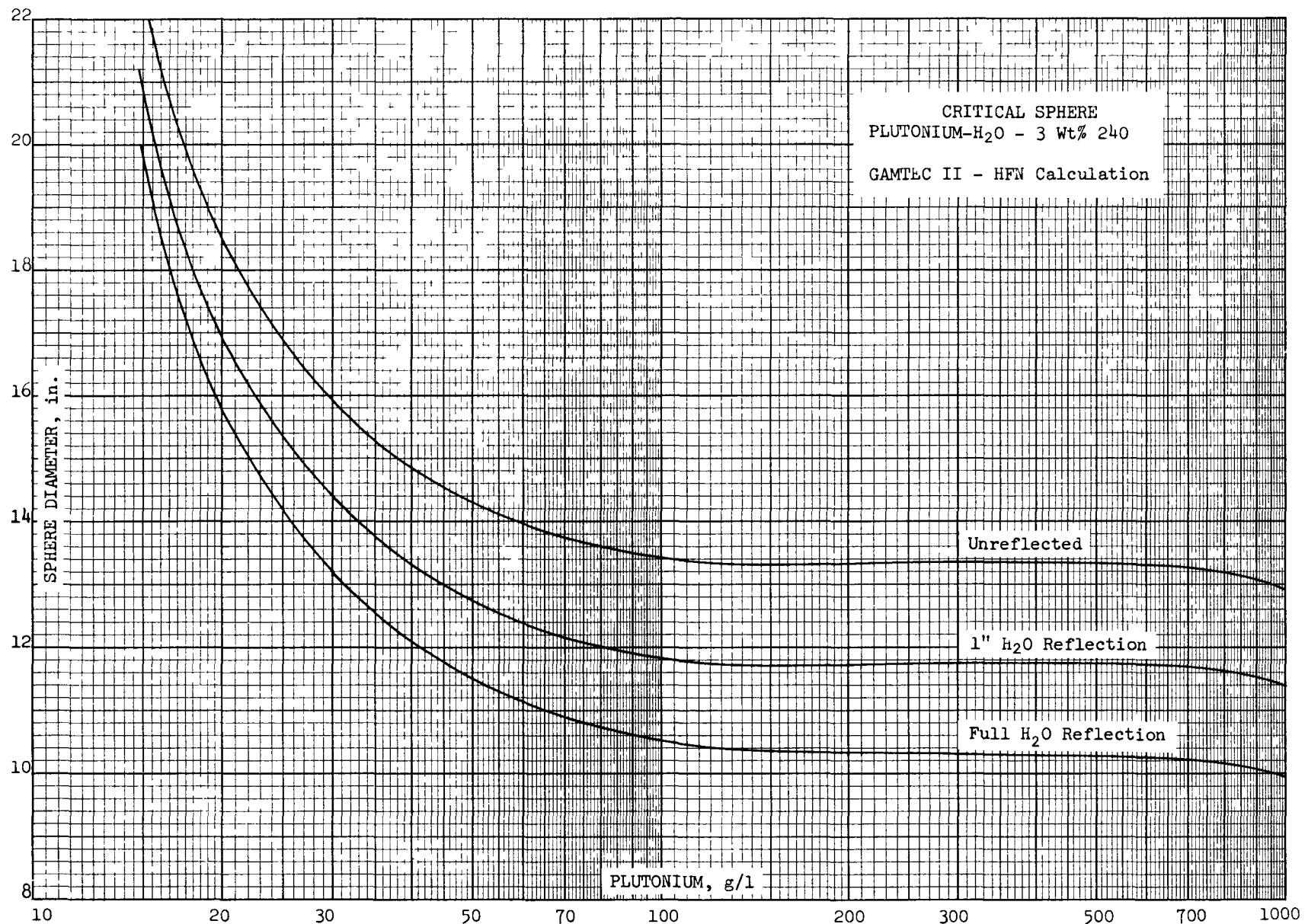
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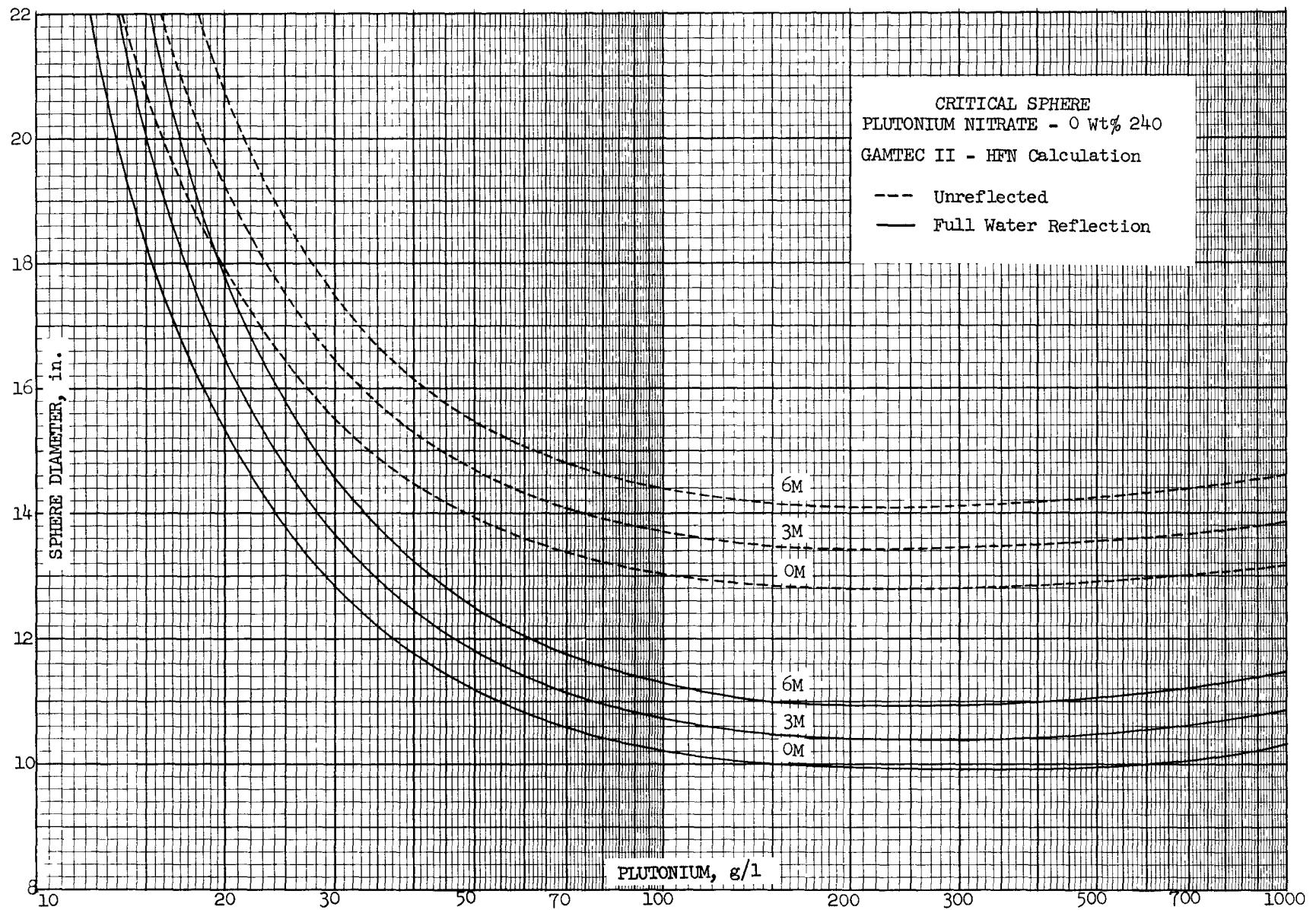
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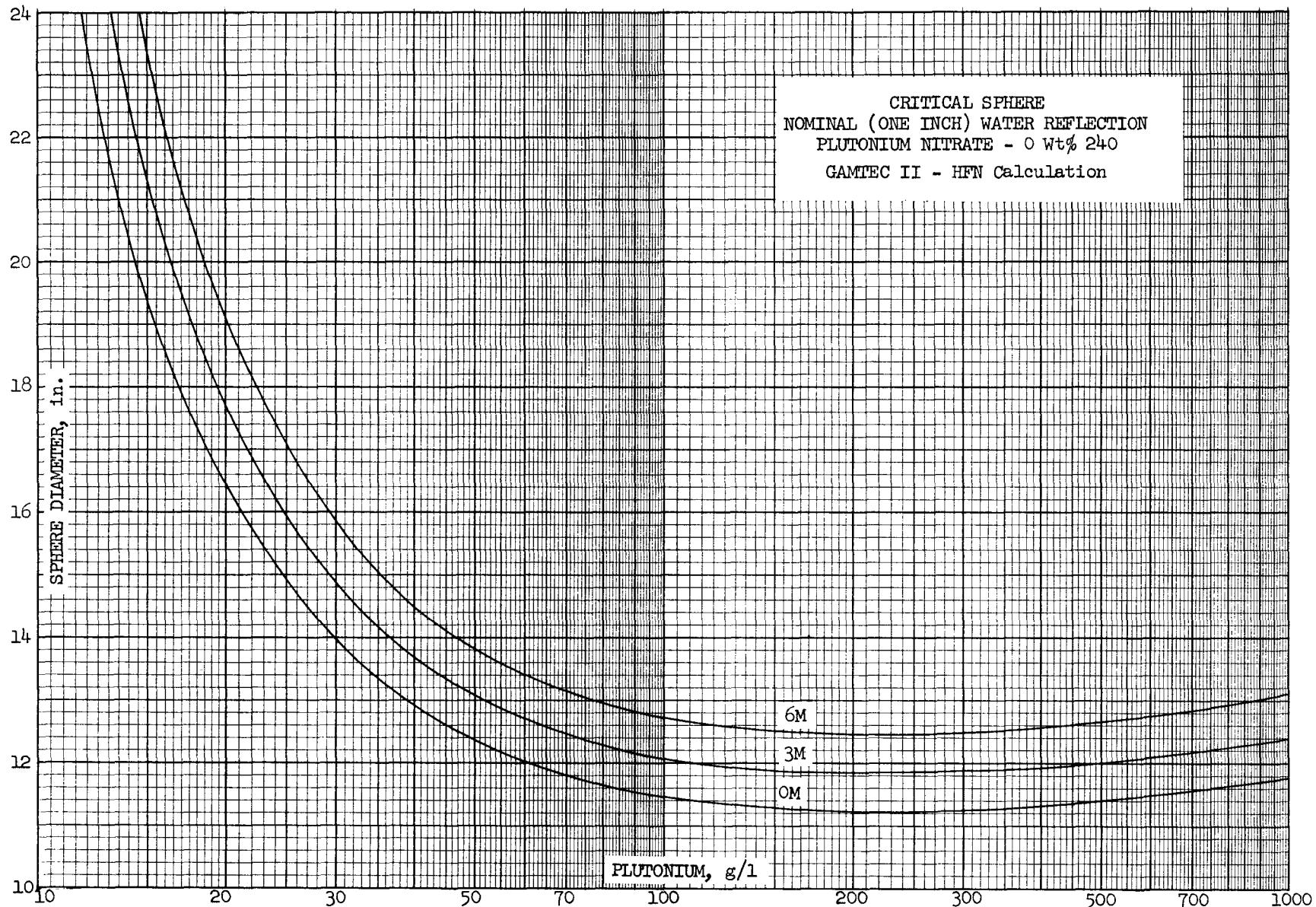


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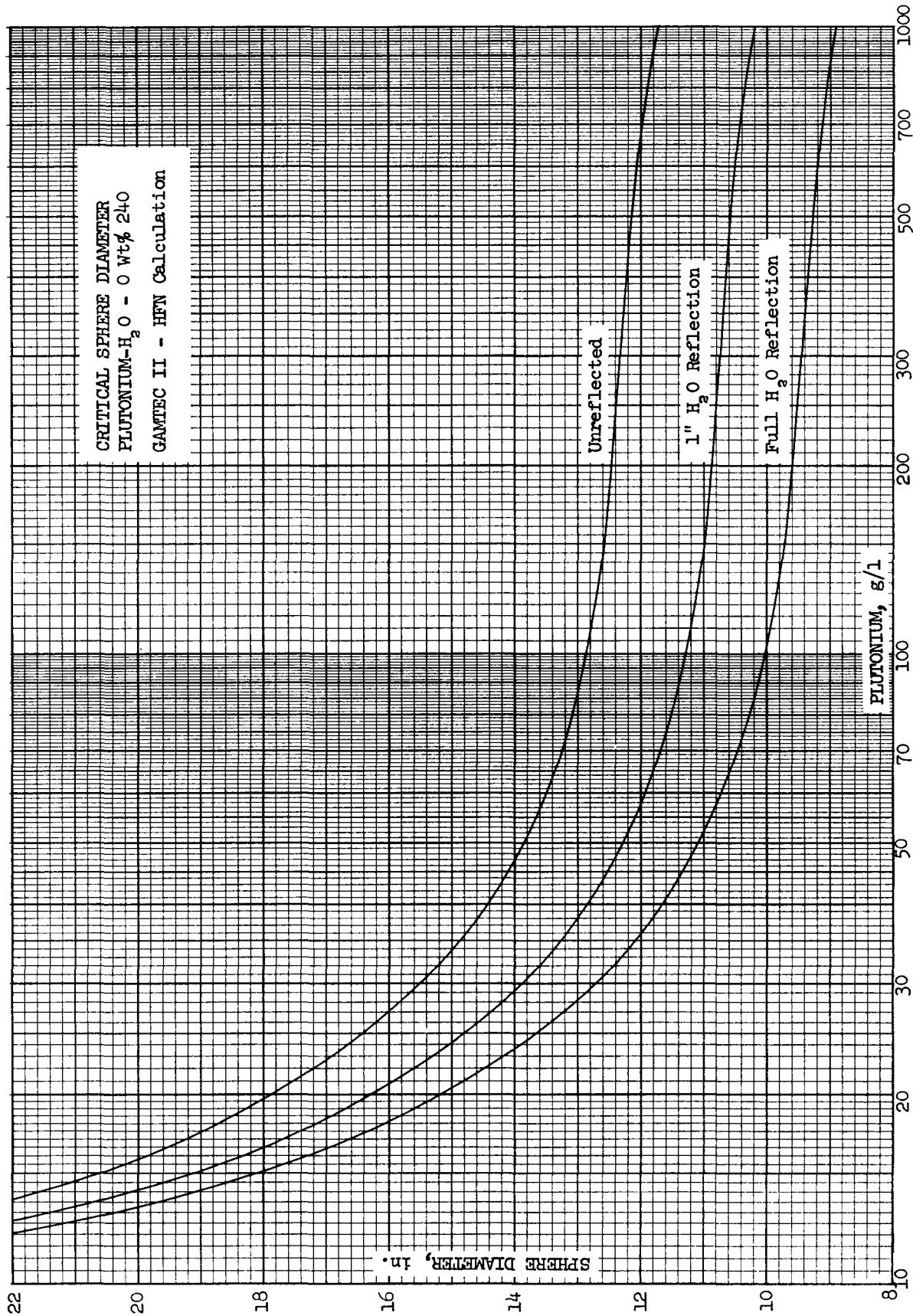
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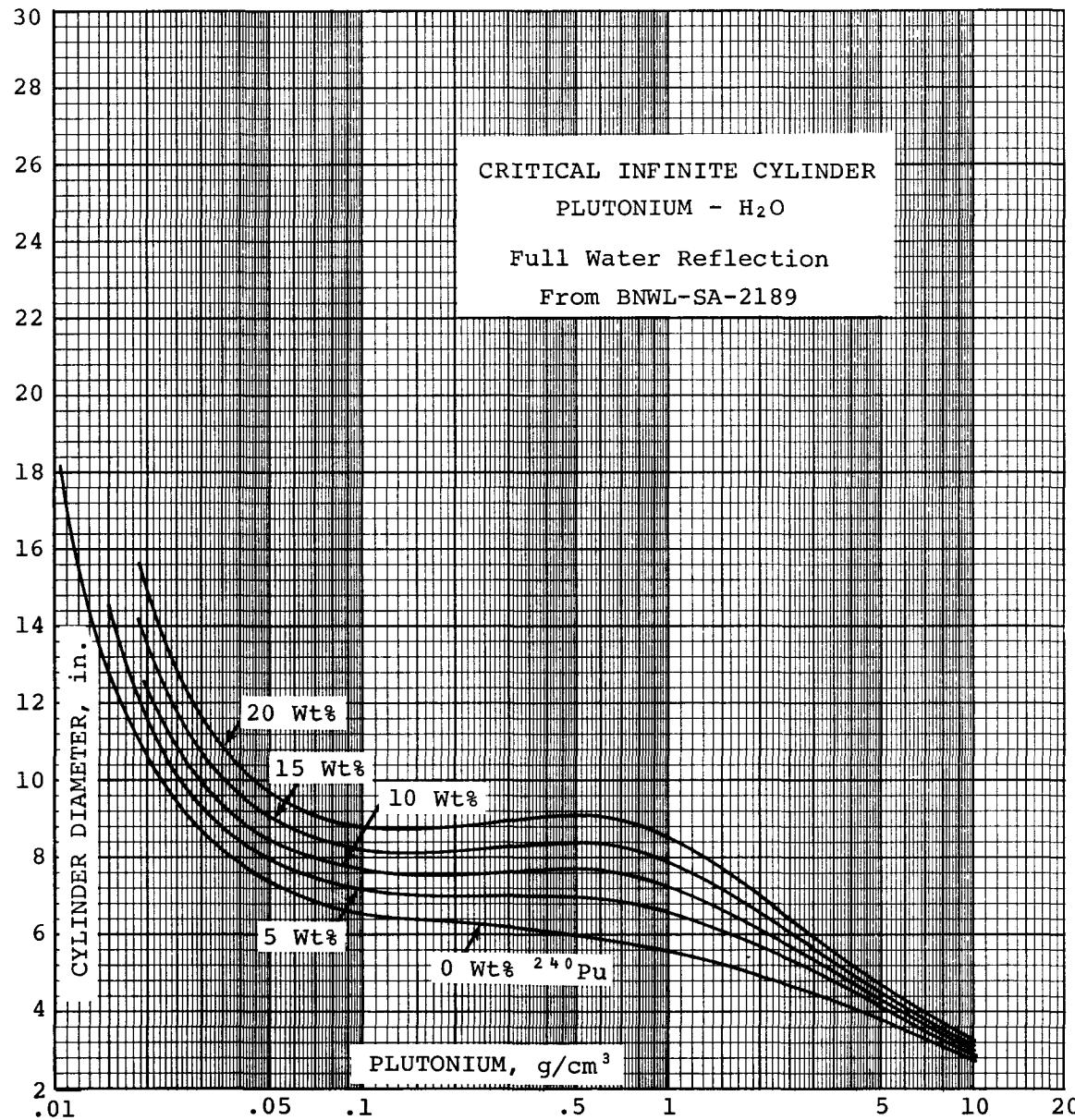
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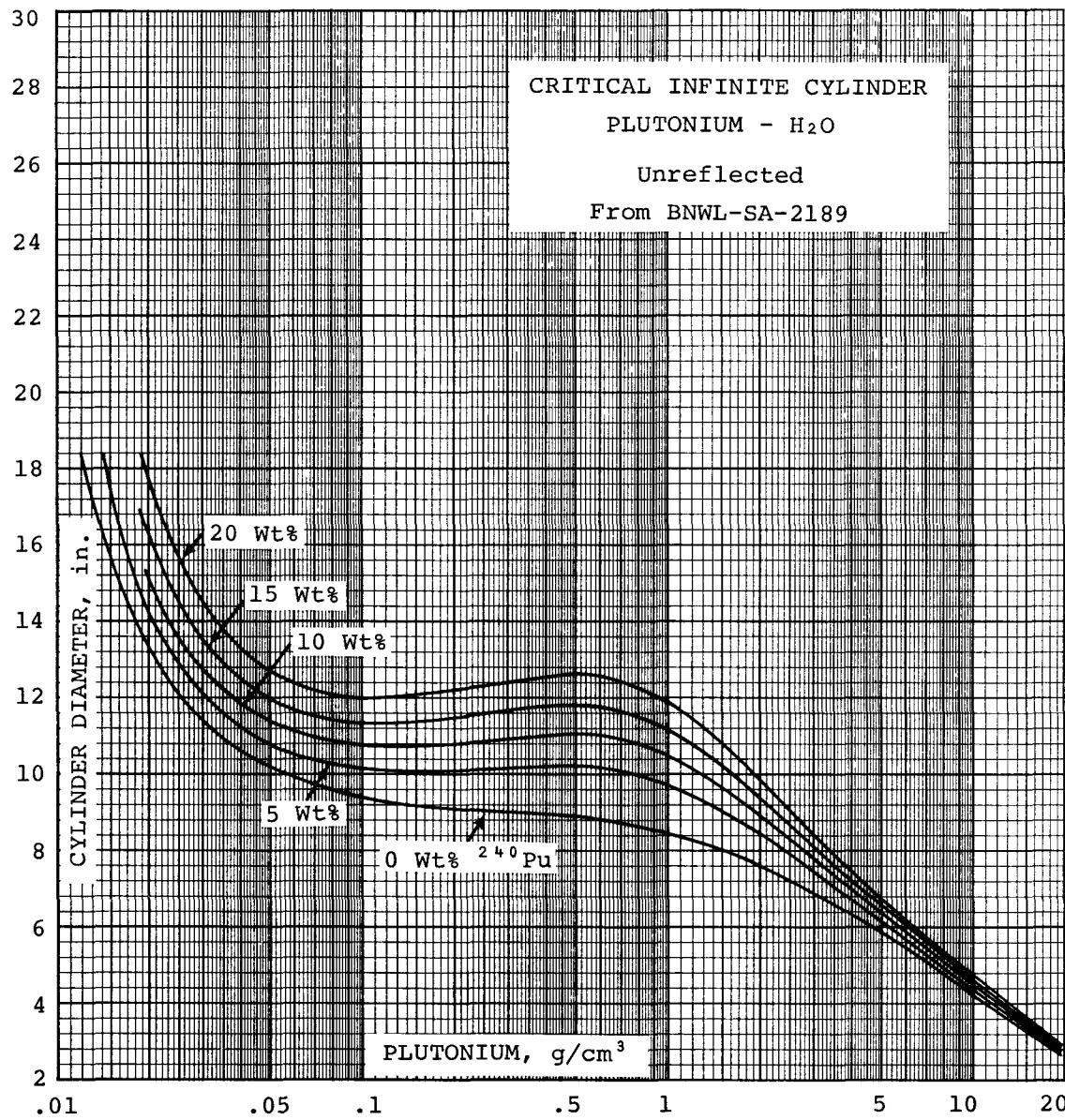


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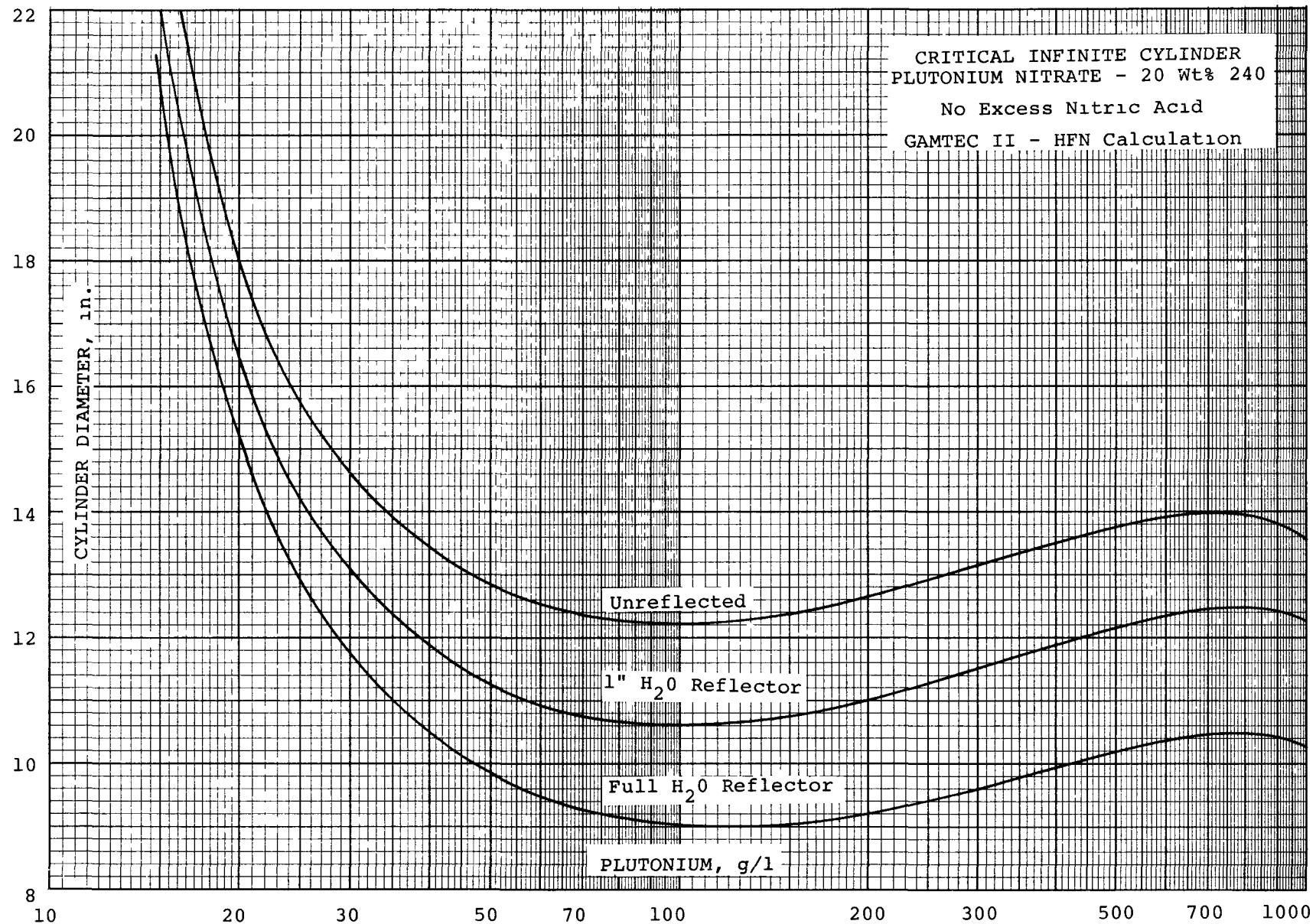


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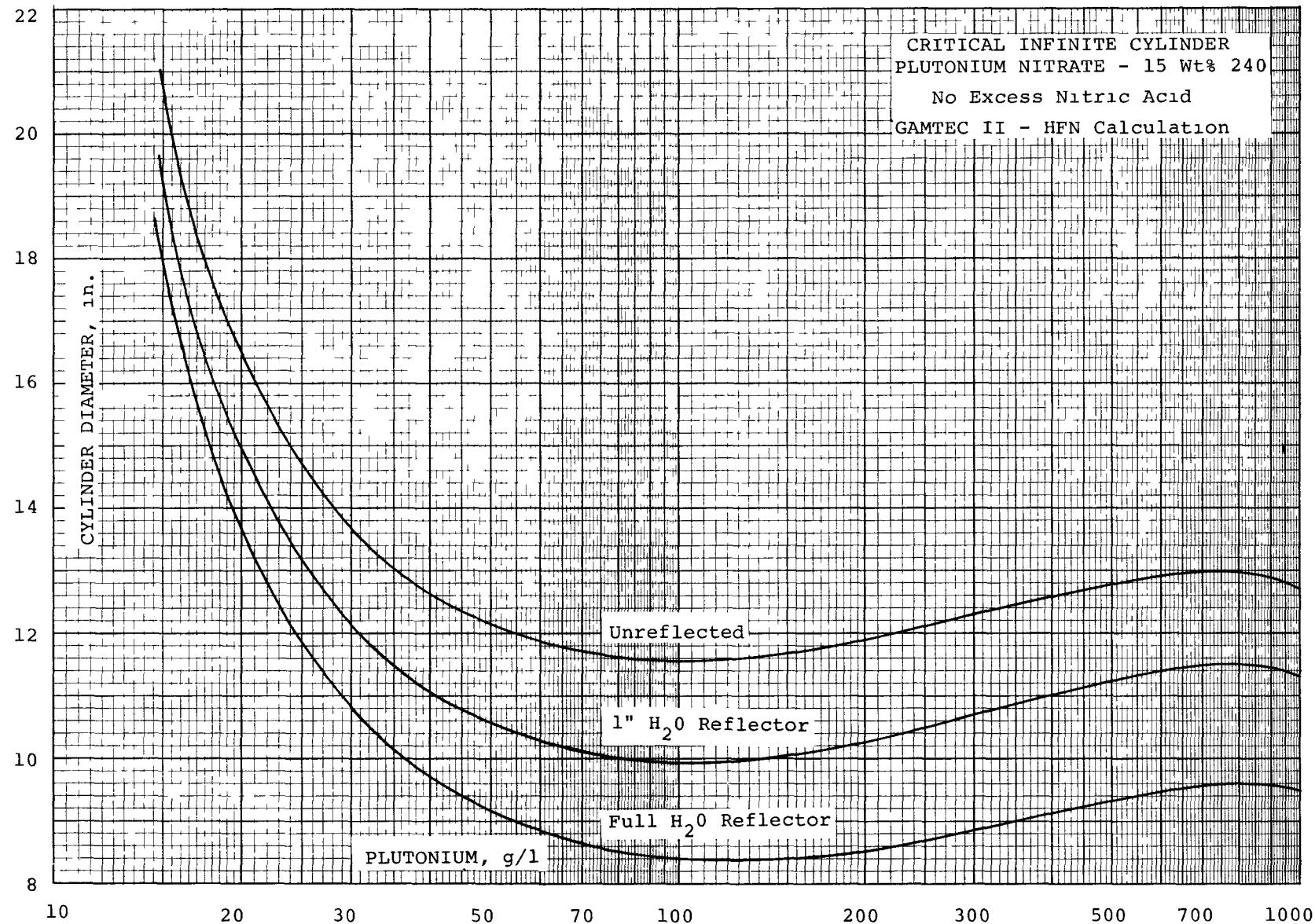
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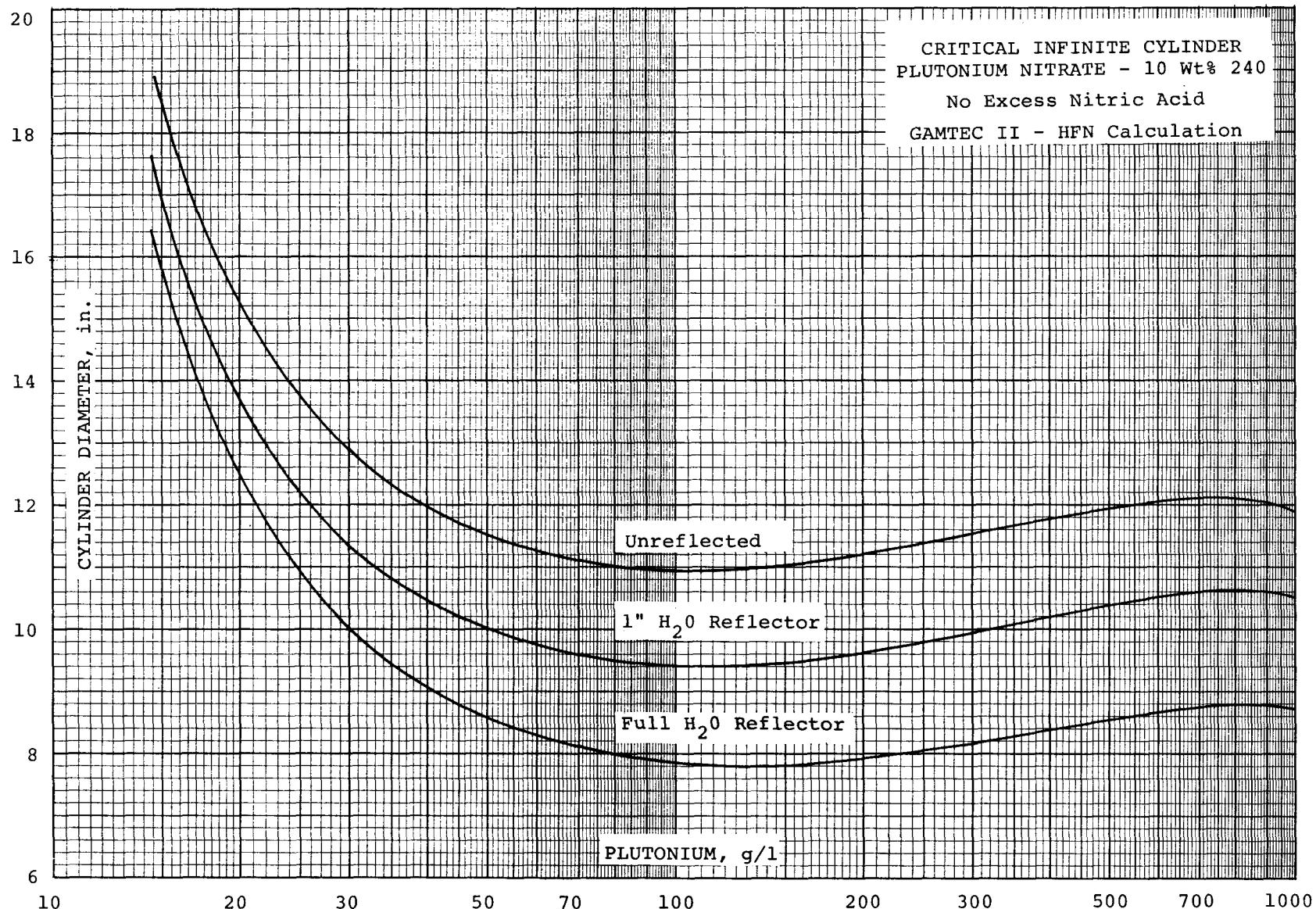


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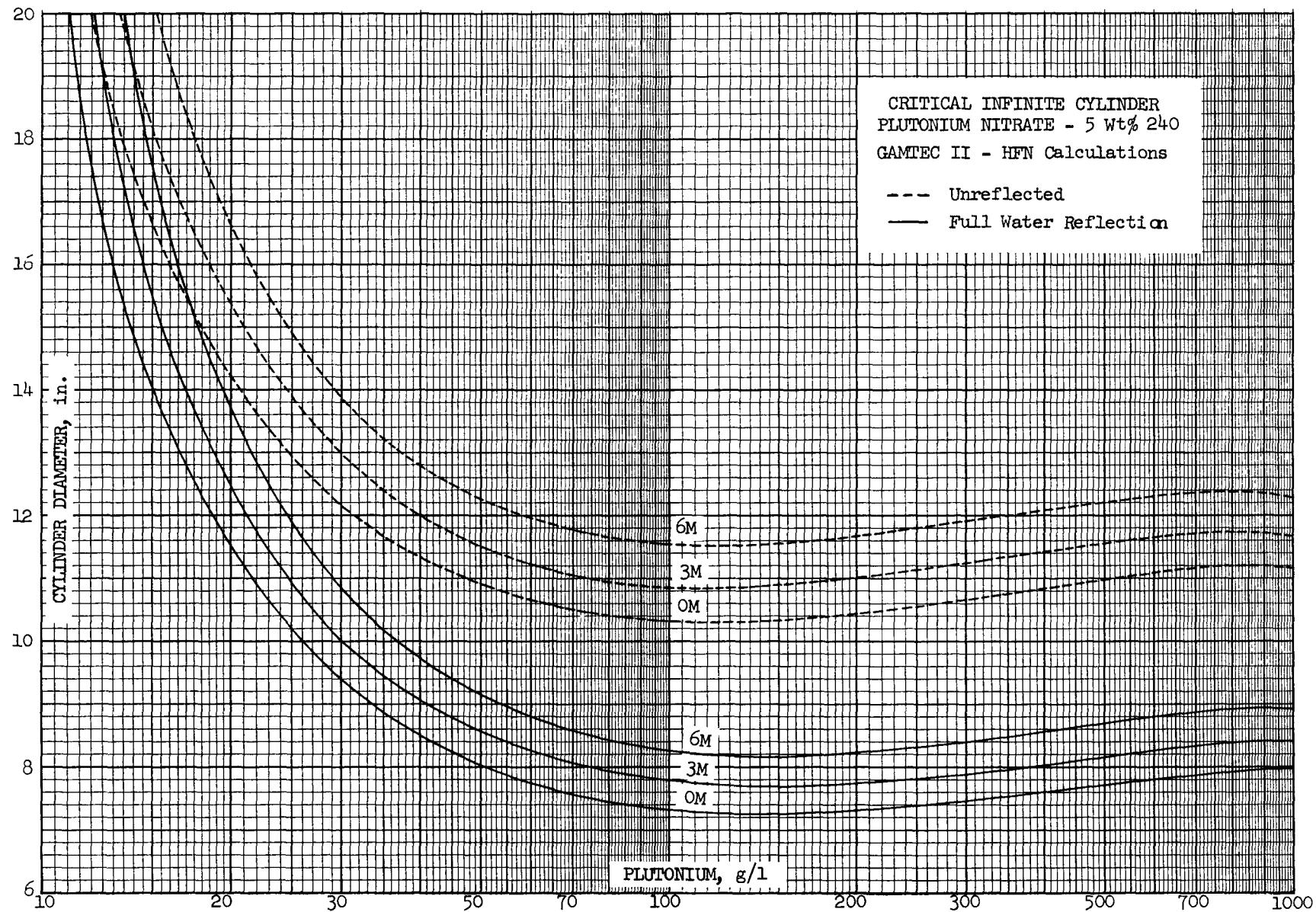
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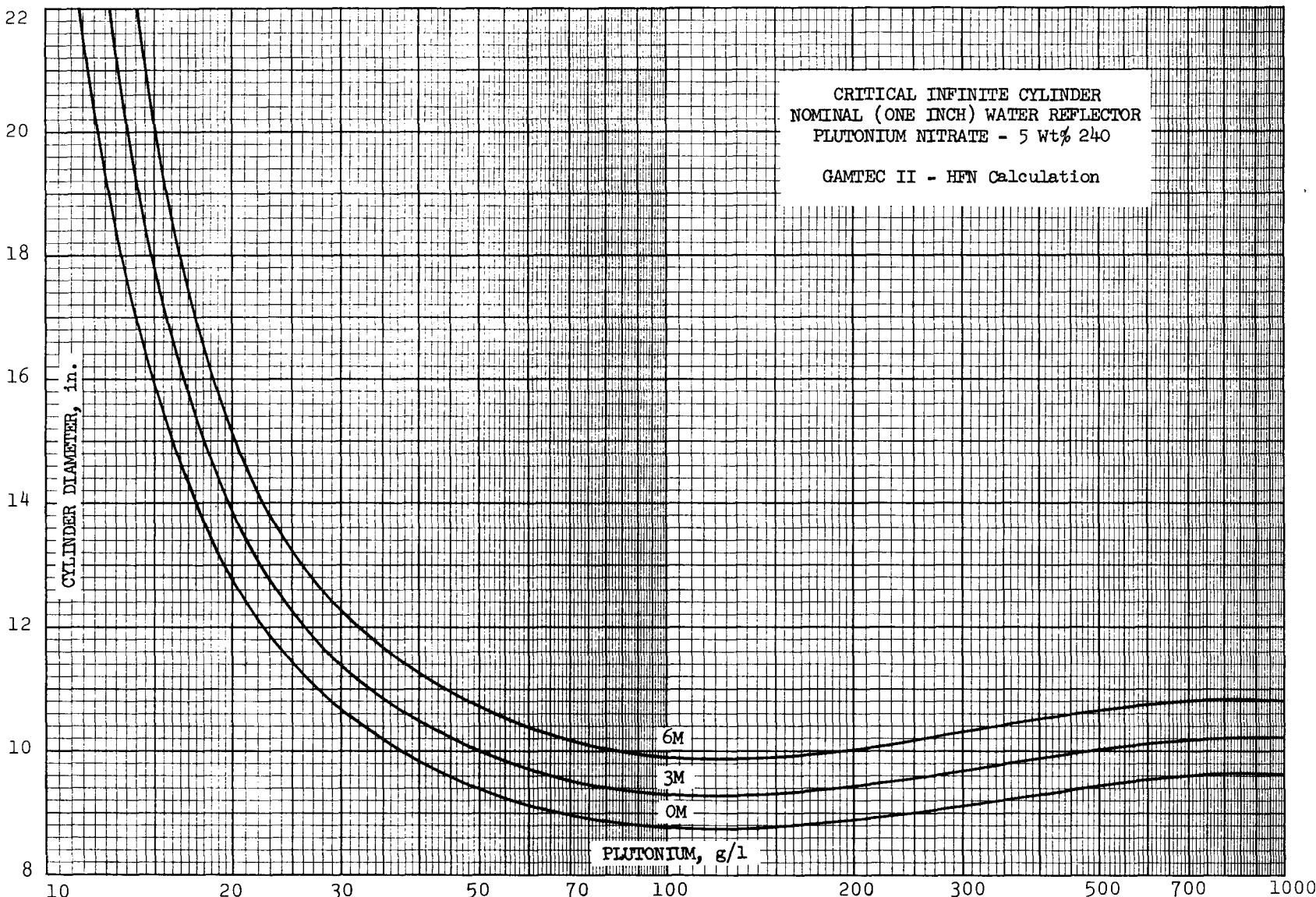
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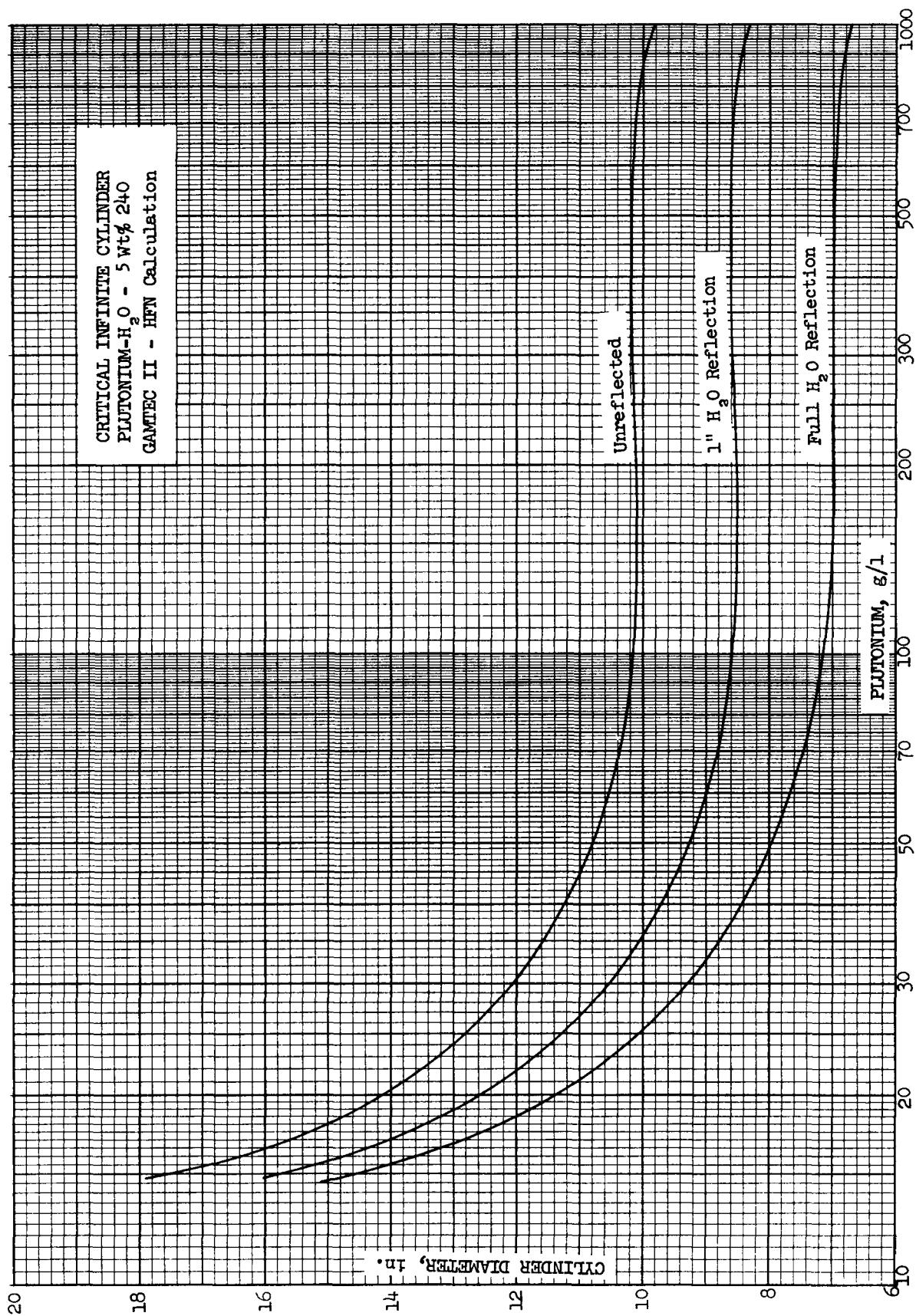
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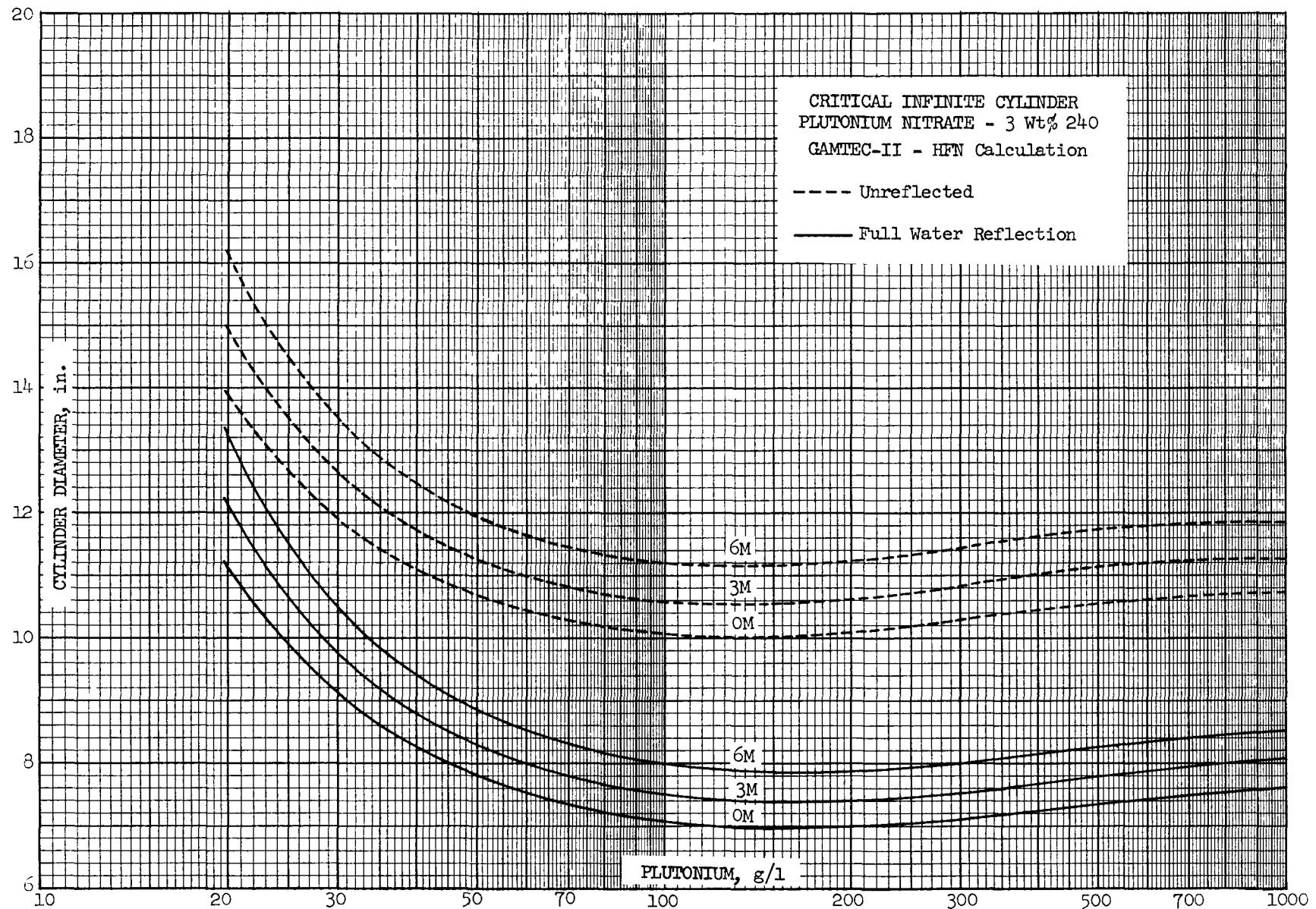
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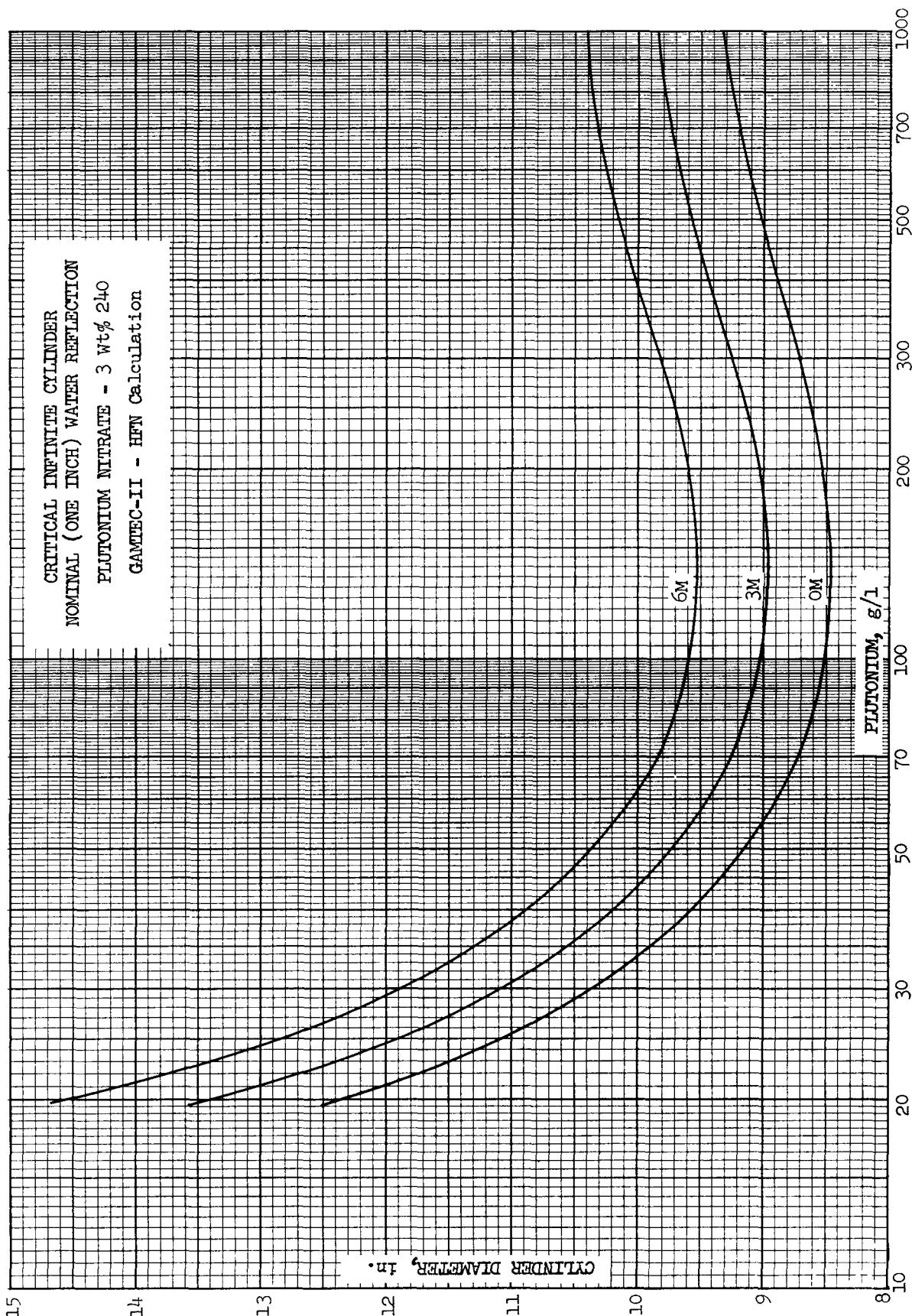
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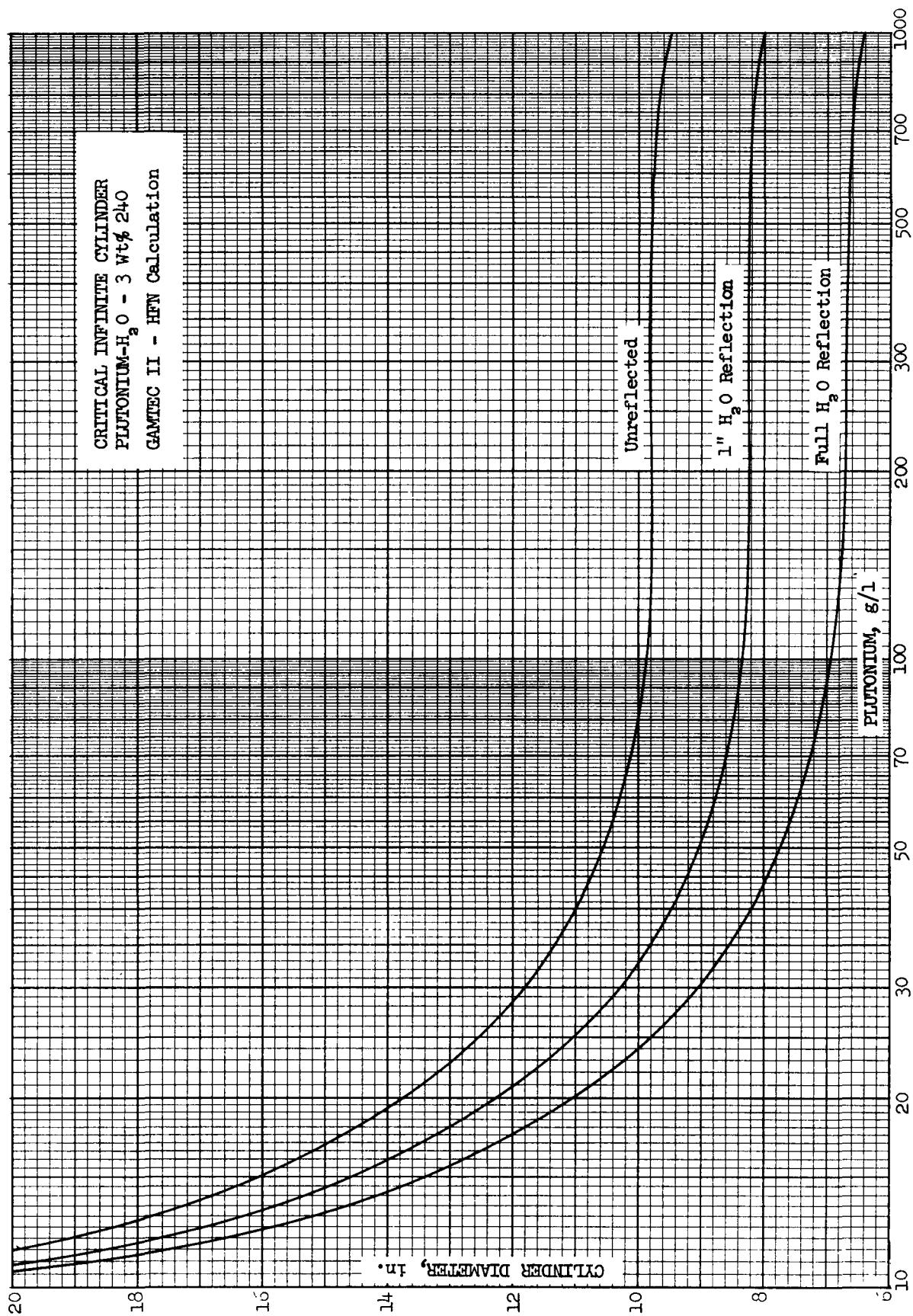
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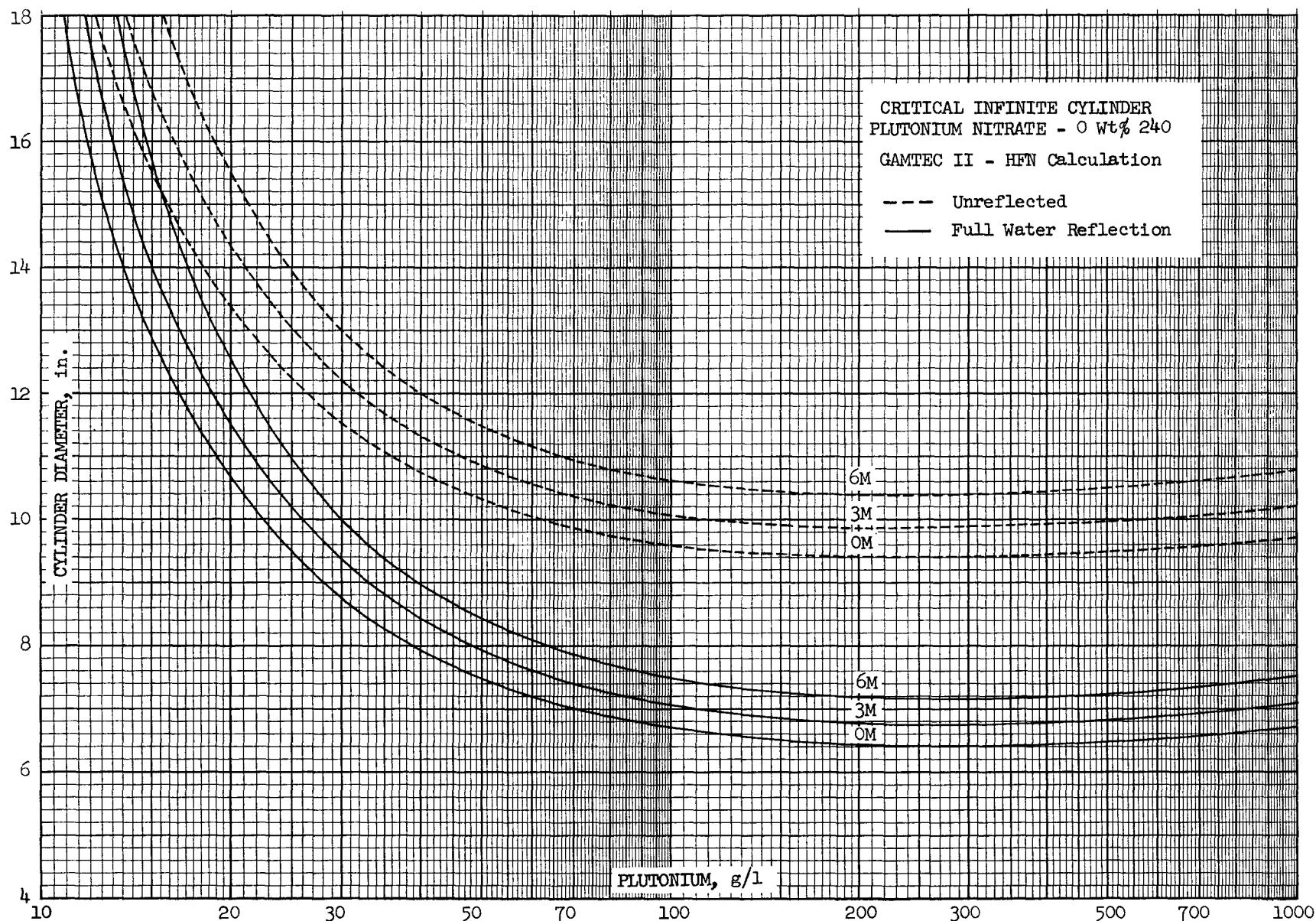
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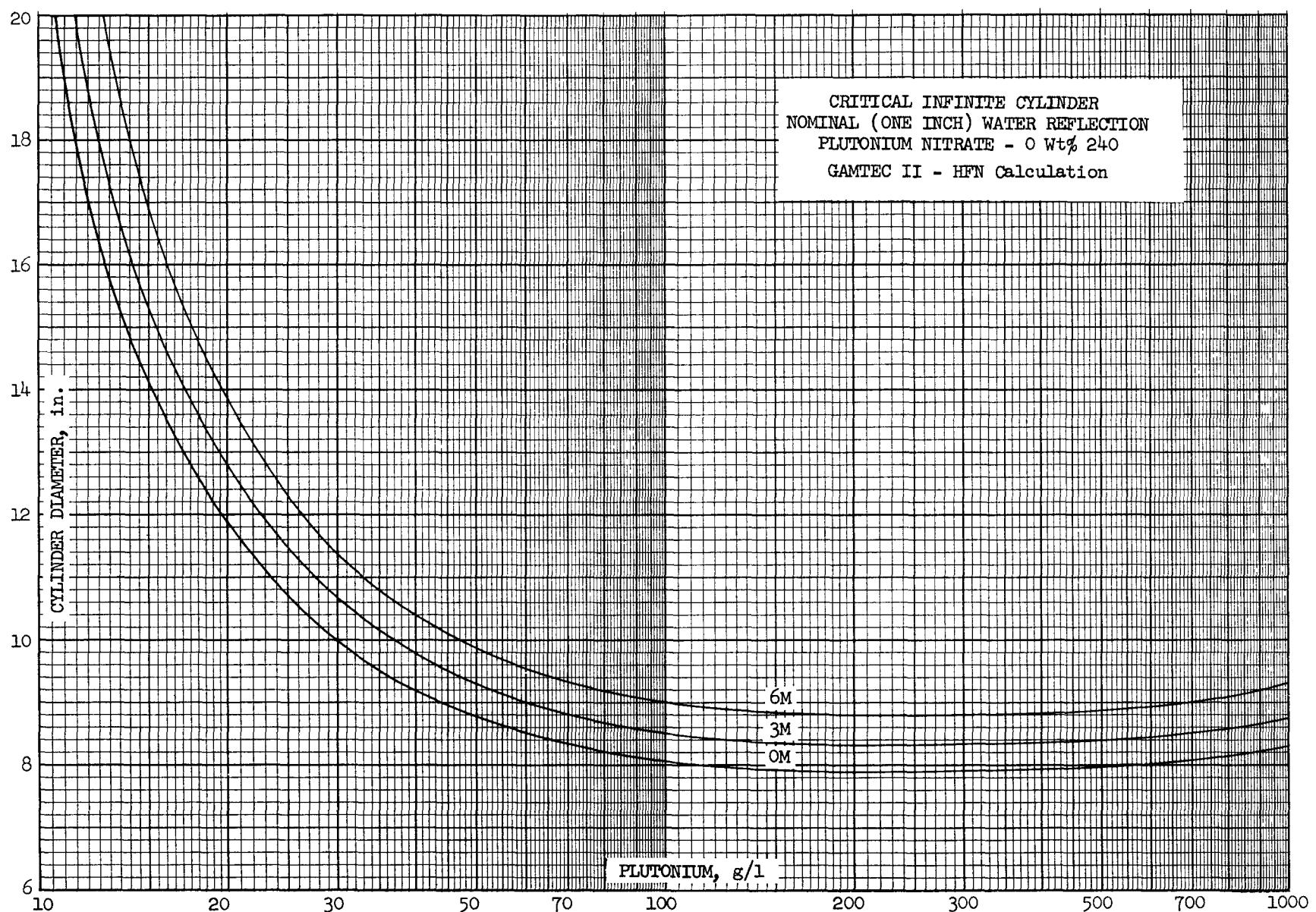
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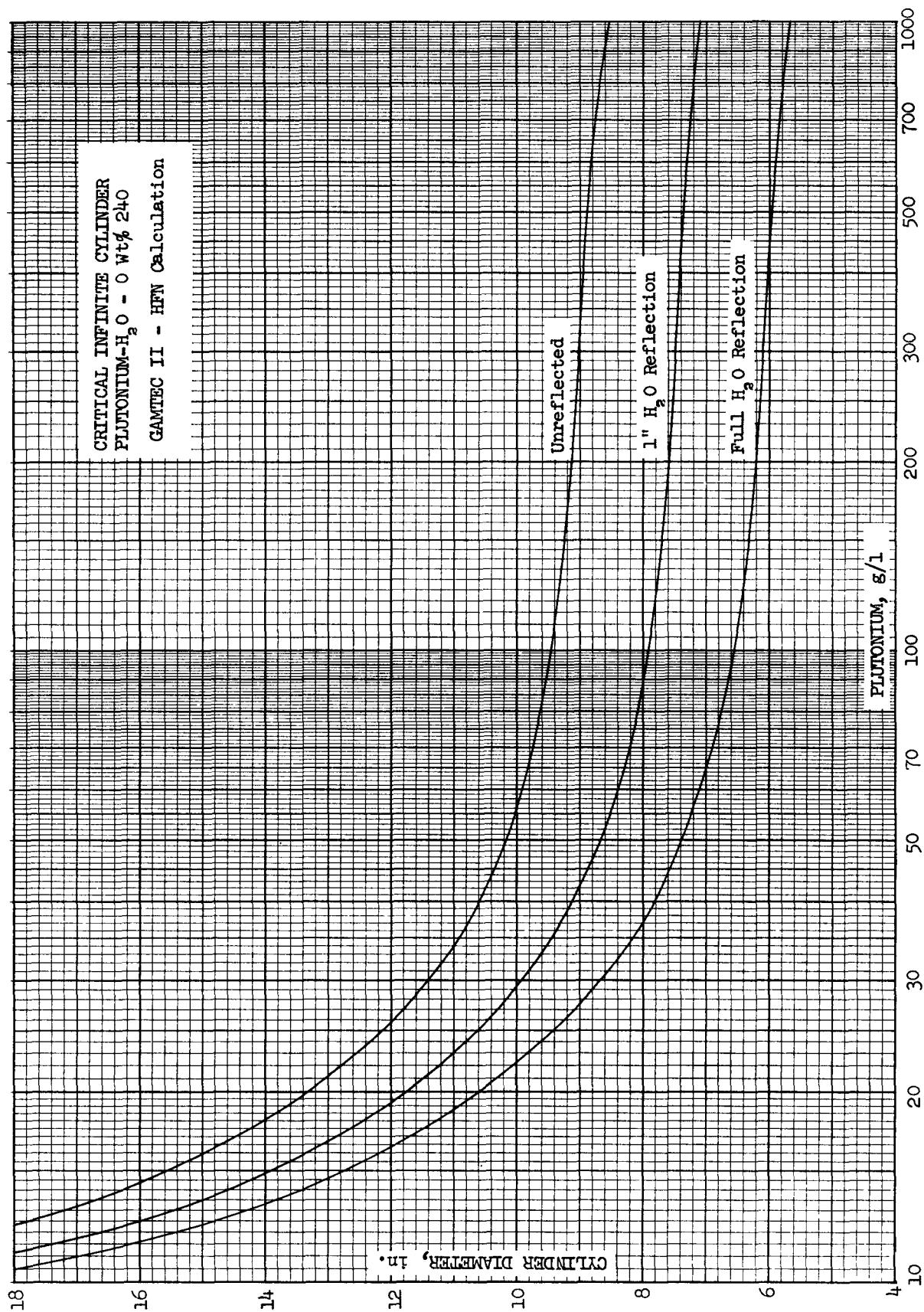
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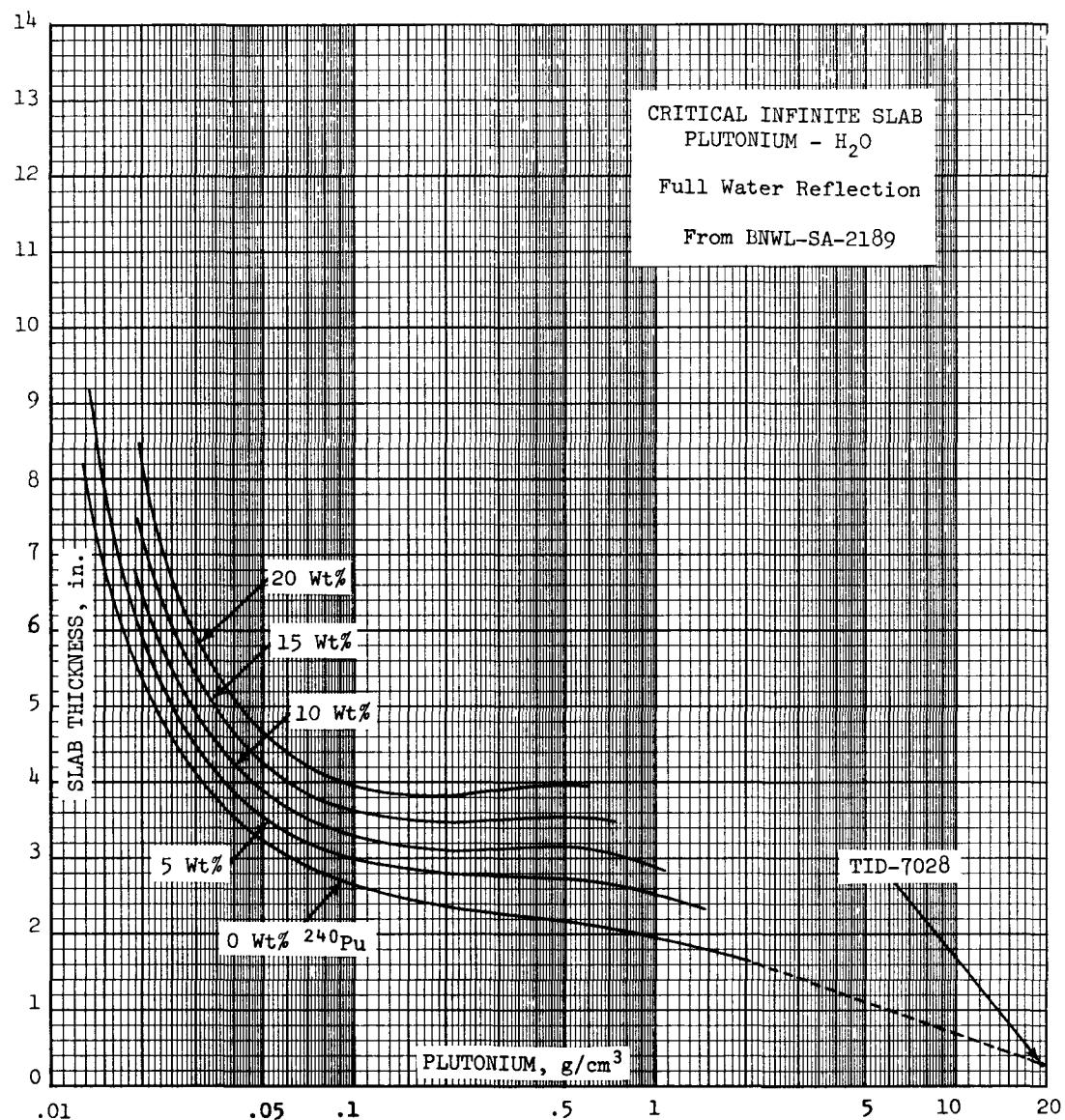
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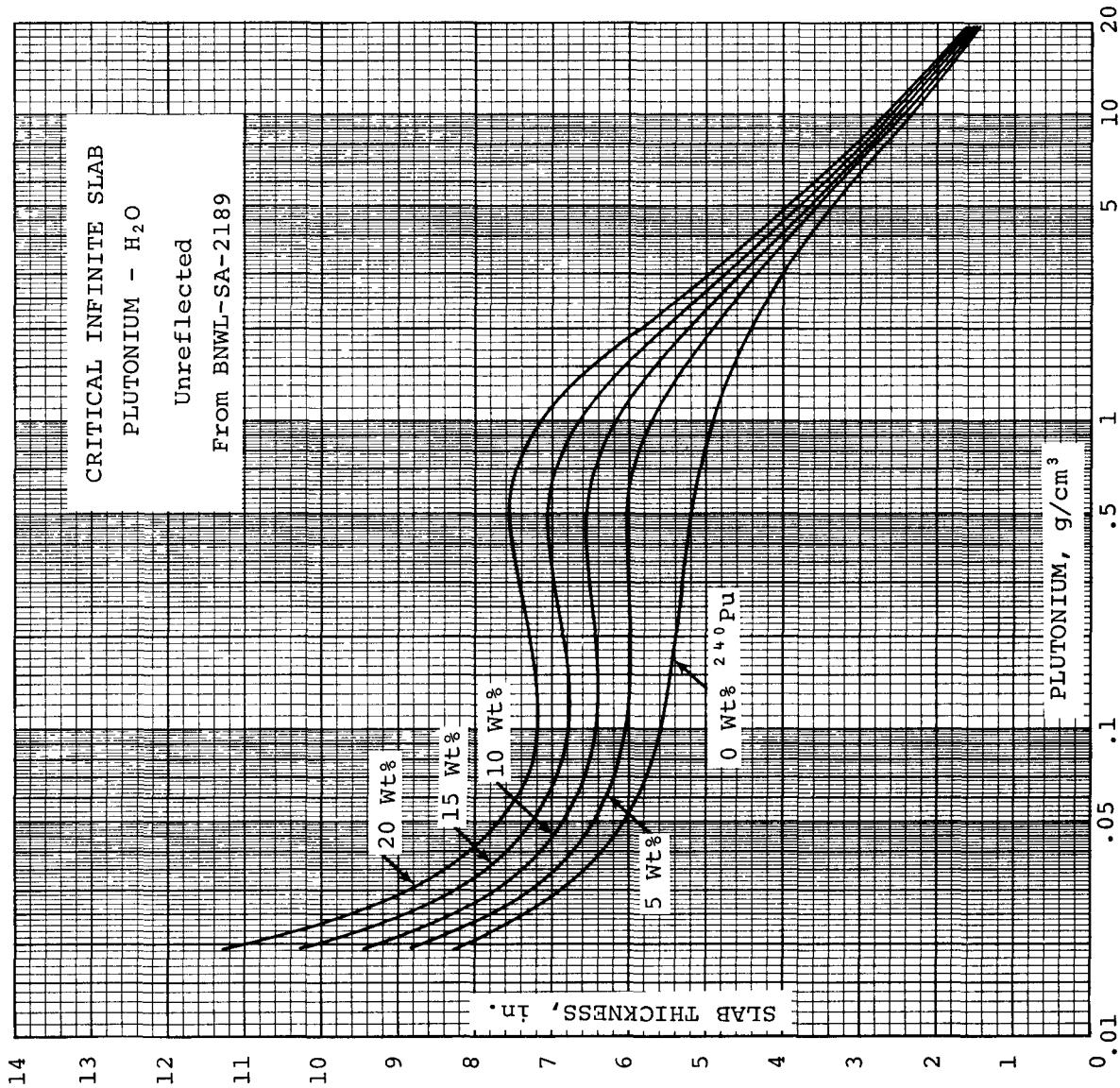
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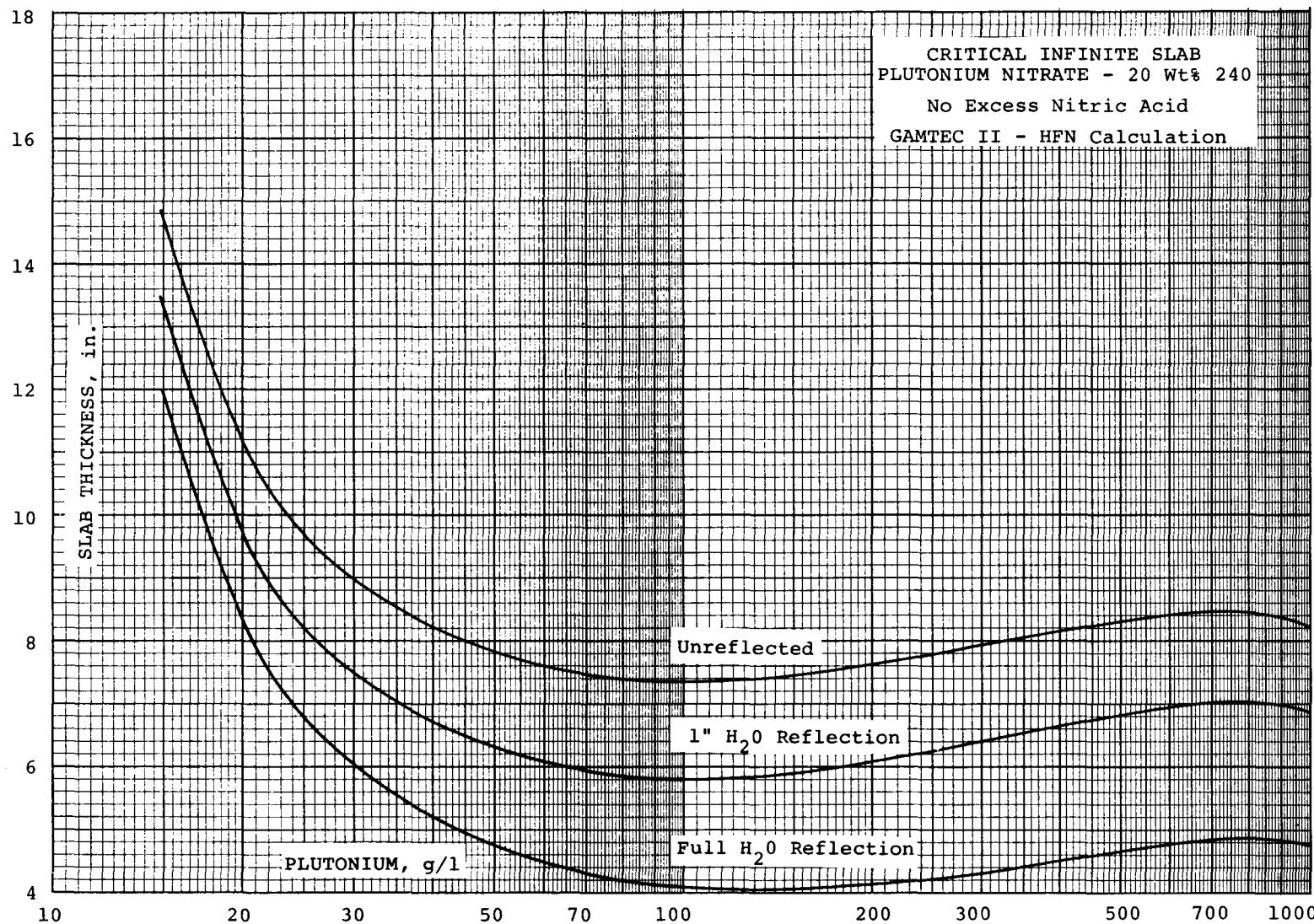
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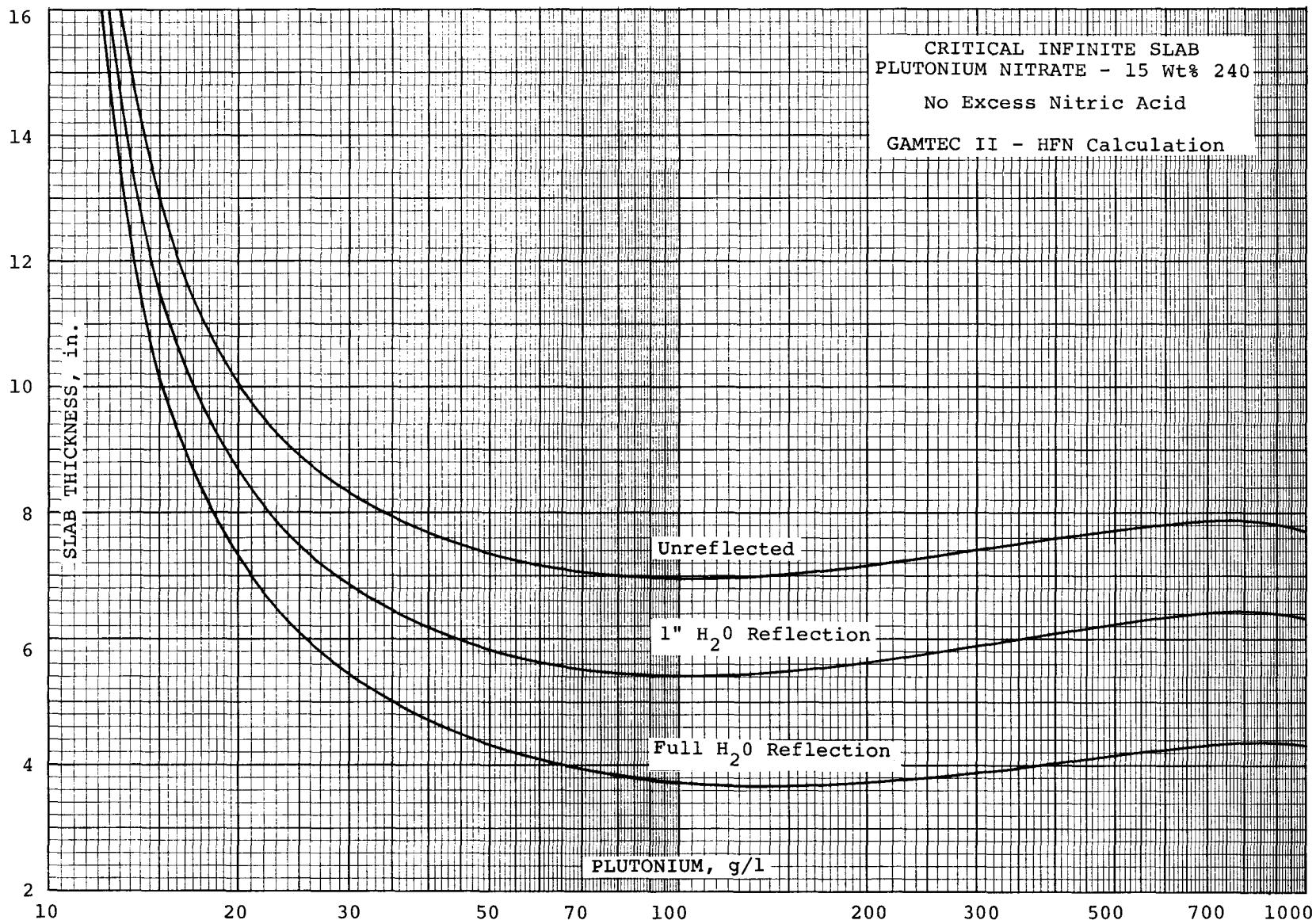


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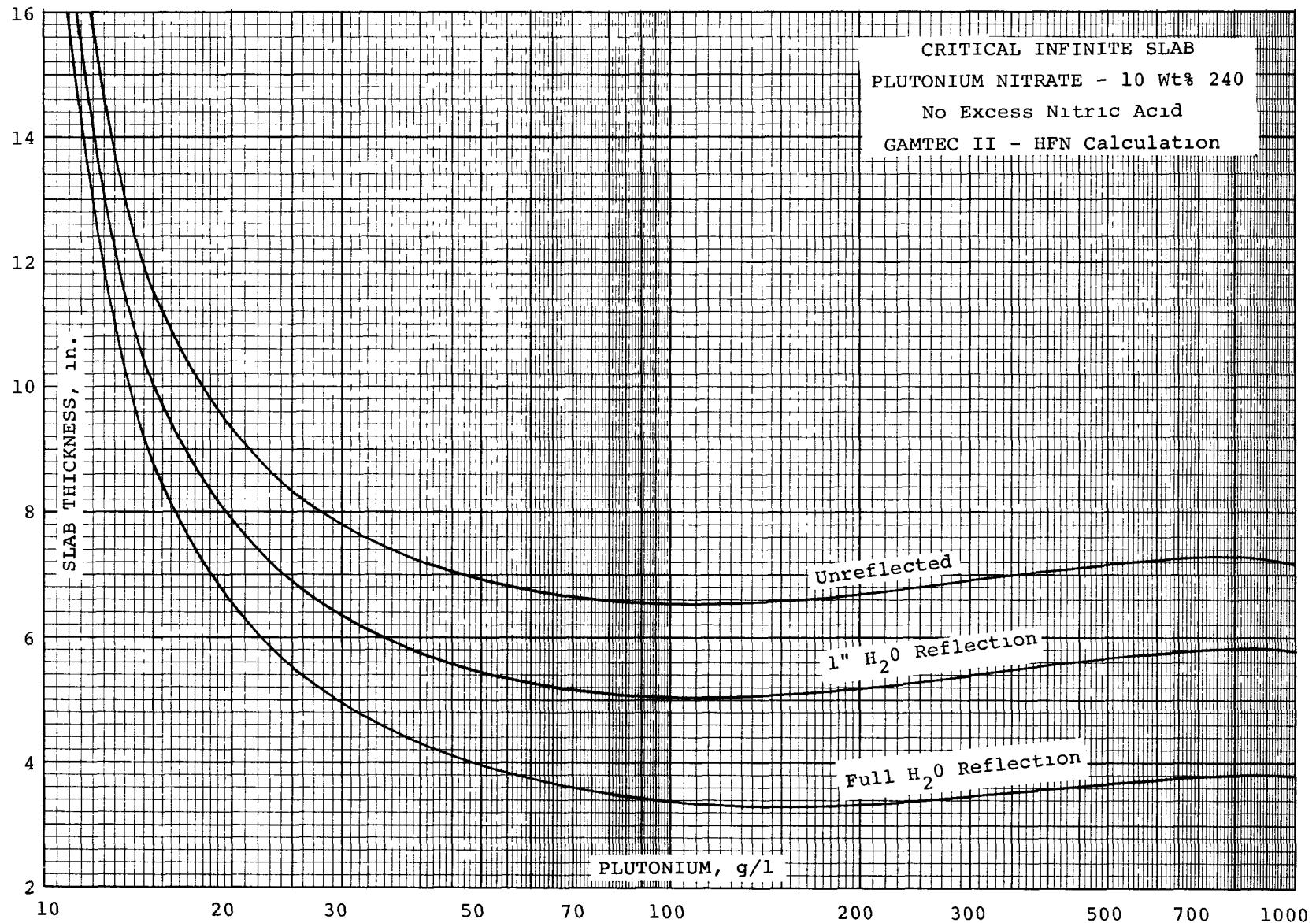


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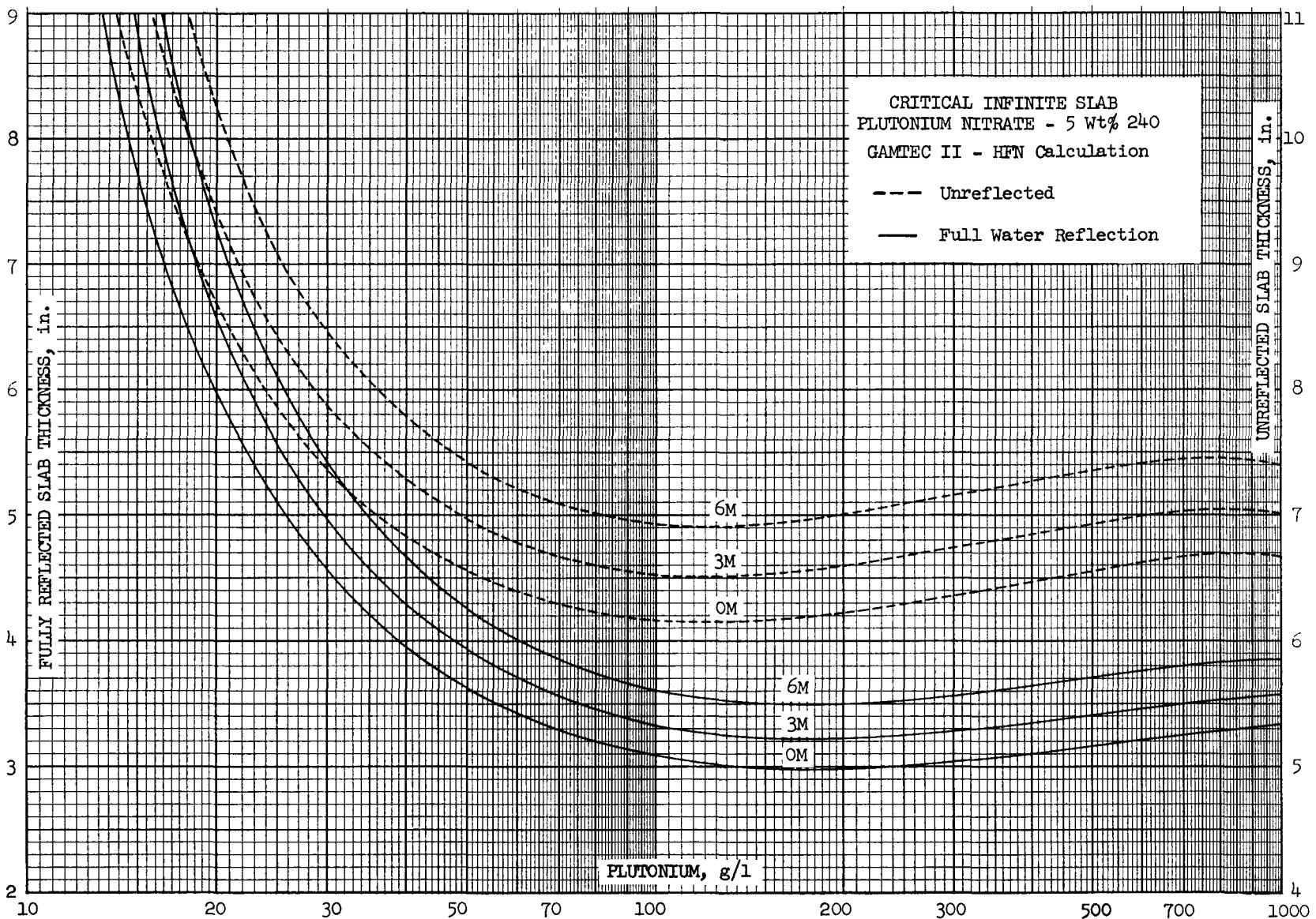
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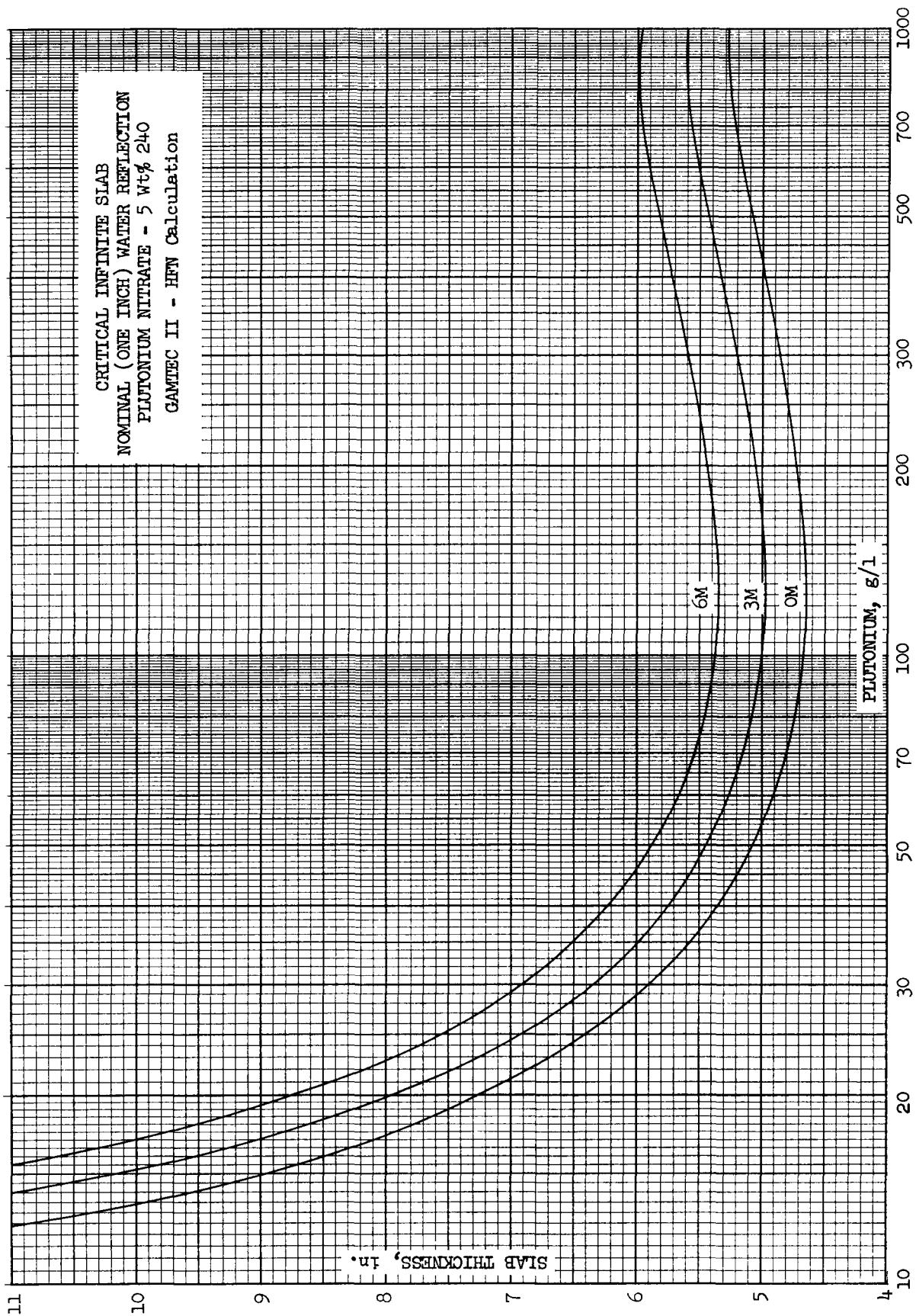
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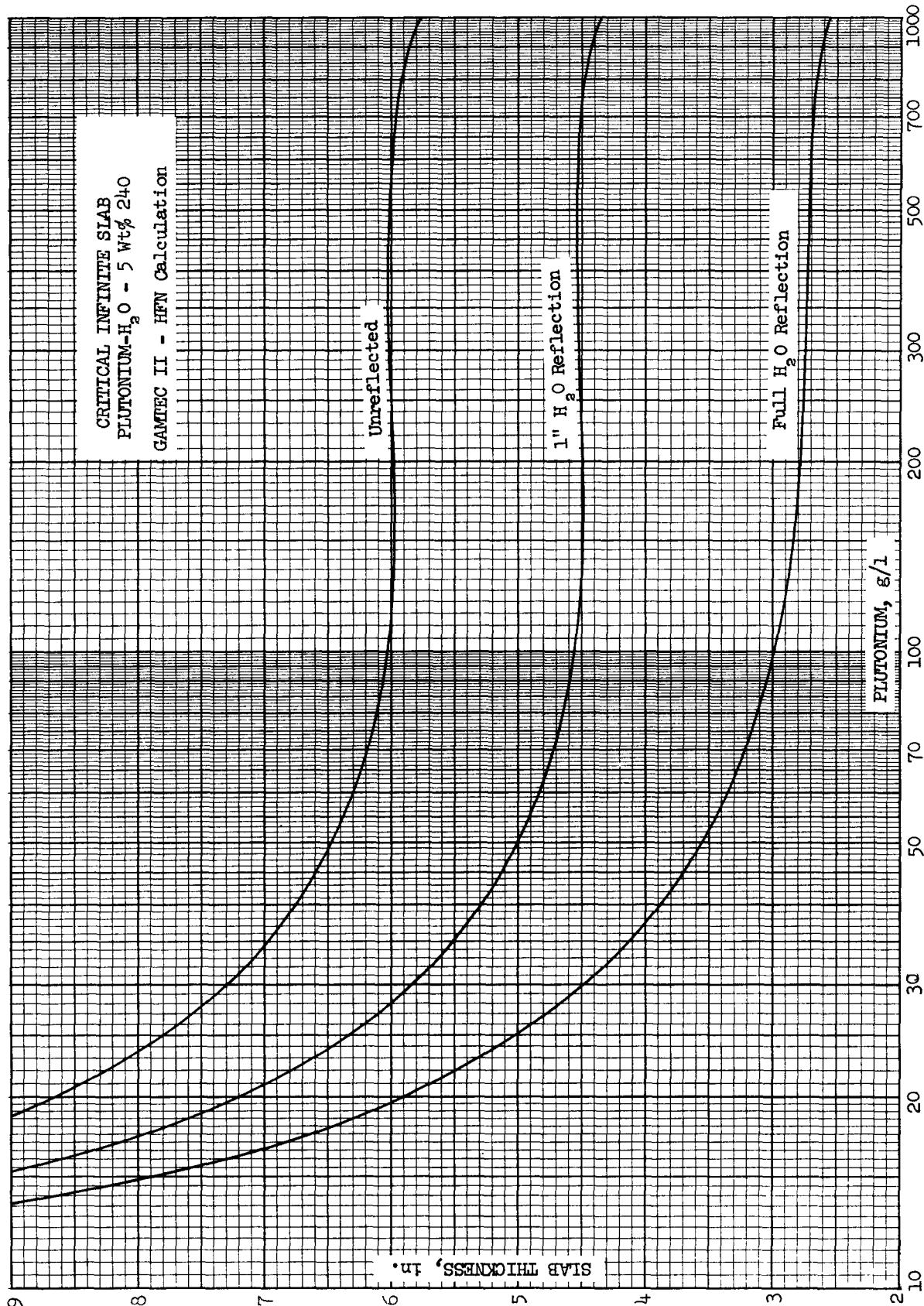
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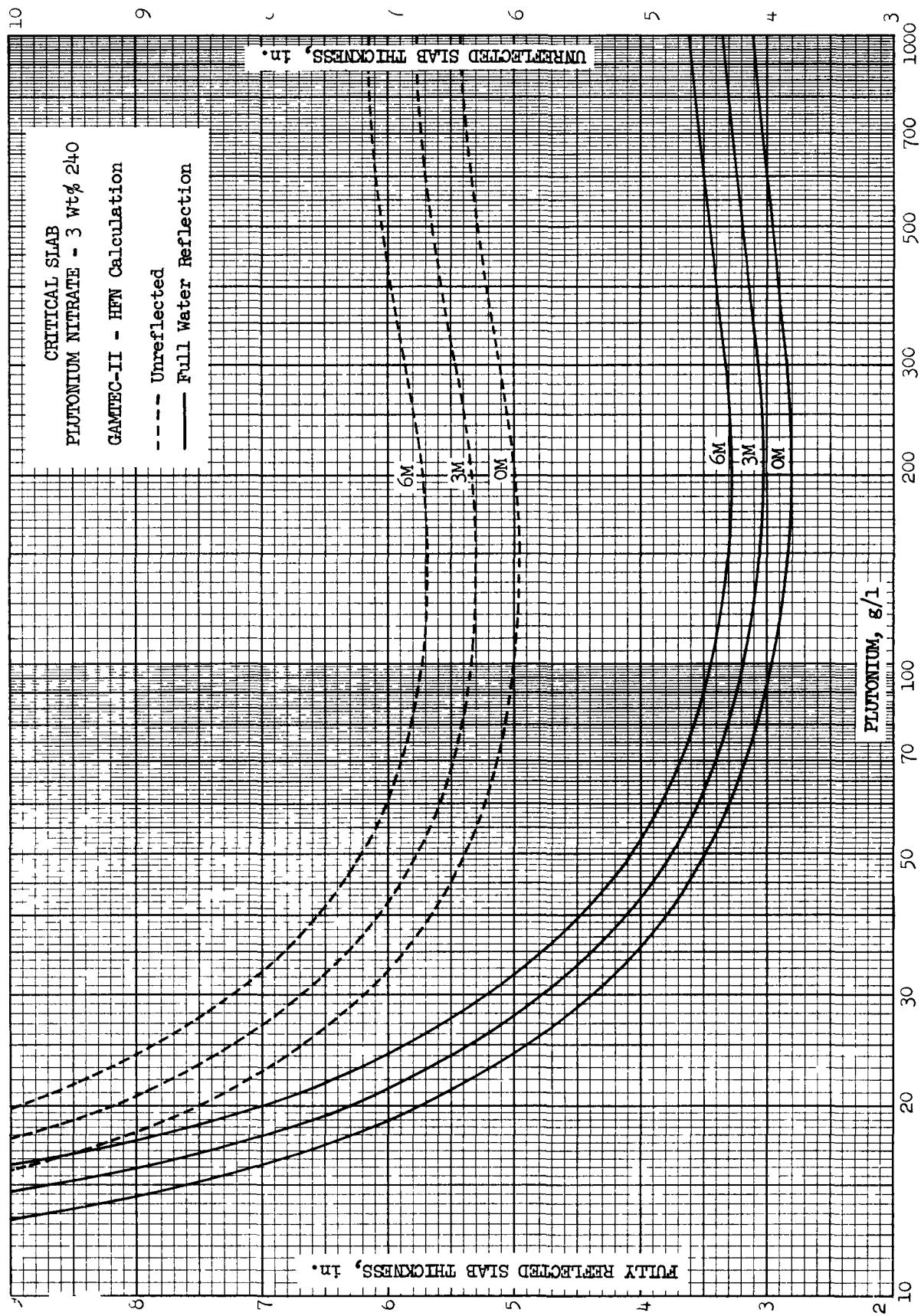
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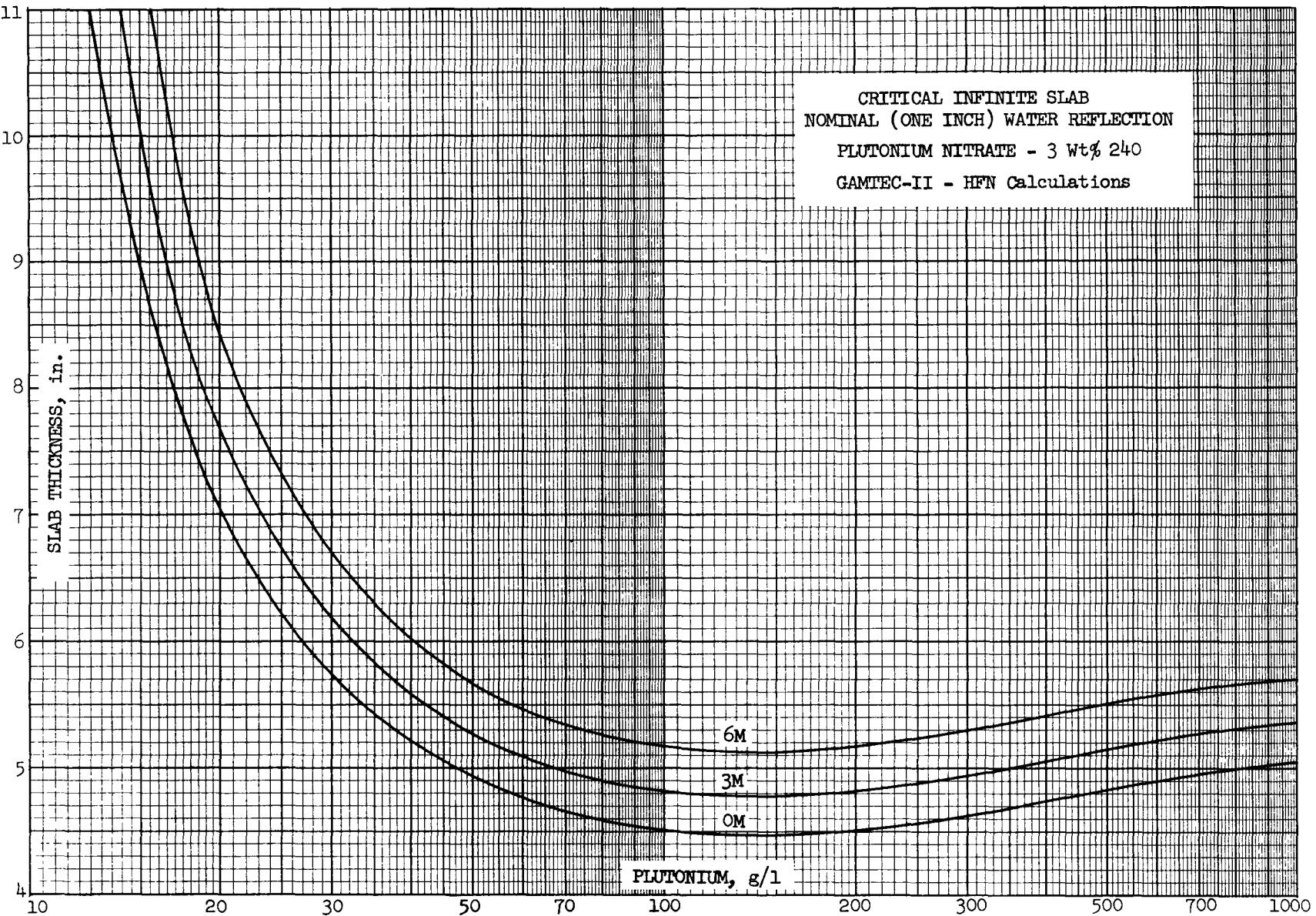


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III.A.5.97-2

ARH-600

CRITICAL INFINITE SLAB
NOMINAL (ONE INCH) WATER REFLECTION
PLUTONIUM NITRATE - 3 Wt% 240
GAMTEC-II - HFN Calculations

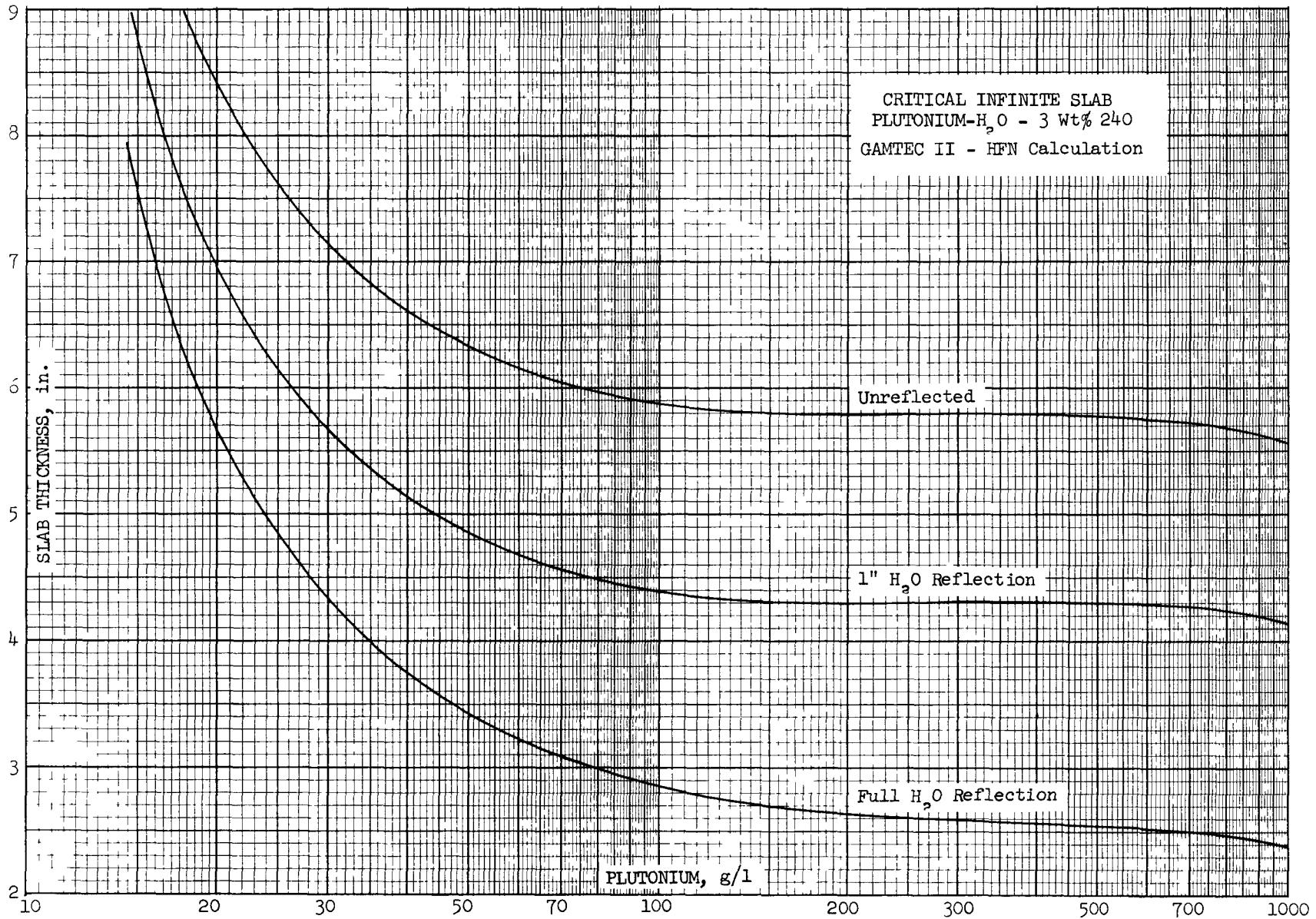


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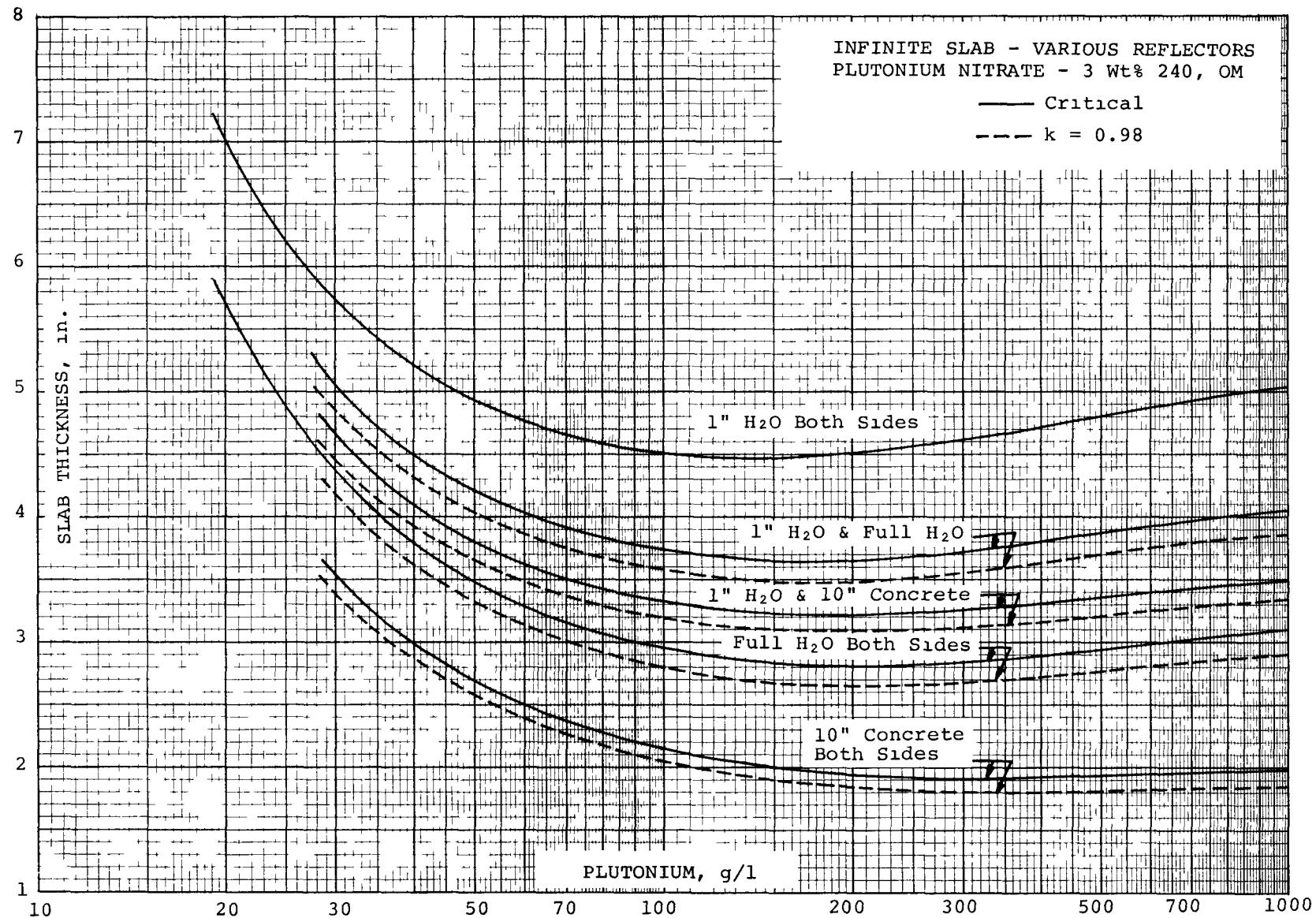


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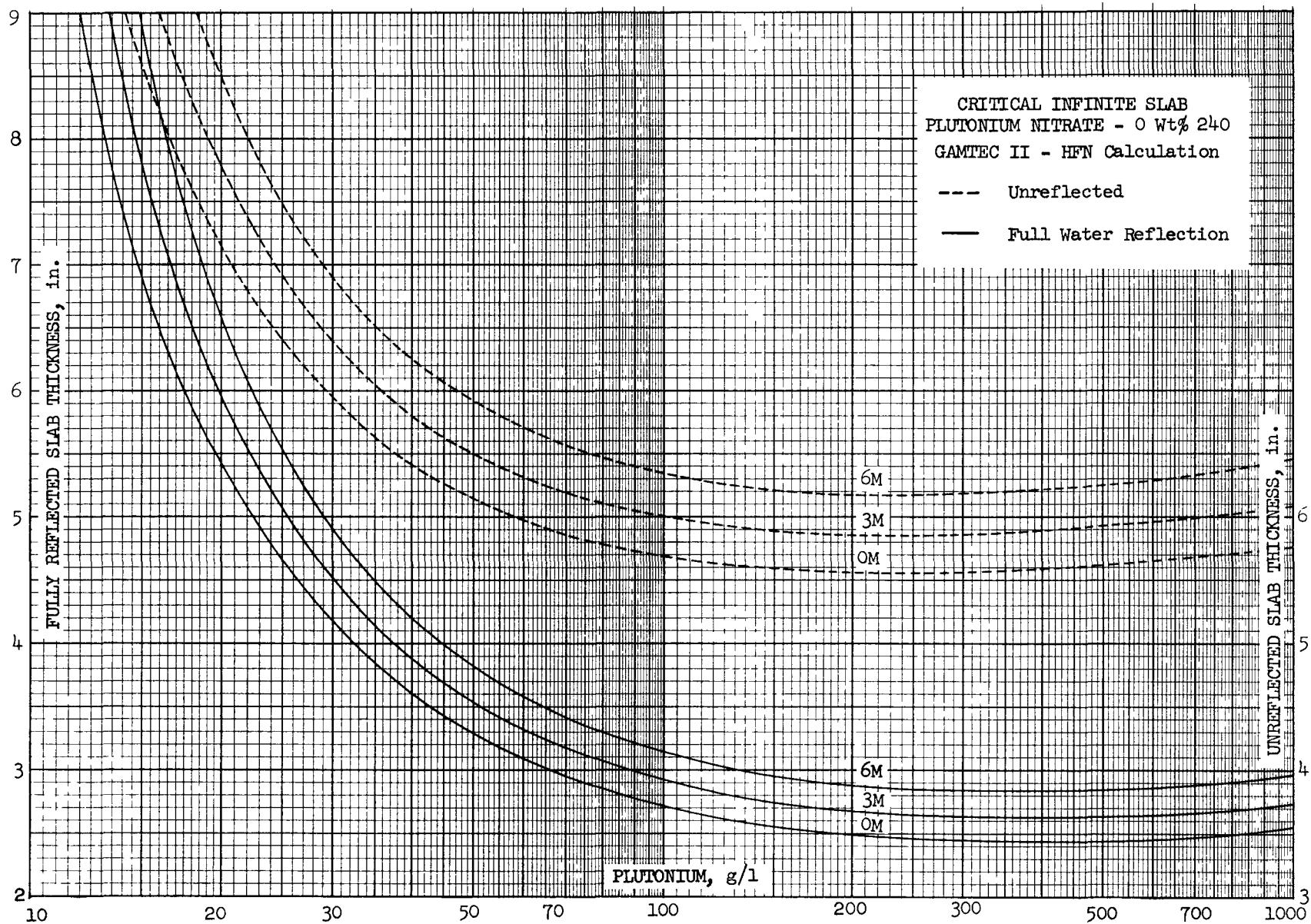


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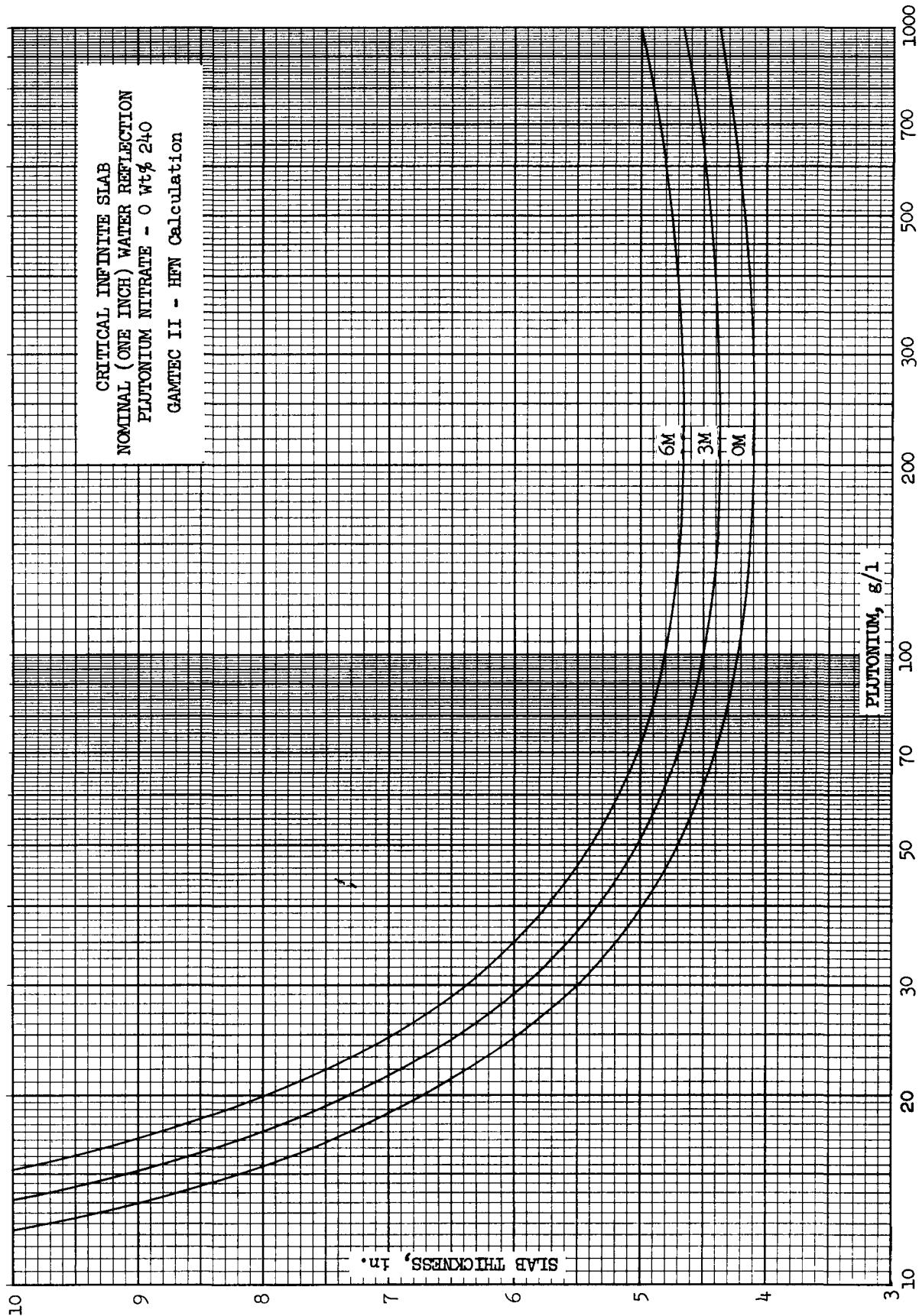
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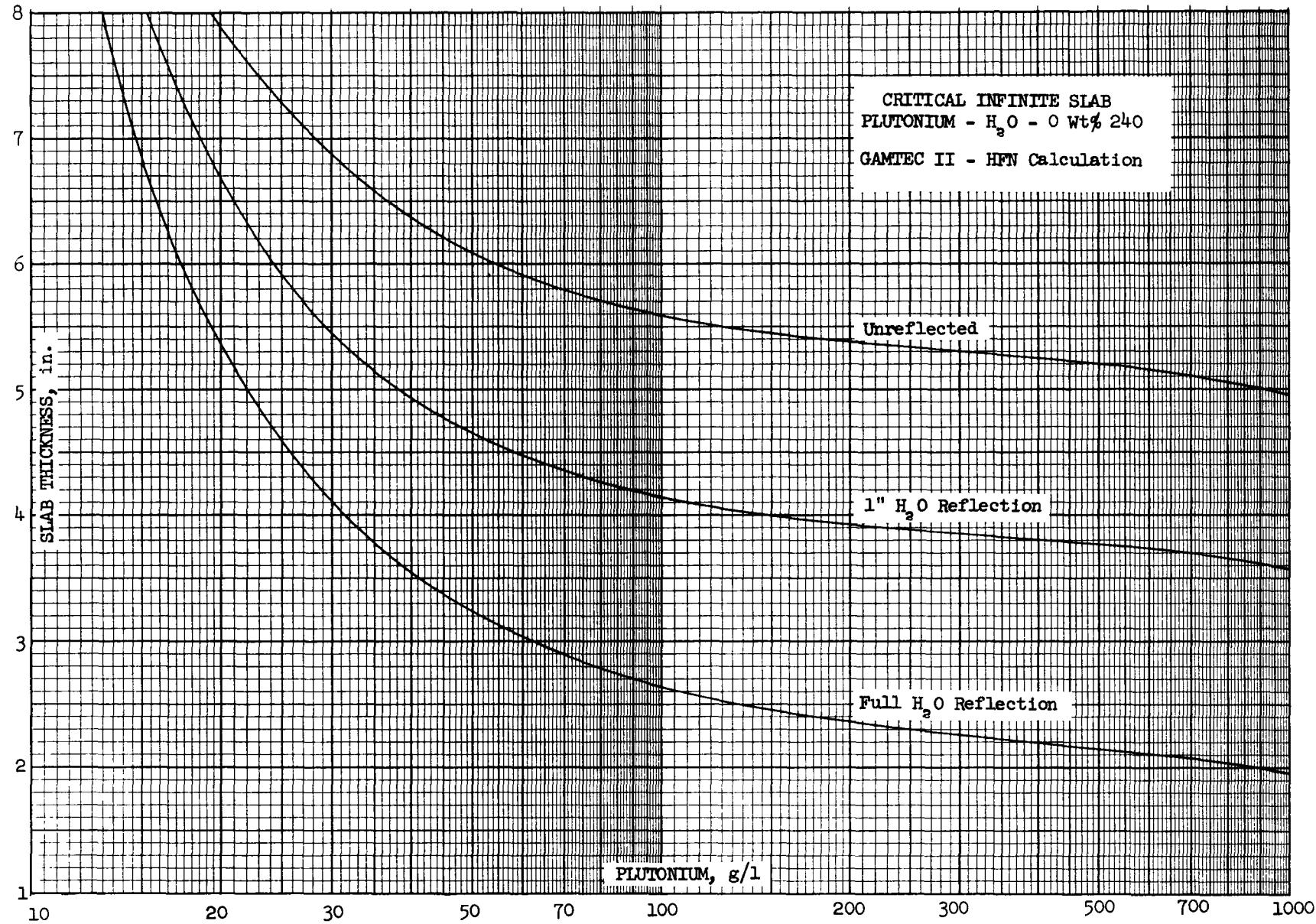


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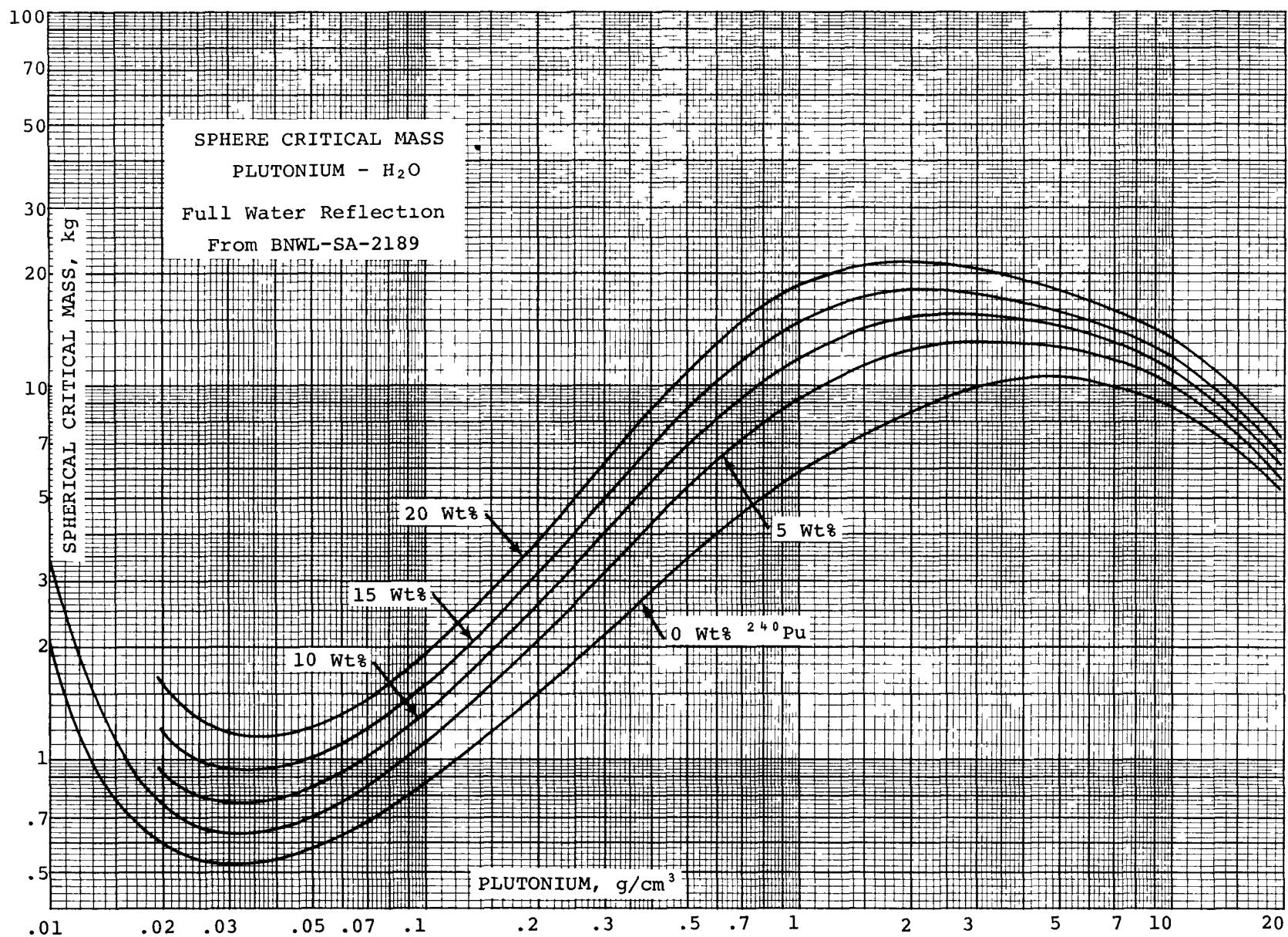
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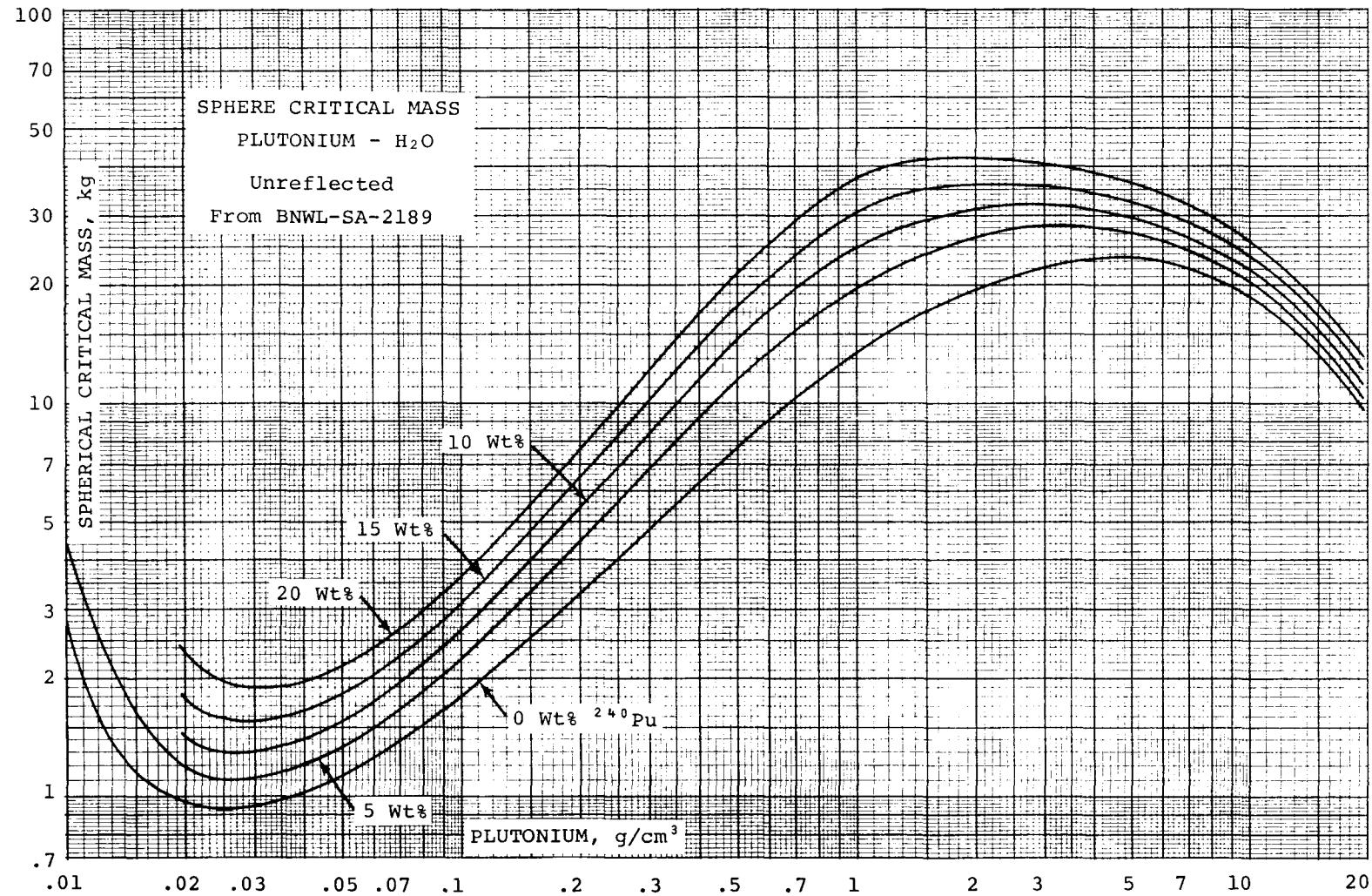
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III.A.6-1

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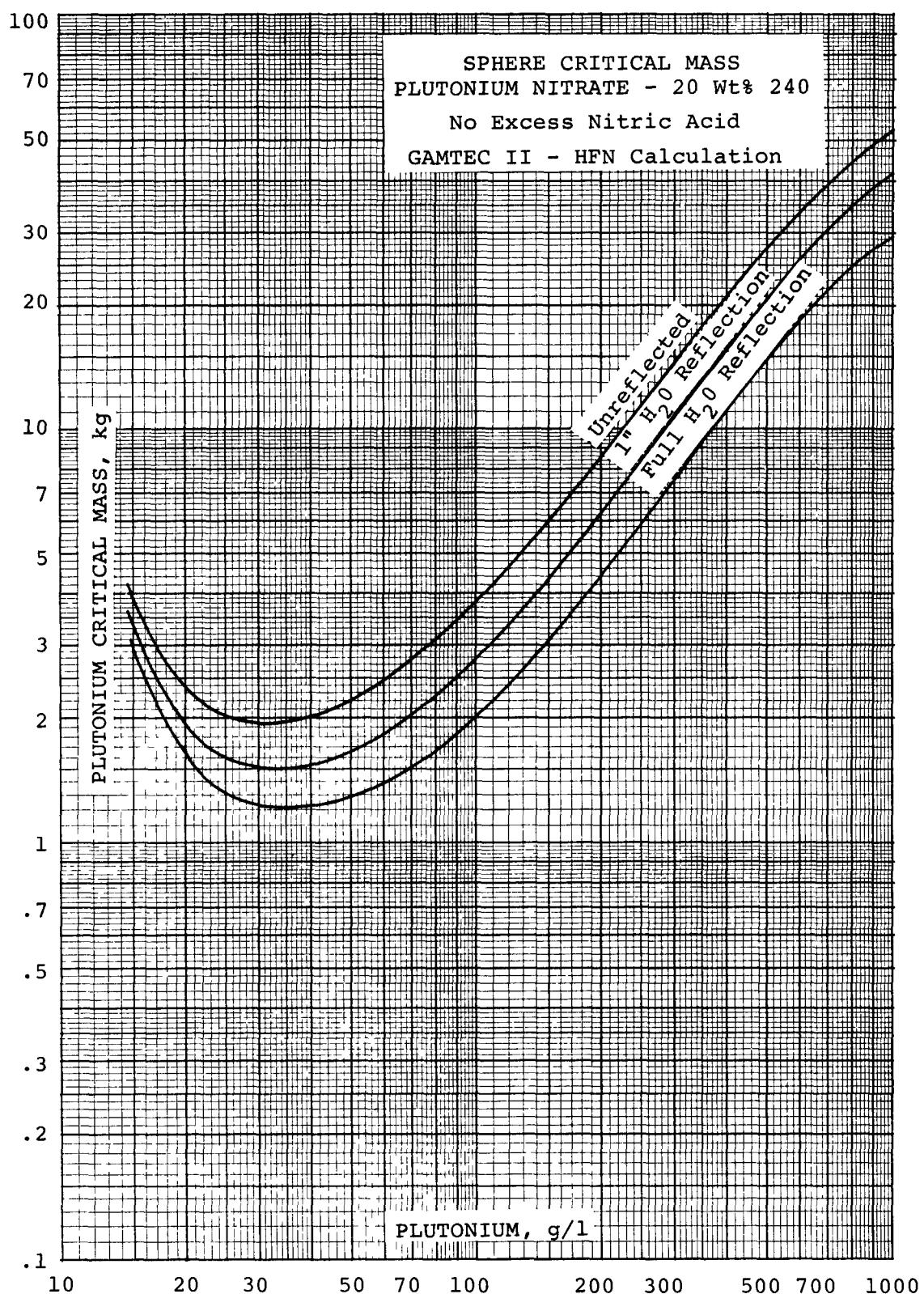
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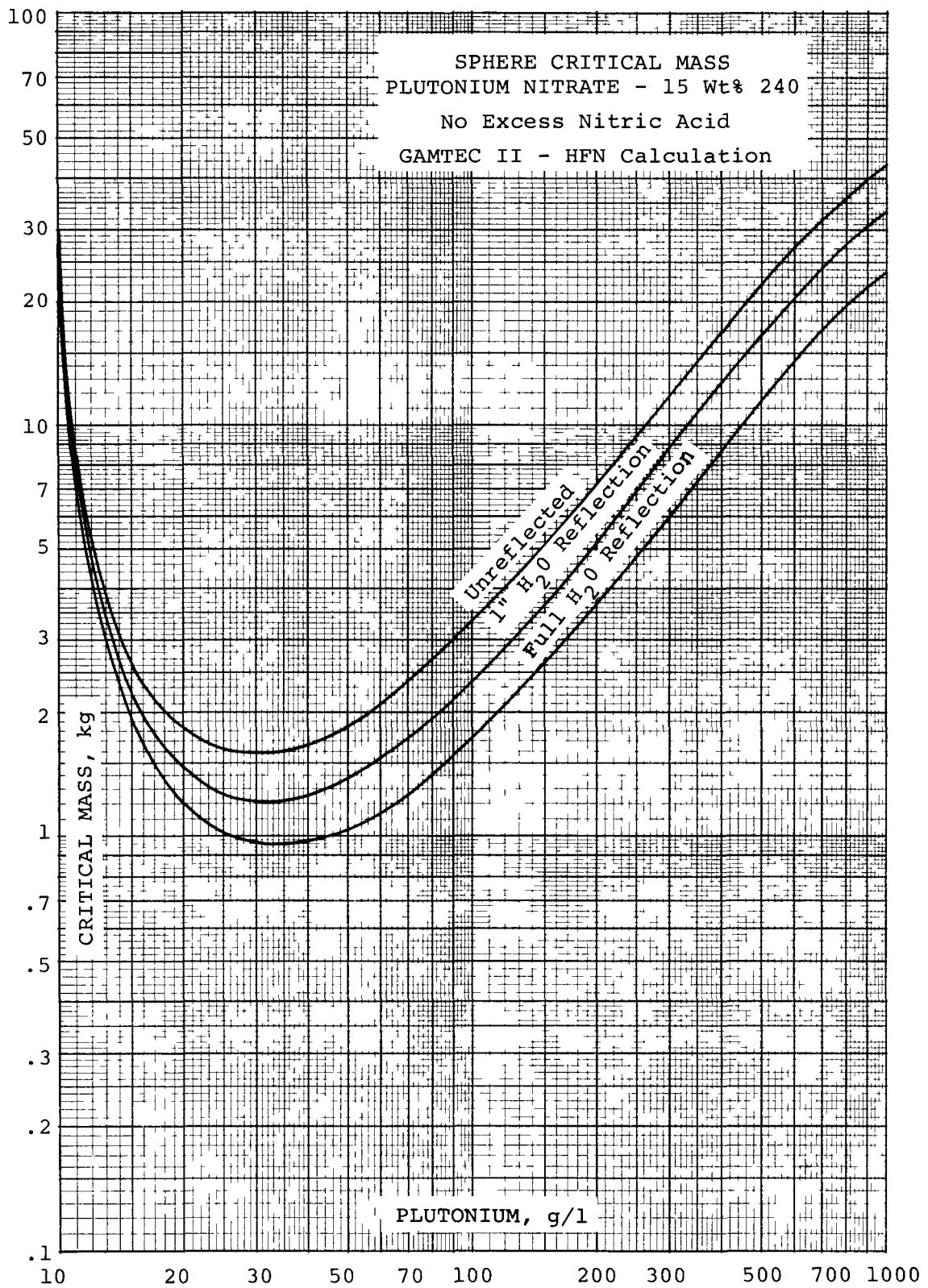


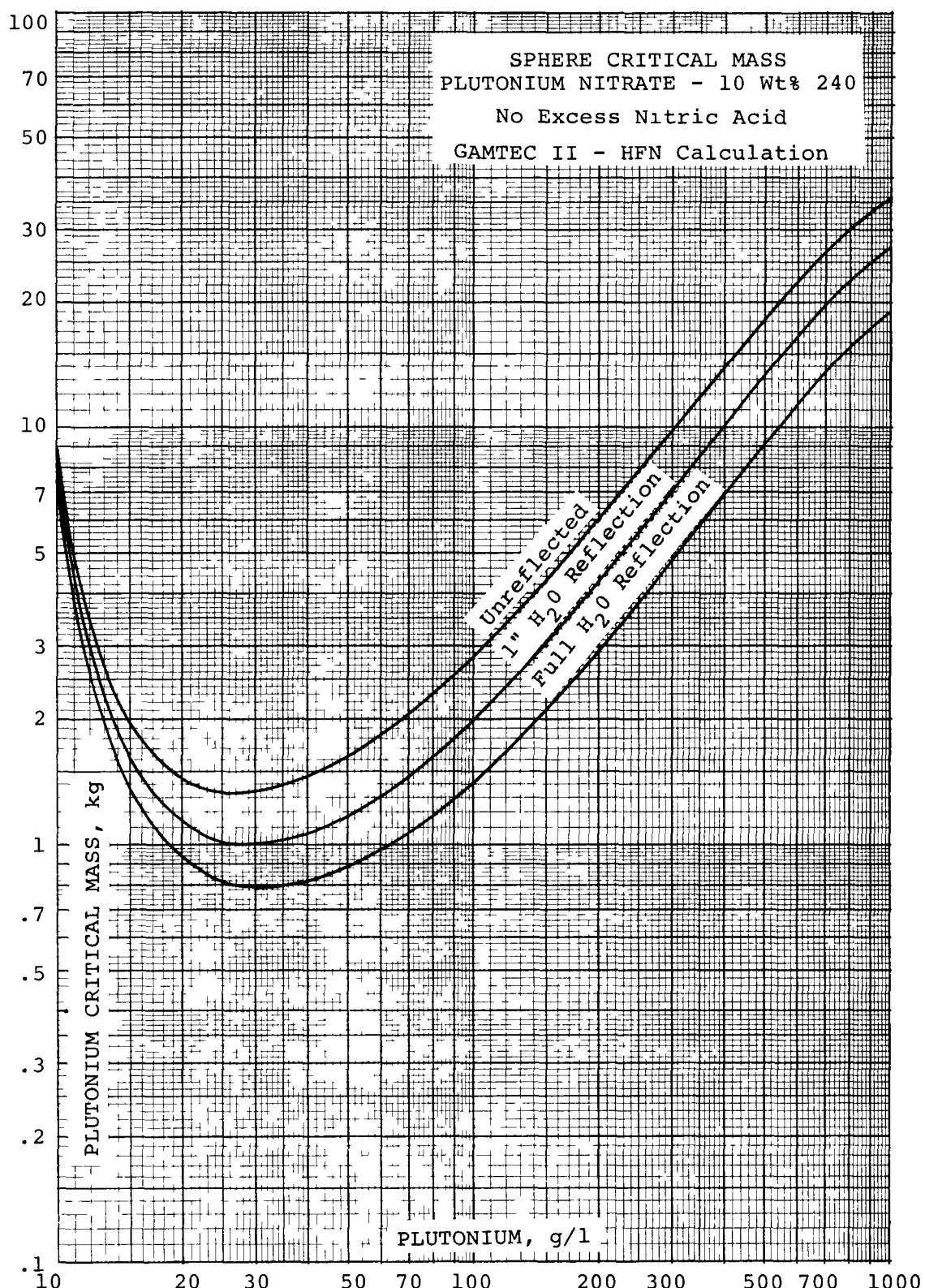
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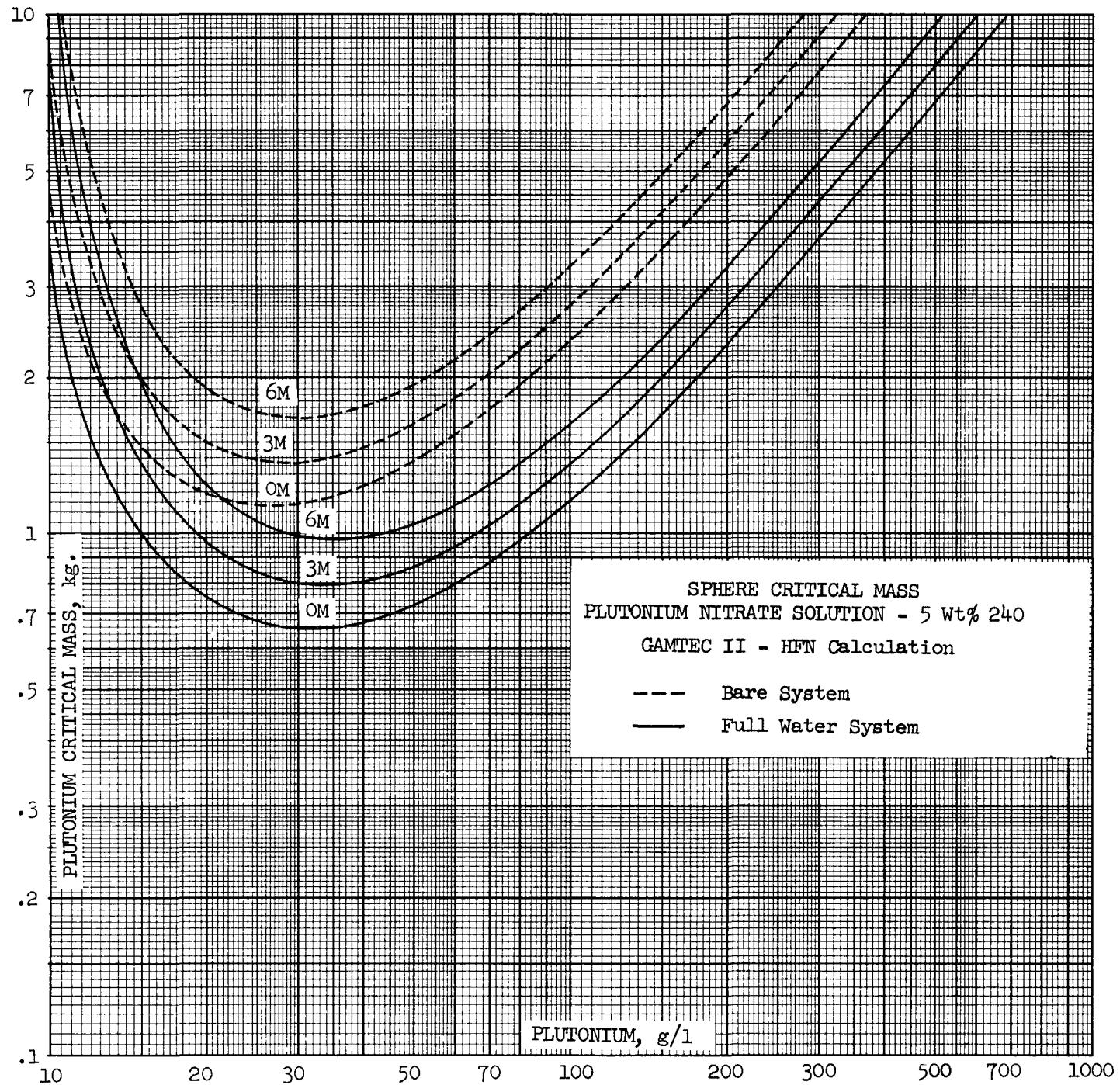
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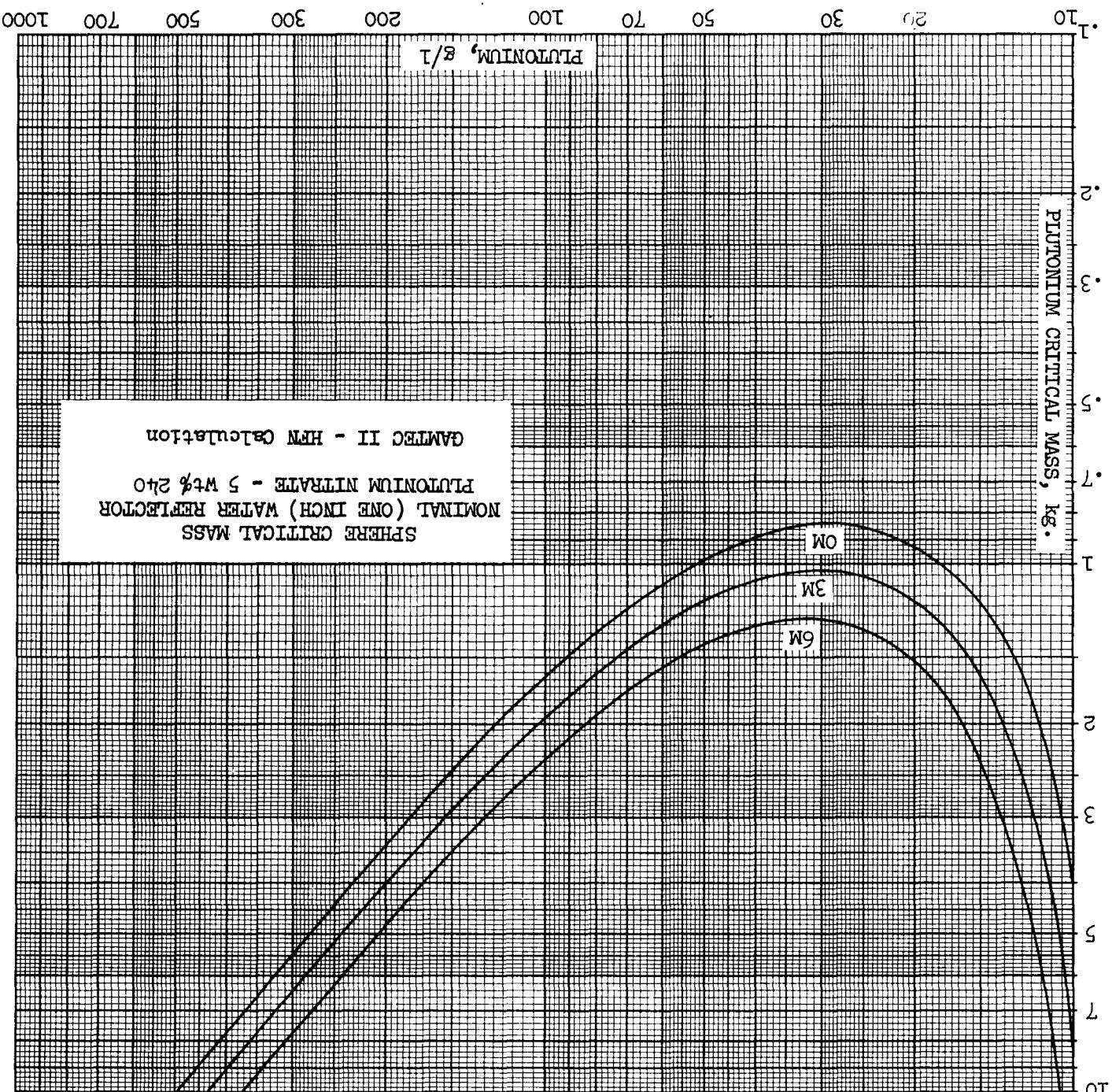








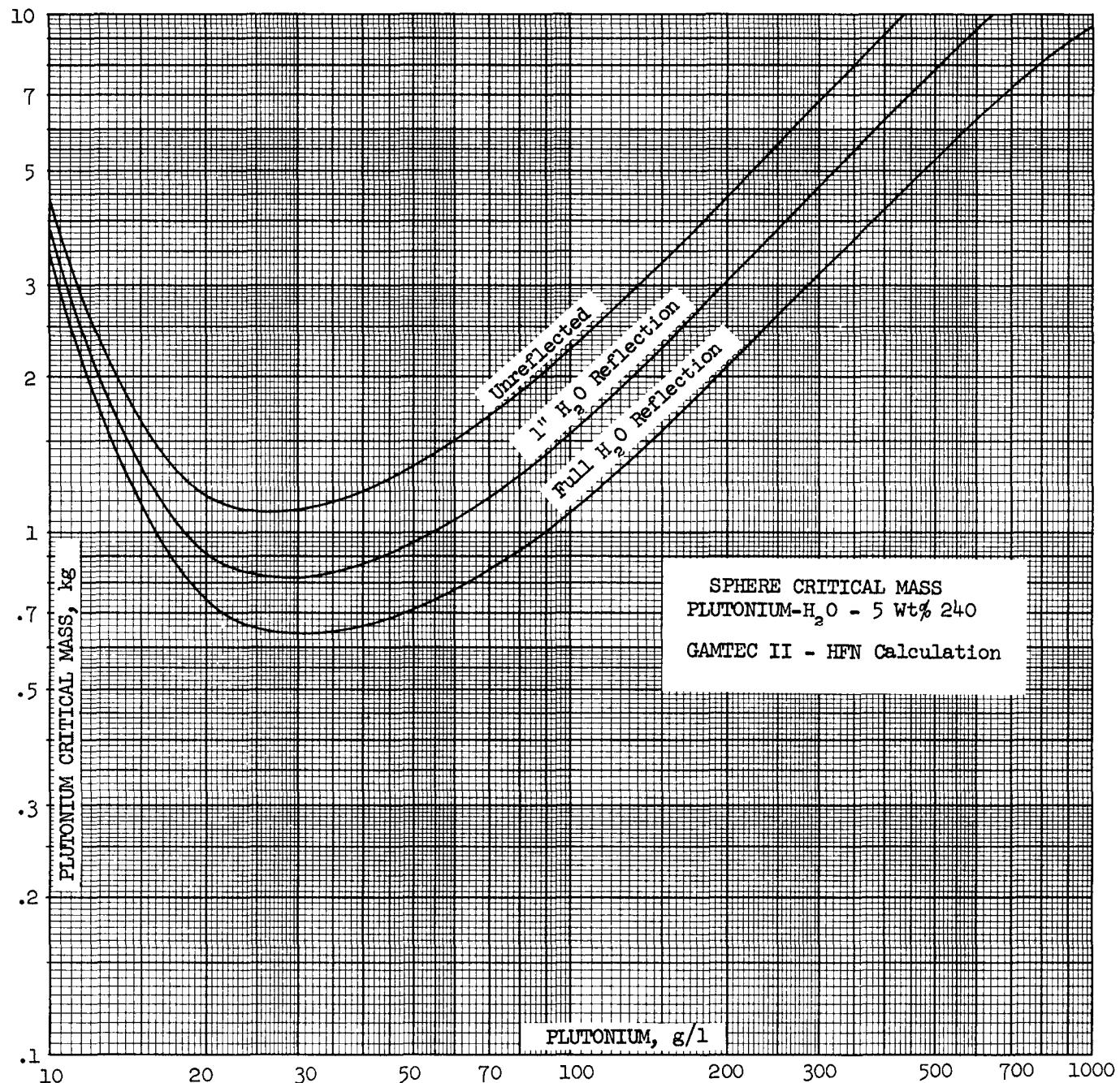
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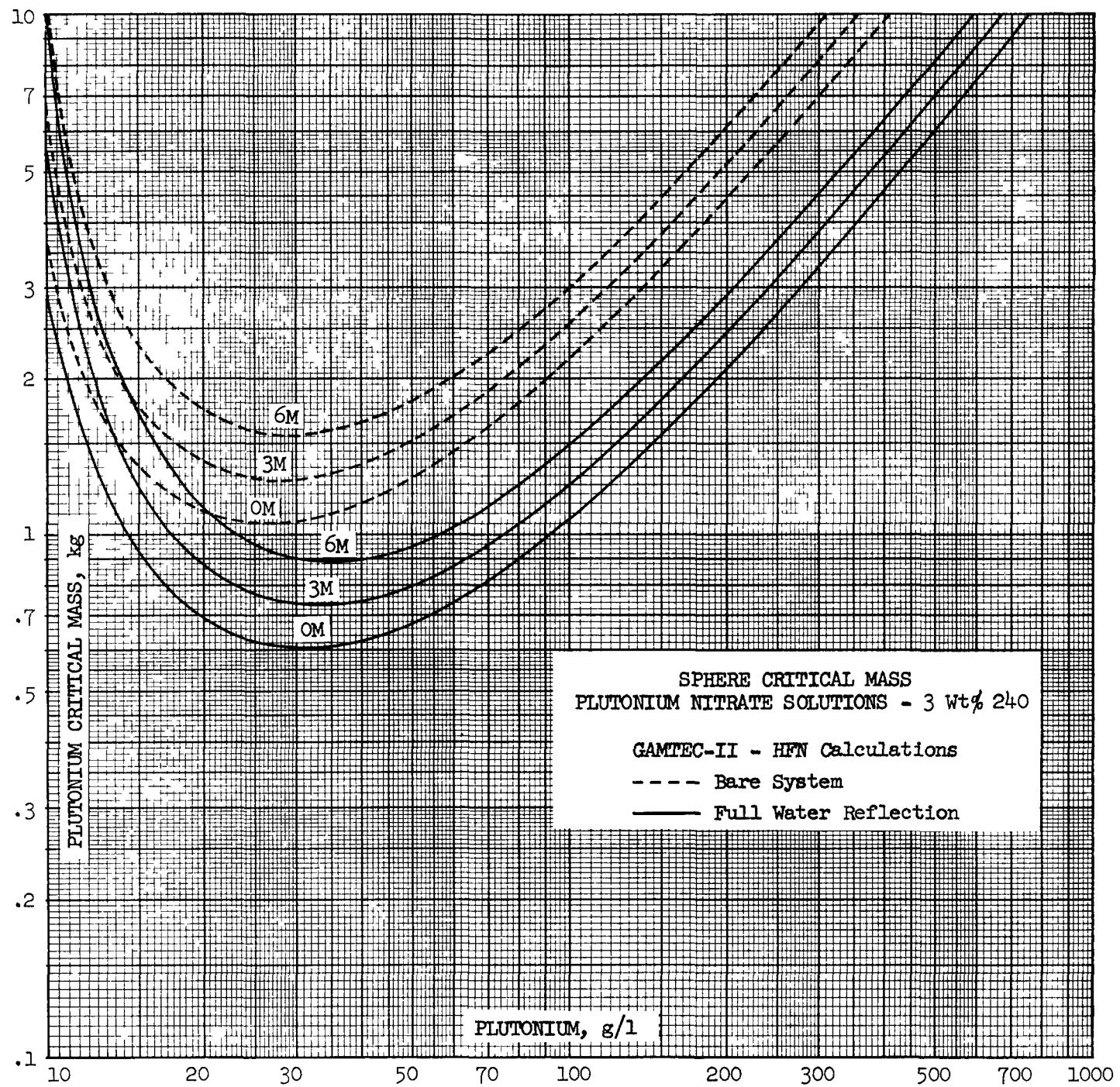
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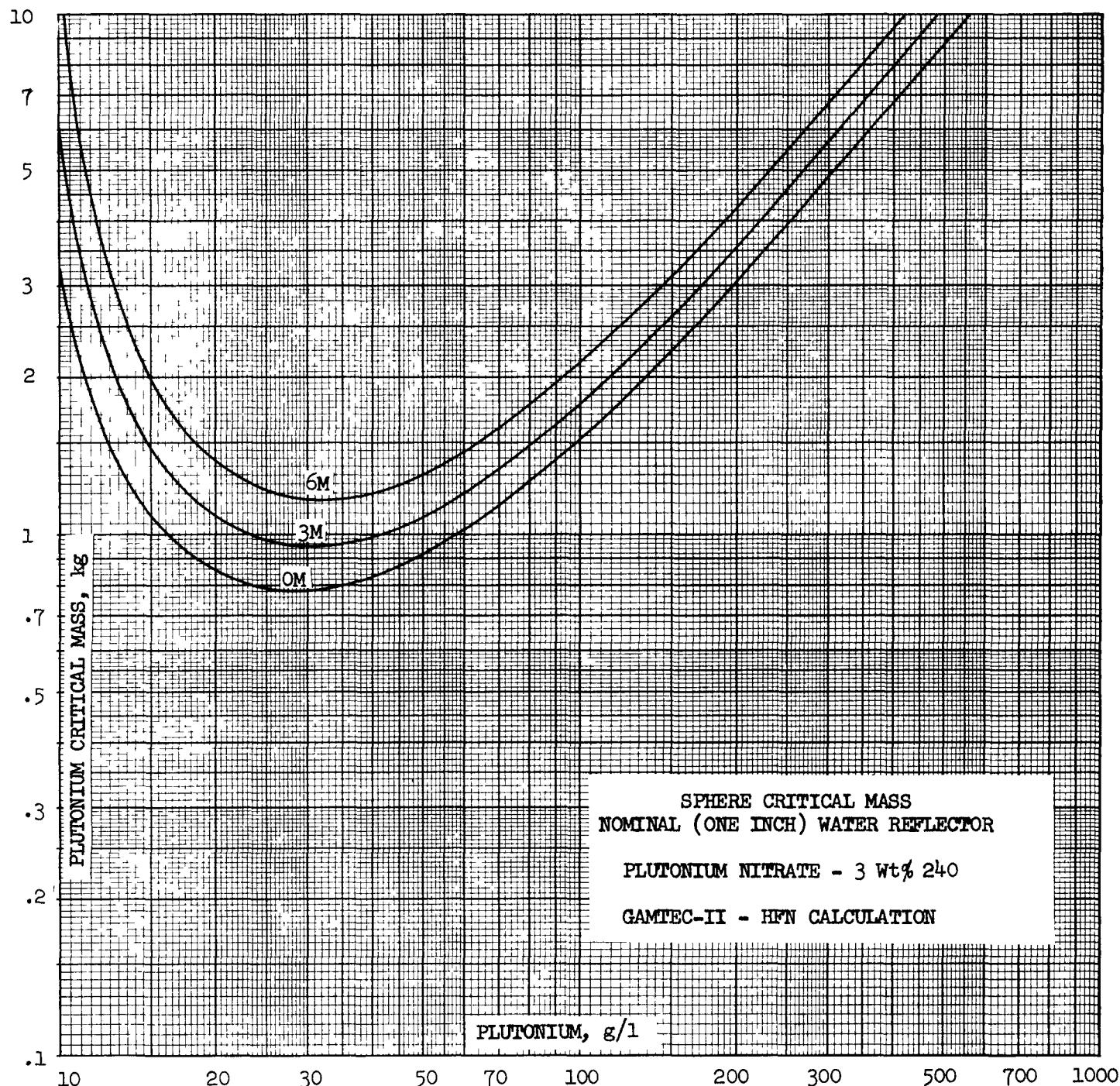
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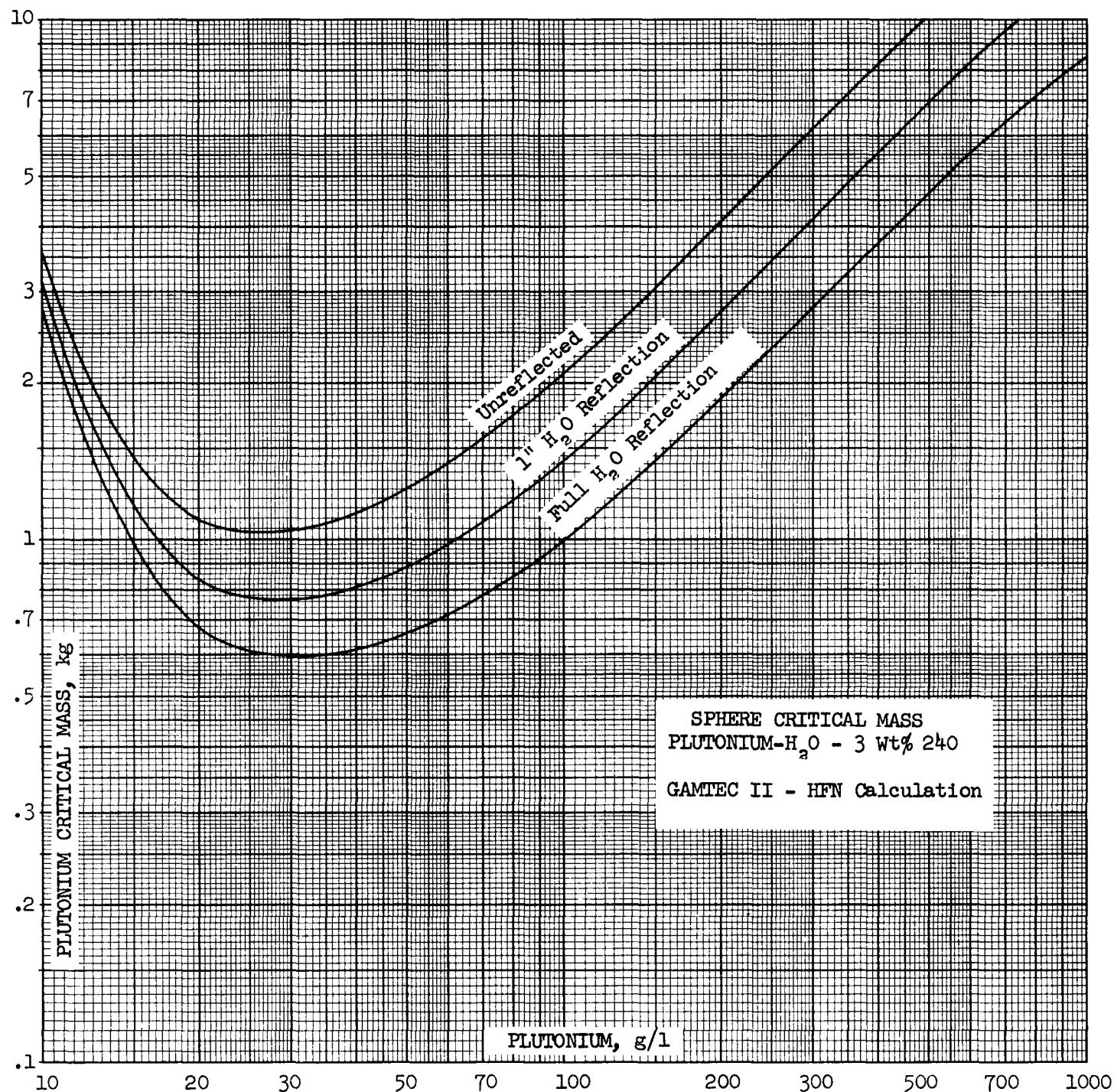
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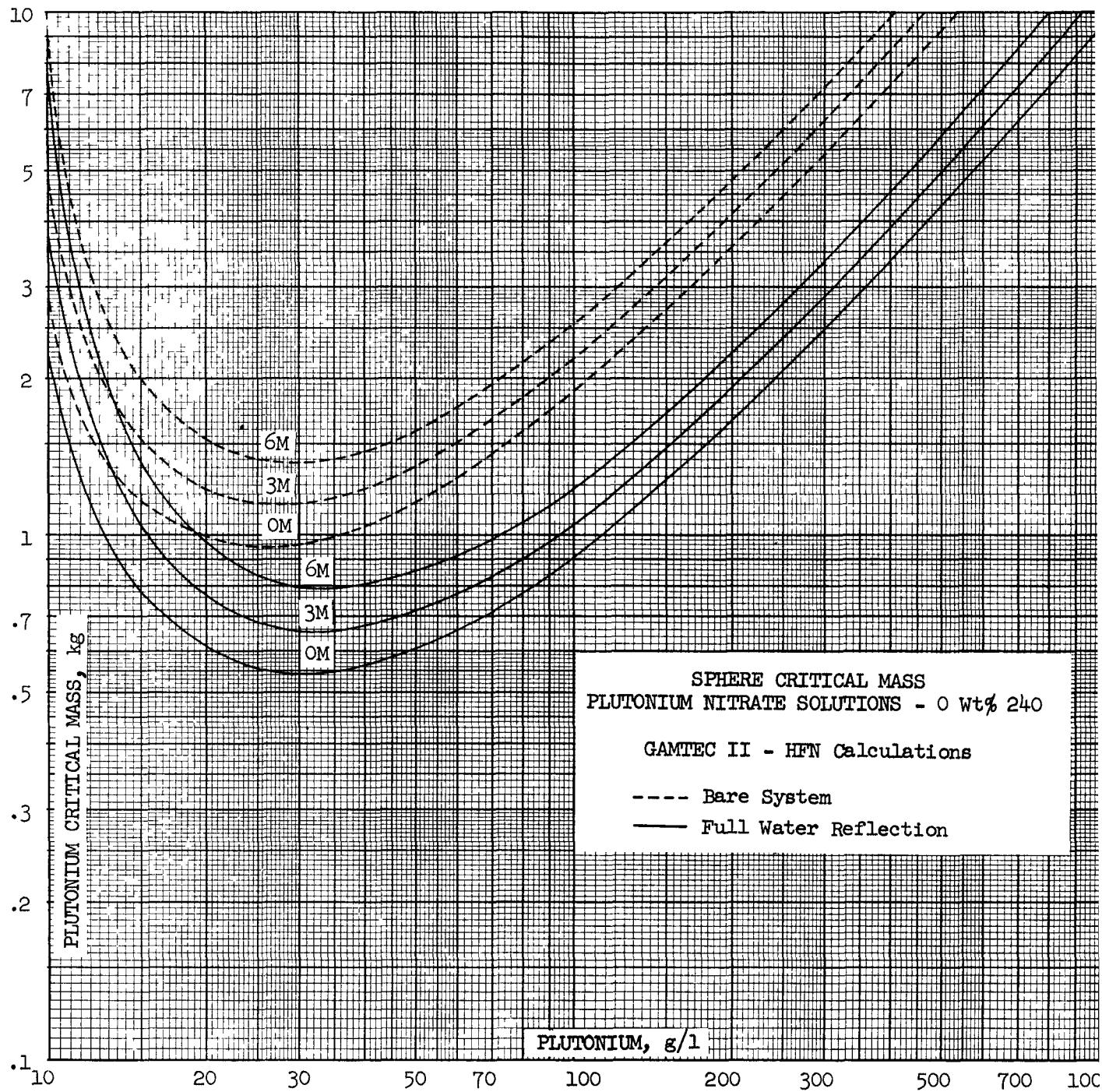


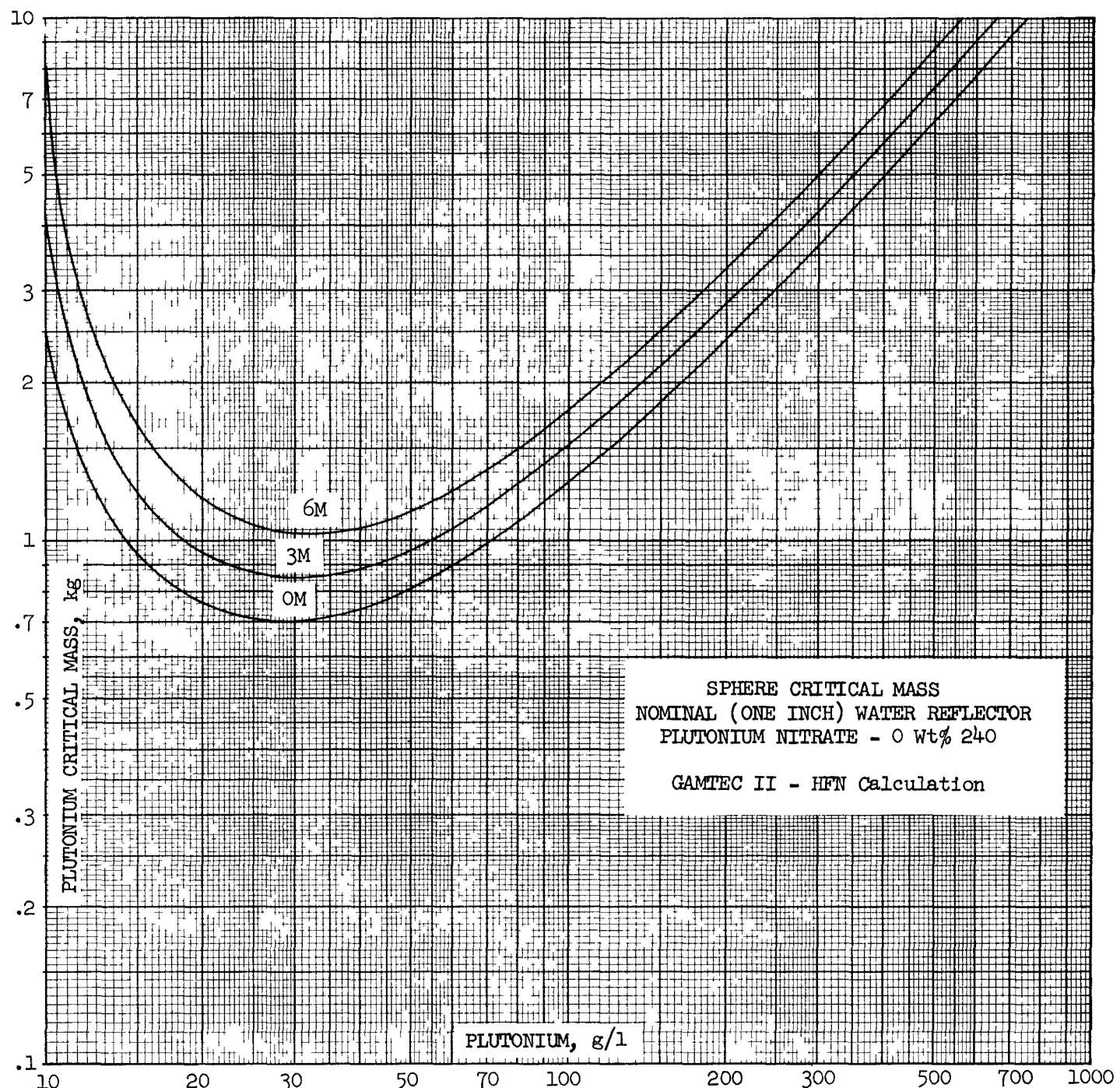
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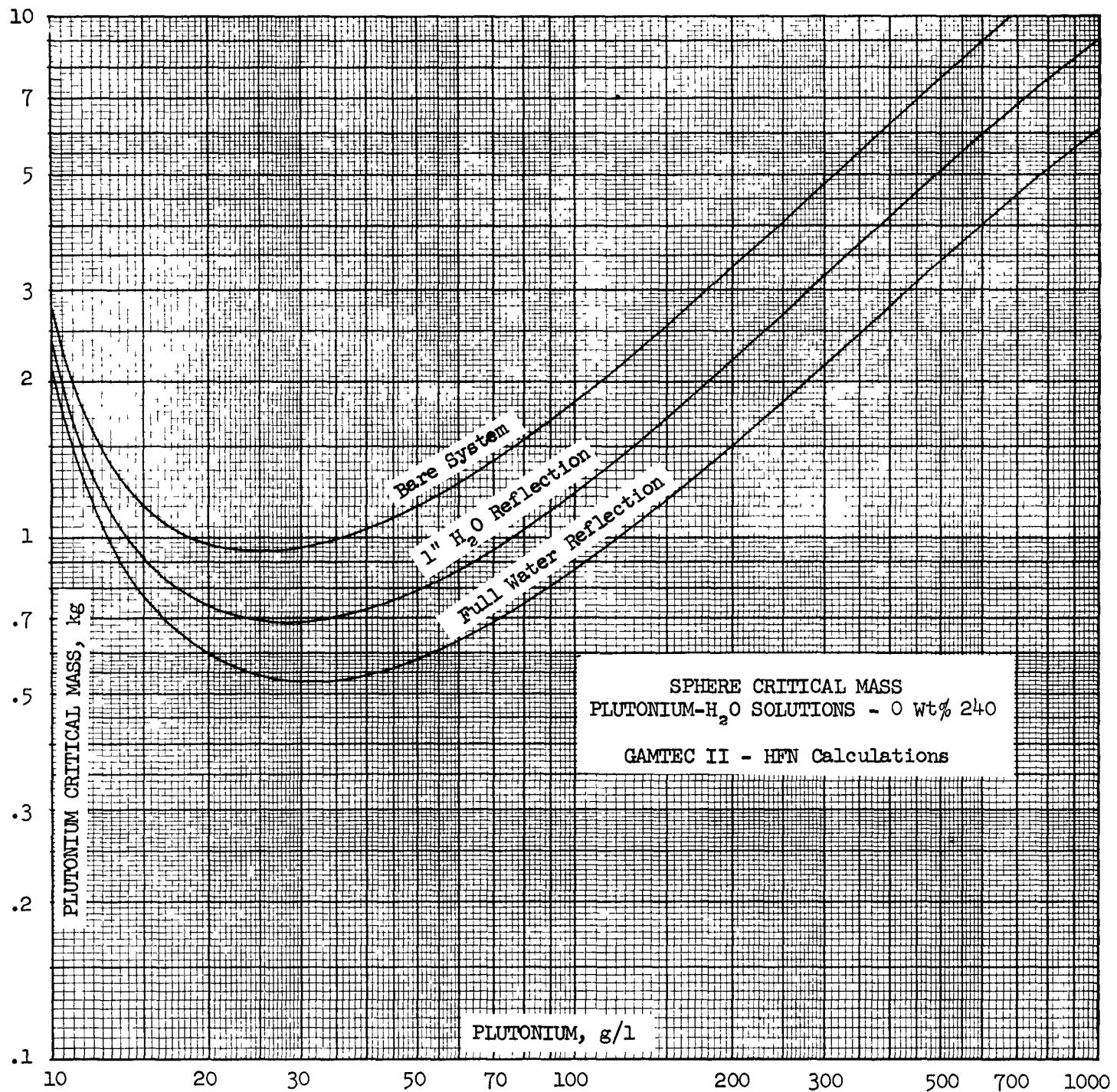


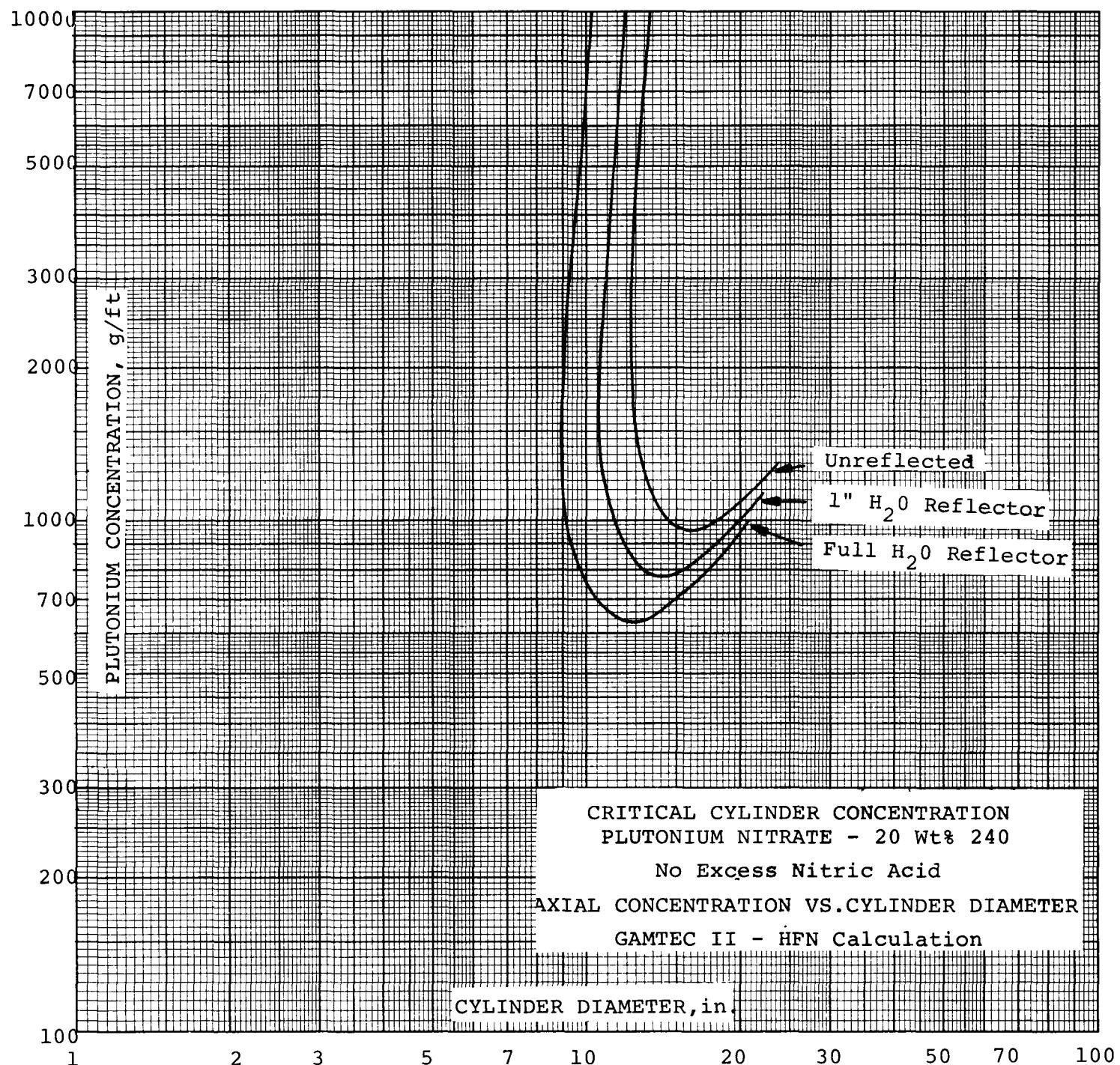


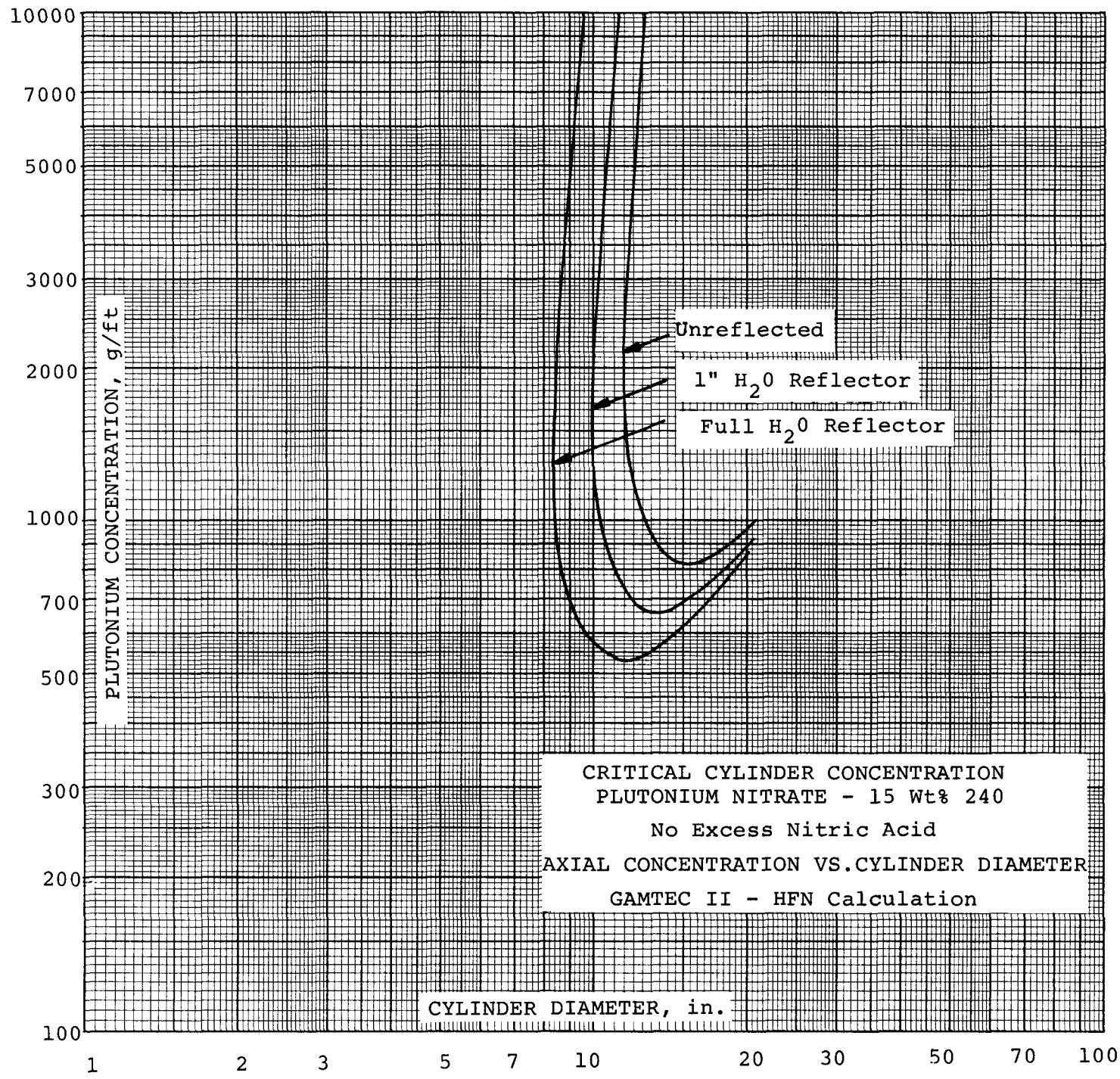








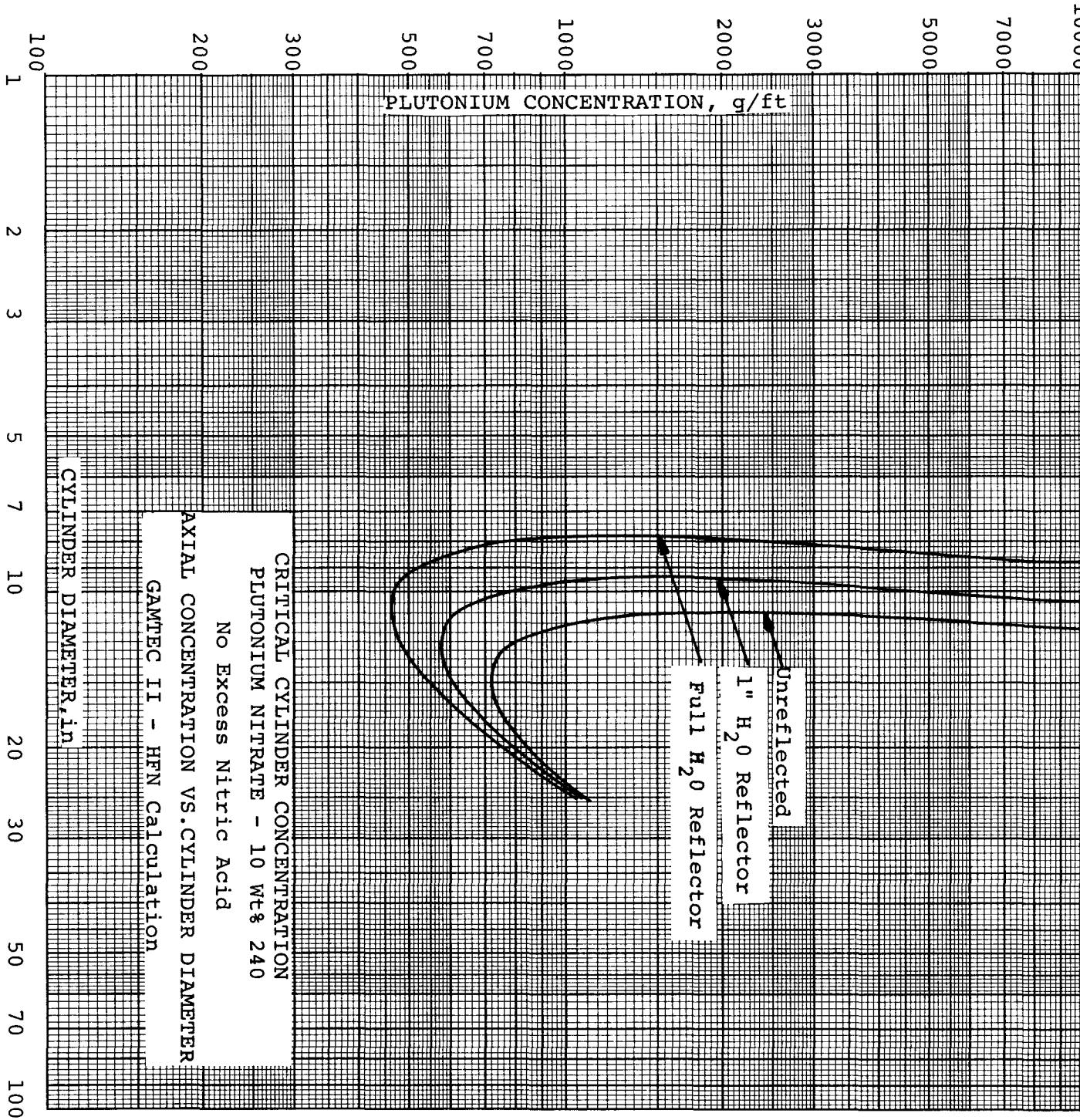


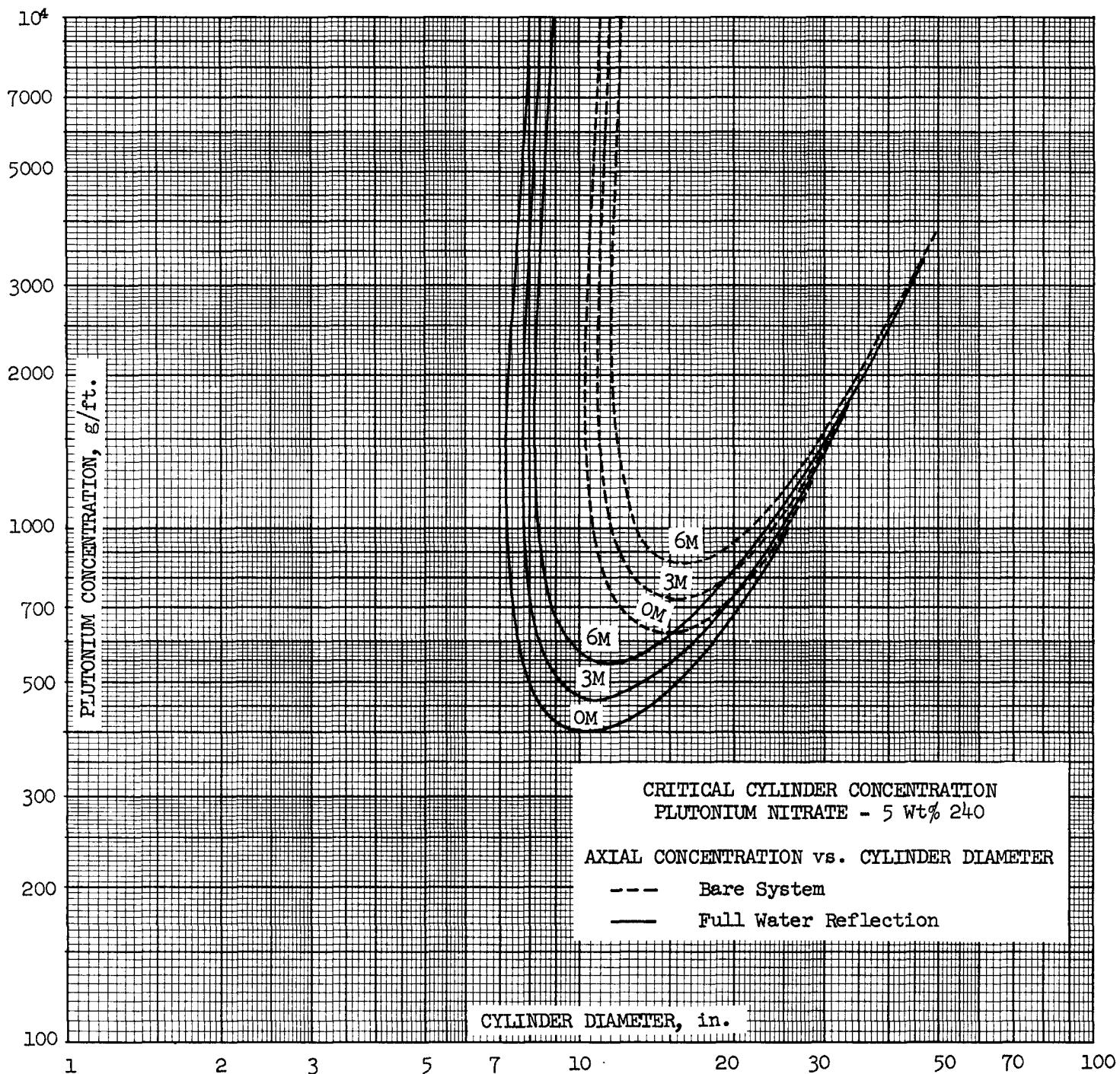


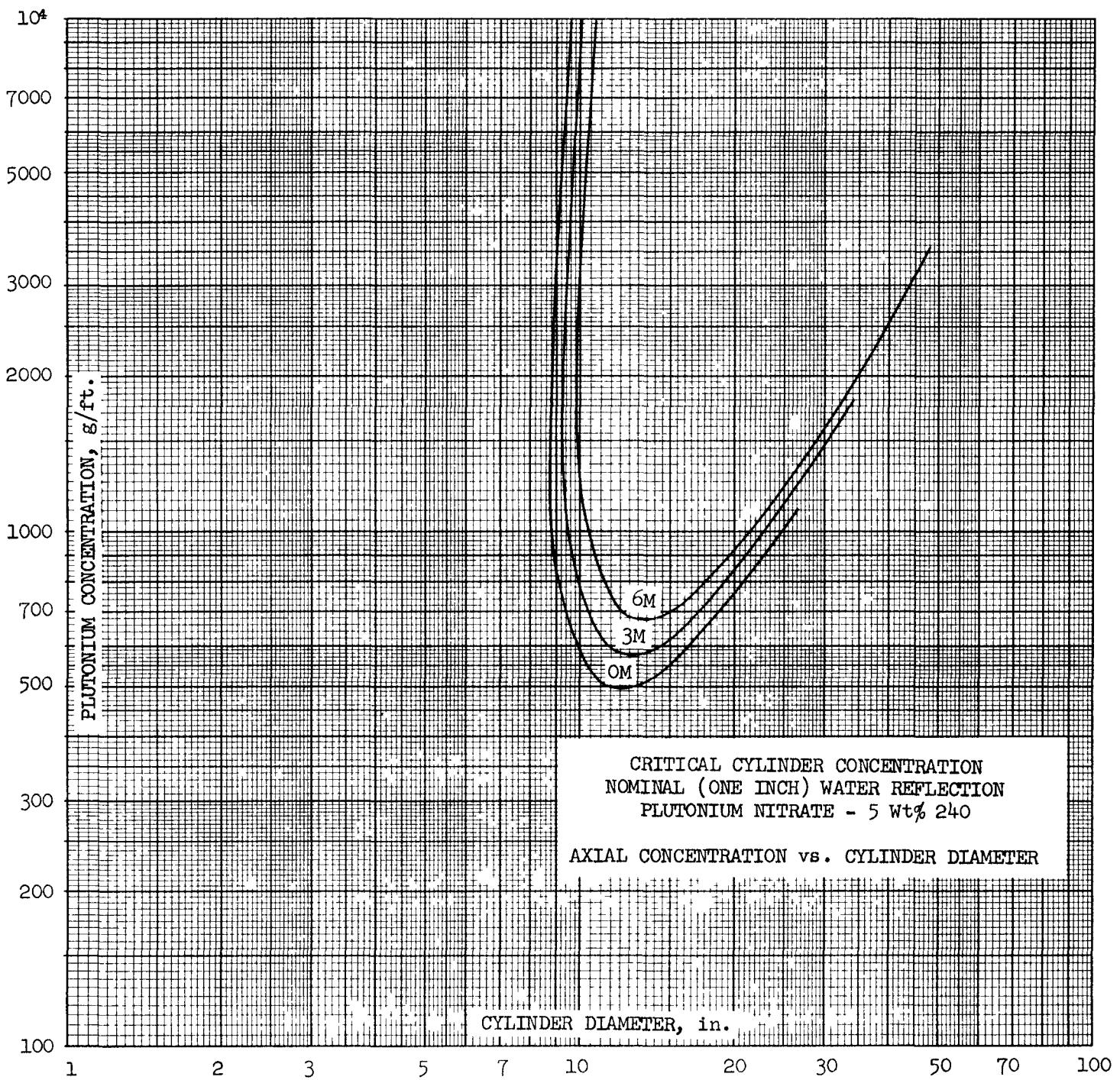
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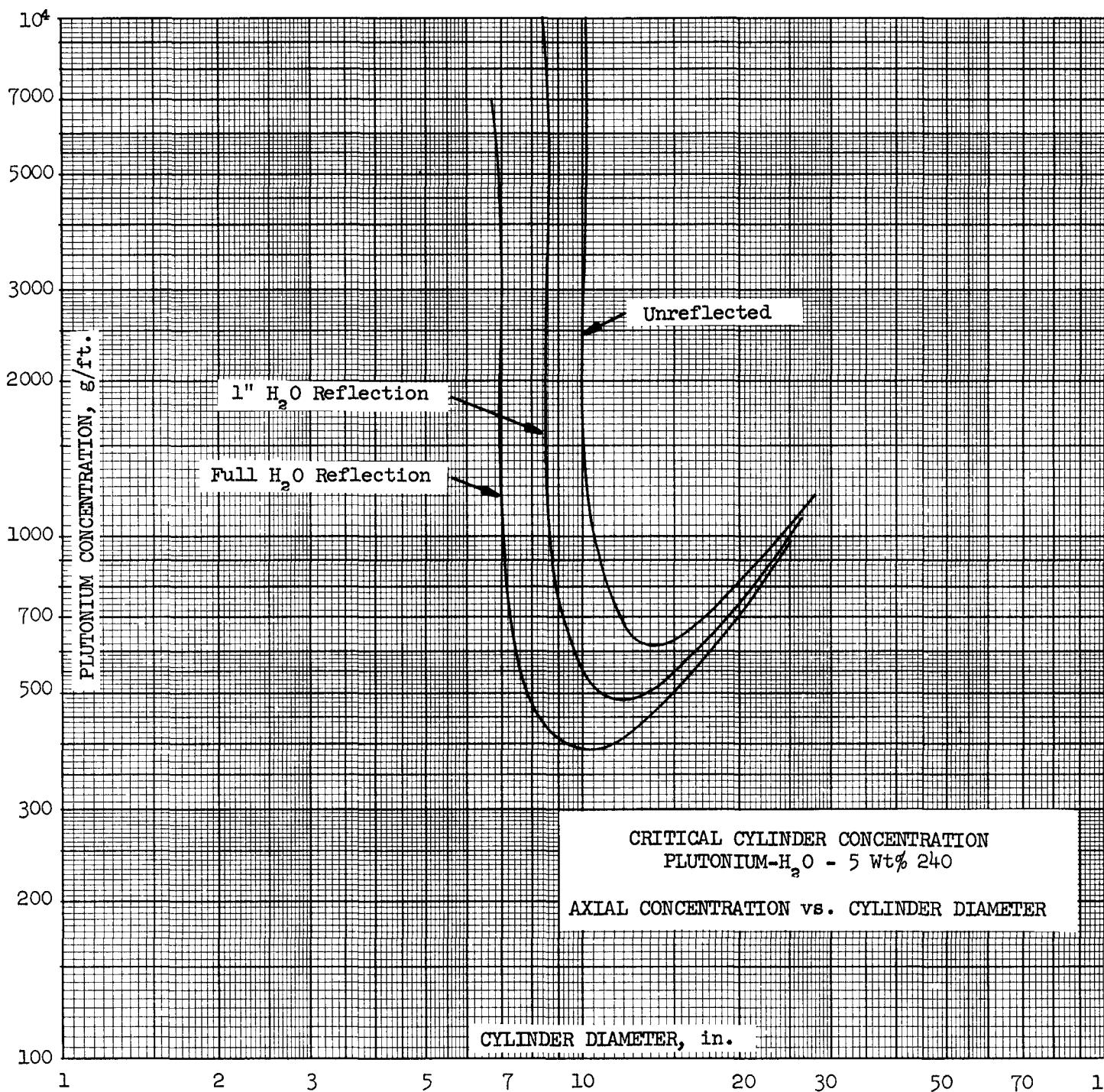
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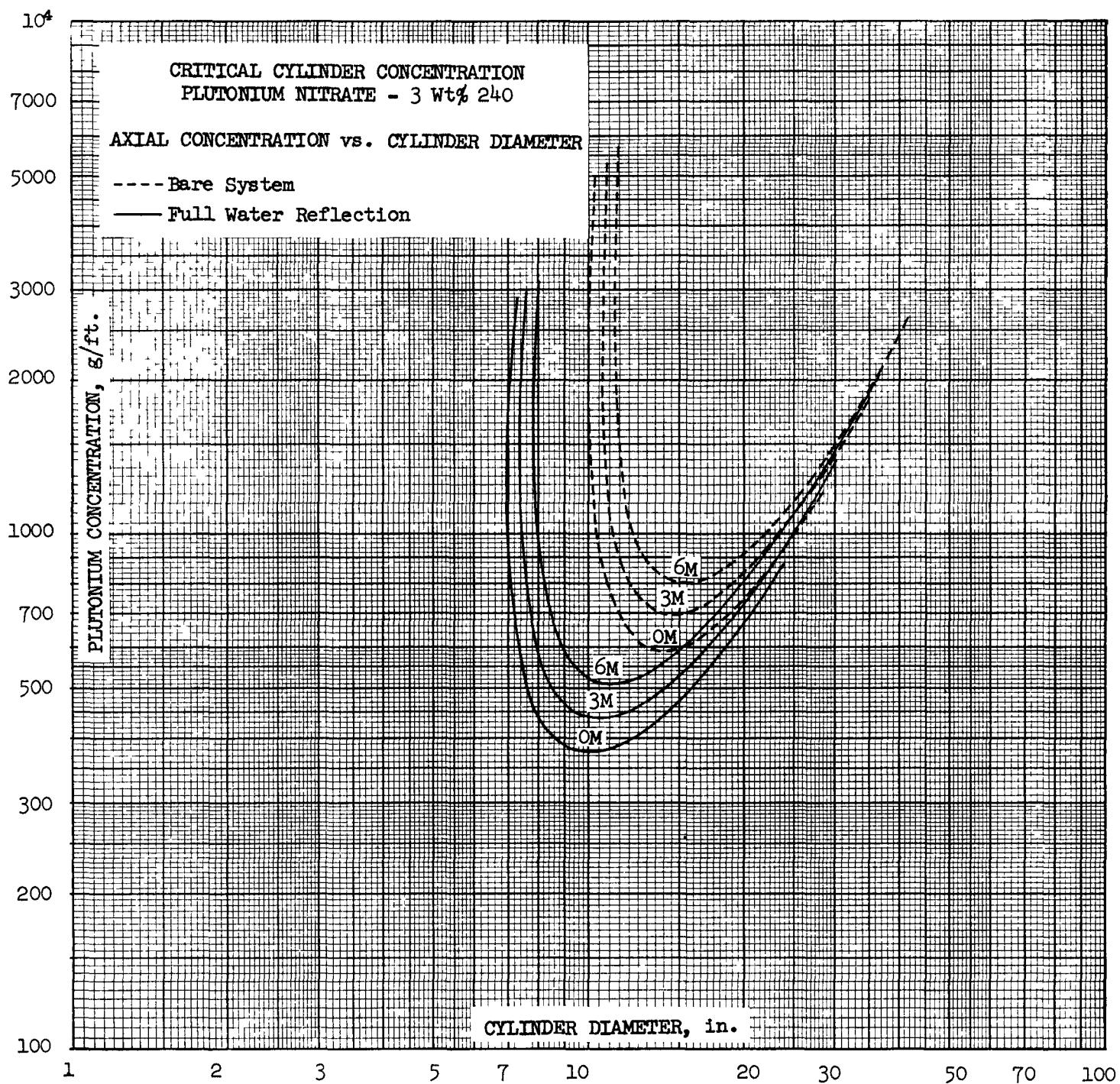
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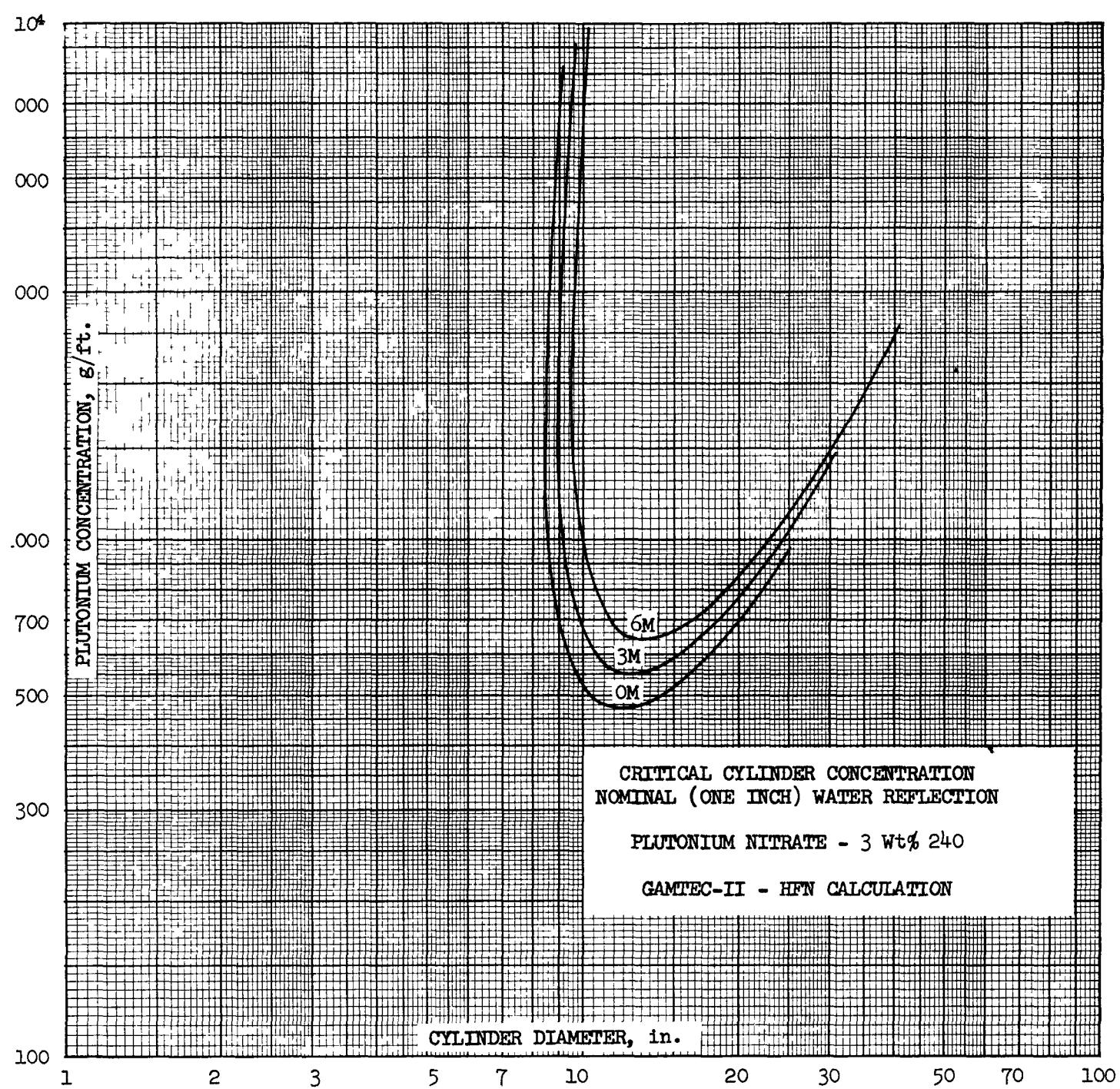


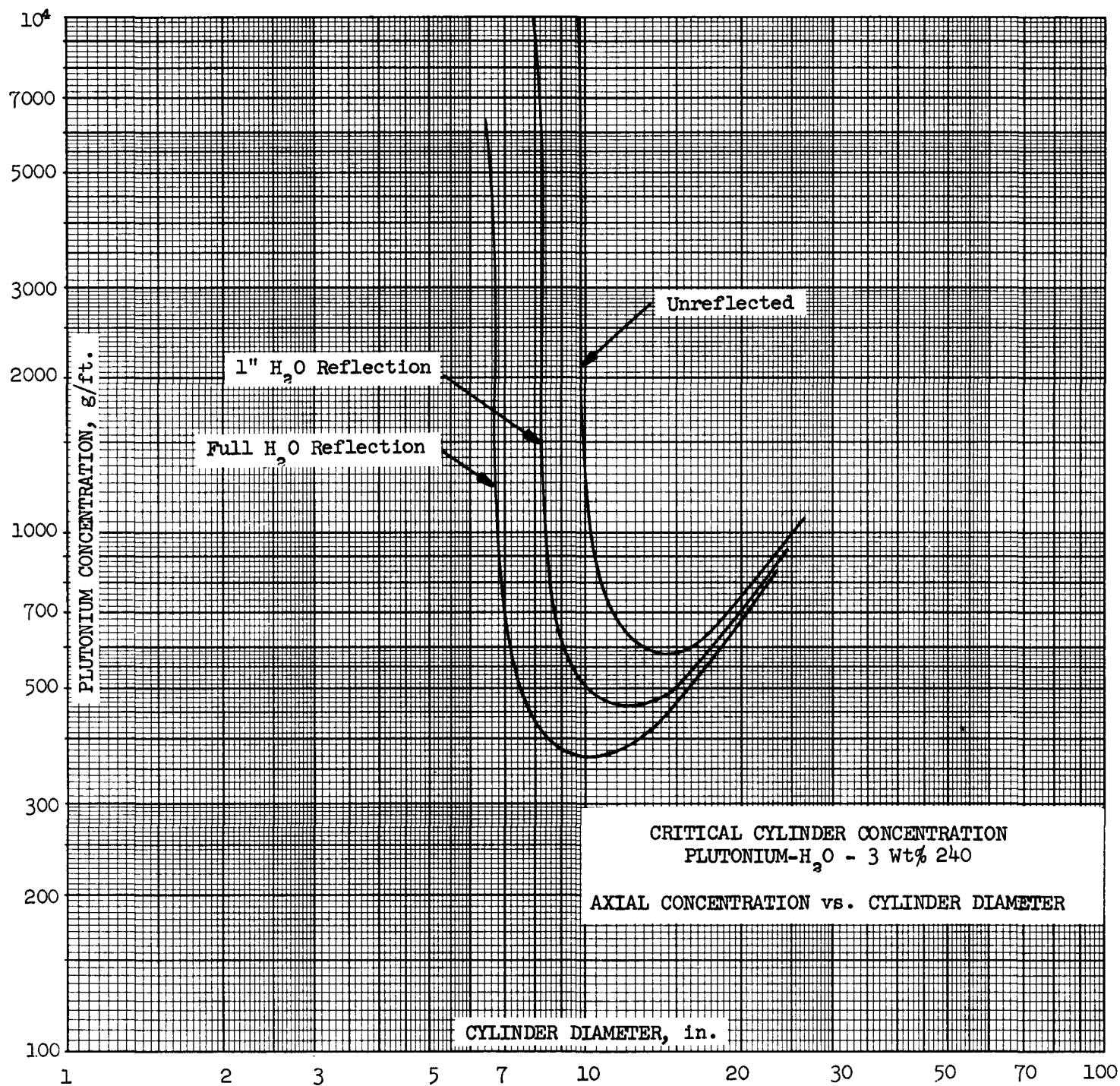


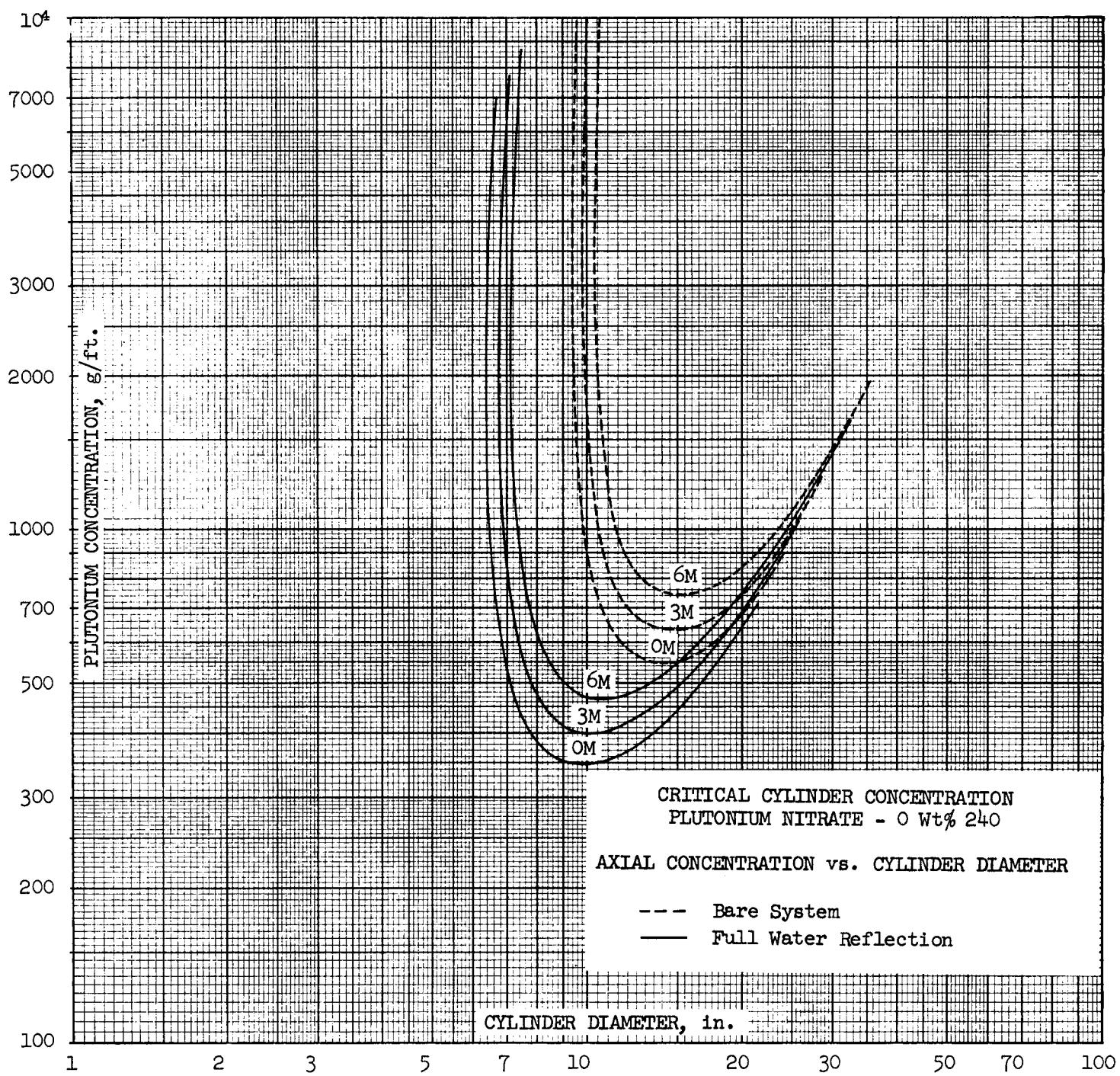


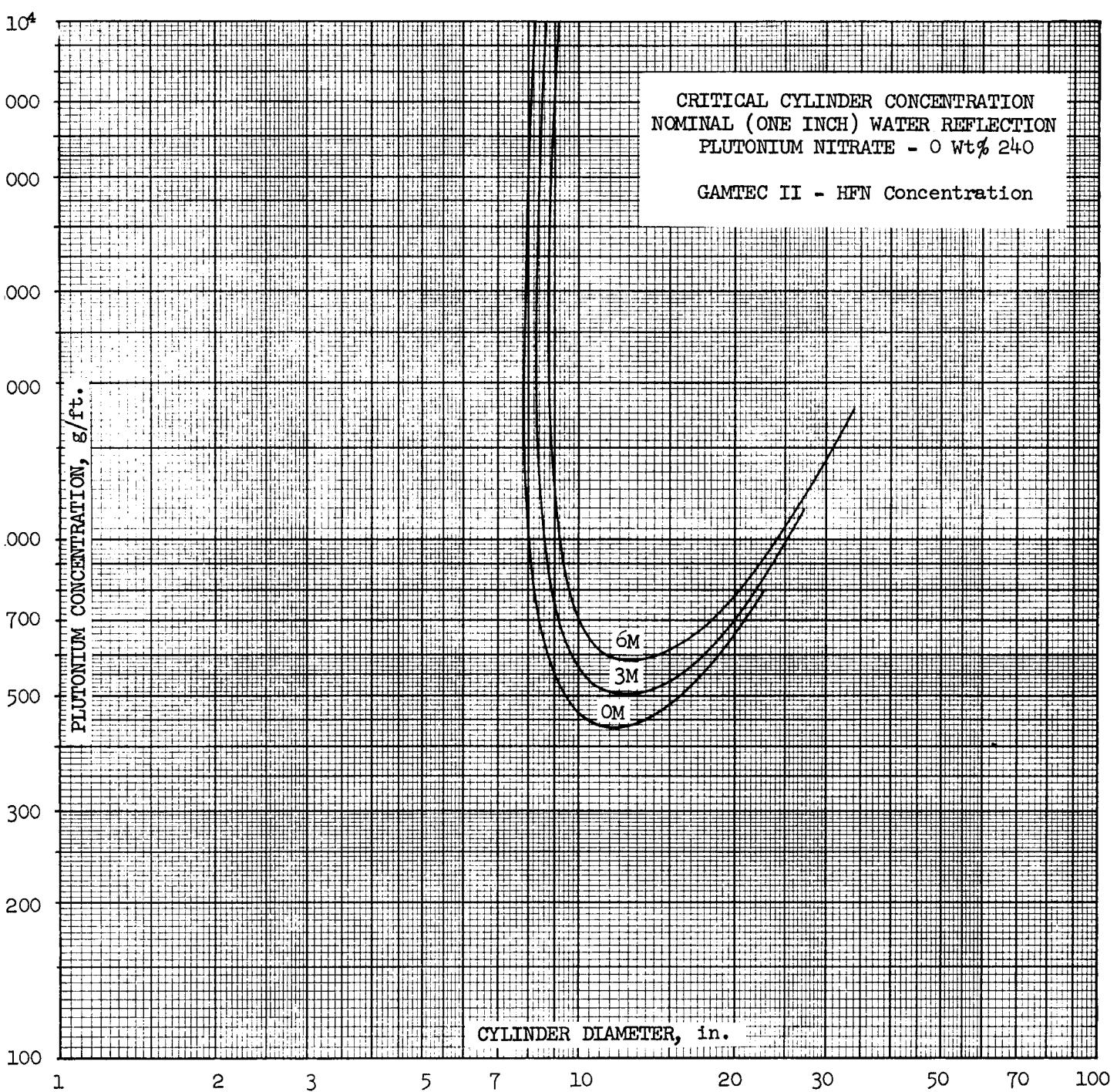


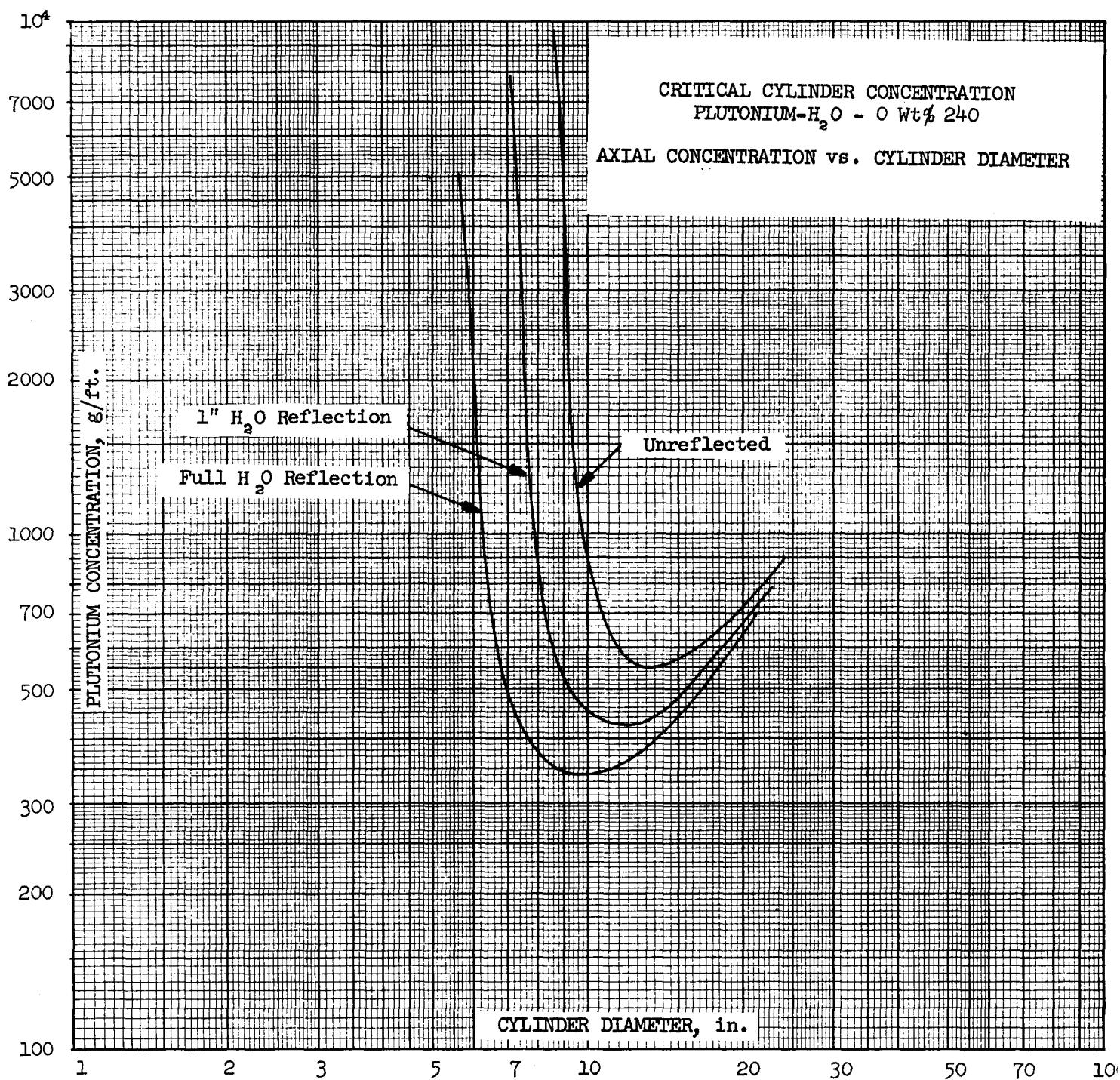


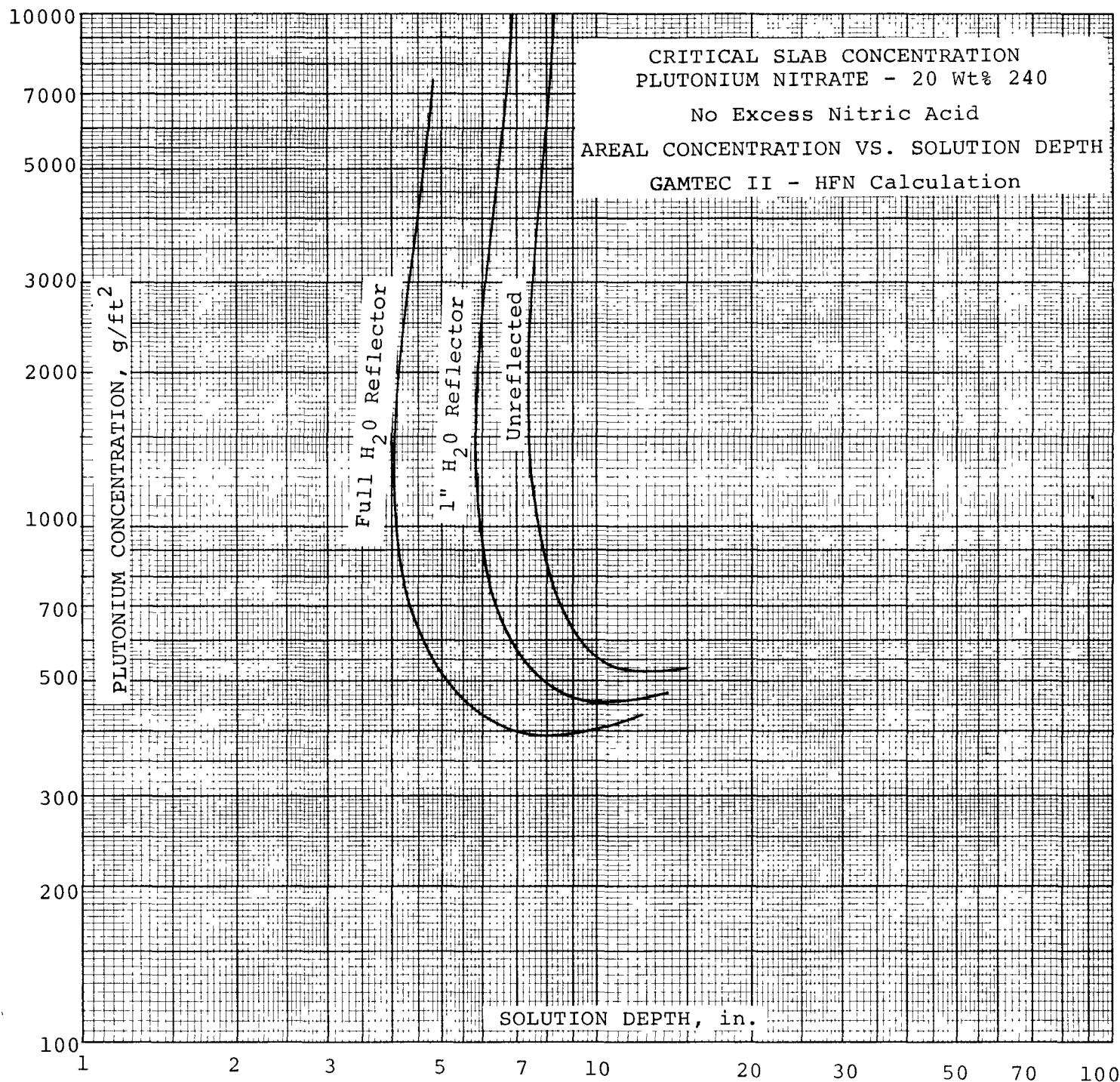


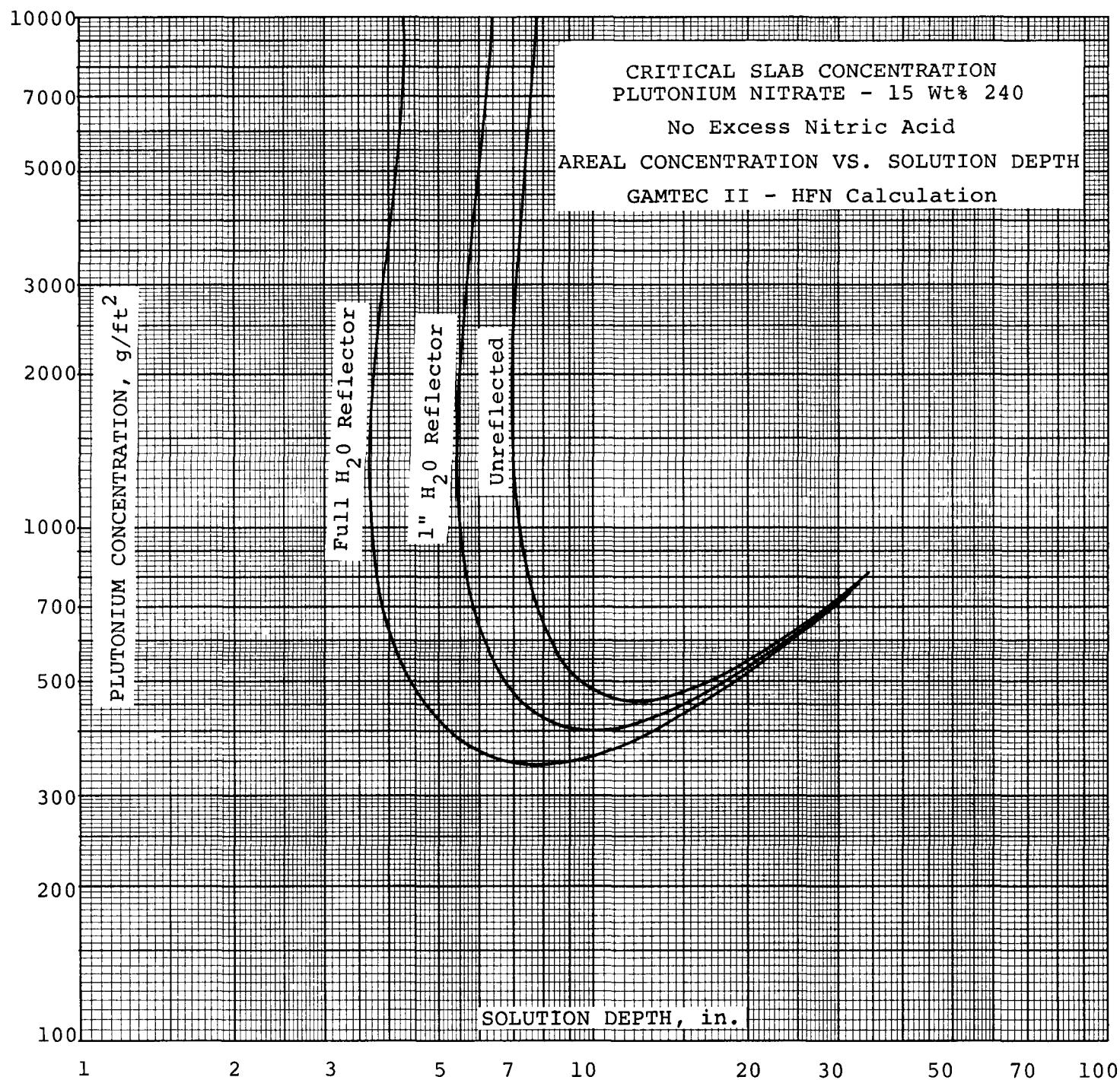


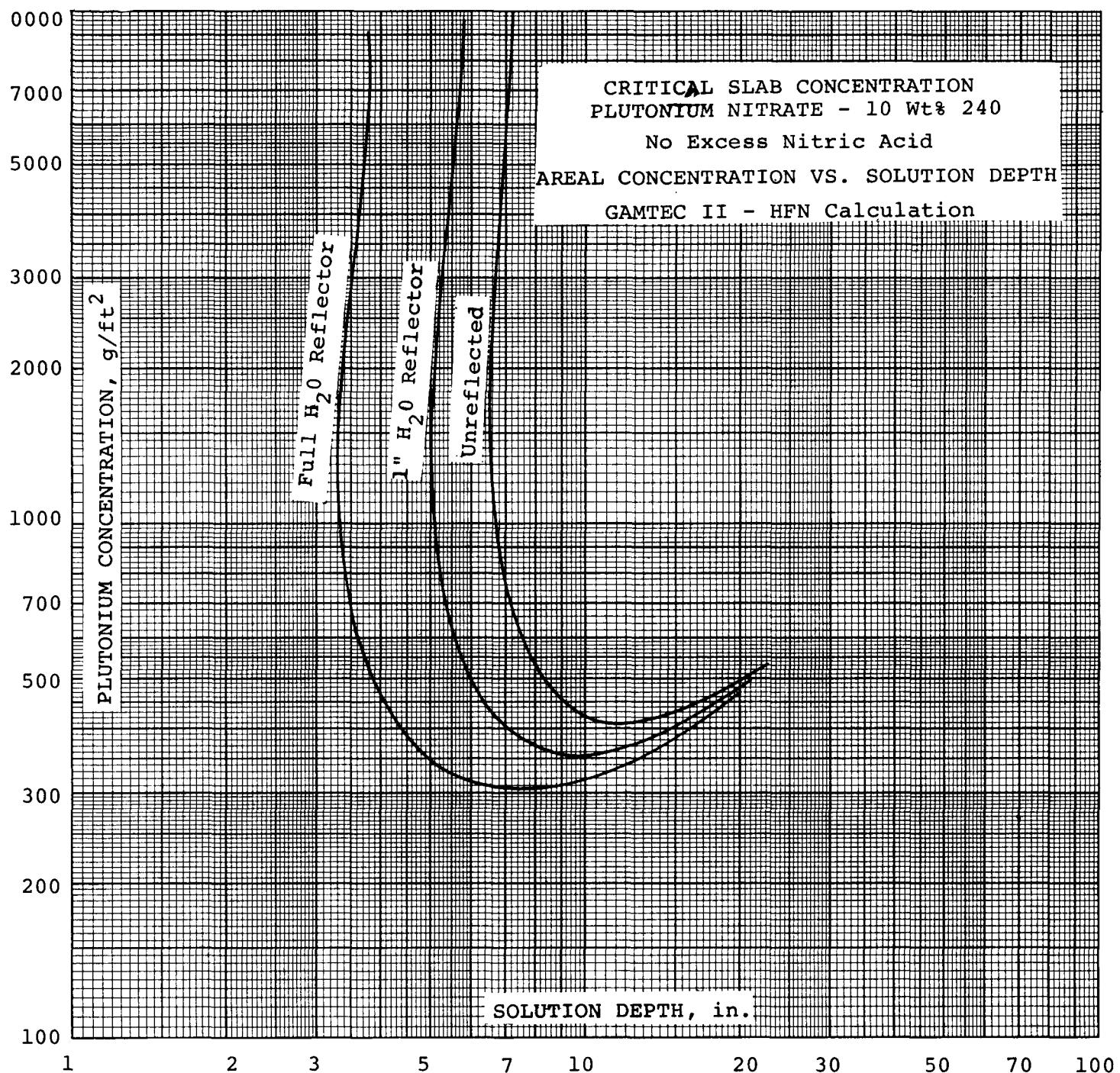


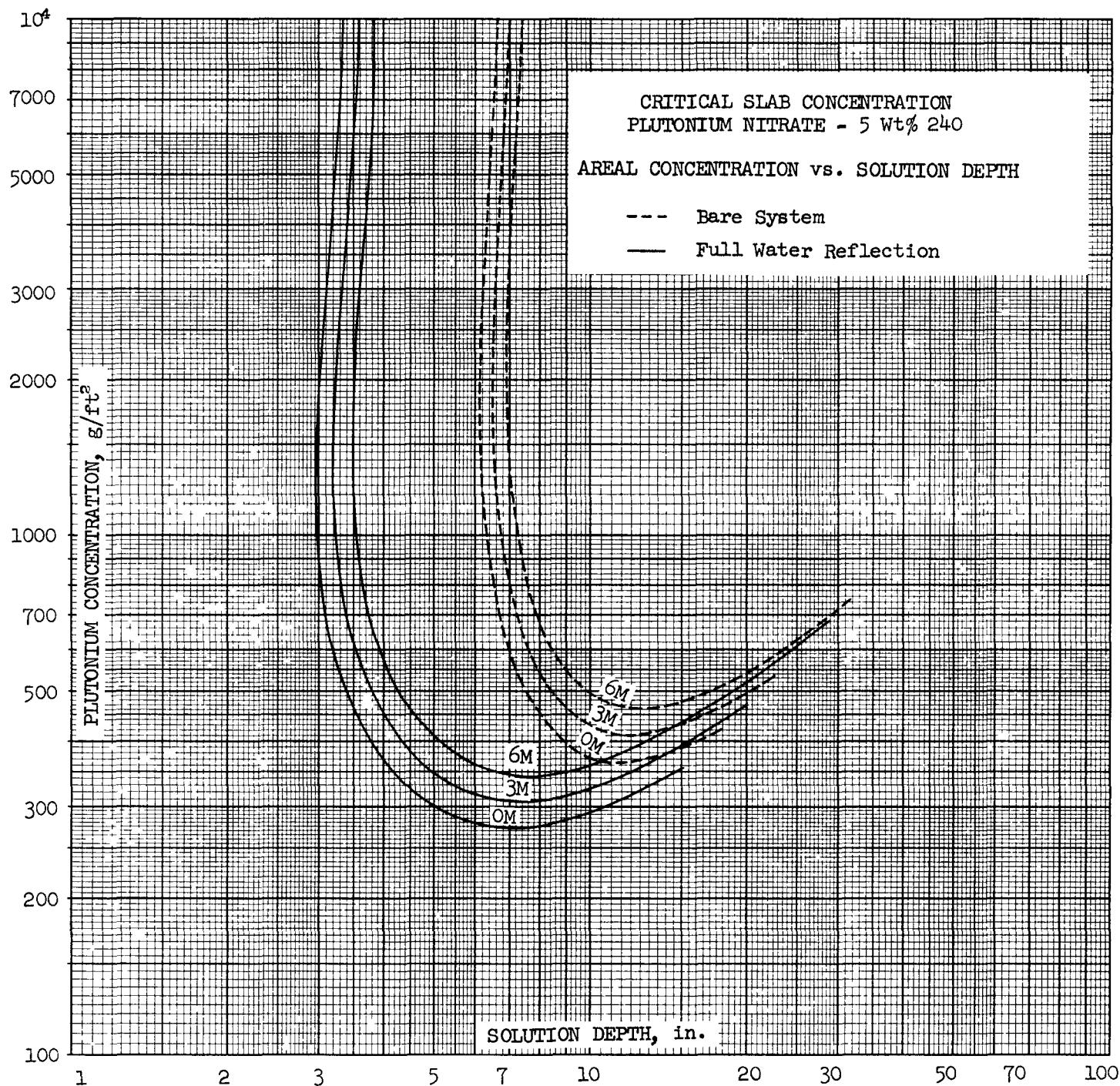








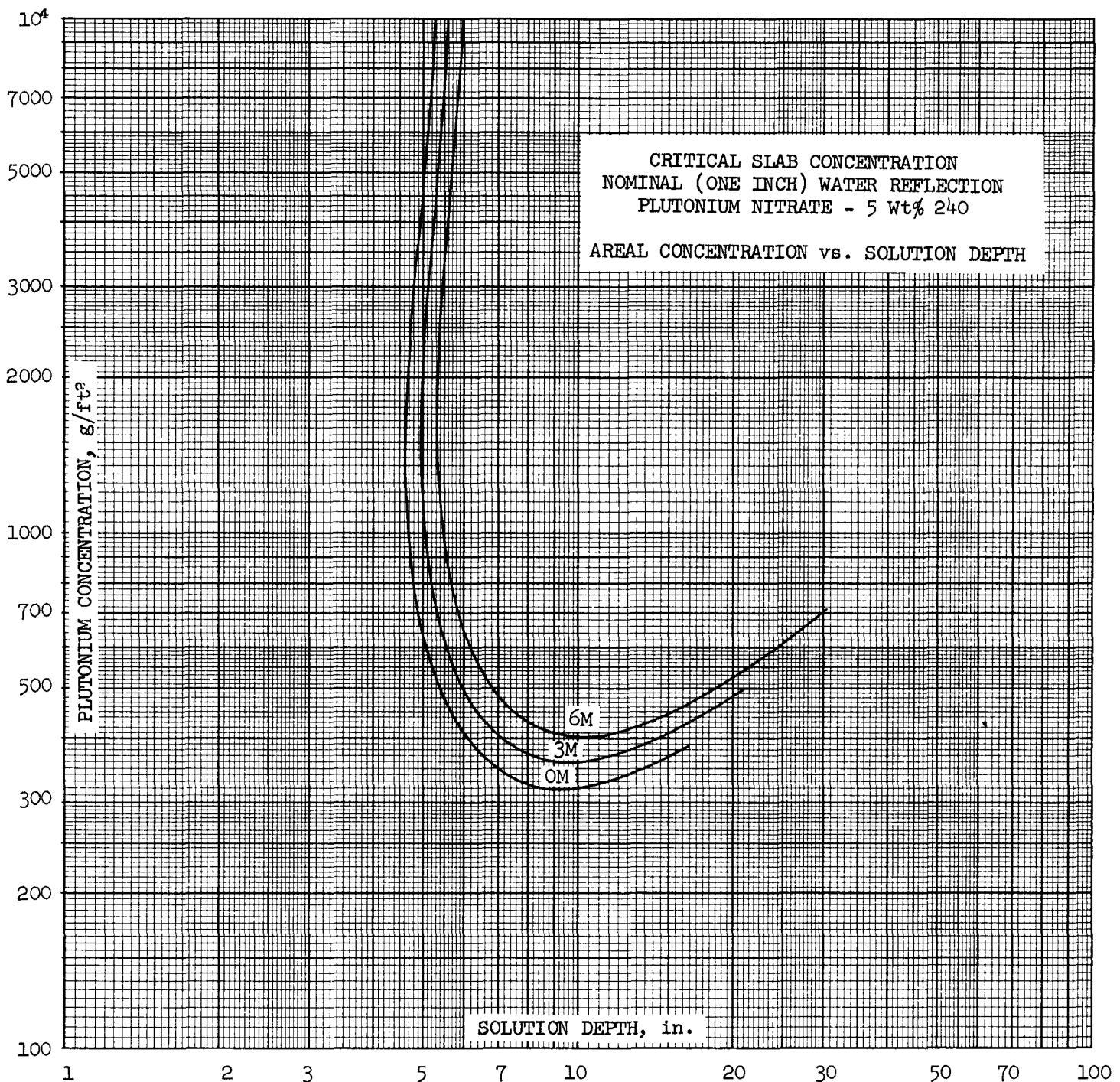




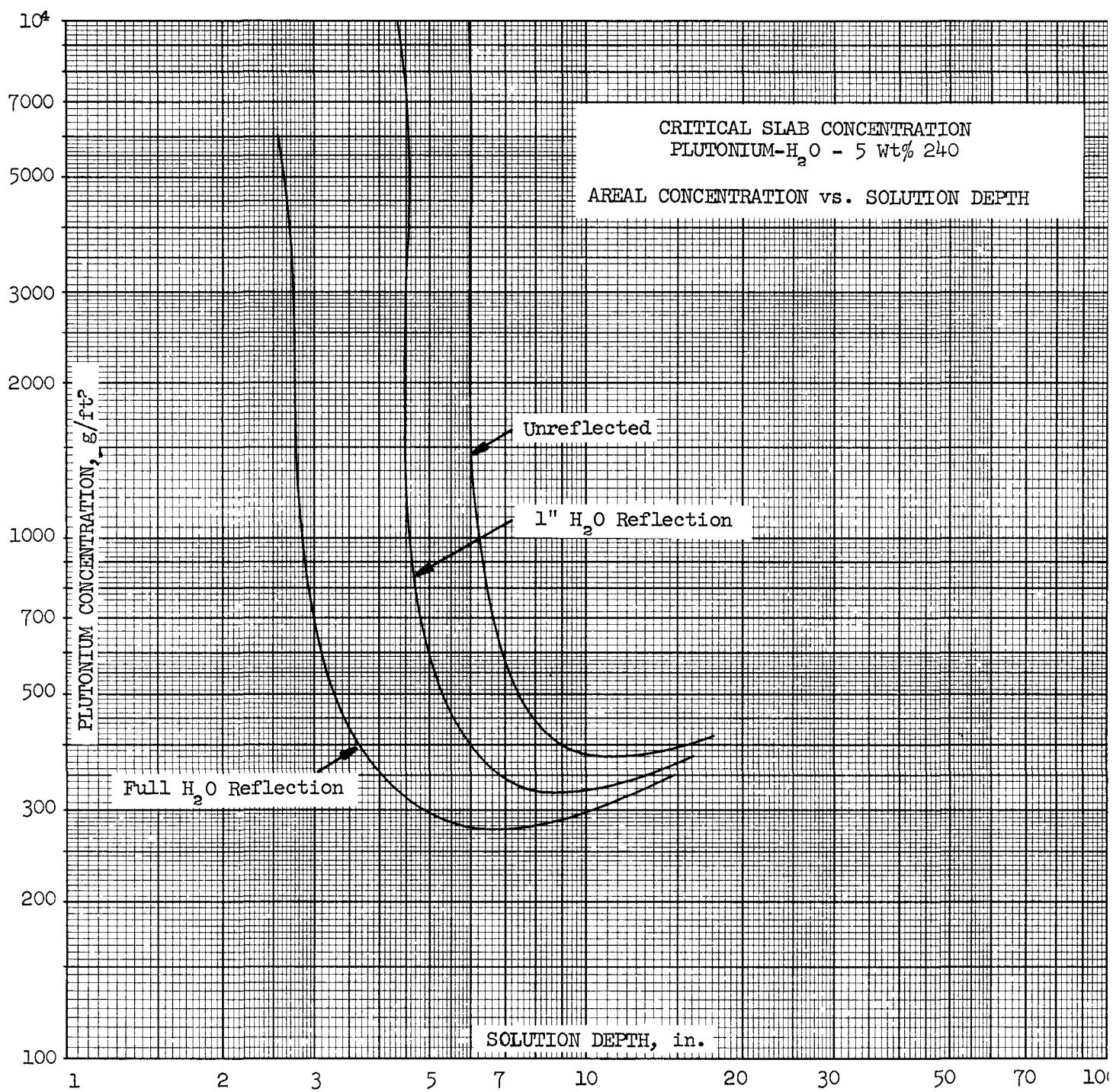
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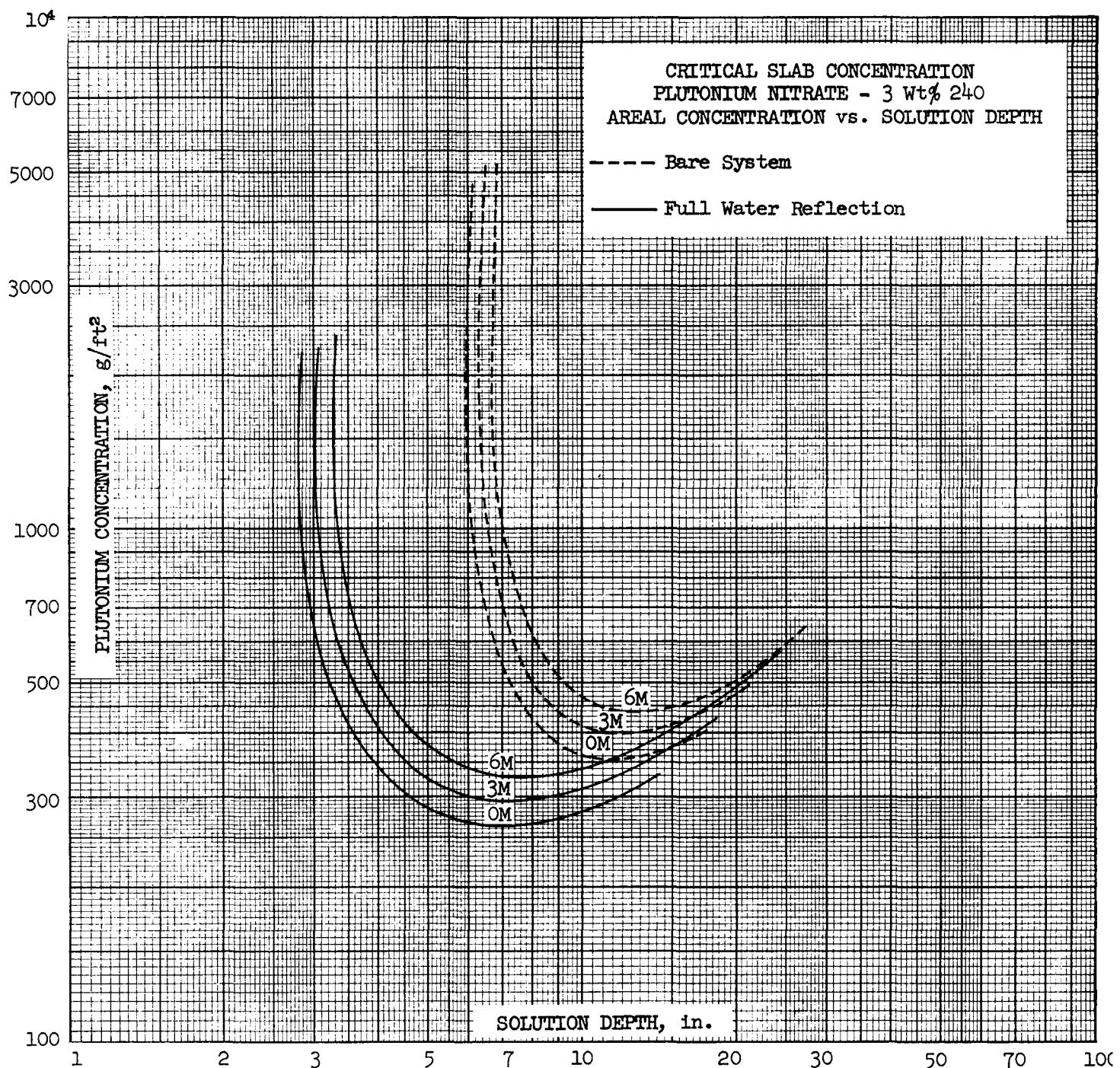
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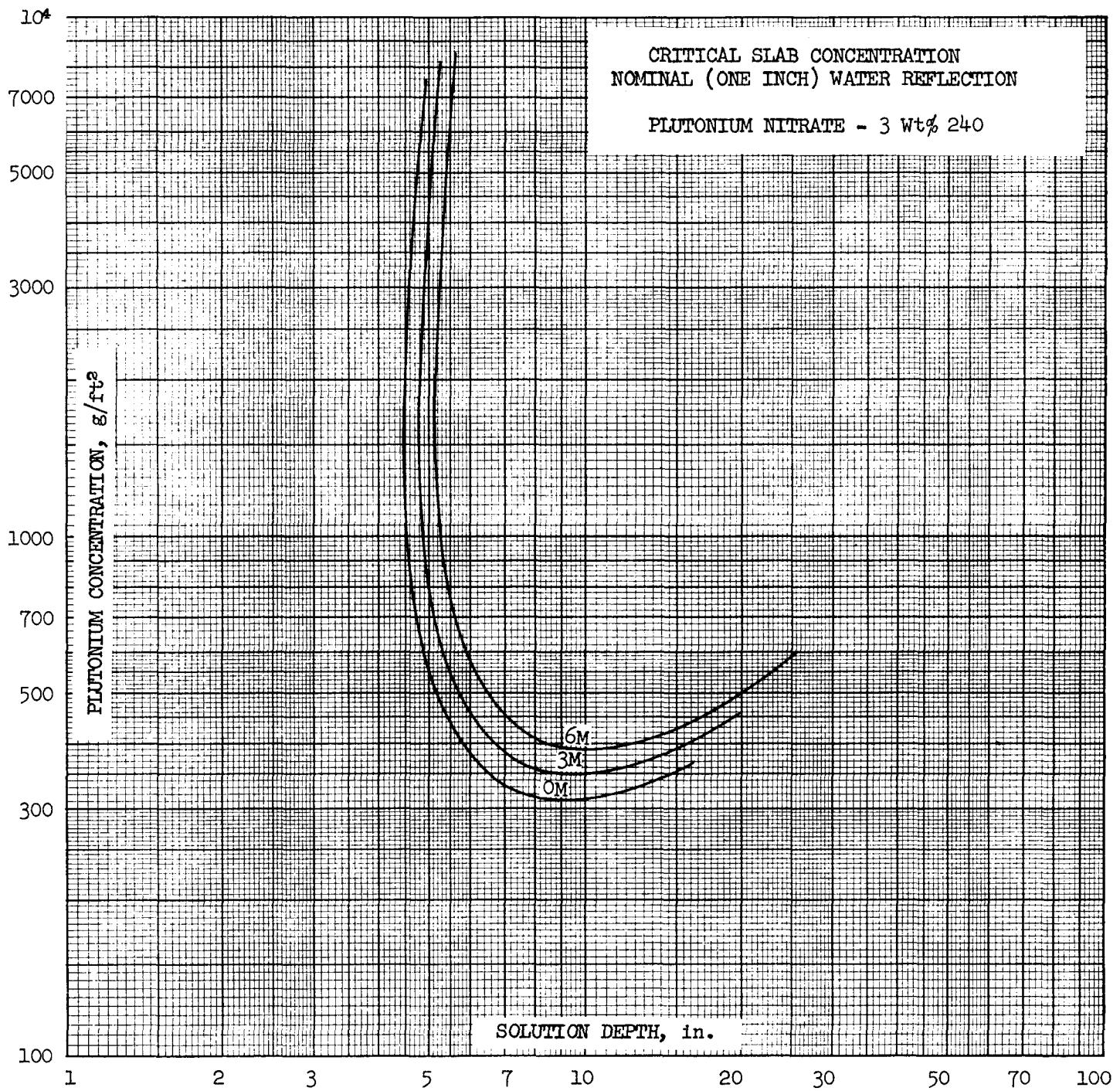
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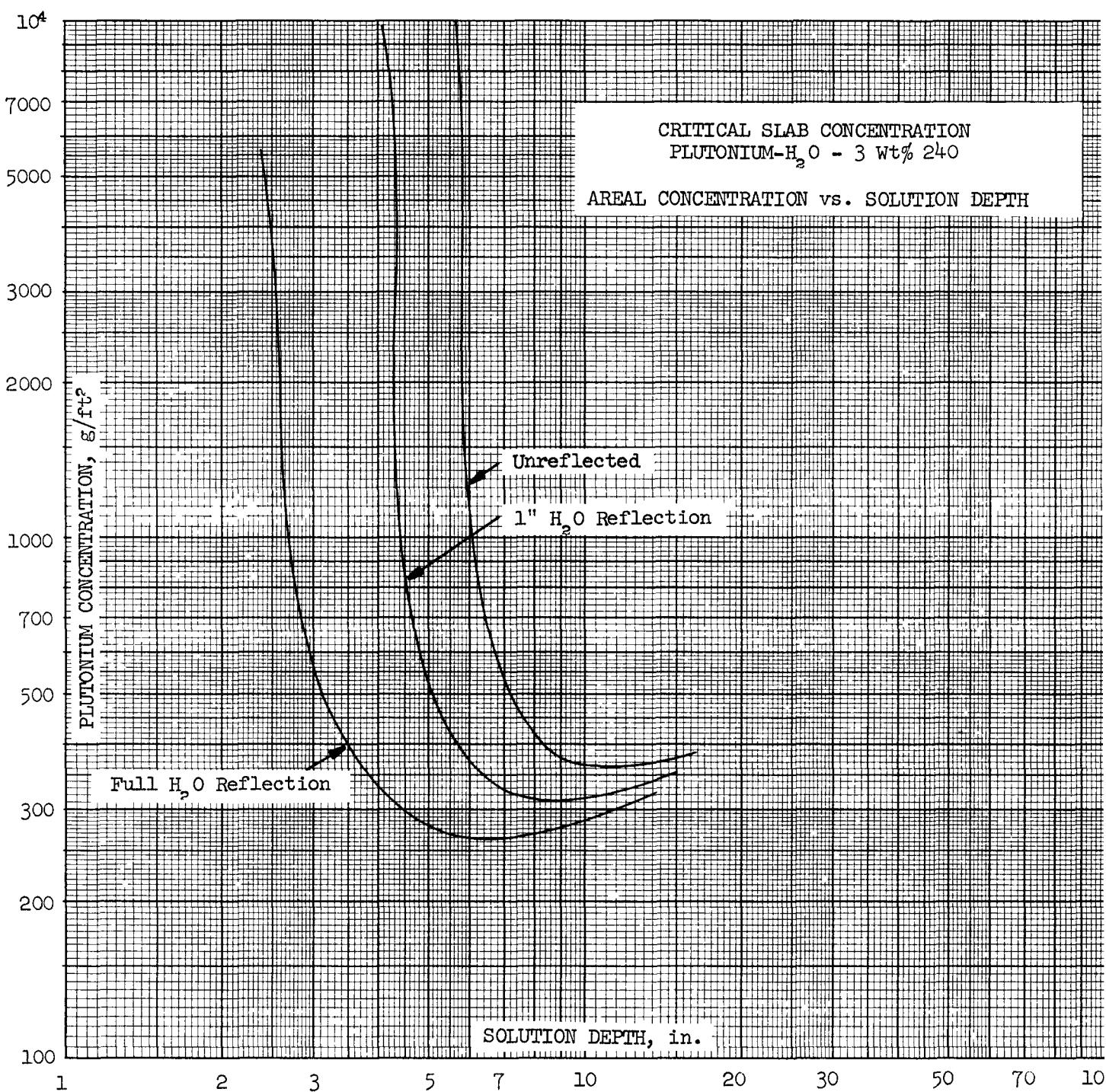


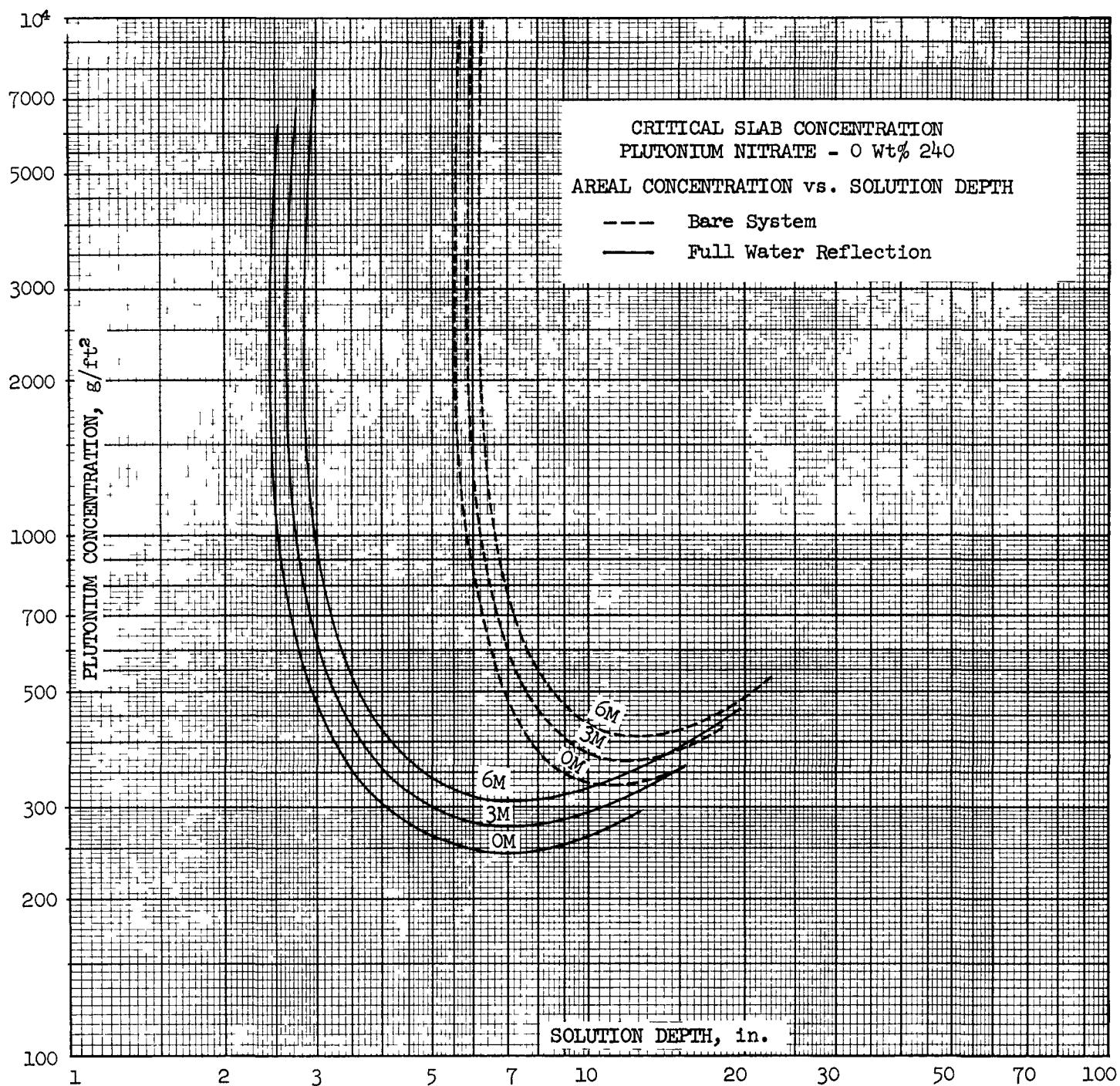
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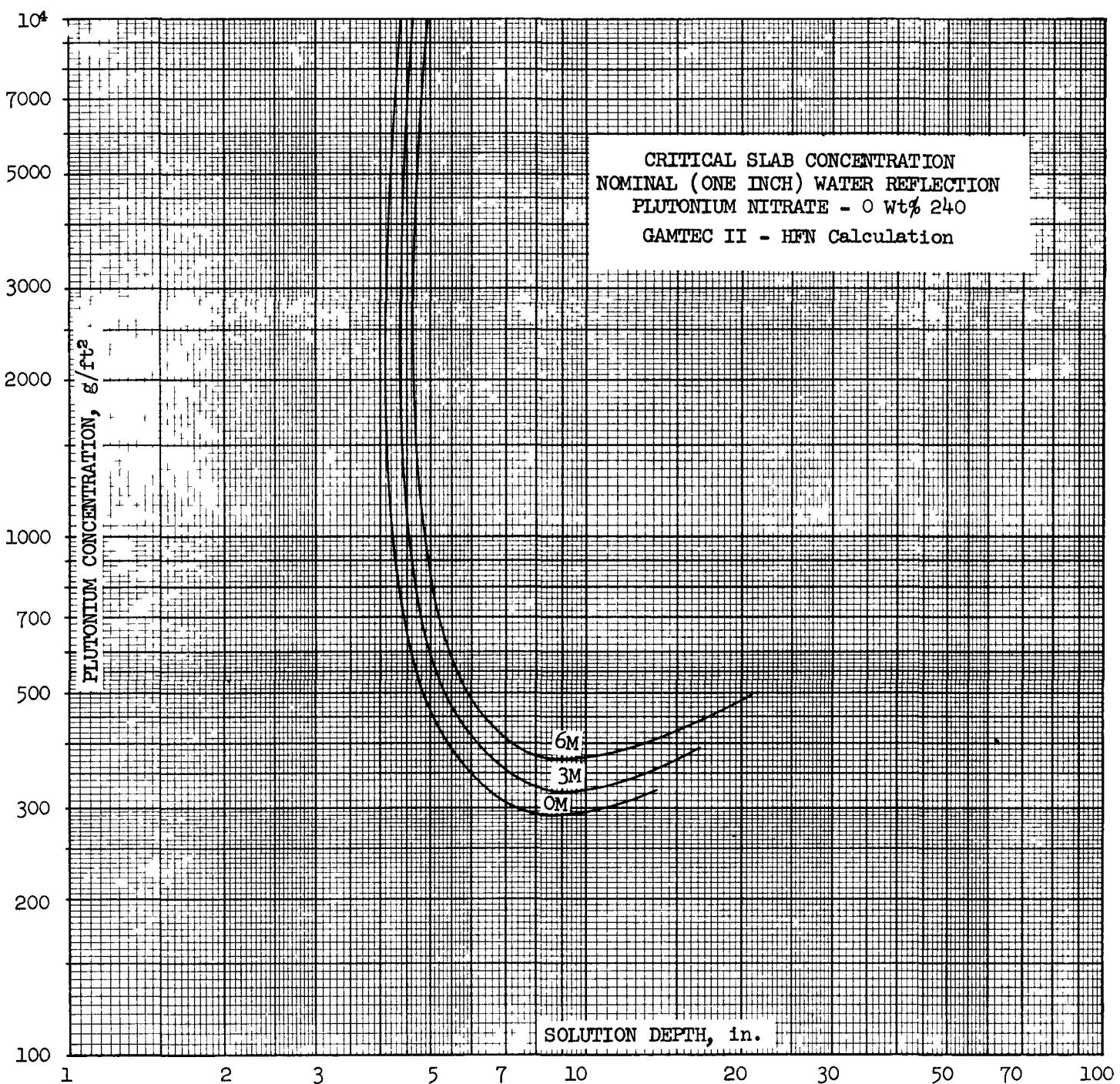


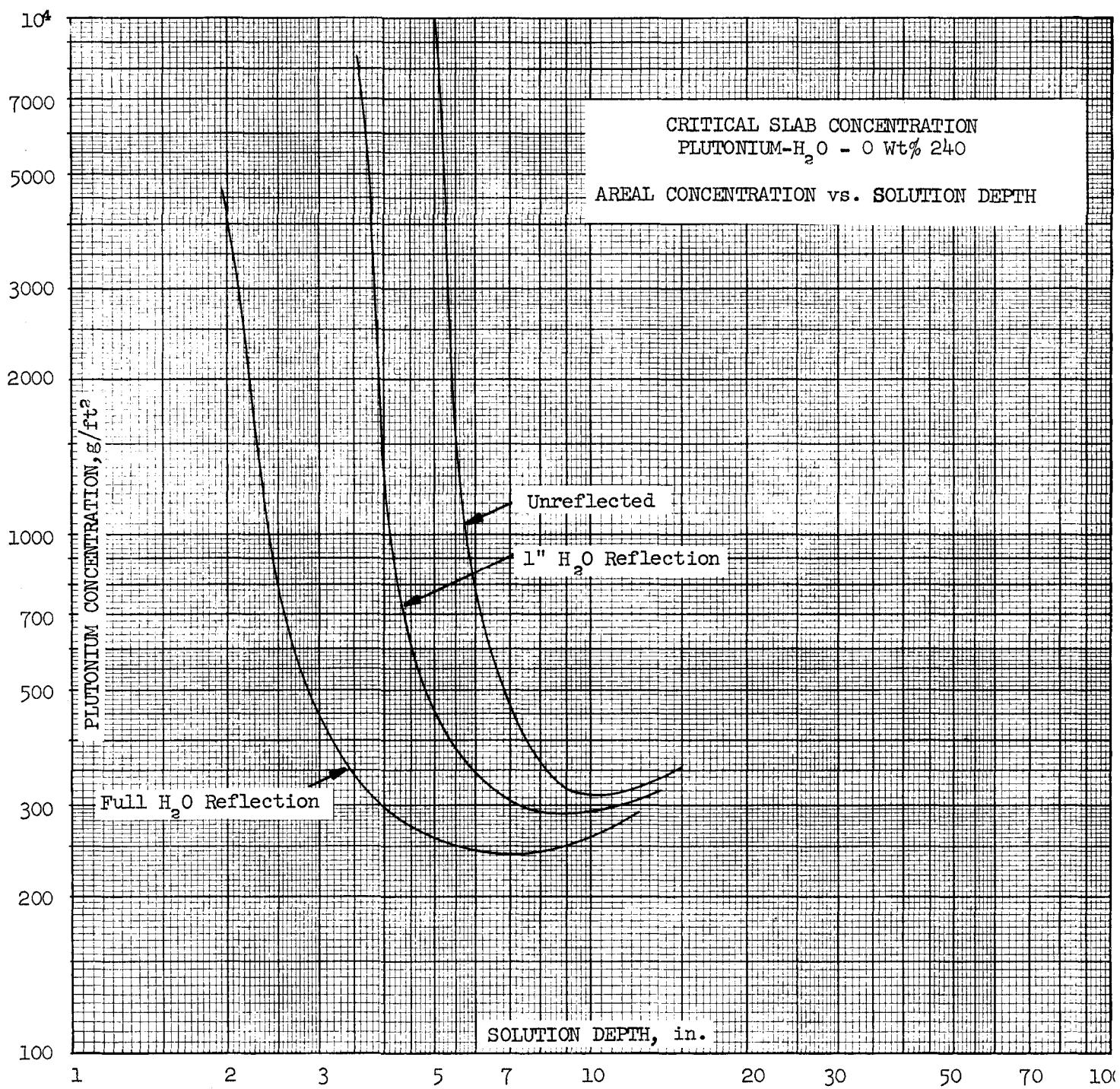








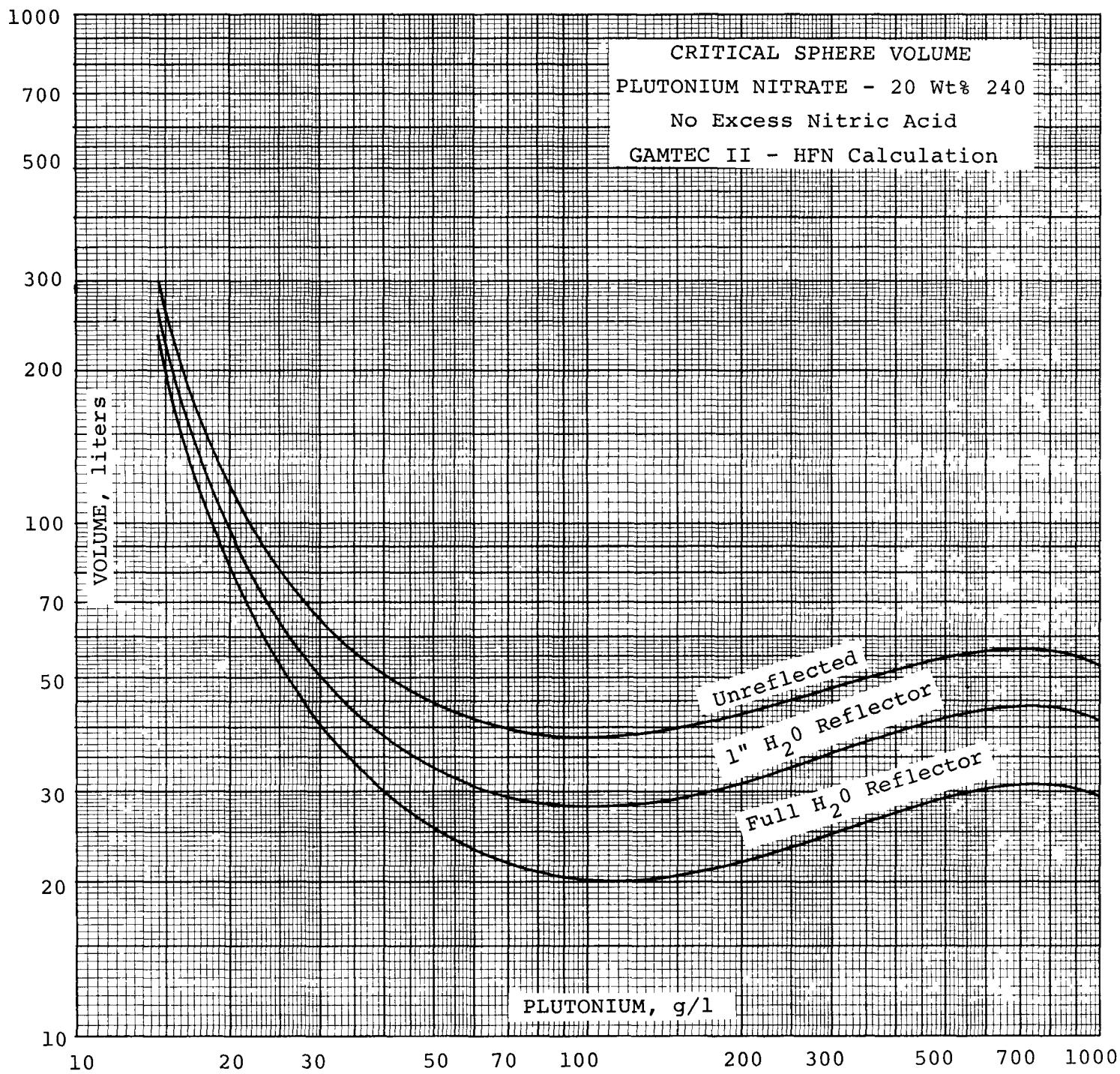




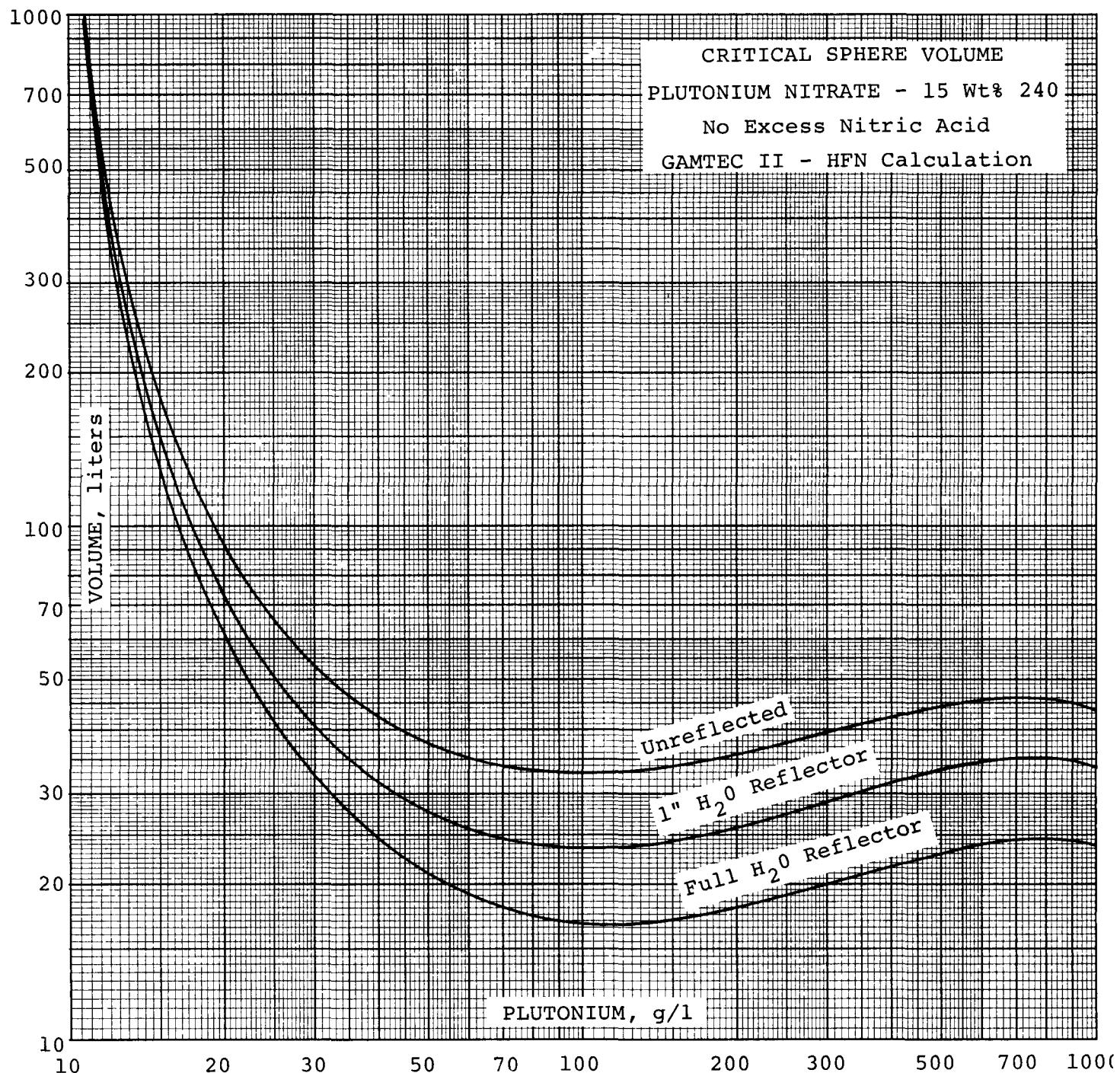
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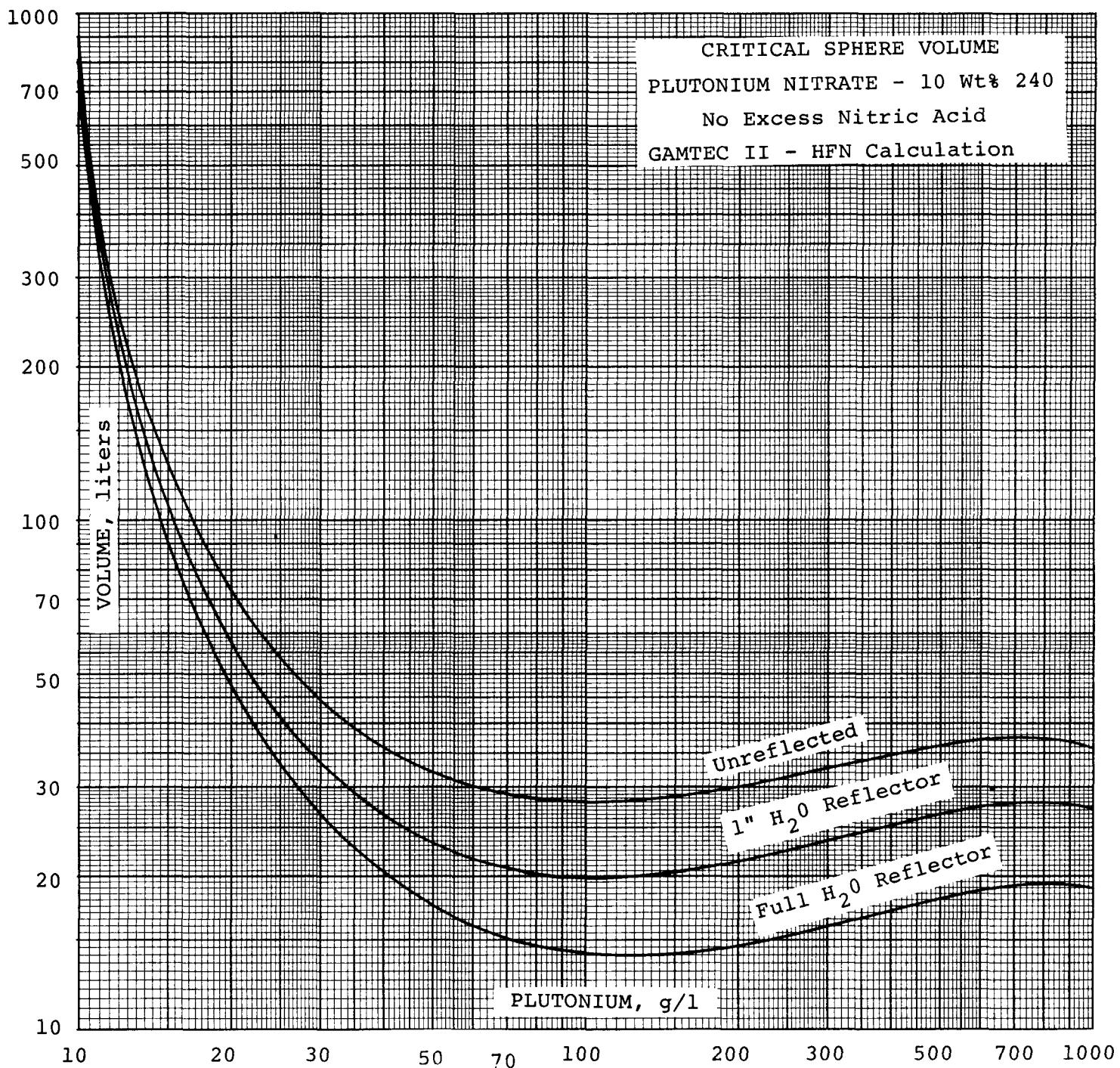
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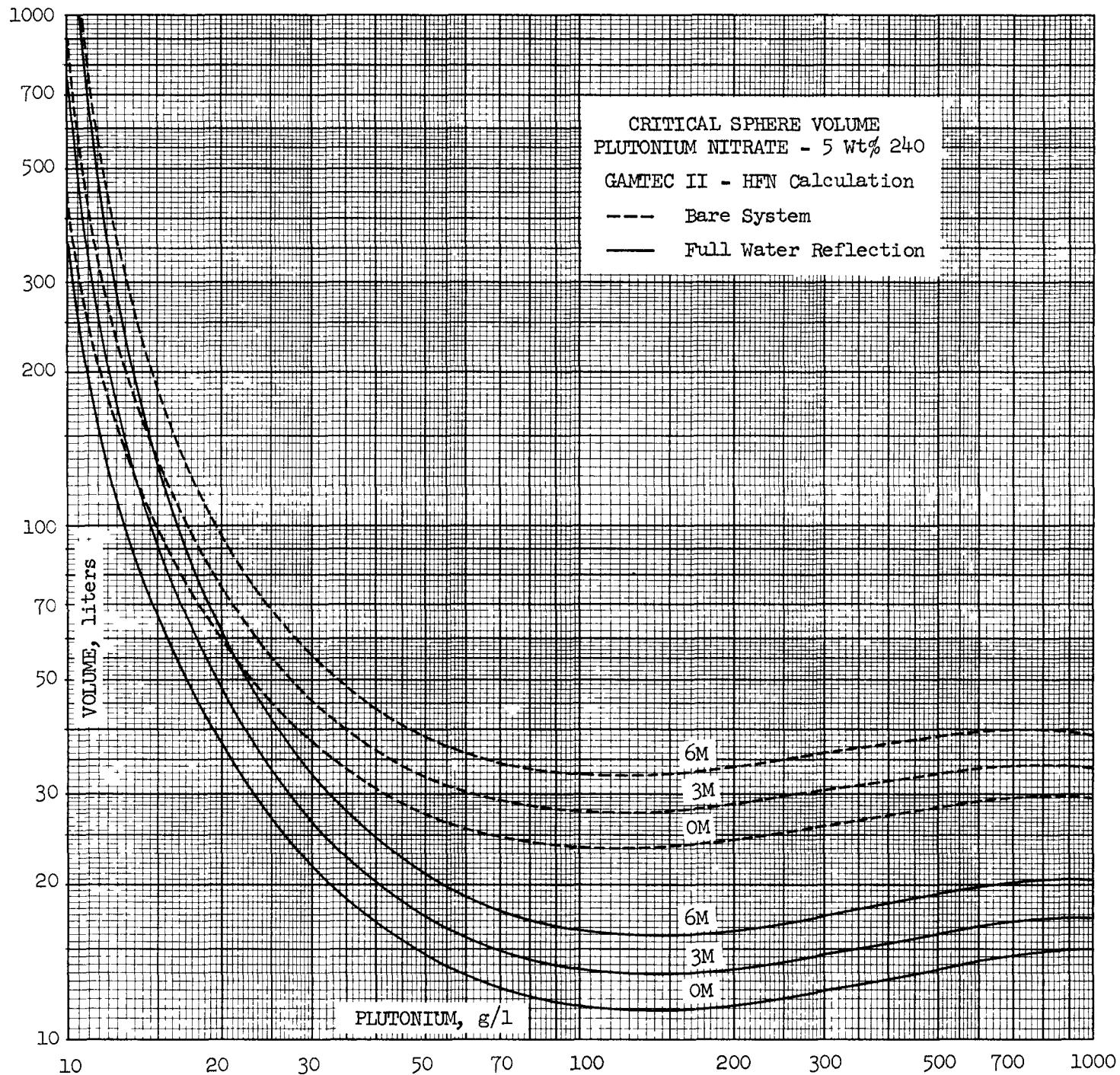
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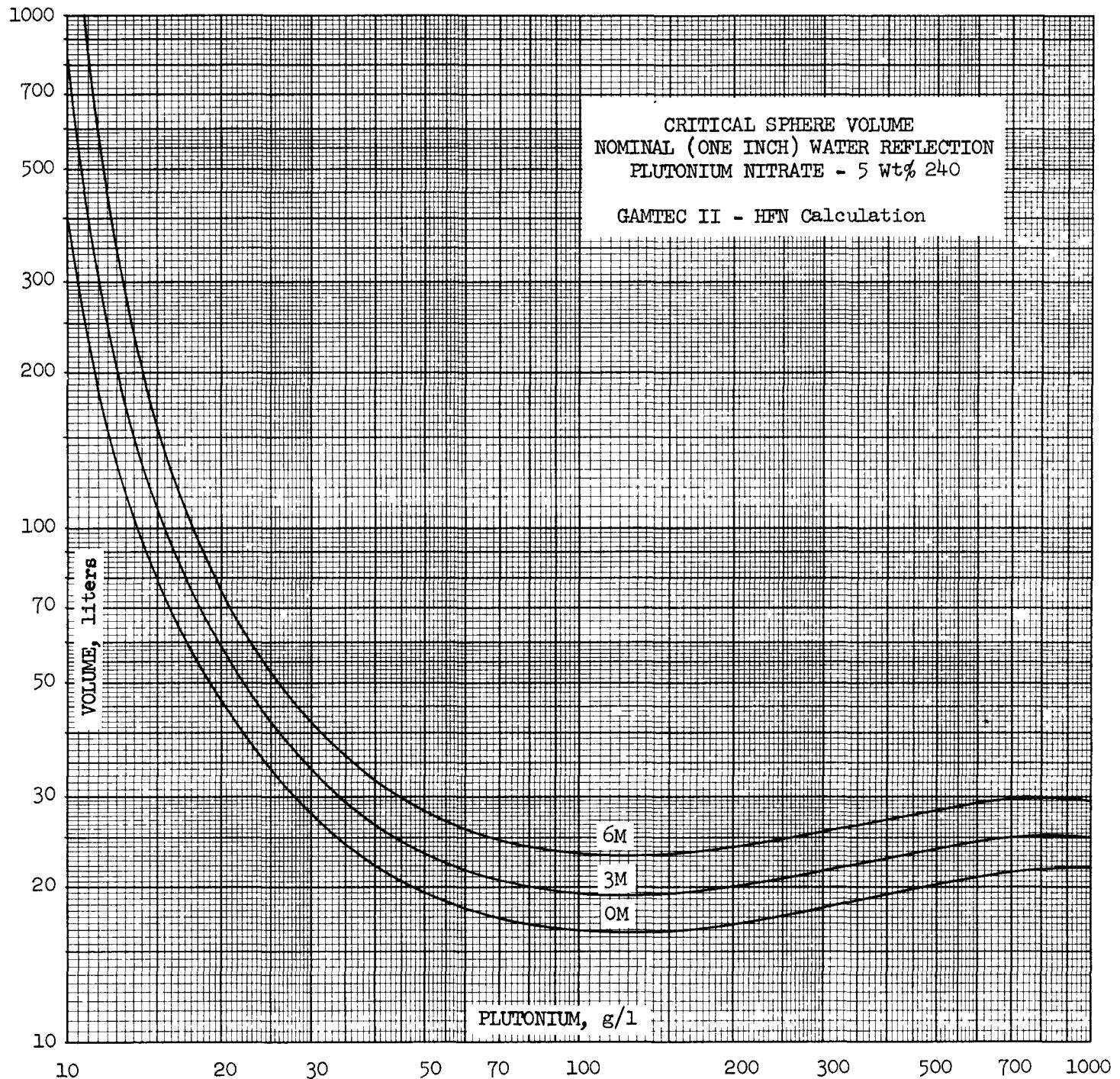


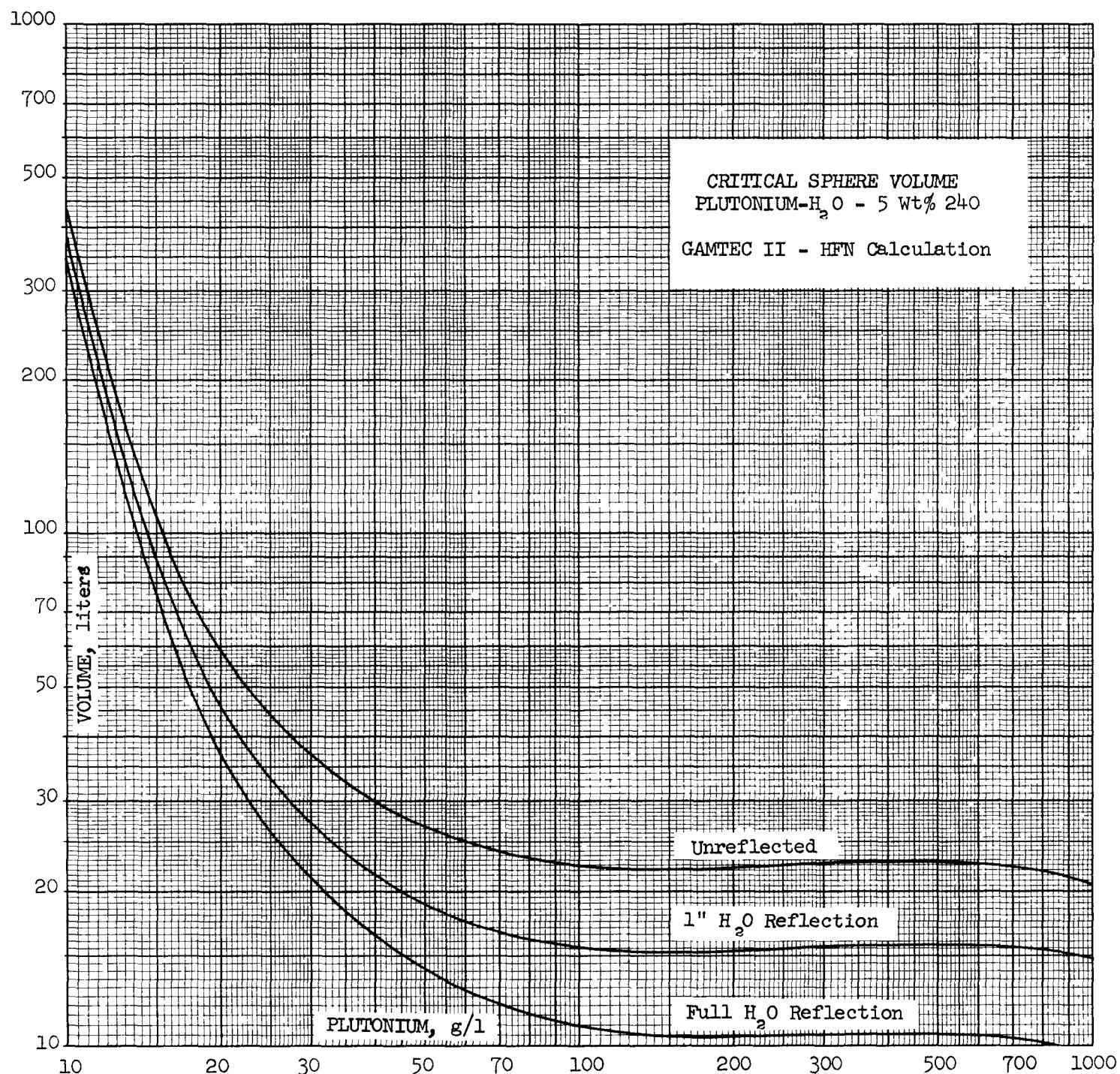
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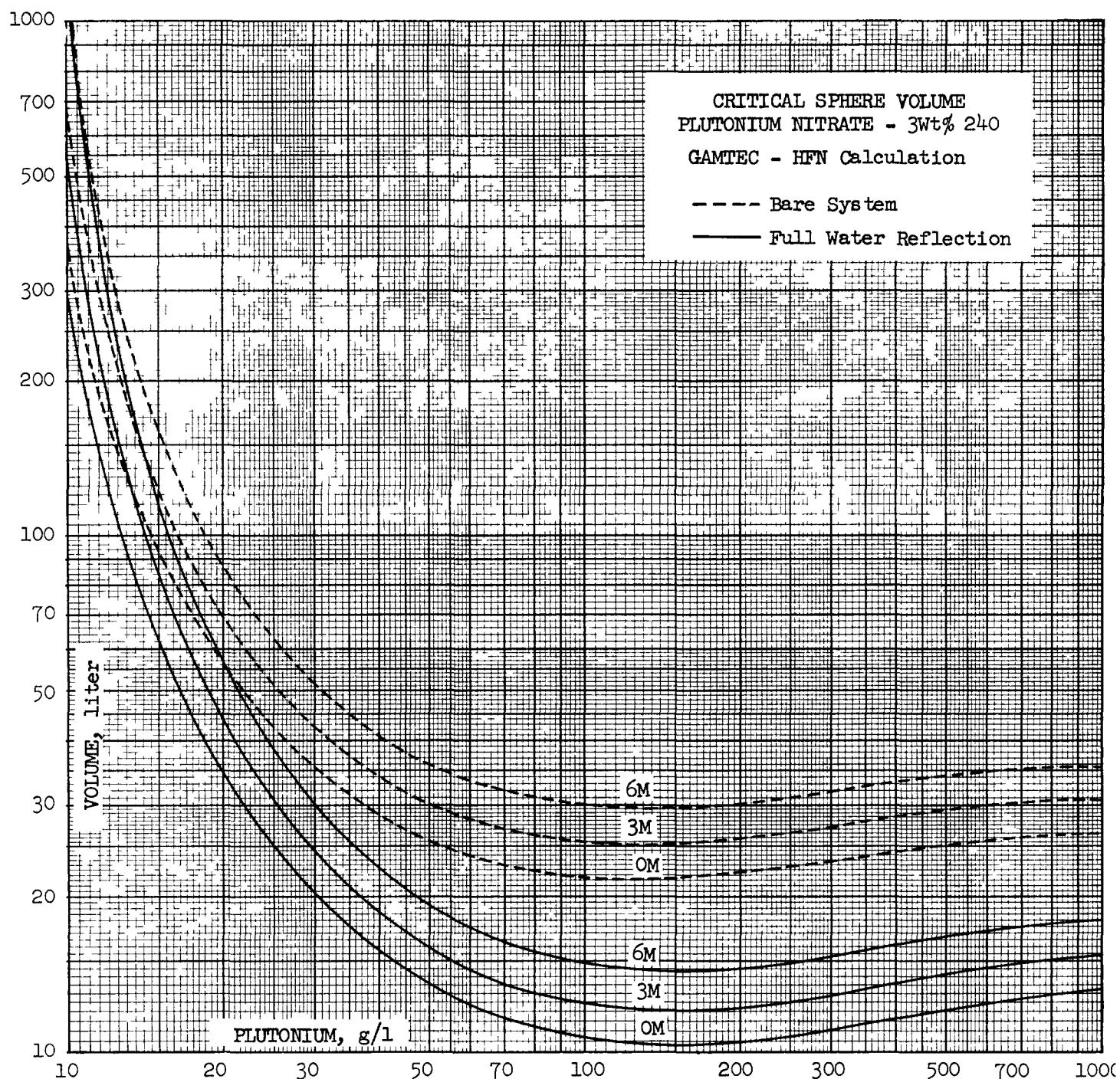


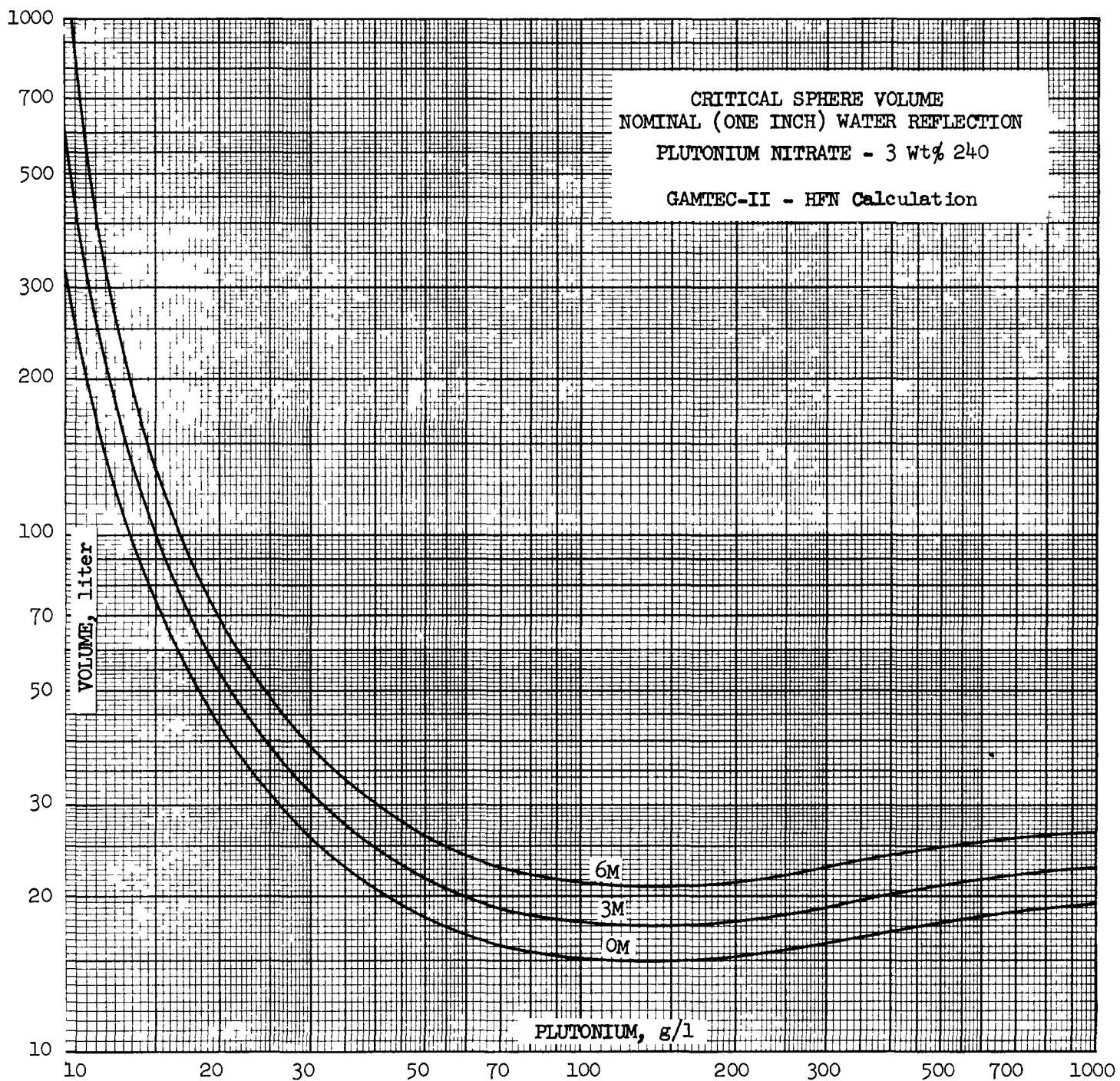


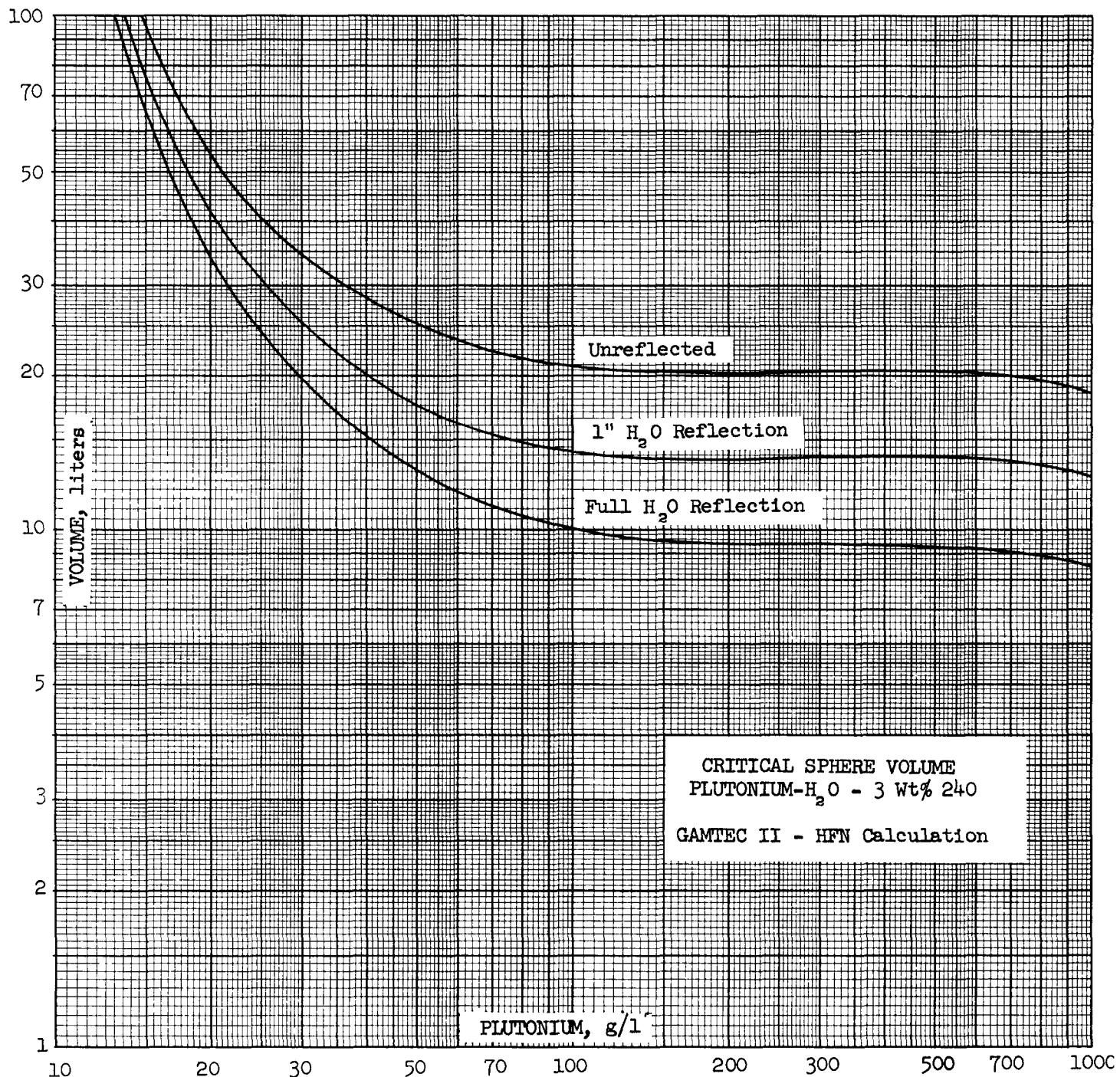


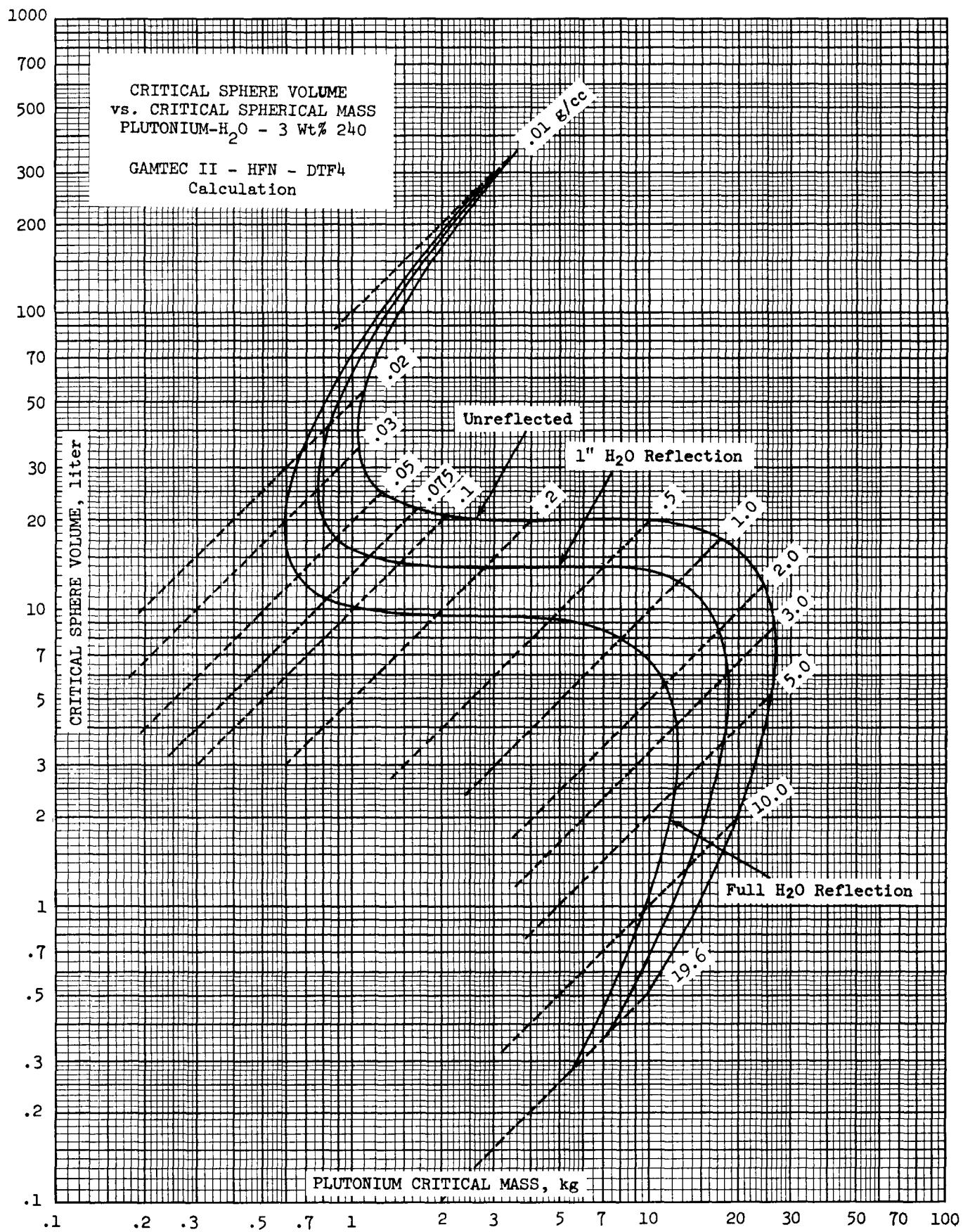


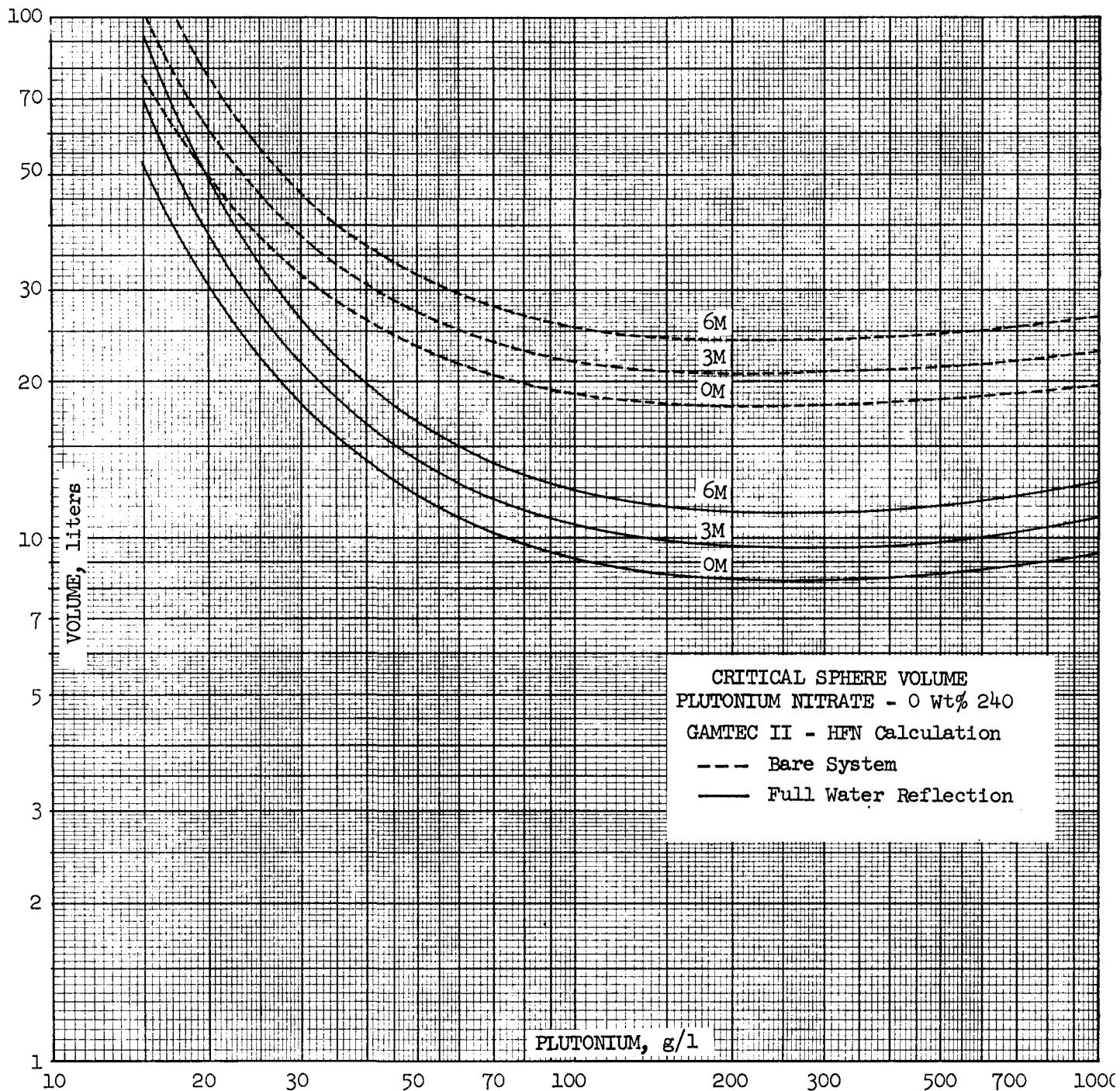








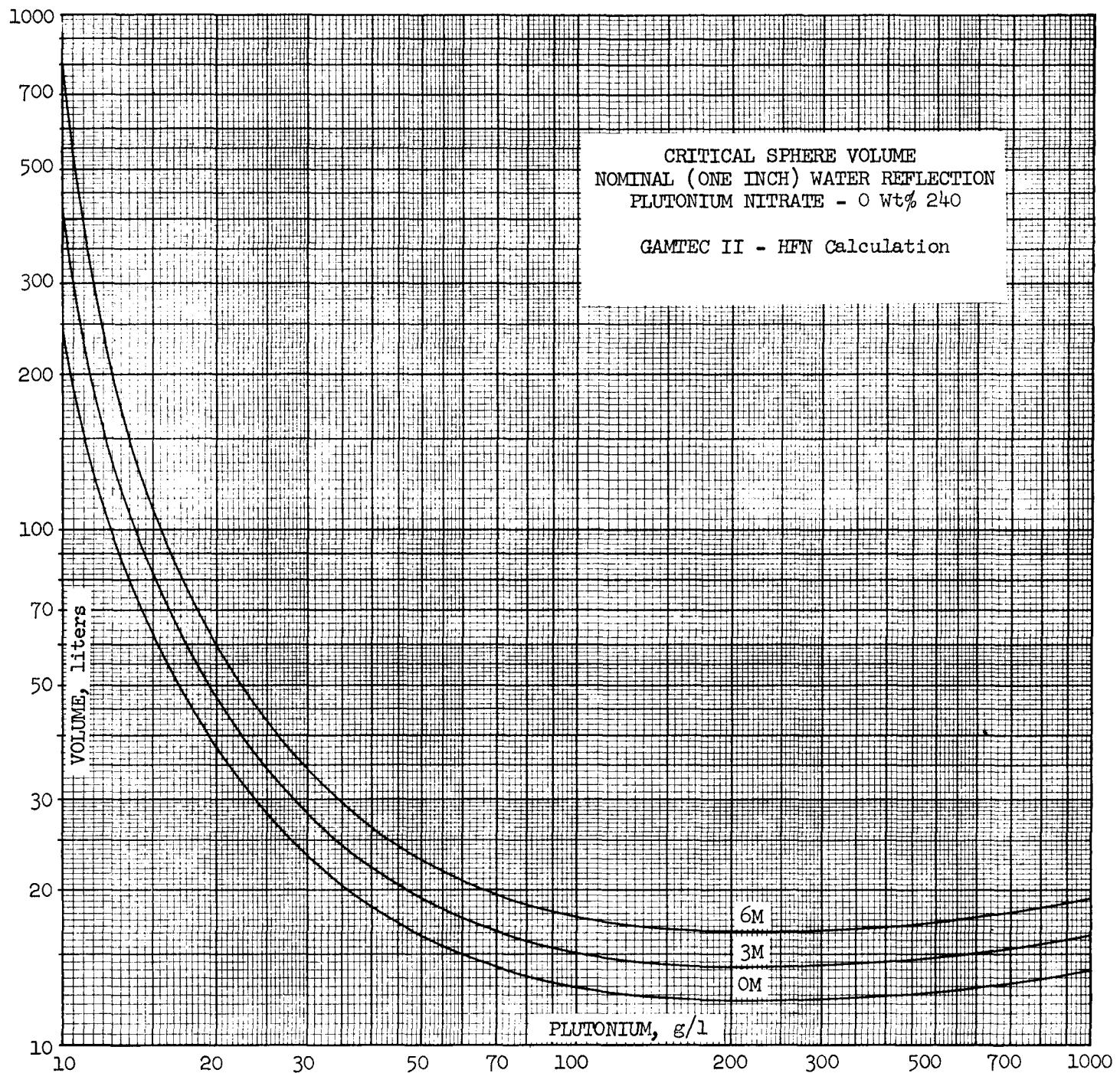




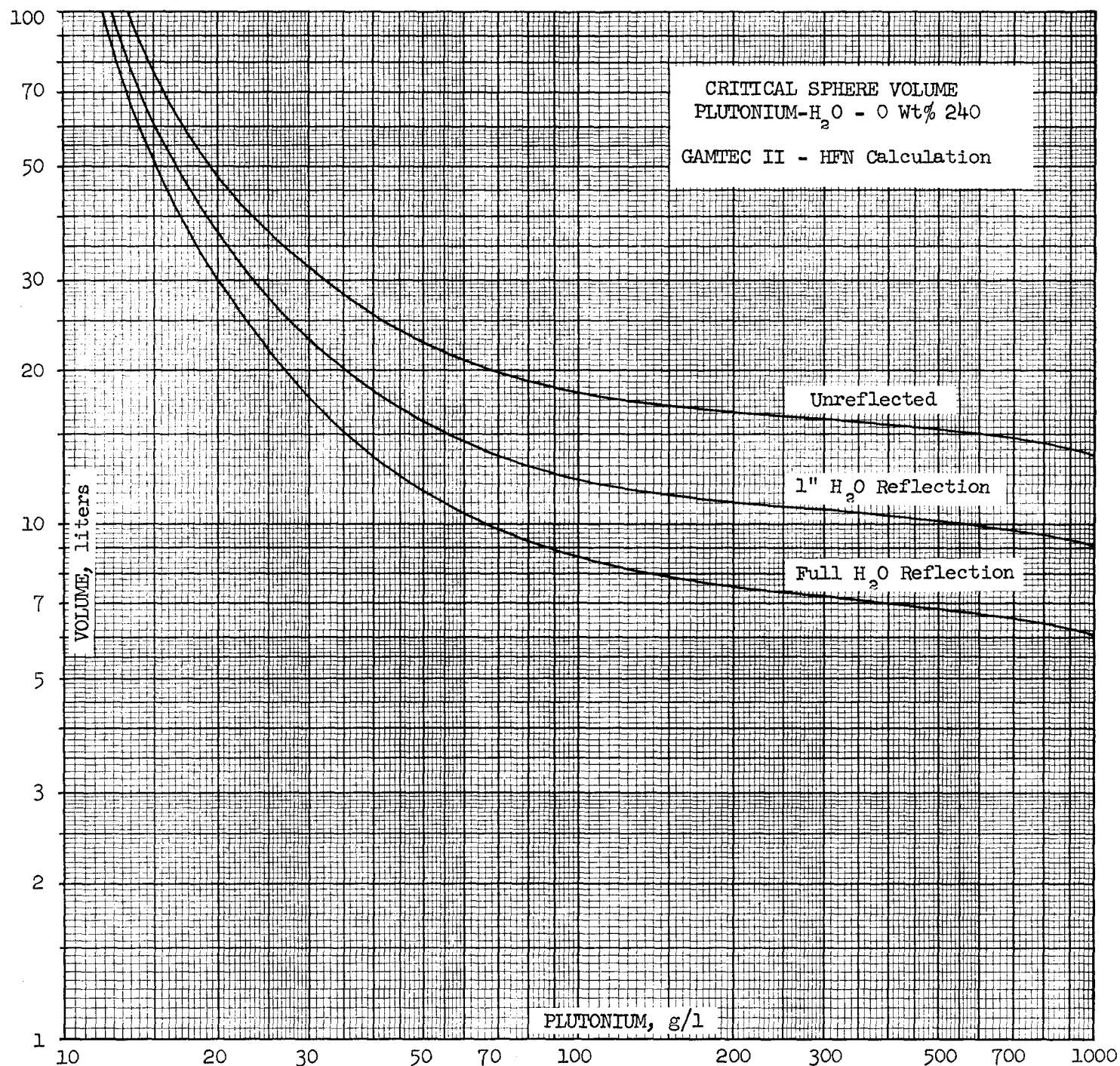
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ARH-600



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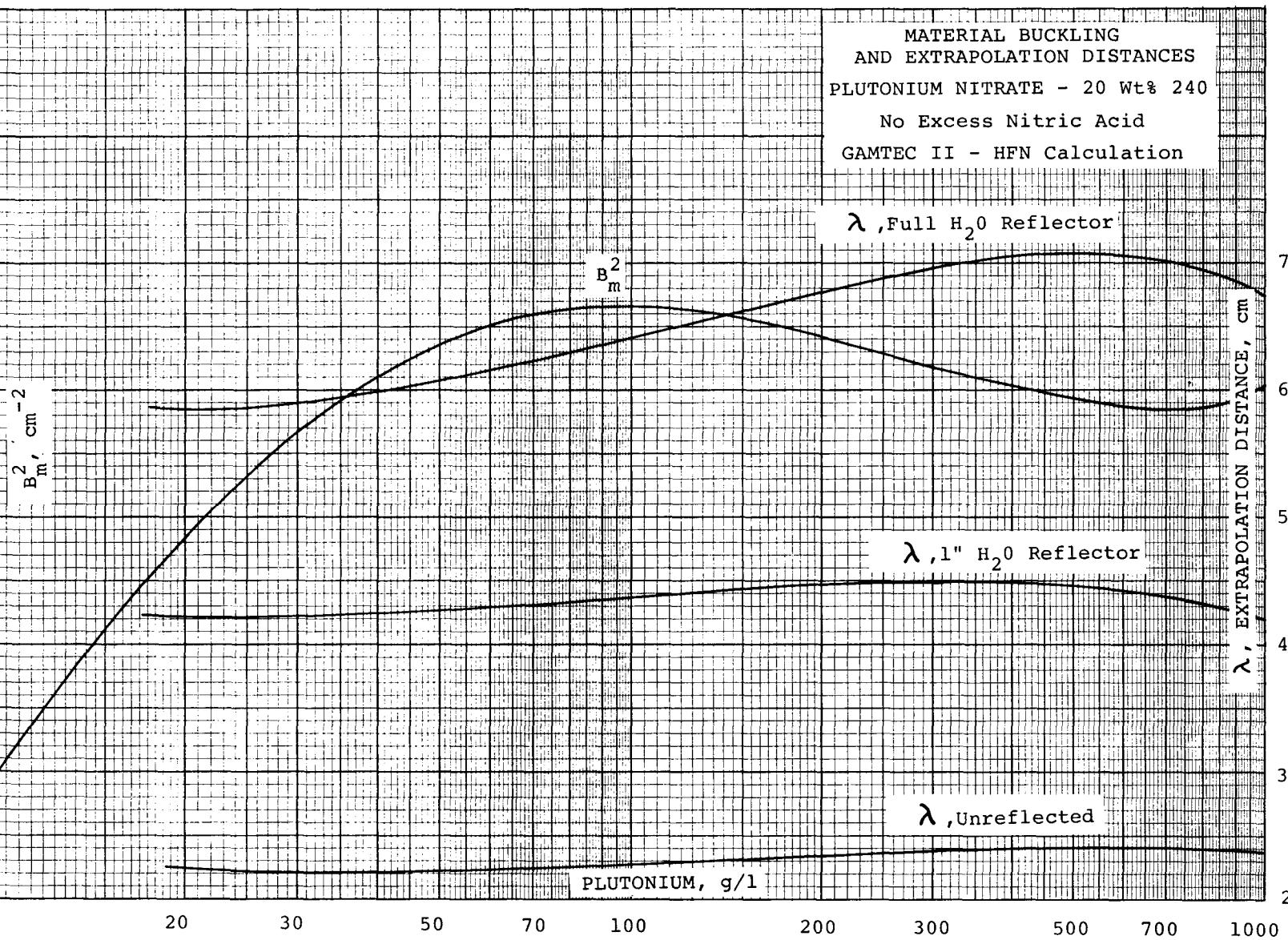
ARH-600

MATERIAL BUCKLING
AND EXTRAPOLATION DISTANCES
PLUTONIUM NITRATE - 20 Wt% 240
No Excess Nitric Acid
GAMTEC II - HFN Calculation

λ , Full H_2O Reflector

λ , 1" H_2O Reflector

λ , Unreflected

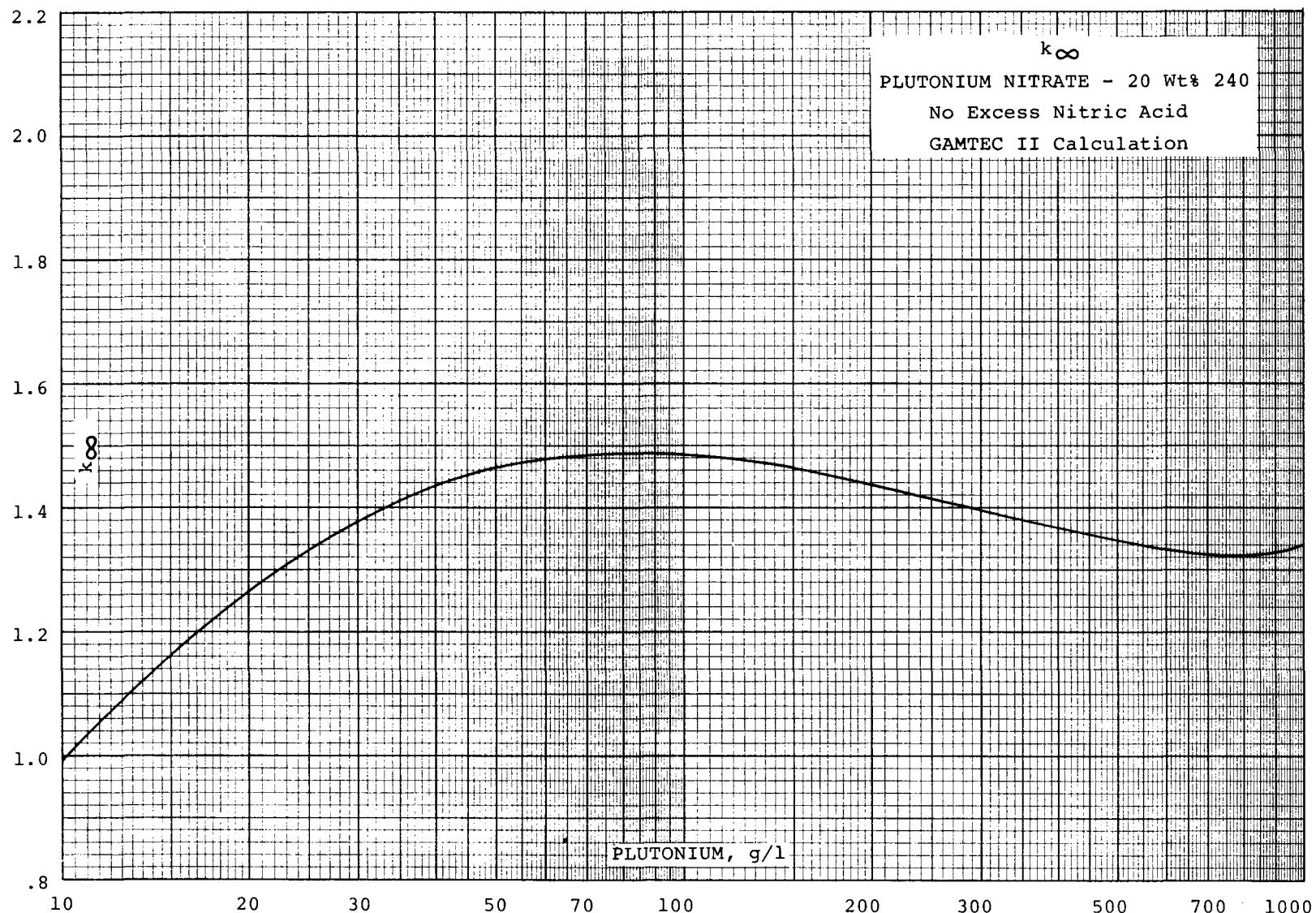


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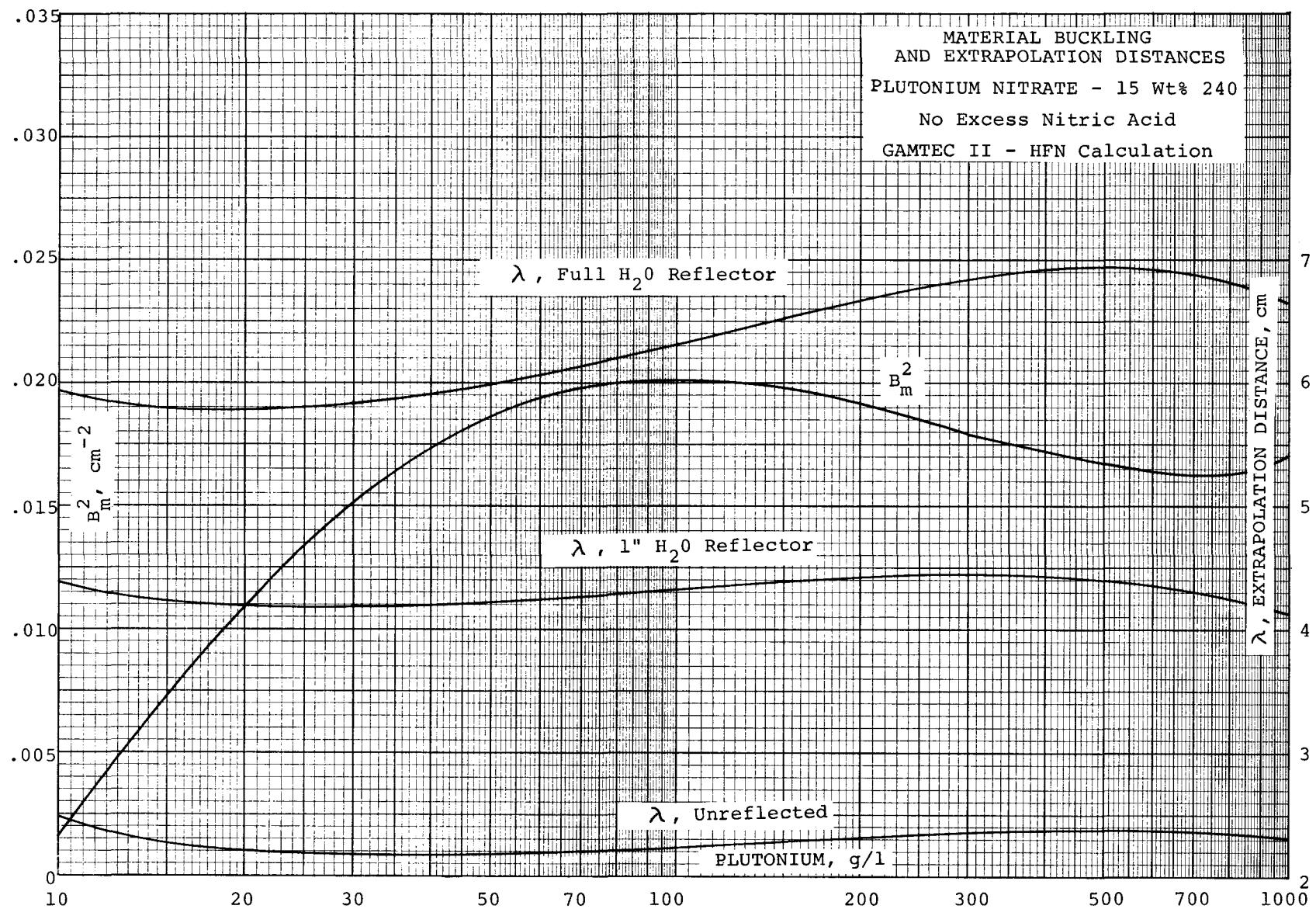


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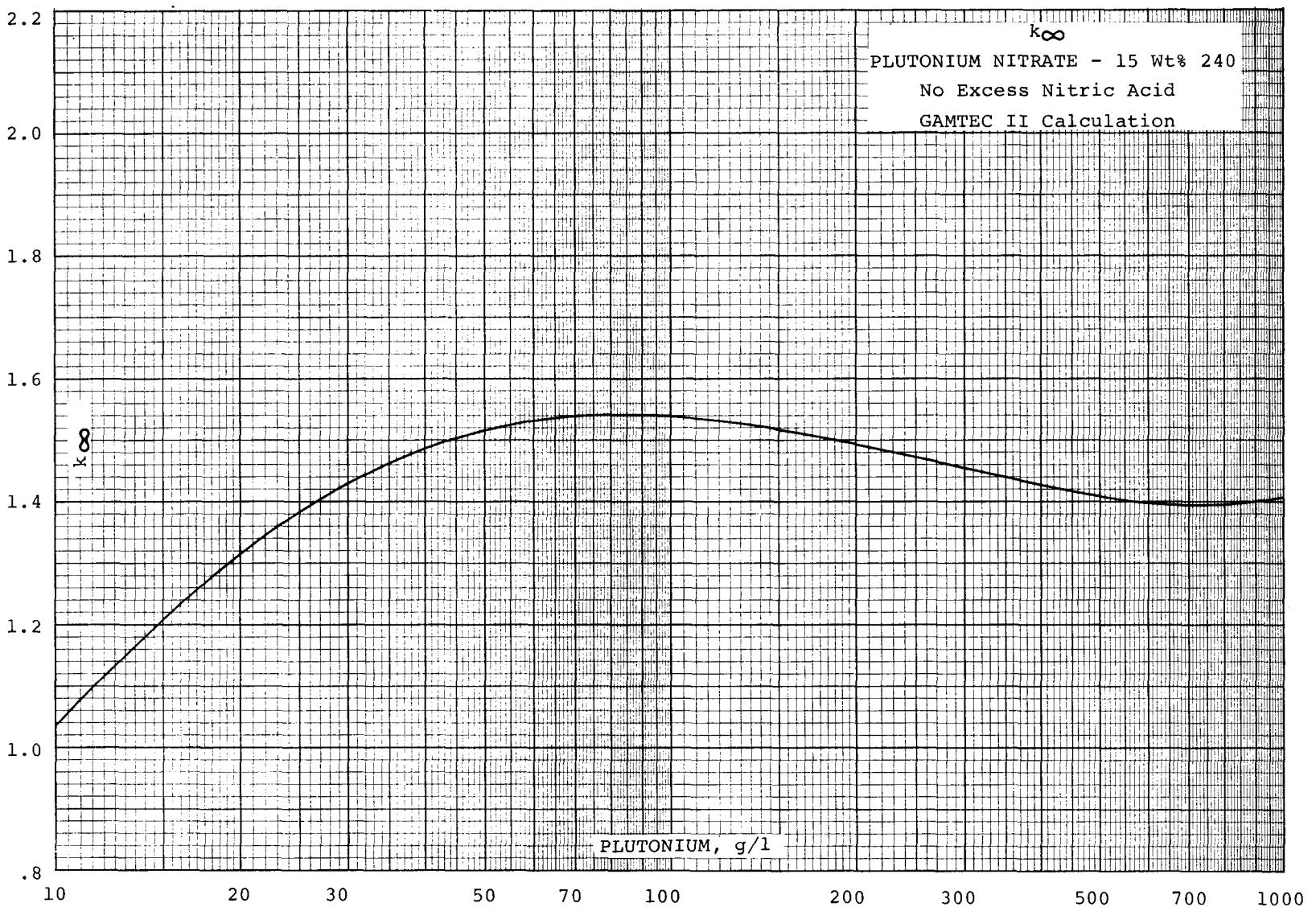
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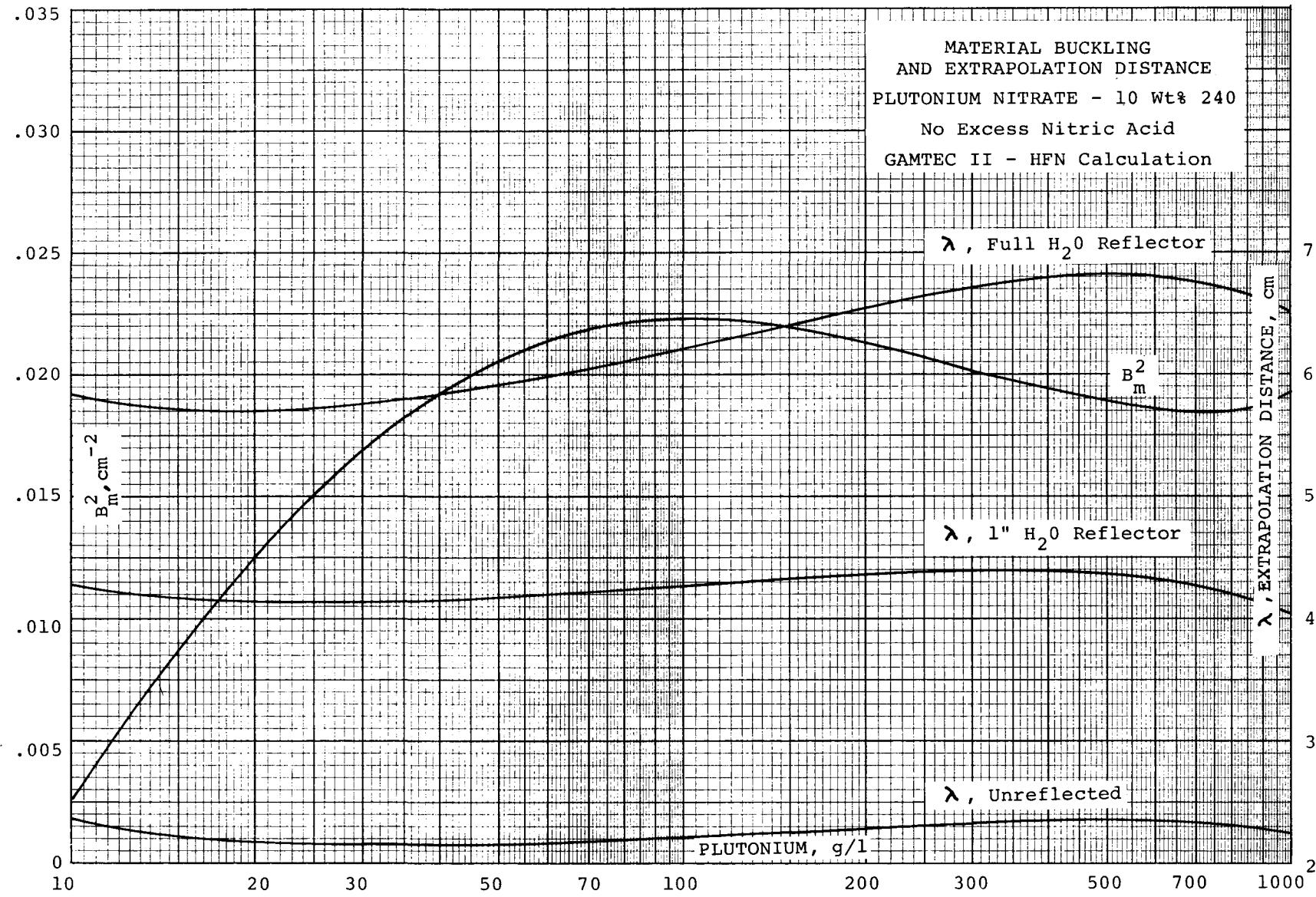
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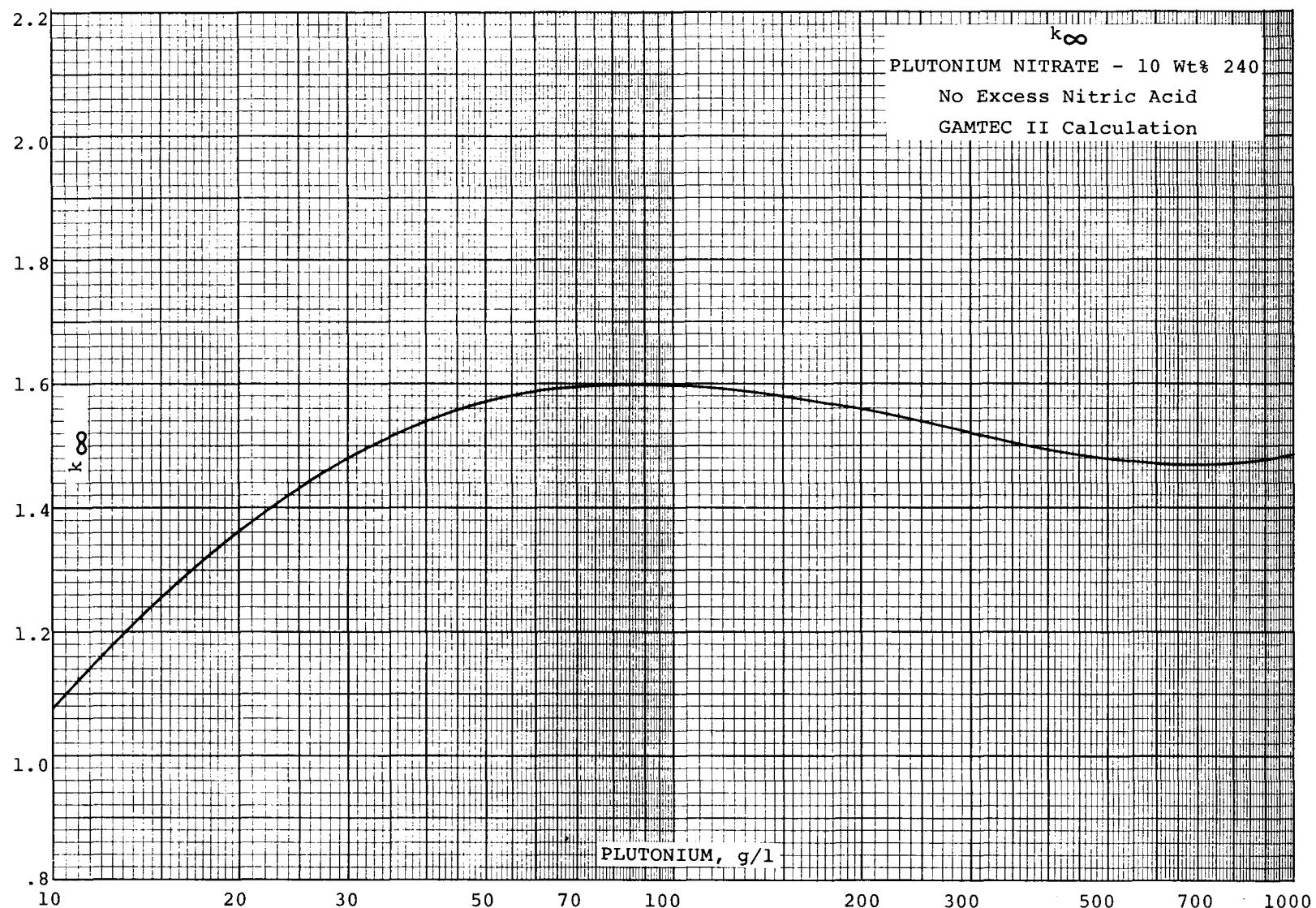
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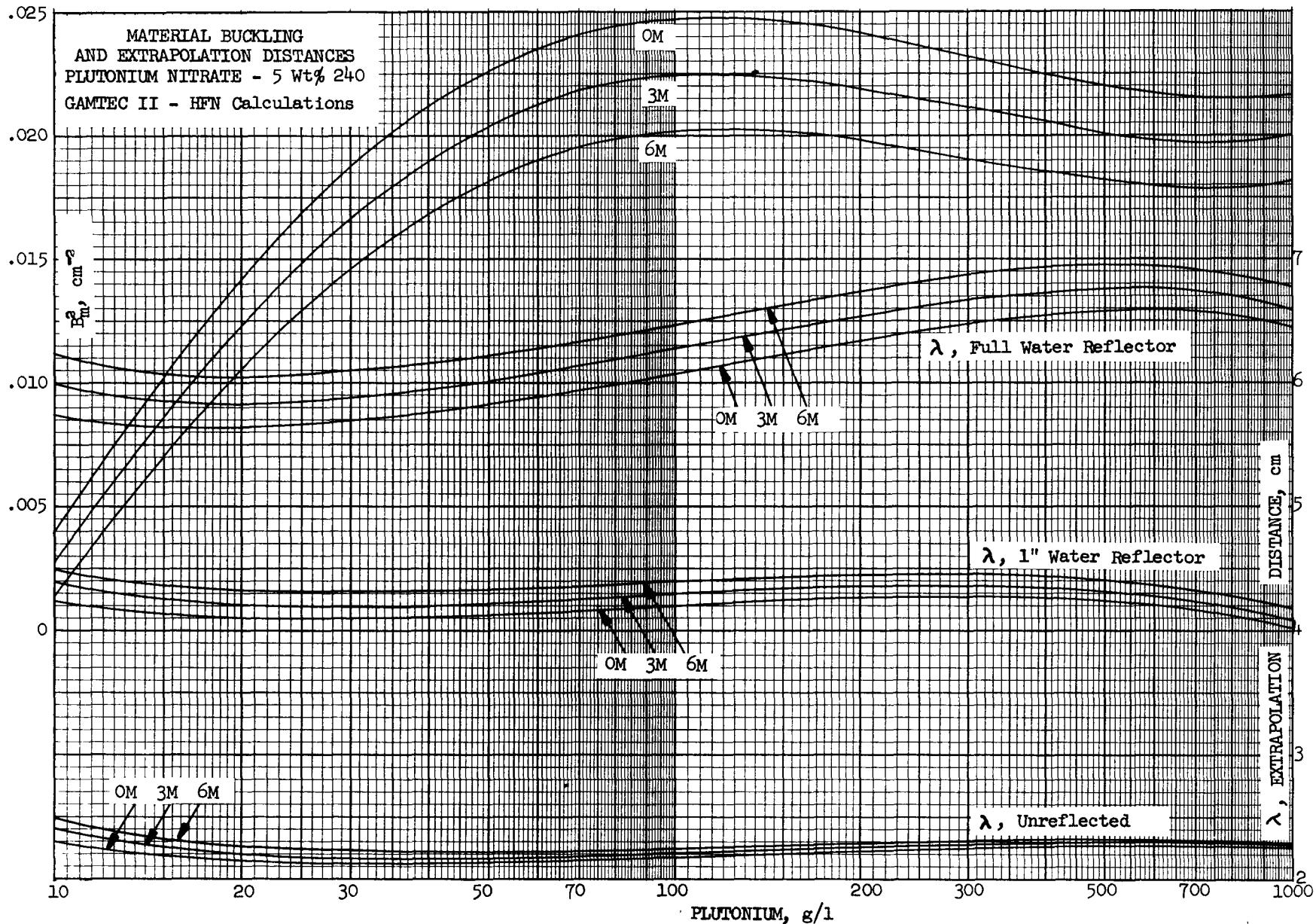


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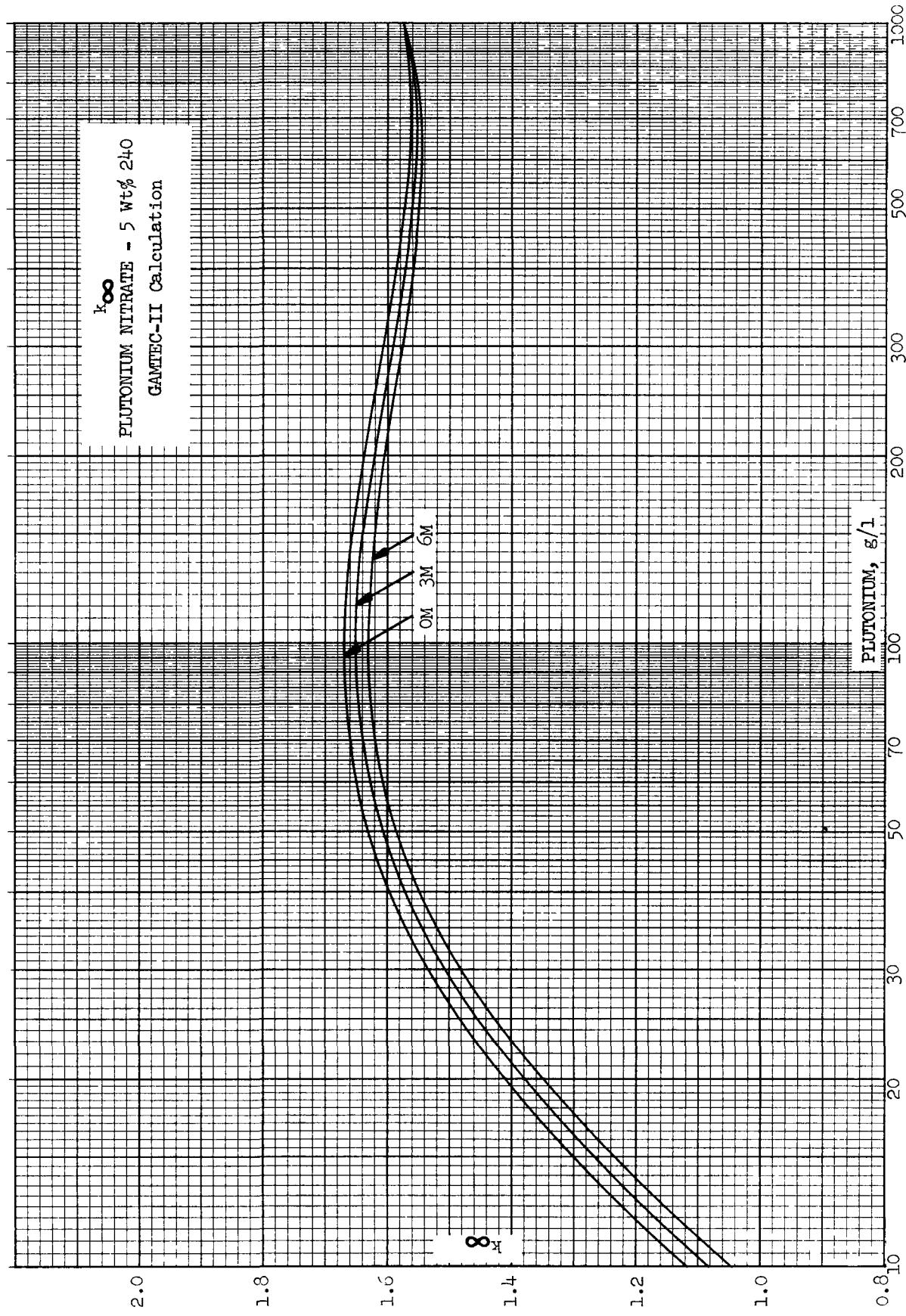
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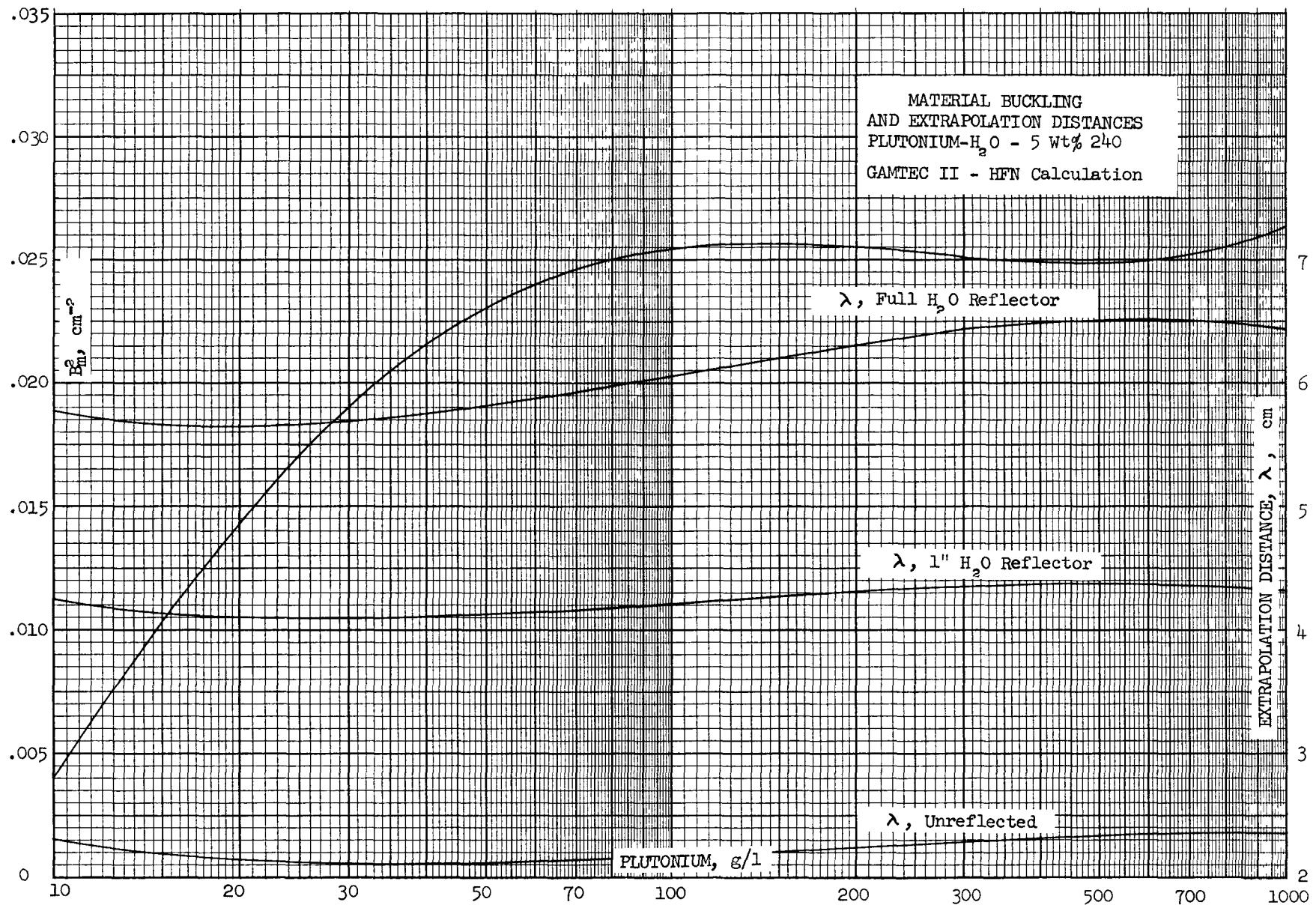


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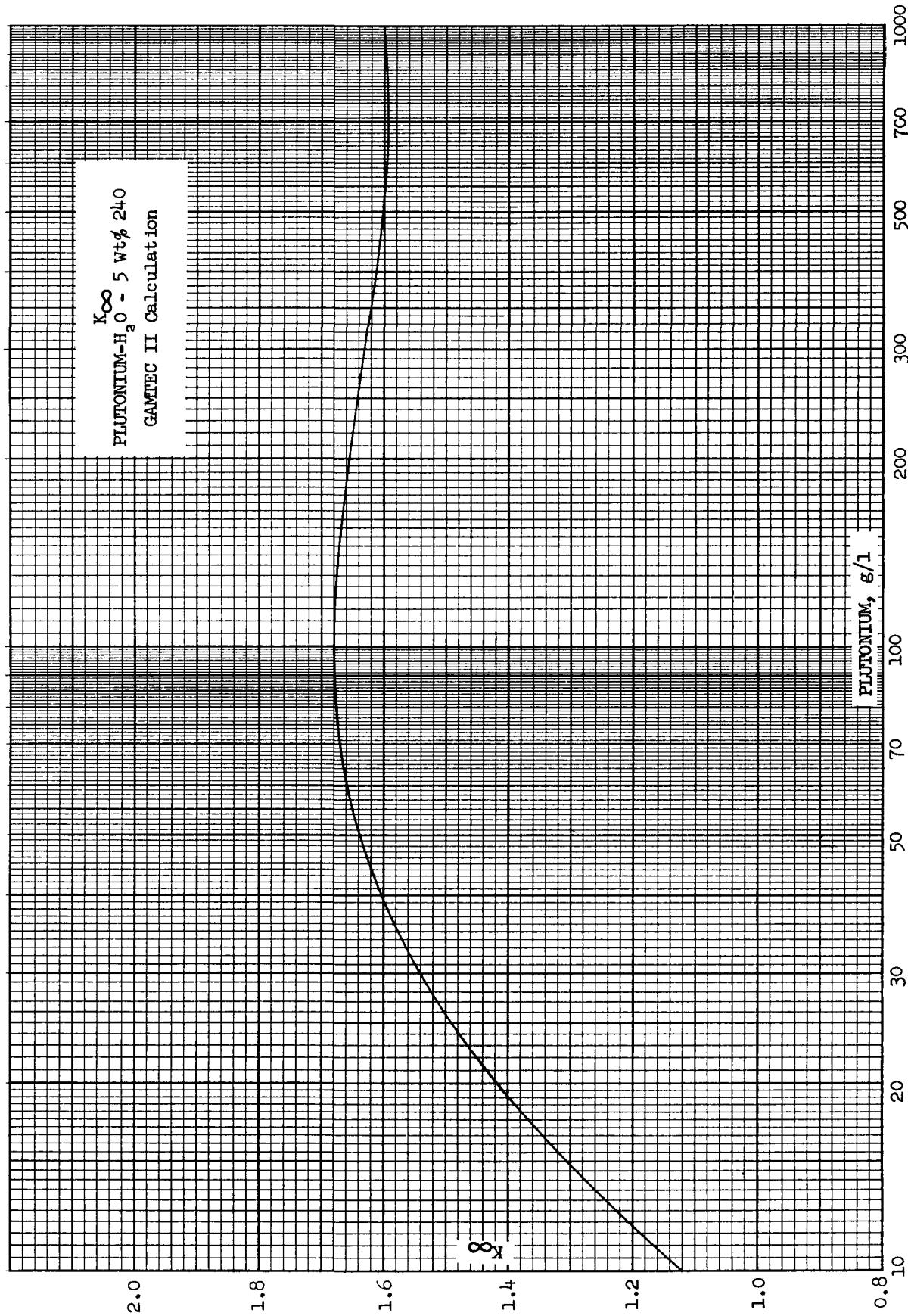
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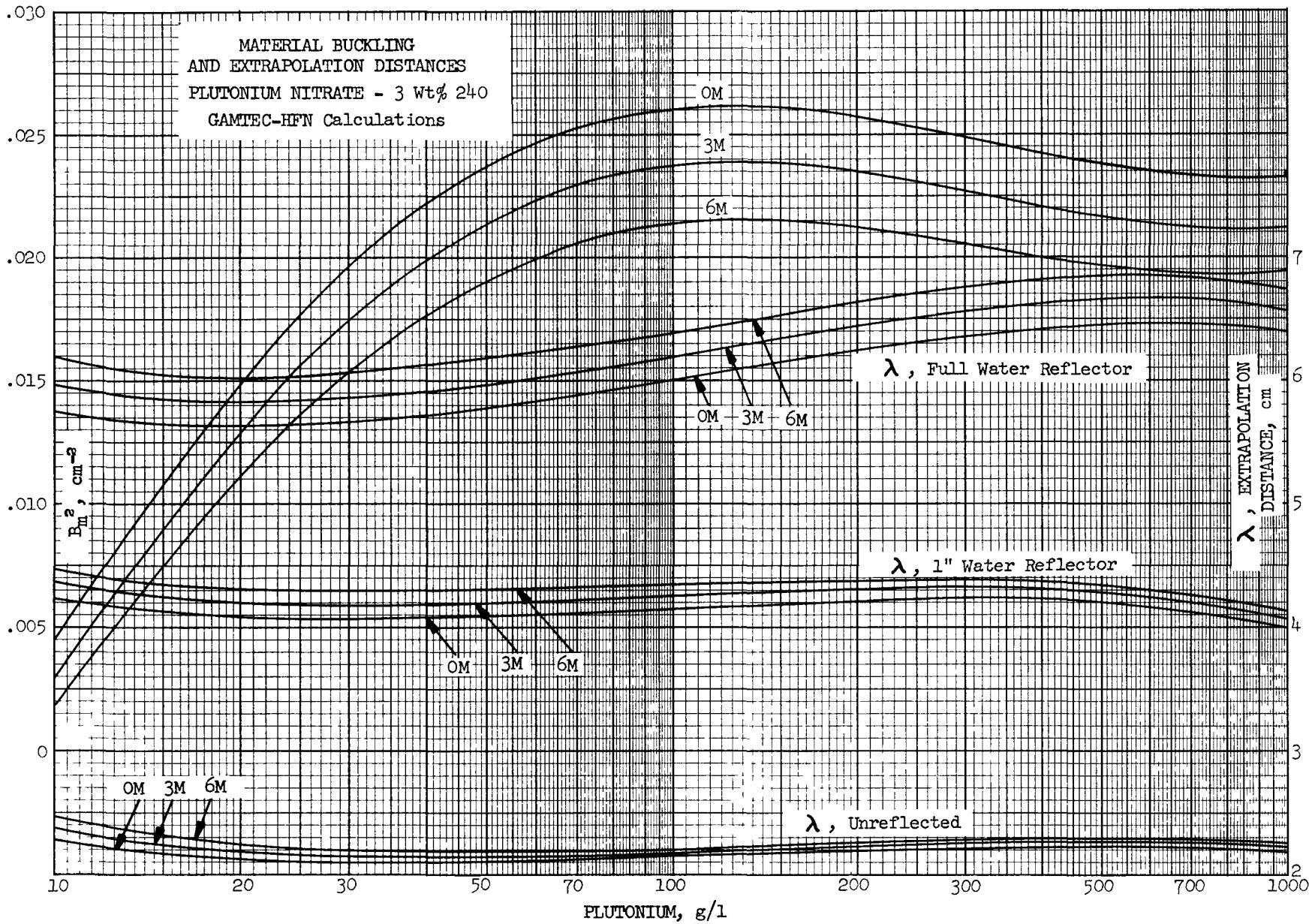


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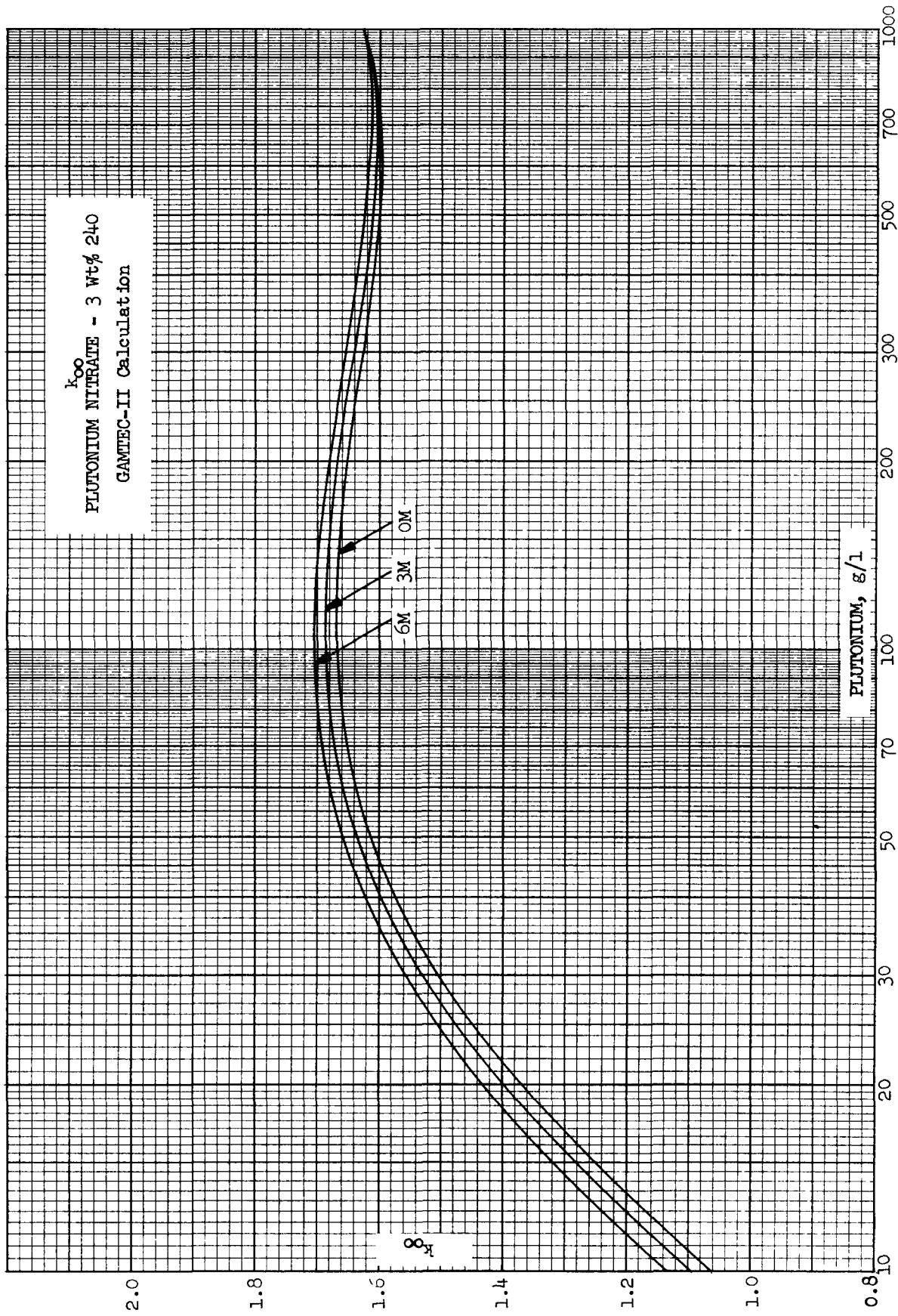
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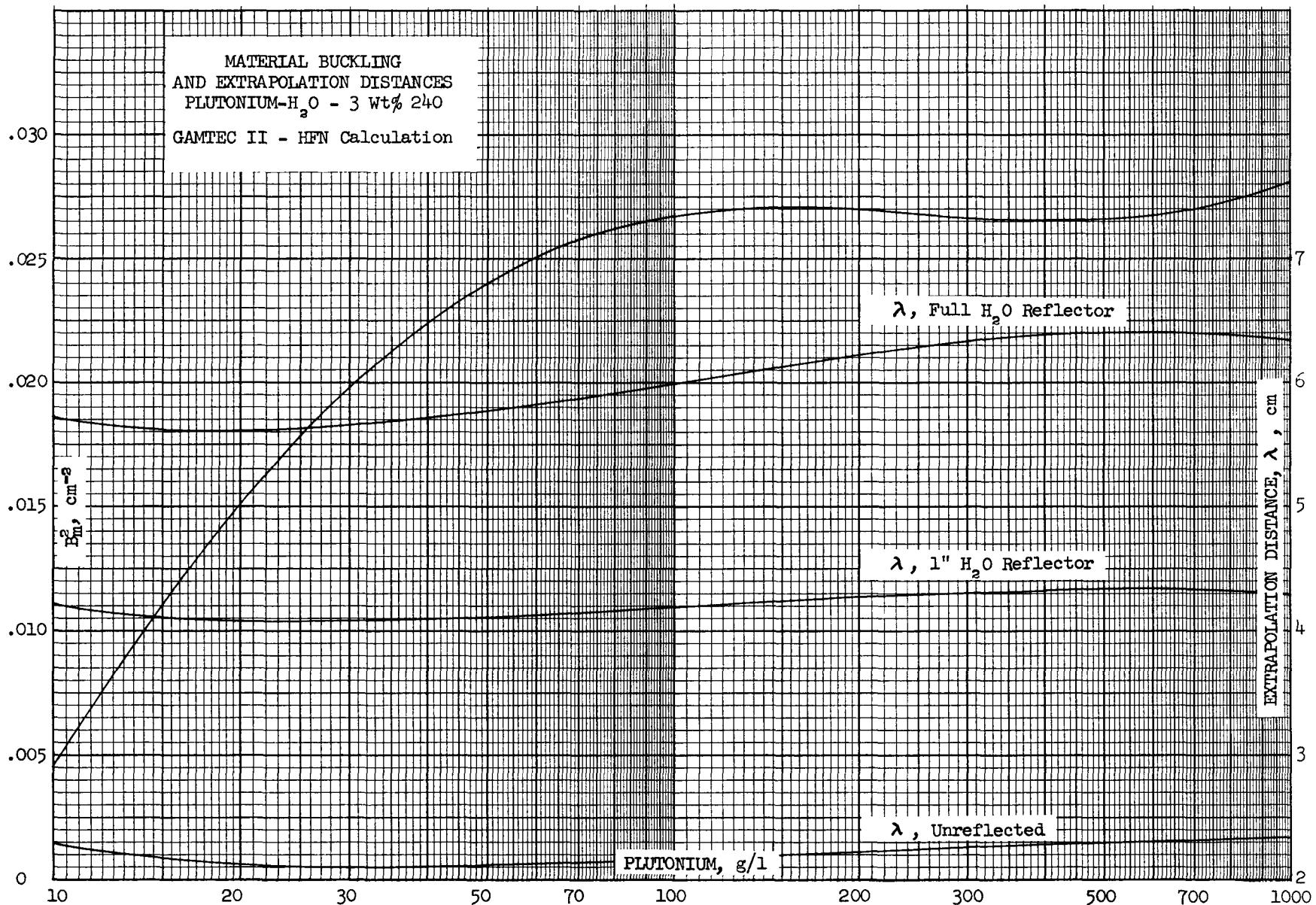


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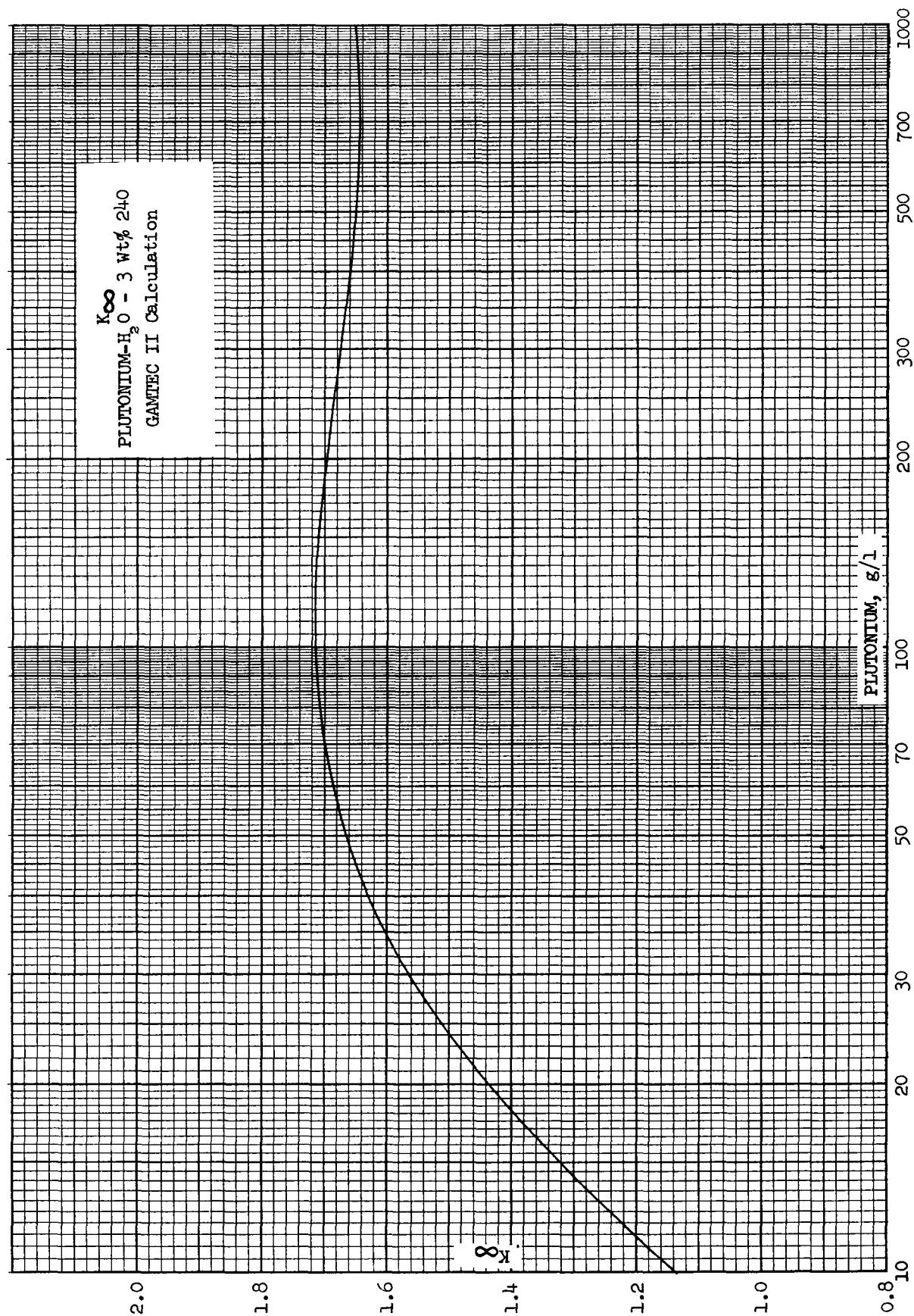
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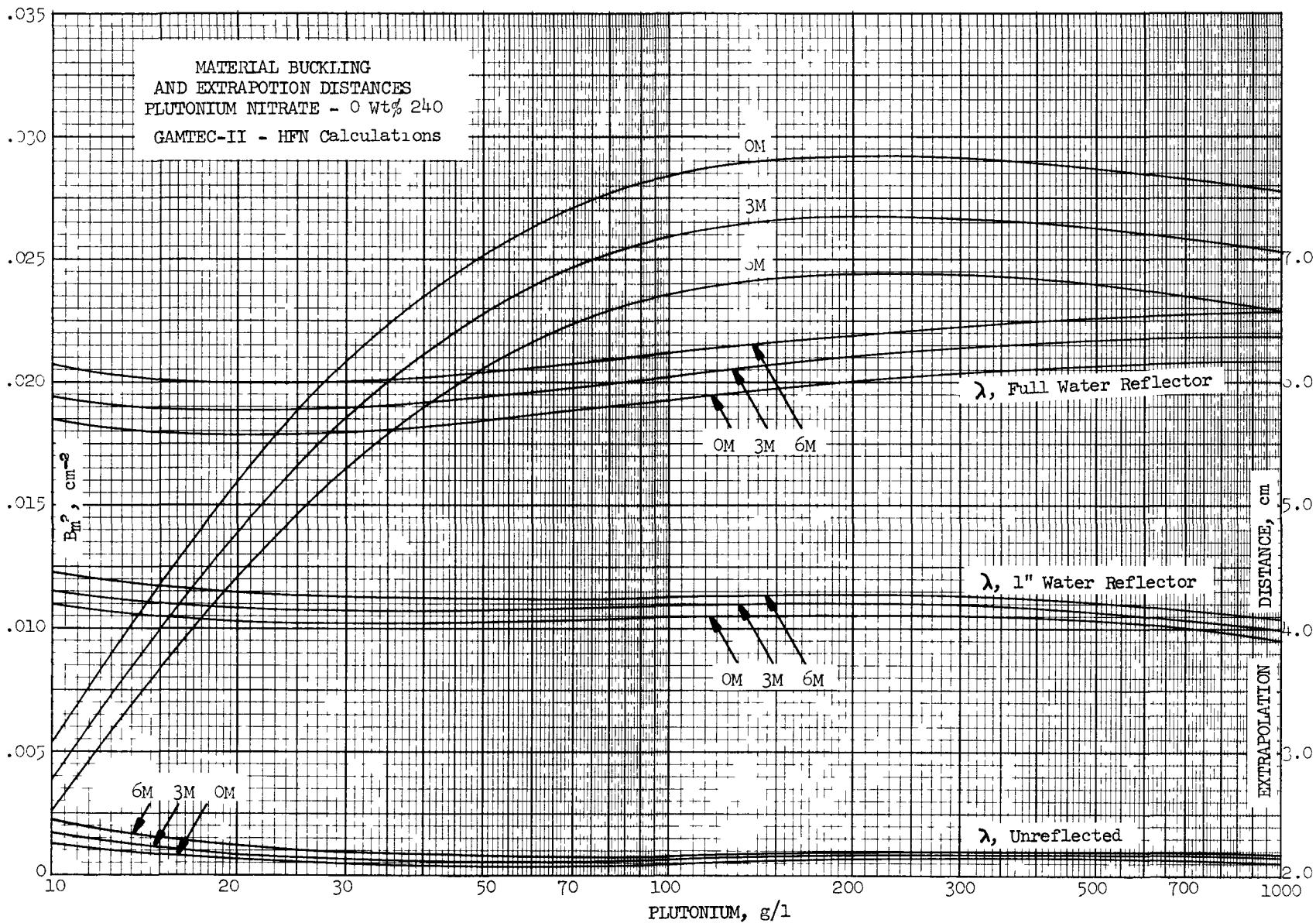


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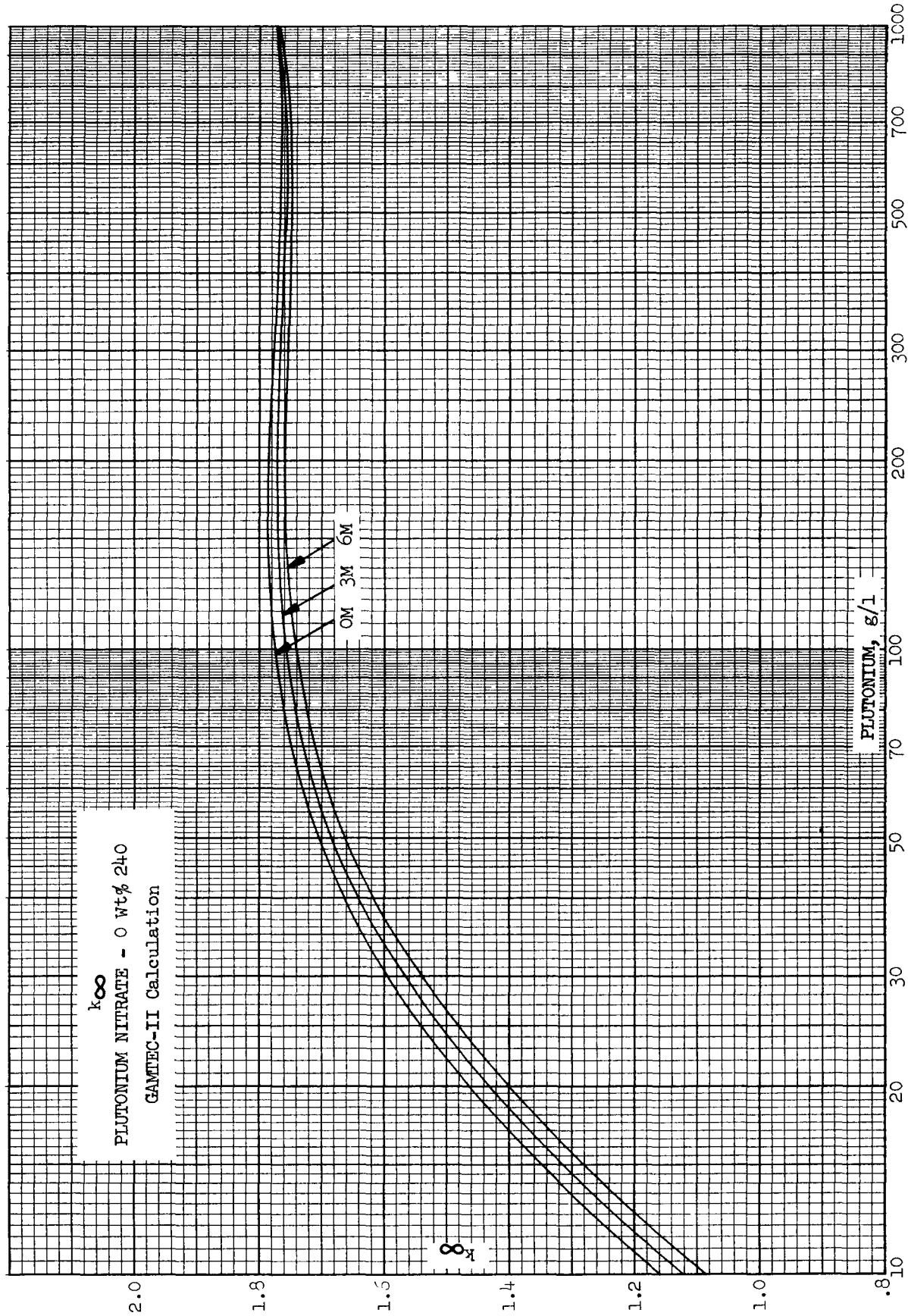


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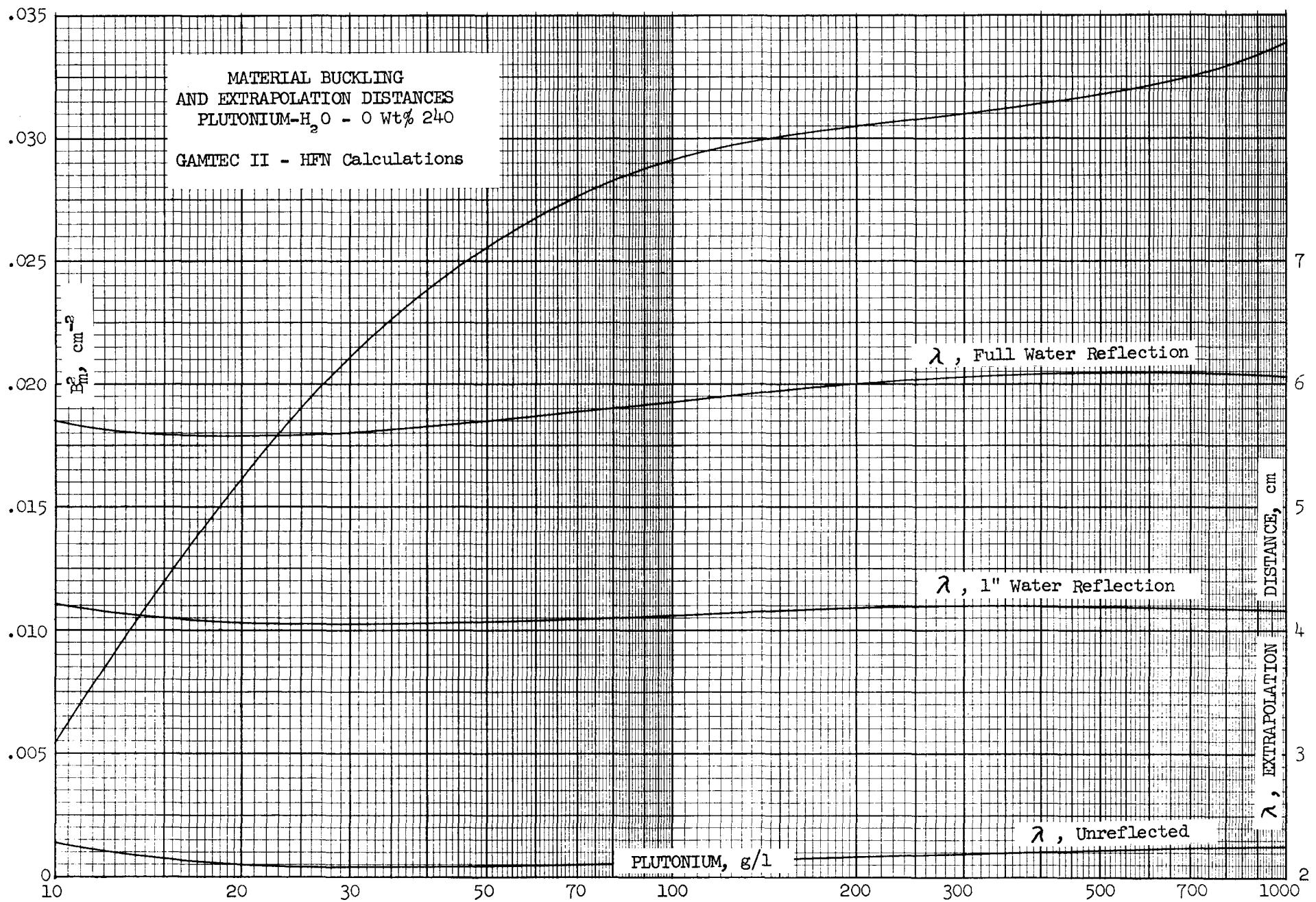


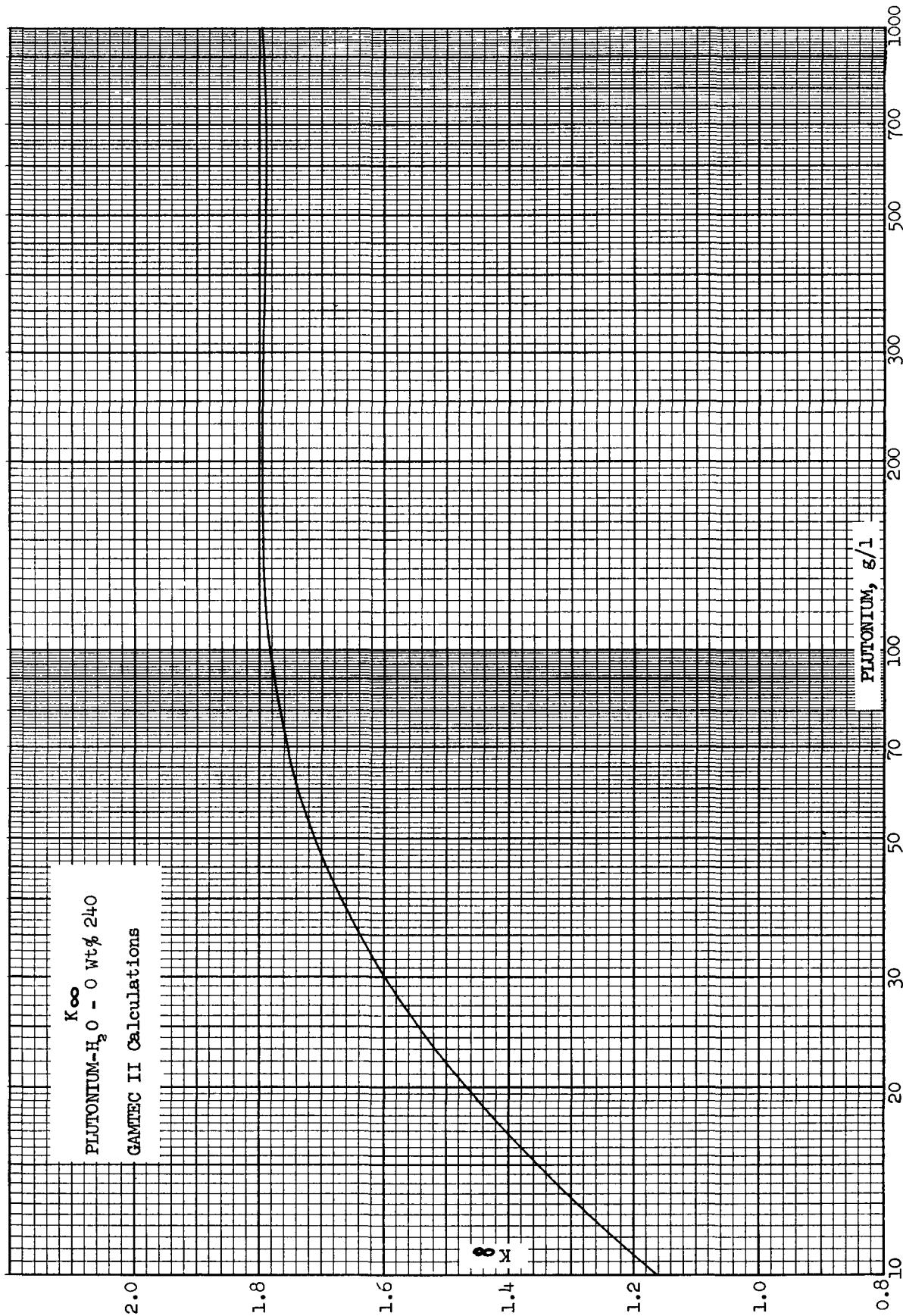
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III.A.10(1C0)-3

AHH-600





III. HOMOGENEOUS DATA

B. URANIUM-235 SYSTEMS

1. Correlation Between Calculation and Experiment
2. E/U versus Uranium g/l Relationship
3. Critical Sphere Dimensions

Earlier graphs within these divisions have the percentage by weight of the major fissile isotope (U-235) as the fourth identification number (e.g., III.B.3.97-2 would signify the second graph showing data for uranium containing 97 weight percent U-235). Because the use of fractional percentages made the page number difficult to read, later graph identification has been changed to set off the weight percent by parentheses, III.B.3(97)-2, in the interest of clarity.

4. Critical Cylinder Dimensions
5. Critical Slab Dimensions
6. Critical Mass - Sphere
7. Critical Mass per Unit Height - Cylinder
8. Critical Mass per Unit Area - Slab
9. Critical Volume
10. Material Bucklings
11. Infinite Multiplication Factor

BASIC URANIUM-235 CRITICAL PARAMETERS

These basic values are taken from references which would normally be used as bases for standards. ARH-600 values compare favorably.

<u>METAL</u>	<u>Full Reflection*</u>	<u>Bare**⁽³⁾</u>
Minimum critical spherical mass, Kg ^{235}U 18.82 g/cm 3	21.85 ⁽¹⁾	
Minimum critical spherical mass, Kg ^{235}U (93.5) 18.8 g/cm 3	22.8 ⁽²⁾	47.
Infinite cylinder diameter, inches, ^{235}U 18.82 g/cm 3	3.0 ⁽¹⁾	4.5
Infinite slab thickness, inches, ^{235}U 18.82 g/cm 3	0.586 ⁽¹⁾	2.2
Minimum spherical volume, liters, ^{235}U 18.82 g/cm 3	1.16 ⁽¹⁾	2.7
<u>HOMOGENEOUS SOLUTIONS⁽⁴⁾</u>		
Minimum critical mass, g ^{235}U	820	1400
Infinite cylinder diameter, inches	5.63	8.5
Infinite slab thickness, inches	1.93	4.5
Minimum spherical volume, liters	6.1	14.0
Minimum areal concentration g/ft 2	390	~520
Minimum critical aqueous concentration, g/l ^{235}U ⁽⁵⁾	12.1	
Minimum enrichment for criticality, Wt% ^{235}U ⁽⁵⁾	1.034 ± 0.010	
Minimum enrichment for criticality for UNH solutions, Wt% ^{235}U ⁽⁶⁾	2.104 ± 0.010	

* Reflector is water unless otherwise specified.

** "Bare" solutions have 1/16-inch stainless steel reflector.

(1) W. H. Roach and D. R. Smith. "Estimates of Maximum Subcritical Dimensions of Single Fissile Metal Units", ORNL-CDC-3, October, 1967, (reflected metal systems).

(2) G. A. Graves and H. C. Paxton. "Critical Masses of Oralloy Assemblies", Nucleonics 15, No. 6, 90, June, 1957, (bare metal systems).

- (3) H. C. Paxton, et al. "Critical Dimensions of Systems Containing ^{235}U , ^{239}Pu and ^{233}U ", TID-7028, June, 1964, (for all "bare" systems unless otherwise noted; solutions are U(93.2)-H₂O with correction for H/U relationships of actual solutions).
- (4) J. W. Webster. "Calculated Neutron Multiplication Factors of Uniform Aqueous Solutions of ^{233}U and ^{235}U ", ORNL-CDC-2, October, 1967, (for reflected U(100)O₂F₂ systems unless noted otherwise).
- (5) H. E. Handler. "Measurement of Multiplication Constant of Slightly Enriched Homogeneous UO₃-H₂O Mixture and Minimum Enrichment for Criticality", USAEC Report, HW-70310, August, 1961.
- (6) S. R. Bierman and G. M. Hess. "Minimum Critical ^{235}U Enrichment of Homogeneous Hydrogenous Uranyl Nitrate", ORNL-CDC-5, June, 1968.

III.B.1 Correlations Between Calculations and Experiment

The data for 3 weight percent uranium trioxide and 93.2 weight percent uranyl nitrate in this section was obtained by the GAMTEC II (reference 1) and HFN (reference 2) codes. The GAMTEC II code was used to produce 18 neutron energy group cross-section sets that, in turn, were used in the HFN one-dimensional diffusion theory code to produce critical sizes, extrapolation distances and material bucklings. Unless otherwise indicated, the material bucklings for the other enrichments and the k_{∞} and migration areas were obtained from the GAMTEC II code alone. GAMTEC II utilizes a special averaging technique to calculate two-group constants, one broad fast group and one thermal group. From these two group constants the code calculates the material buckling and k_{∞} .

These parameters for low enriched uranium and the correlation of the GAMTEC II code to experimental data have been reported previously (reference 3).

The migration areas provided by the GAMTEC II code are high compared with those calculated using HFN material bucklings and GAMTEC k_{∞} . When using the GAMTEC migration areas and material buckling, a k_{eff} within one percent of that calculated using HFN migration areas and material bucklings will result. Therefore, these GAMTEC 2-group parameters are included until the more accurate GAMTEC-HFN calculations for desired enrichments are justified.

The calculated effective multiplication constant of critical experiments obtained from GAMTEC II - DTF IV (reference 4) (18 groups) are also shown in this section. These results are included to show the calculational accuracy of the DTF IV code using multigroup constants of uranium provided by GAMTEC II.

In some cases, comparison is made with data from the criticality handbook issued by the United Kingdom Atomic Energy Authority(5) and is referenced as AHSB(U.K.) or U.K.

(1) L. L. Carter, C. R. Richey, C. E. Hughey, "GAMTEC II," BNWL-52, 1965.

(2) J. R. Lillie, "Computer Code HFN," HW-71545, 1961.

(3) K. R. Ridgway, "Calculated Critical Parameters of Low Enriched Uranium," ISO-174 and ISO-SA-4, 1966.

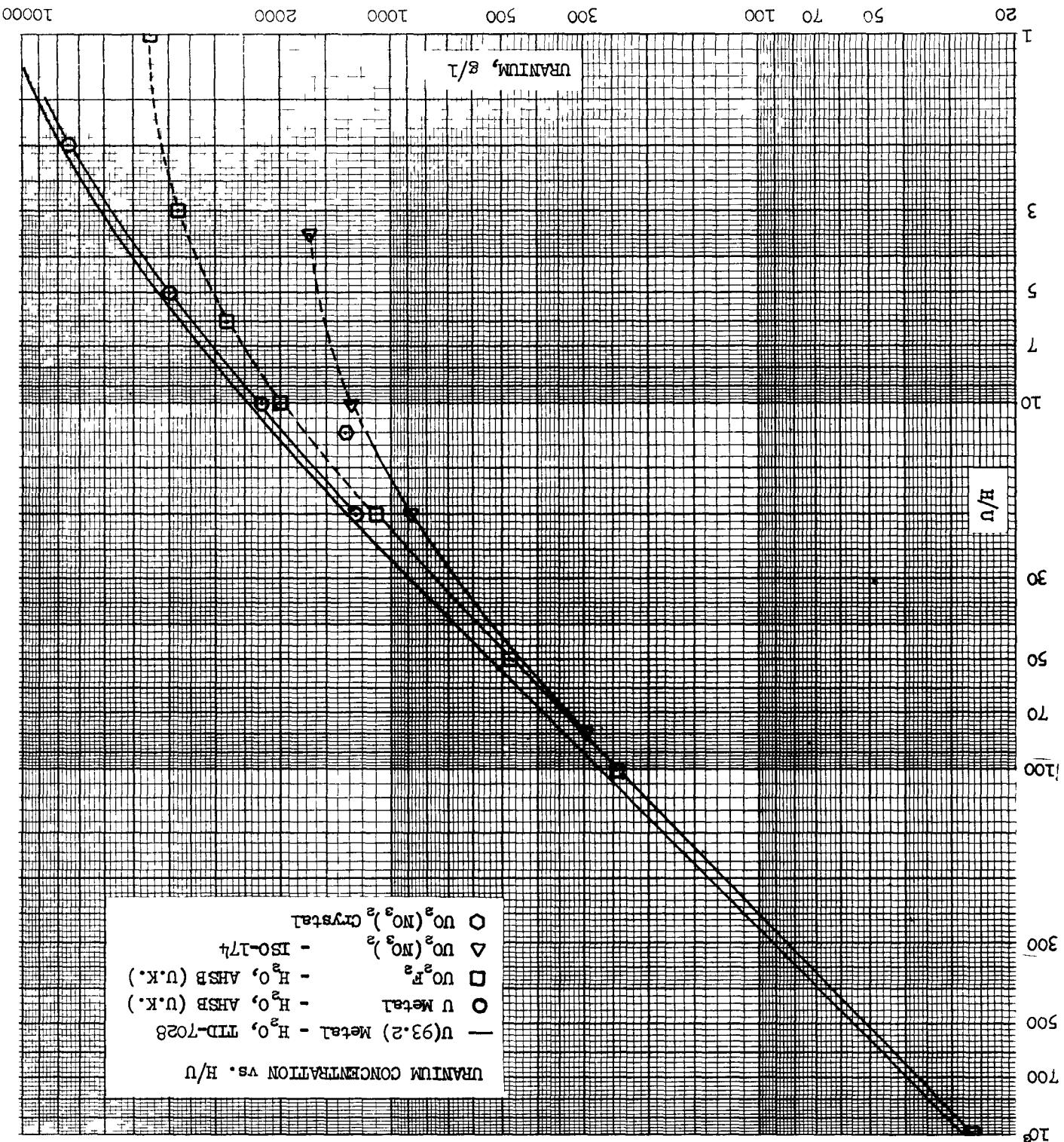
(4) K. D. Lathrop, "A Fortran IV Program for Solving the Multigroup Transport Equation with Anisotropic Scattering," LA-3376, 1965.

(5) J. H. Chalmers, et al, "Handbook of Criticality Data, Vol. 1," AHSB(S) Handbook 1, (1st Revision), 1967.

GAMTEC II - HFN and DTF IV calculations of critical experiments are listed below:

	K-Effective	
	GAMTEC-HFN	GAMTEC-DTF
<u>ORNL-TM-1195 U(4.98)O₂F₂ 901 g U/l</u>		
15.39" I.D. Cylinder 40.04" high	0.989	0.996
<u>ORNL-2968 U(4.89)₃O₈ In Sterotex 47.9 g U-235/l</u>		
Bare 24" x 24" x 18.8"	0.995	0.993
Full H ₂ O Reflection 20" x 20" x 13.1"	0.988	0.987
<u>ORNL-1926 U(93.2)O₂F₂</u>		
20" x 20" x 2.75" Full Reflection, 347.7 g U-235/l	0.9951	
6" I.D. Aluminum Cylinder 35.43" high, Full Reflection, 830.9 g U-235/l		1.0080
10" I.D. Aluminum Cylinder 5.17" high, Full Reflection, 830.9 g U-235/l		0.9773
10" I.D. Aluminum Cylinder 15.17" high, Bare, 830.9 g U-235/l		1.0028
<u>ORNL-3973 U(4.98)O₂F₂ 910.18 g U/l, Bare</u>		
19.99 I.D. stainless steel (.020") sphere		1.0041
15.5" I.D. stainless steel (.031") bare		1.0042
<u>ORNL-2367 U(93.2)O₂F₂ 331.4 g U-235/l, 10" O.D.</u>		
<u>Aluminum (4/16") Annular Tank, Full Reflection on Outside Except Top</u>		
4" I.D. filled with H ₂ O 9.37" high		0.9973
4" I.D. with air 10.87" high		1.0491
4" I.D. 20 mil Cd sheet & air 12.56" high		1.0300
4" I.D. 20 mil Cd sheet & H ₂ O 17.87" high		0.9754

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ARH-600

III.B.2-1

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III.B.2-2

ARH-600

1000

500

300

100

70

50

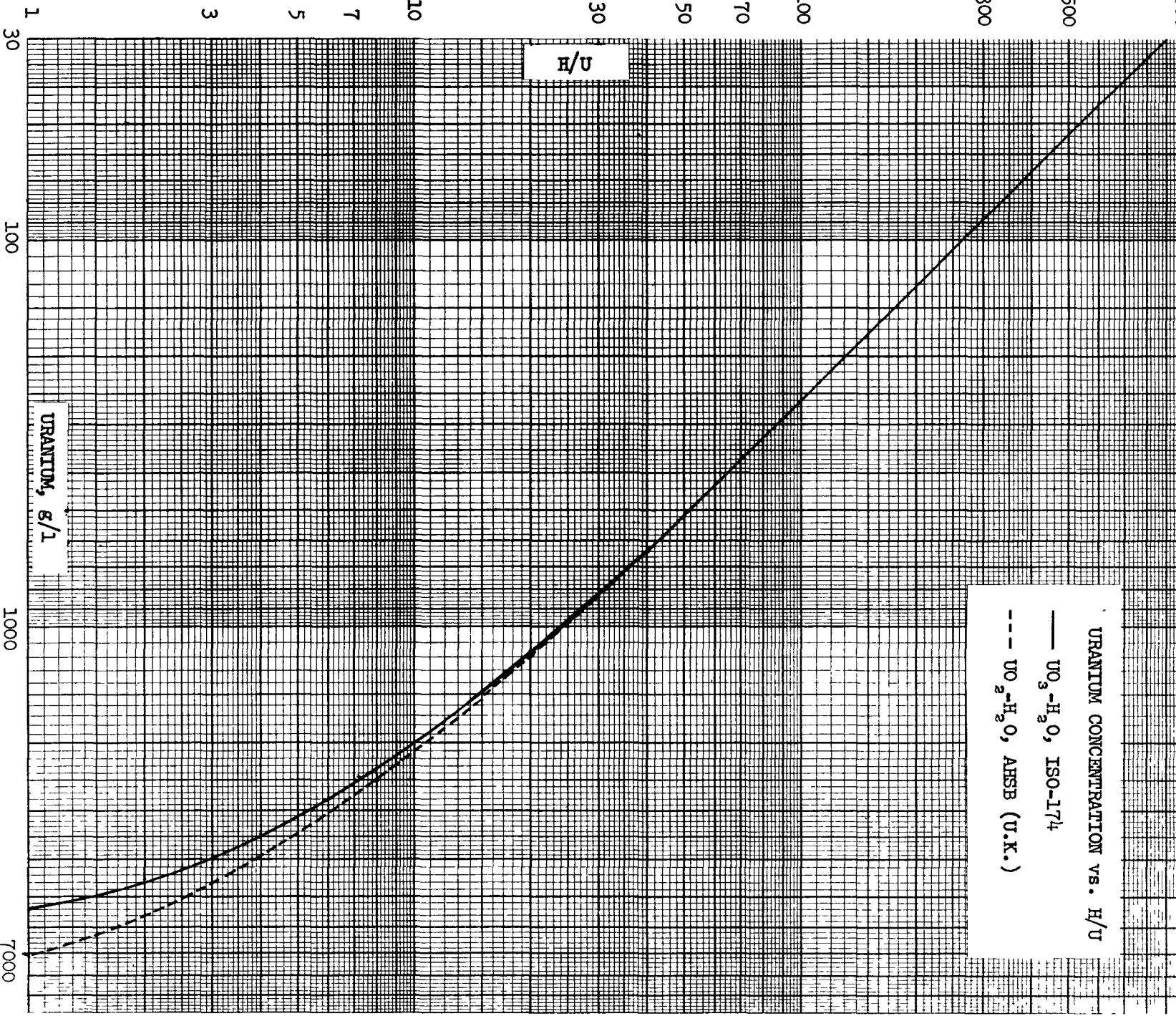
30

$\frac{U}{H}$

URANIUM CONCENTRATION vs. H/U

— UO_3-H_2O , ISO-17⁴

-- UO_2-H_2O , AHSB (U.K.)

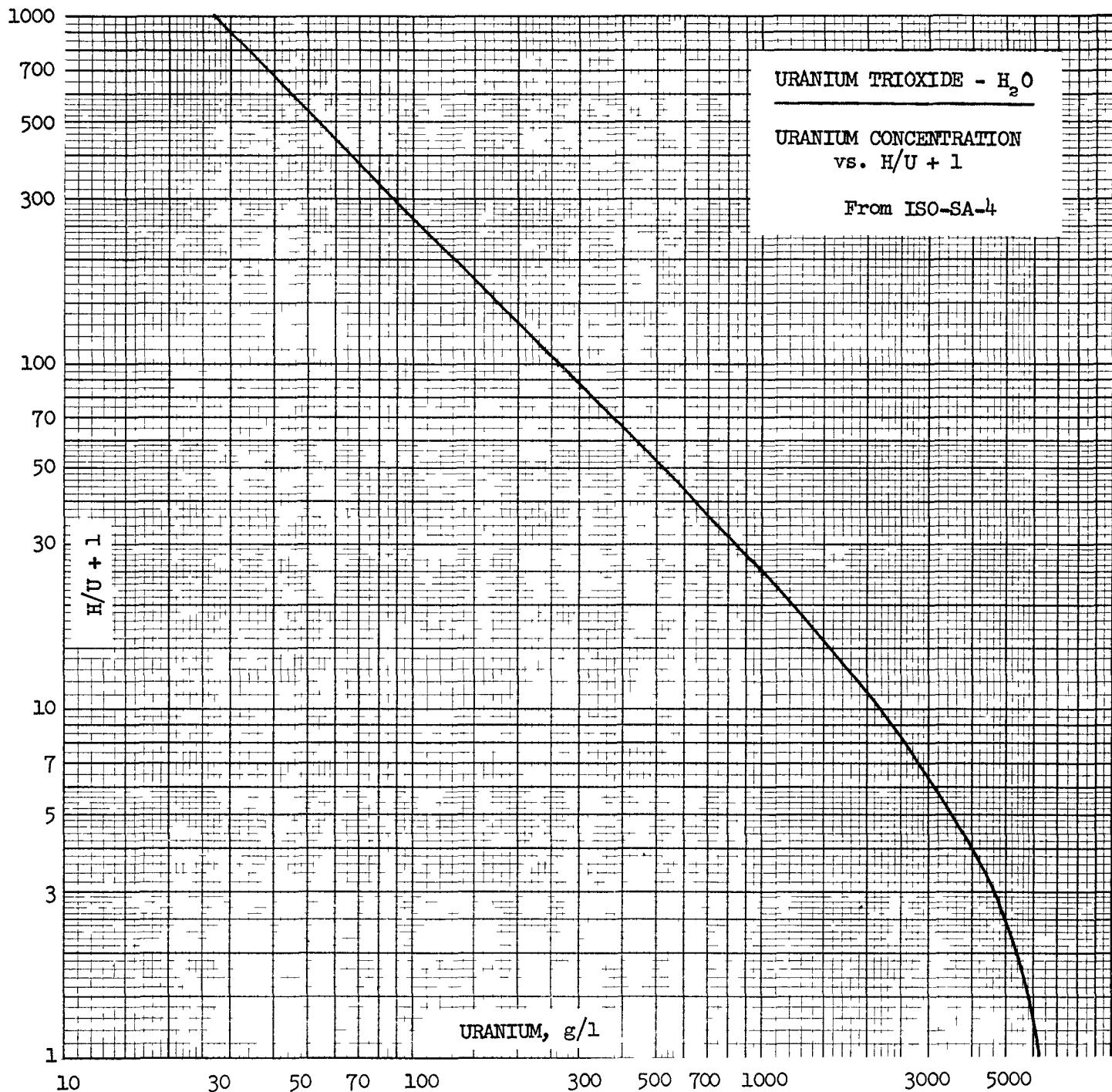


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III.B.2-3

ARH-600



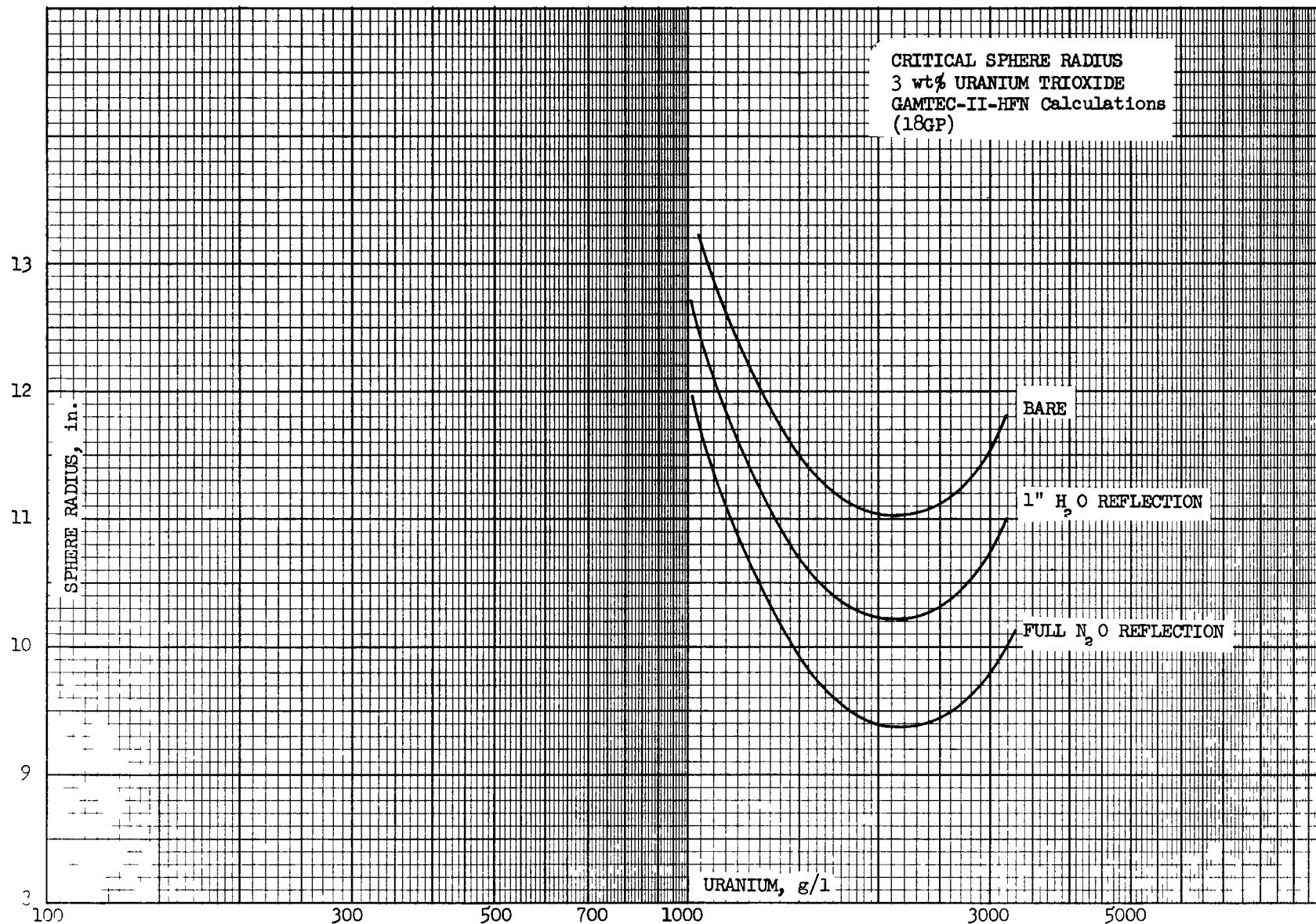
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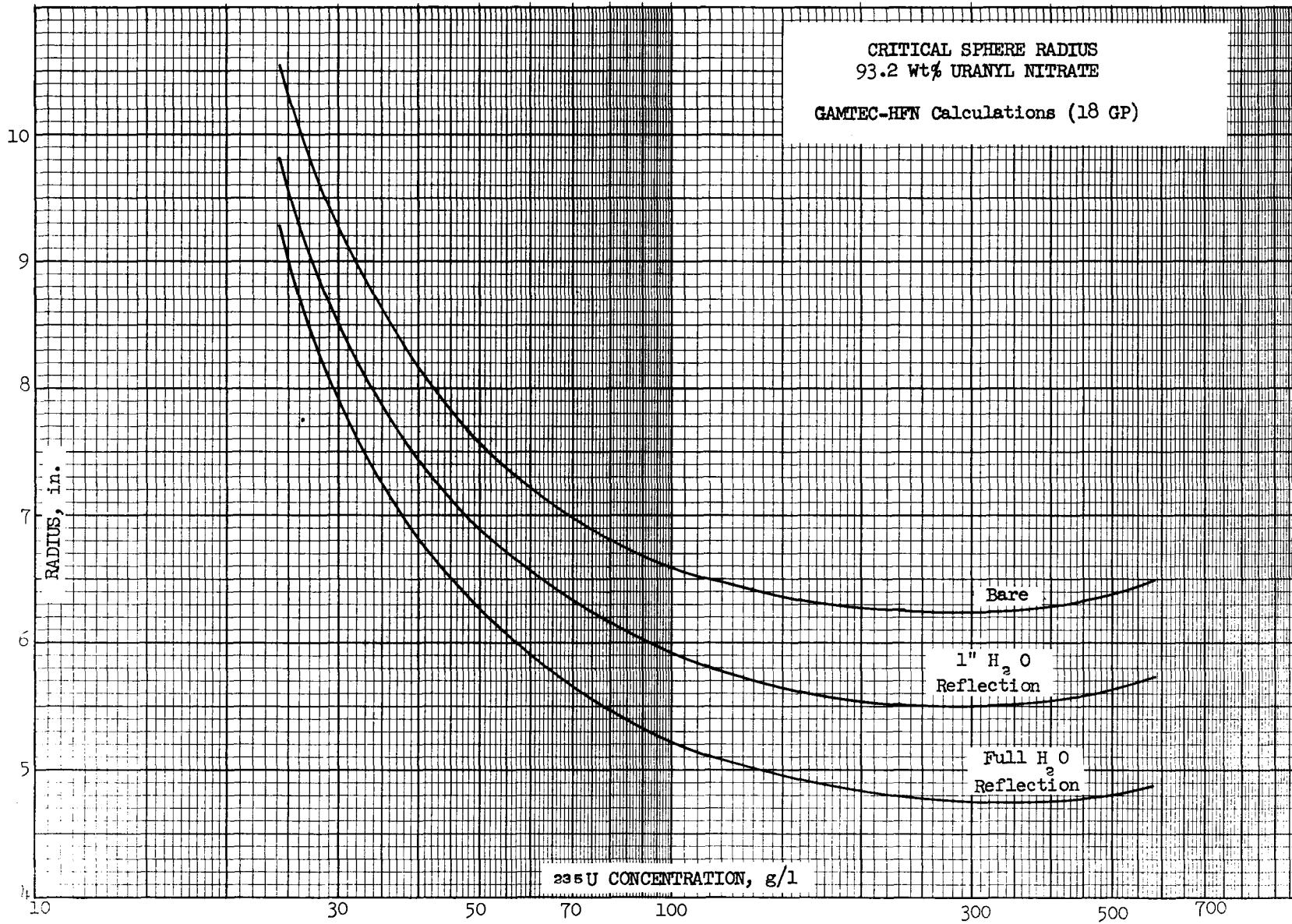
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III.B.3(3)-1

000-HRAY

CRITICAL SPHERE RADIUS
3 wt% URANIUM TRIOXIDE
GAMTEC-II-HFN Calculations
(18GP)

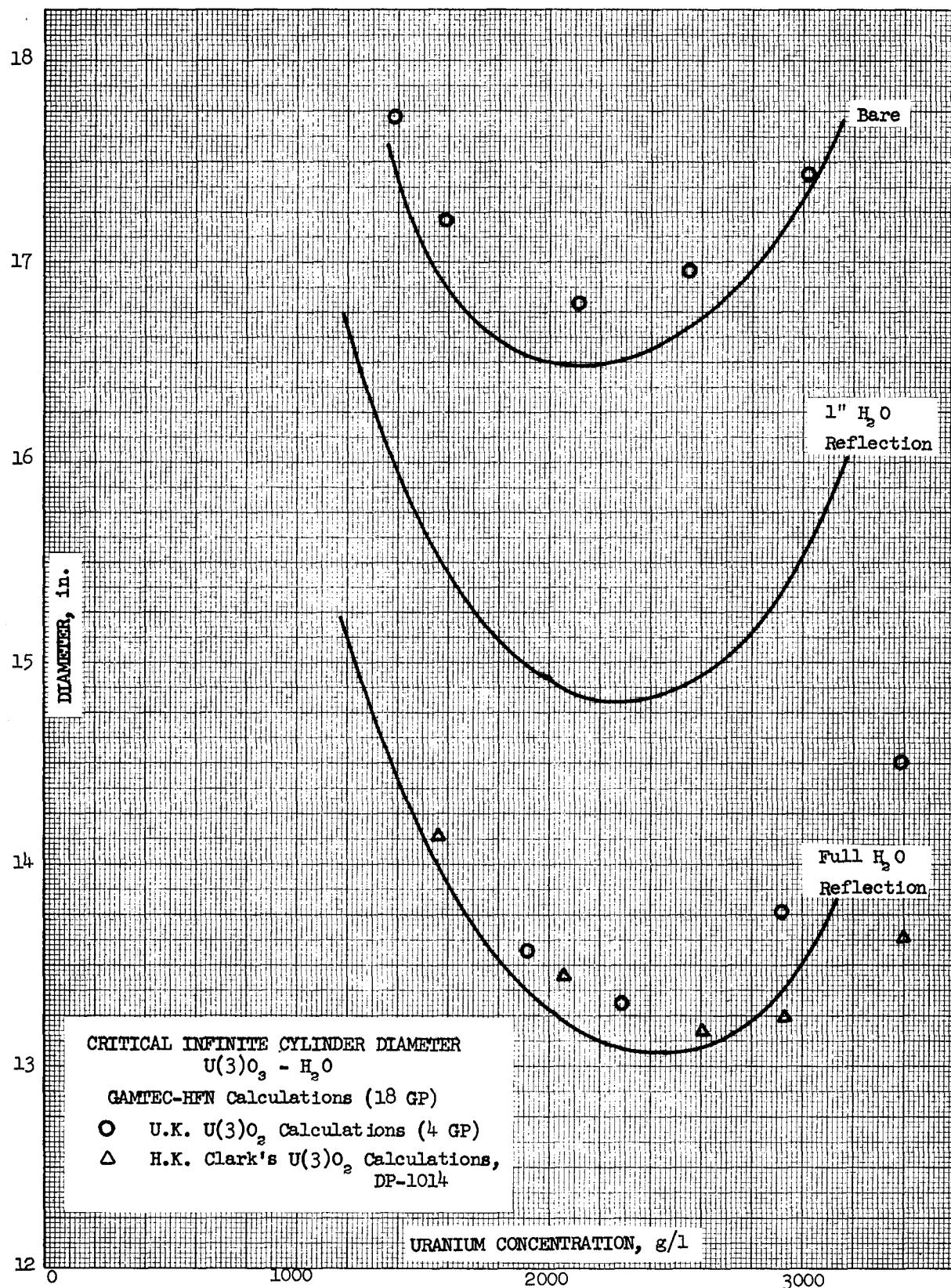




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III.B.3(93)-1

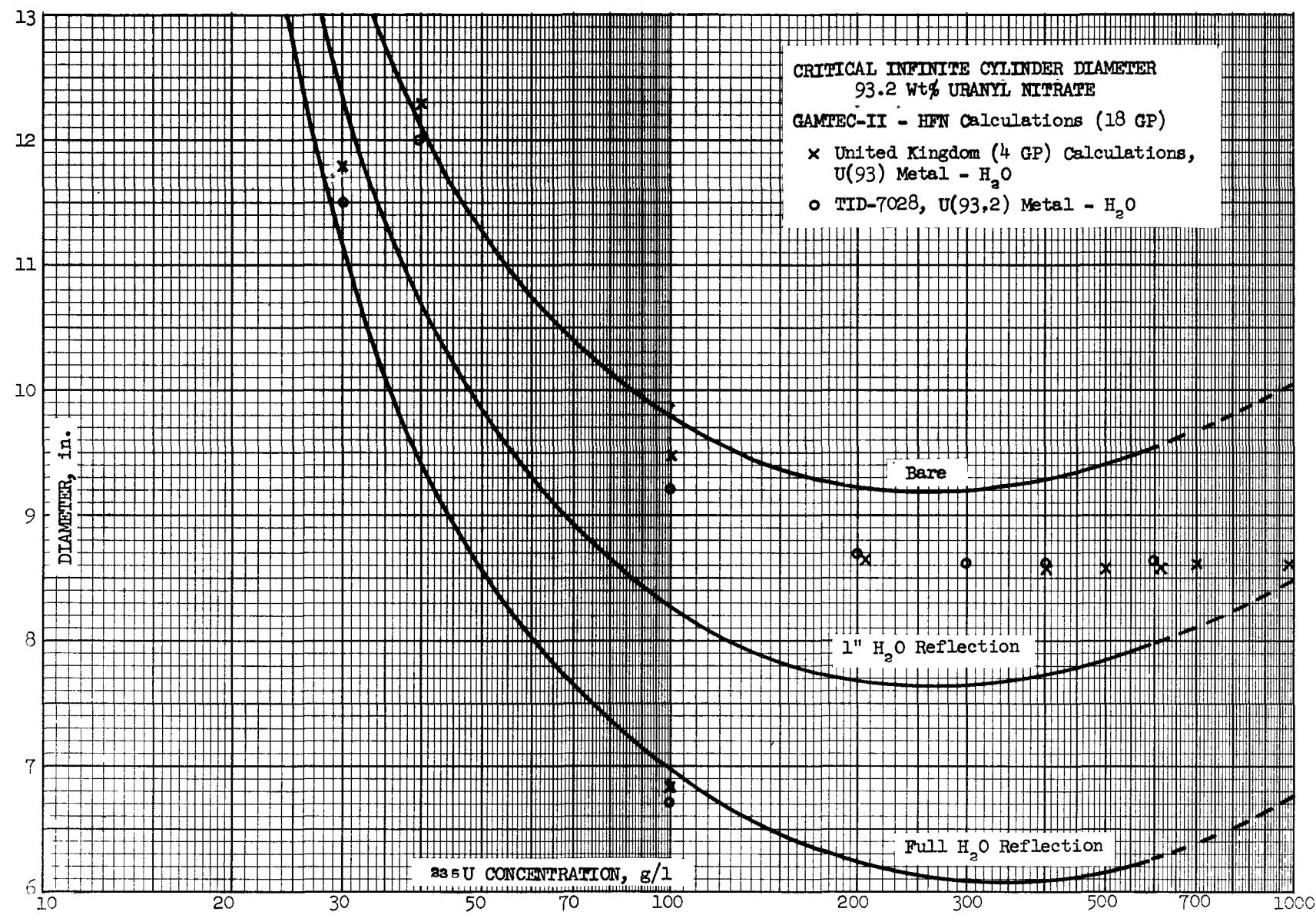
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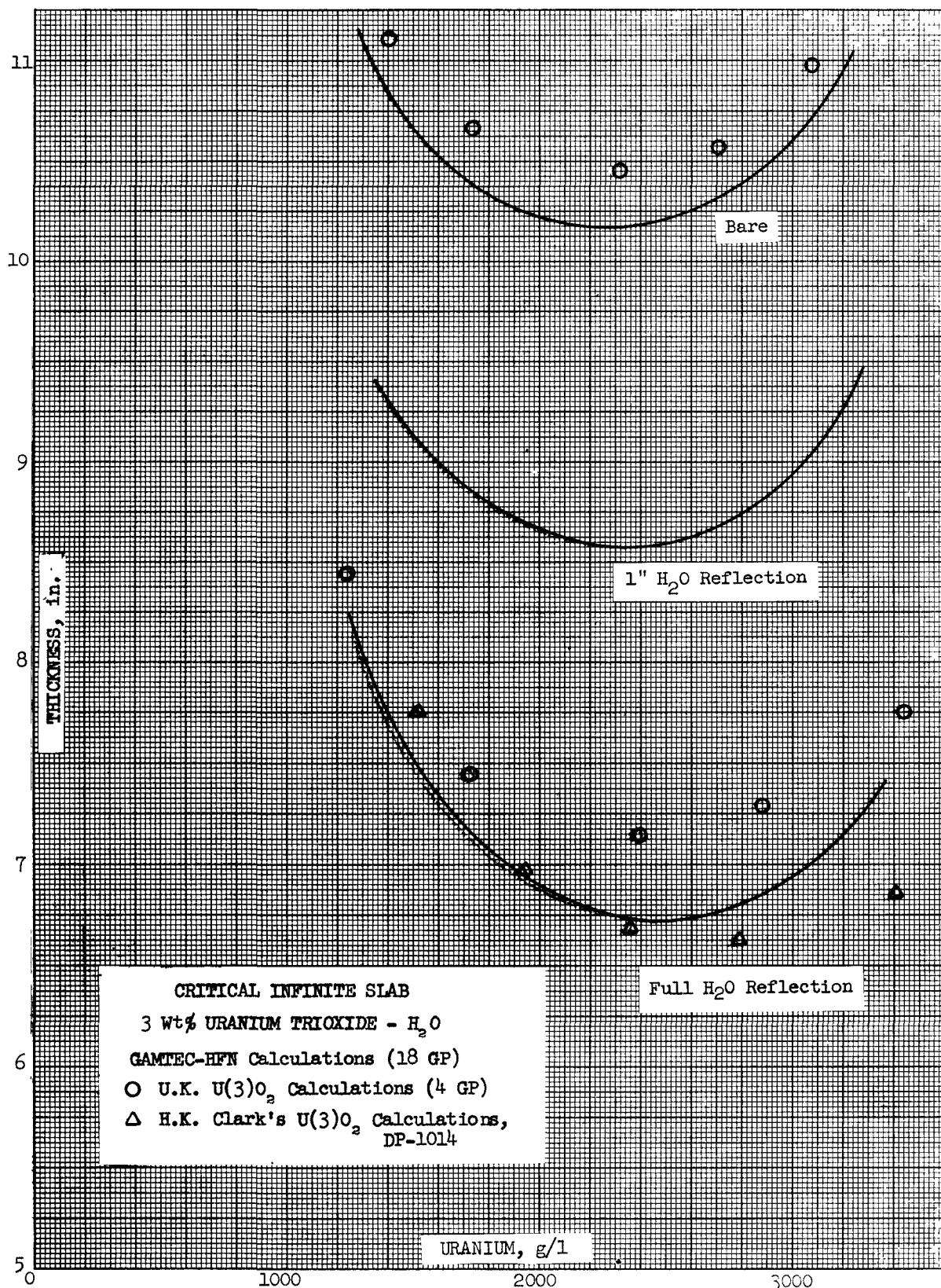


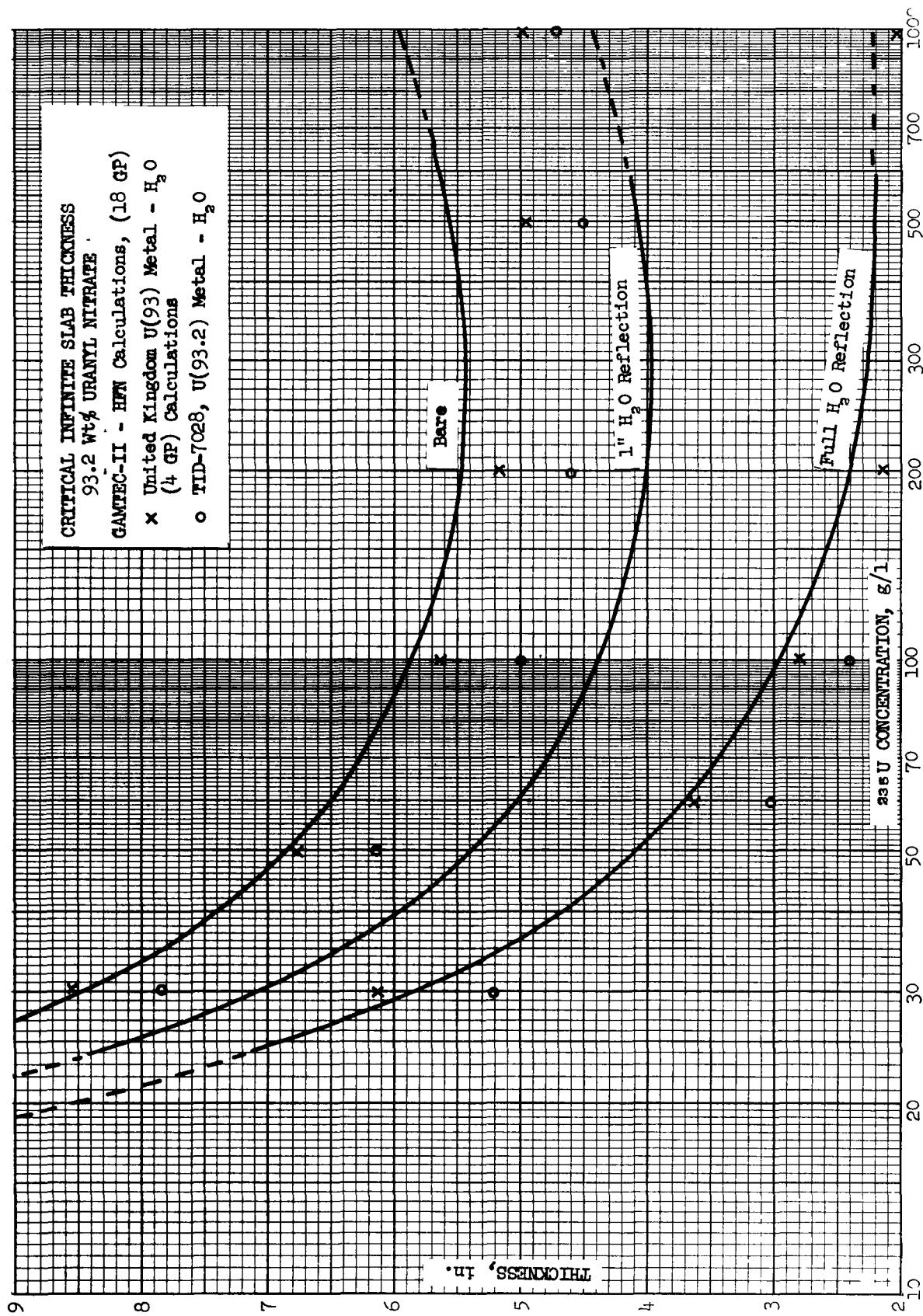
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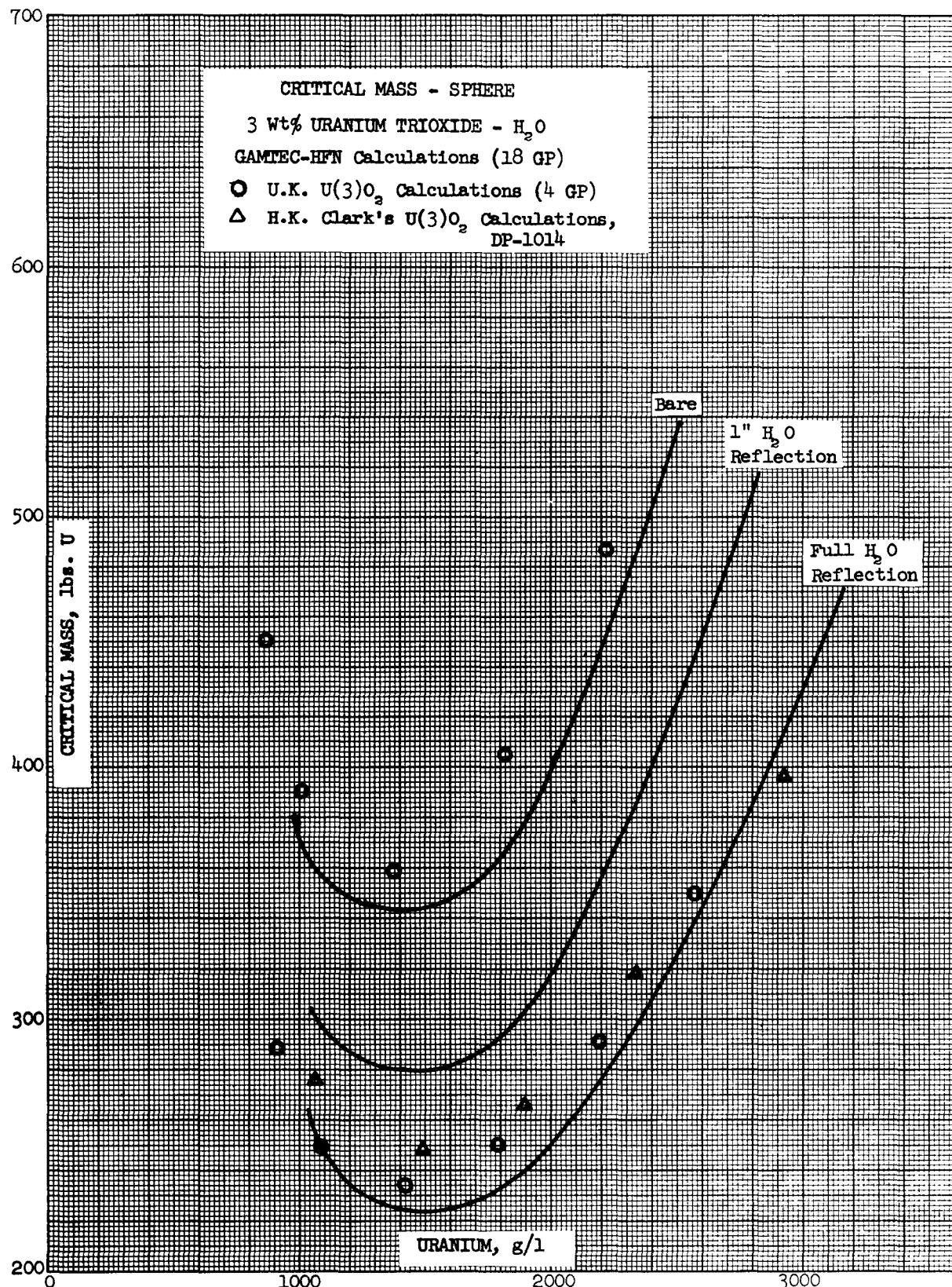
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ARL-7C





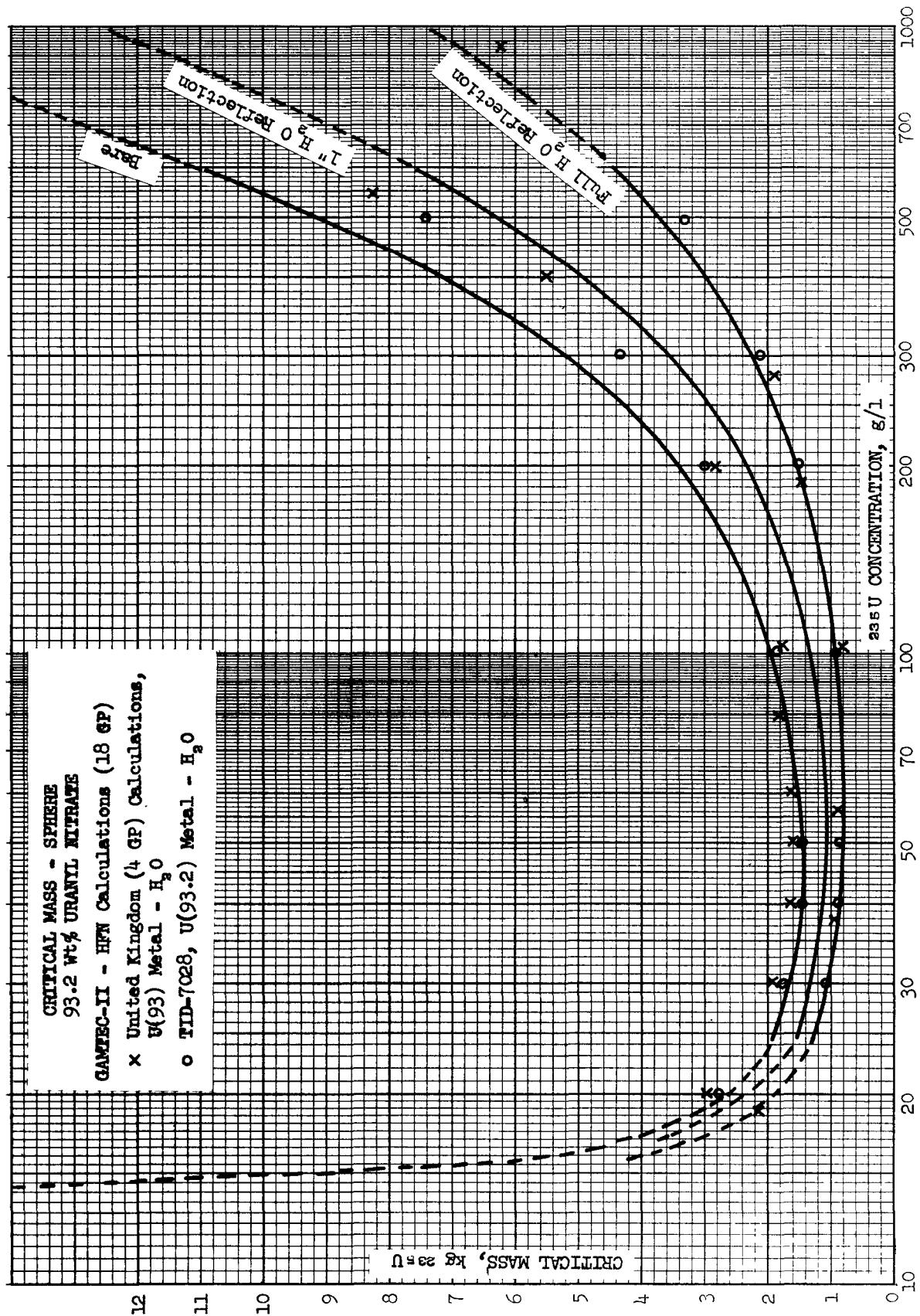




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III.B.6(93)-1

ARH-600

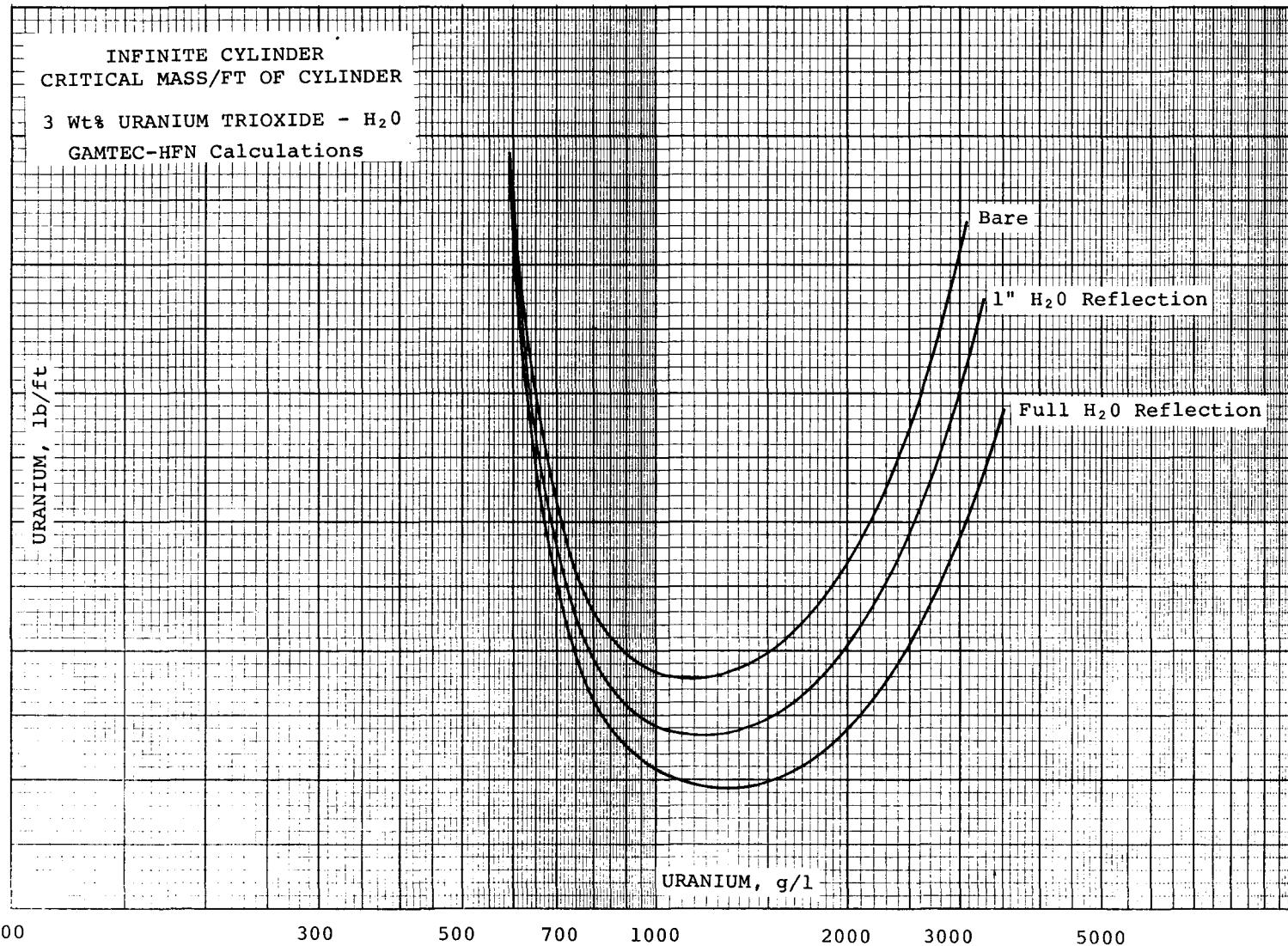


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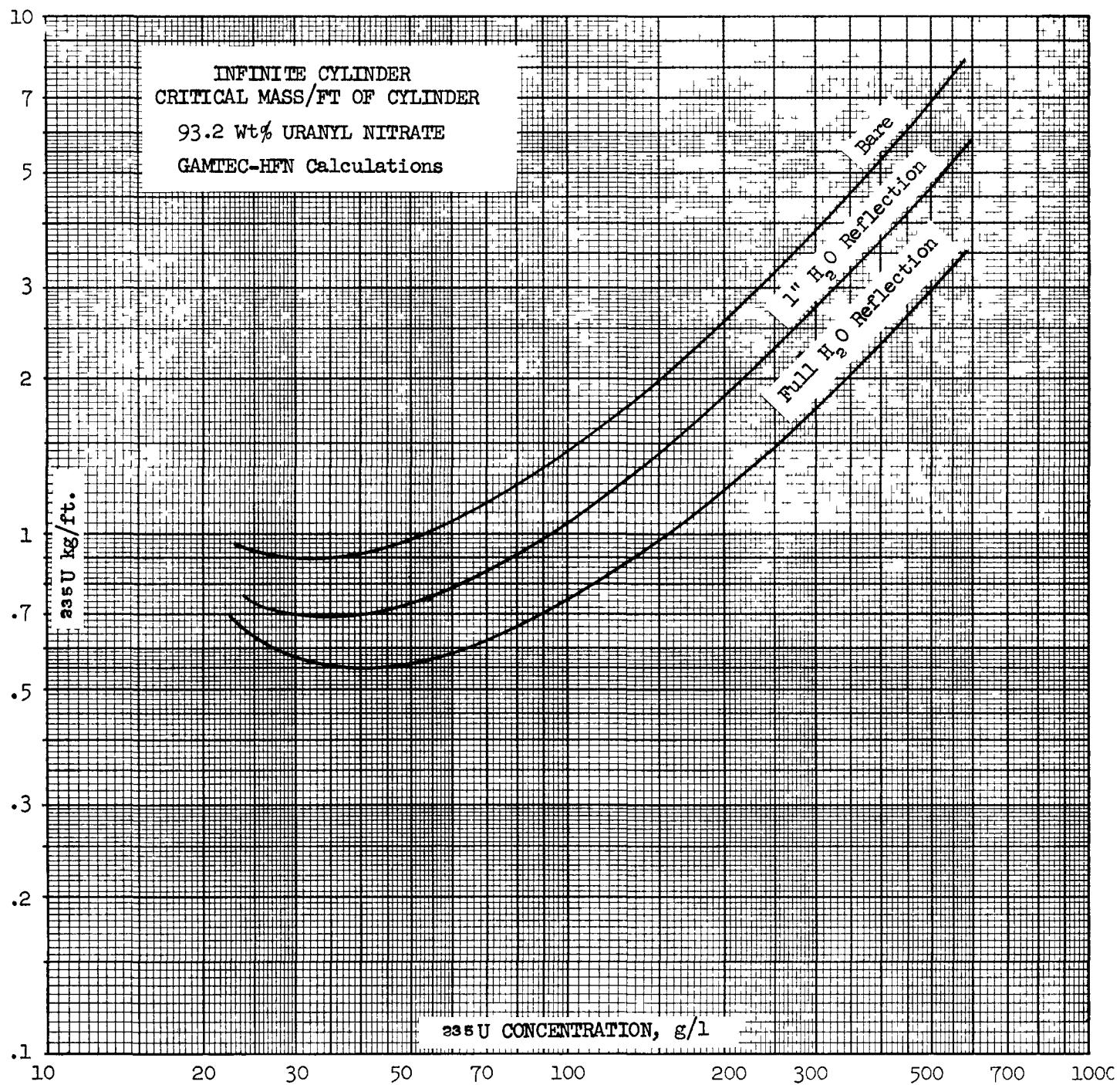
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ARH-600



Revised - 7/10/69

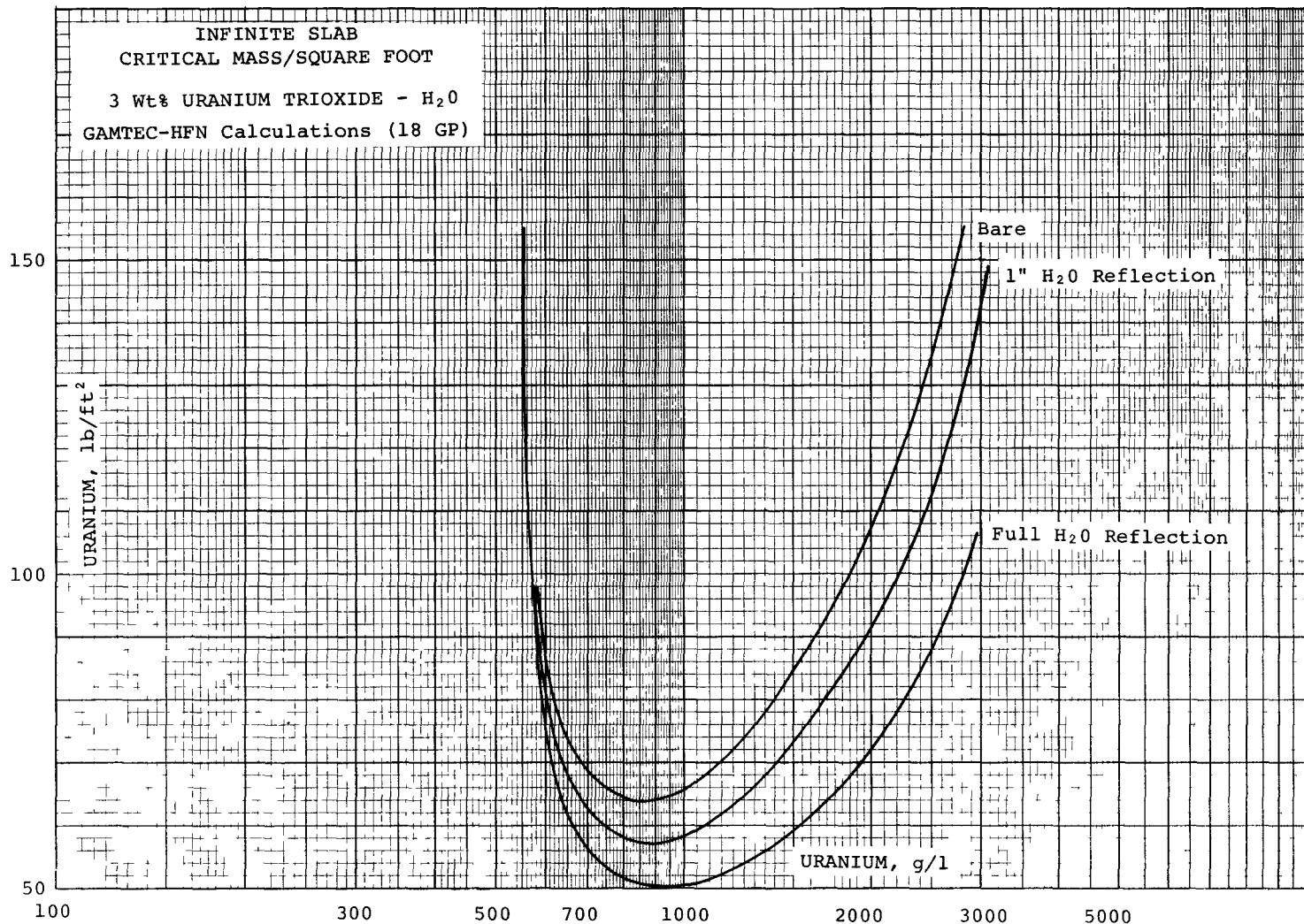
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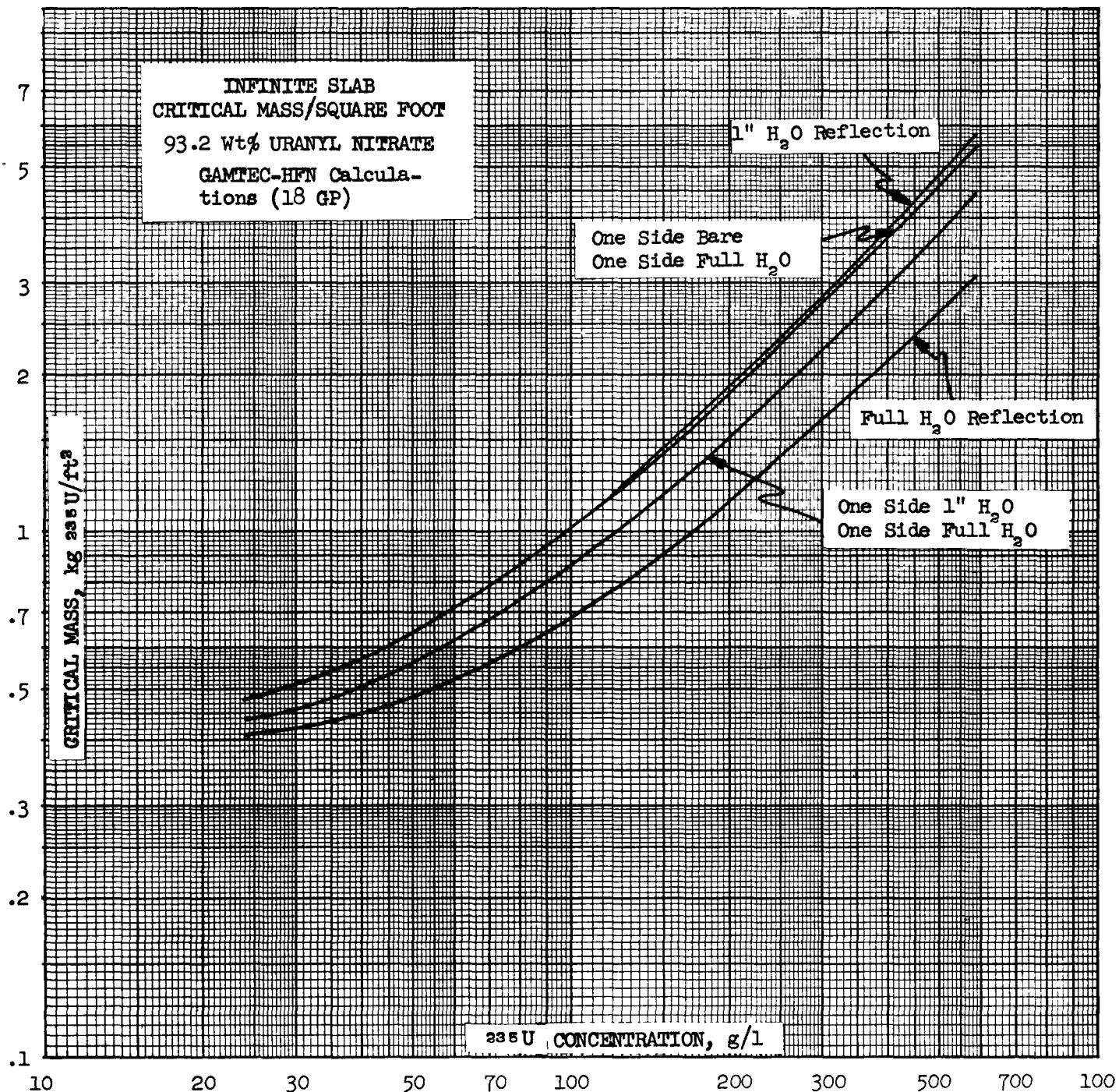
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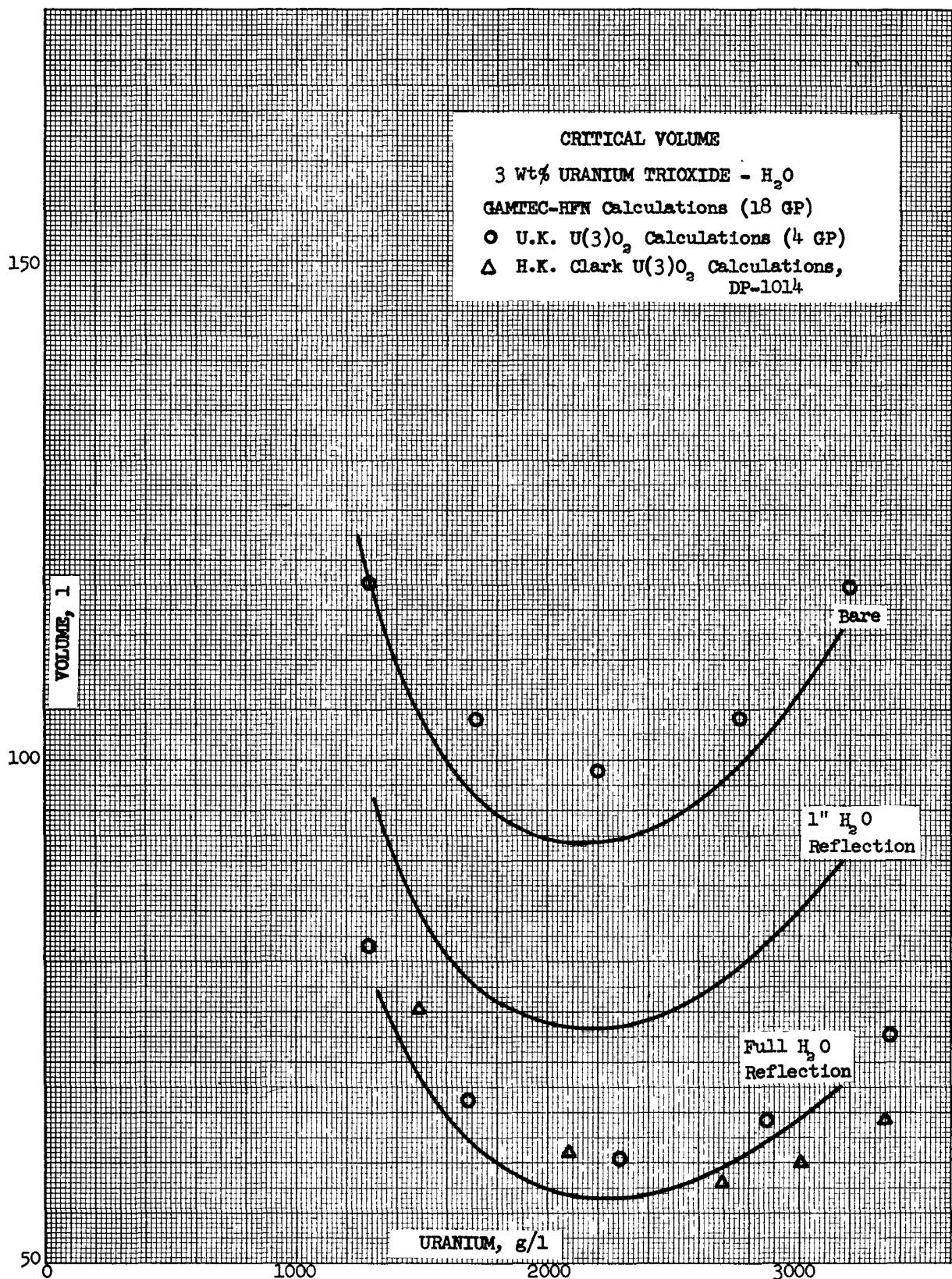
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Revised - 7/10/69

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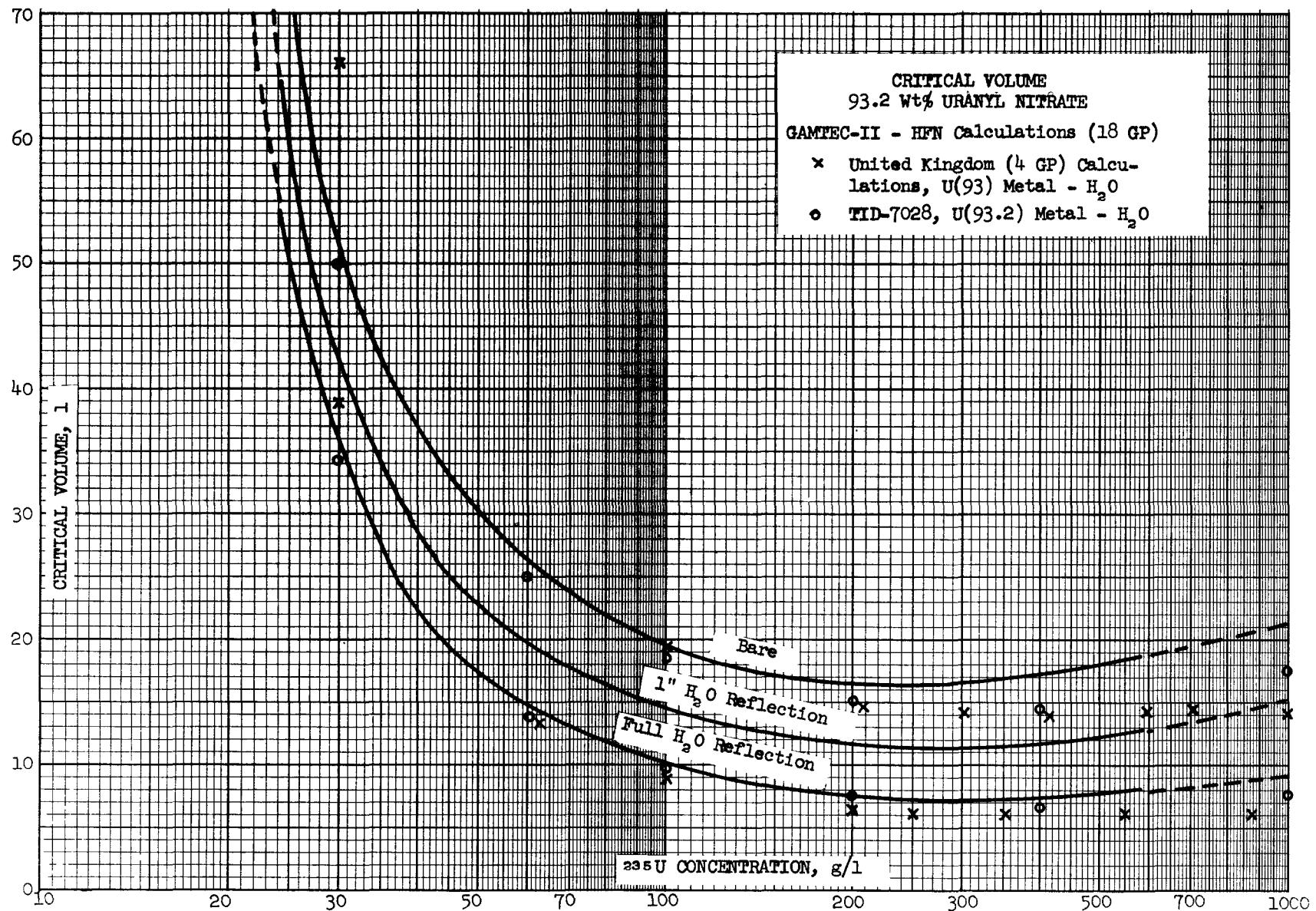




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III.B.9(93)-1

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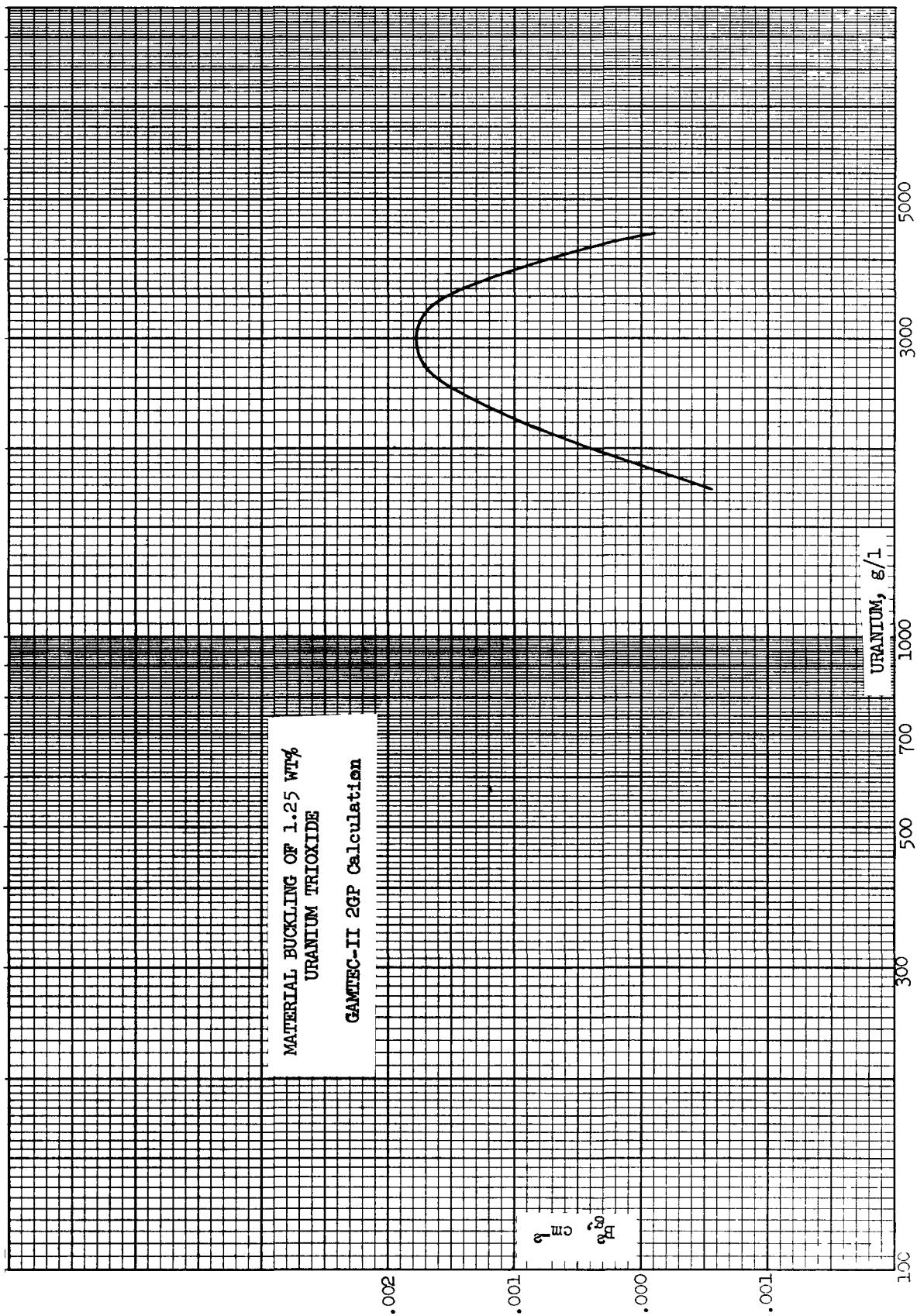


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III.B.10(1.25)-1

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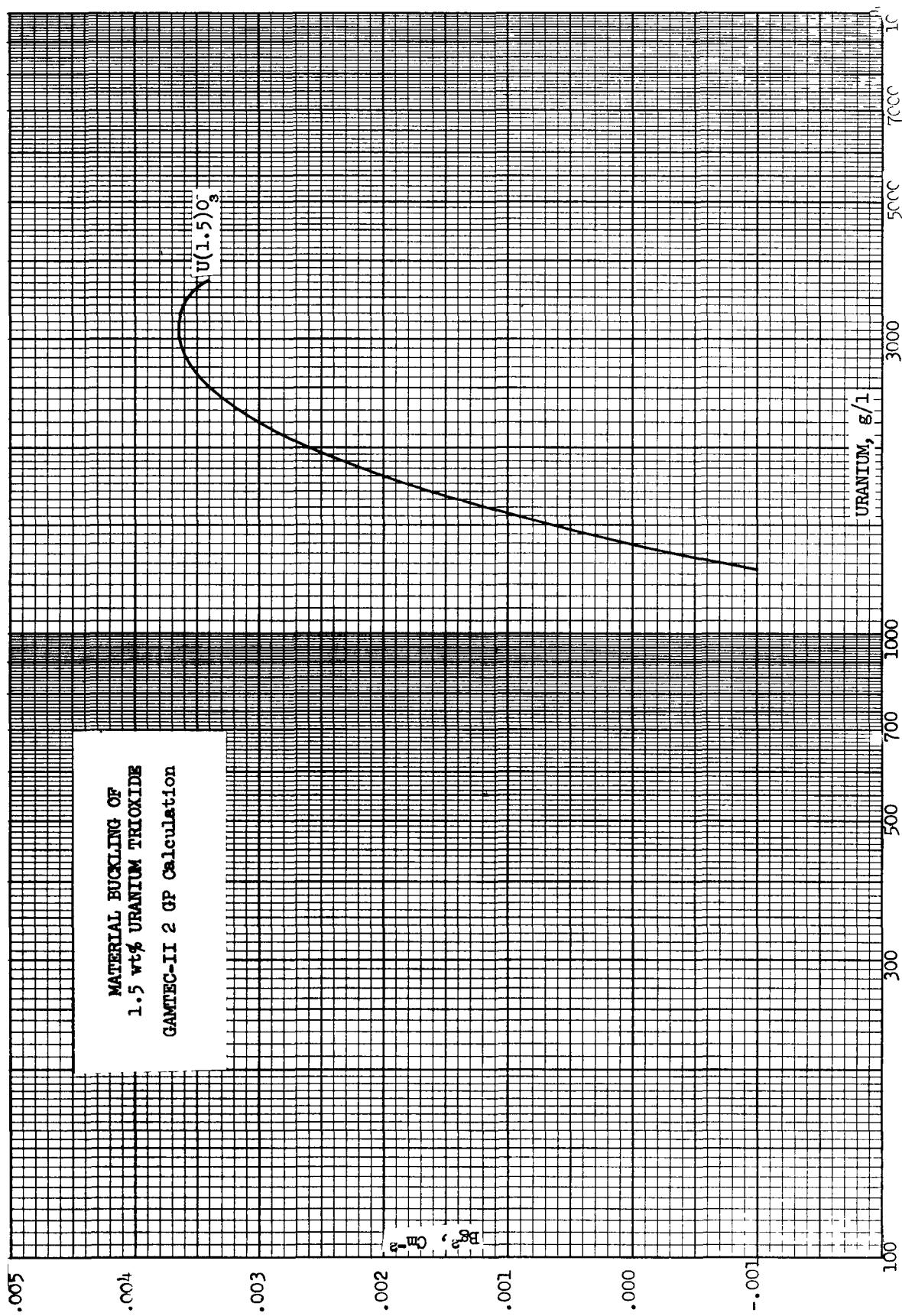


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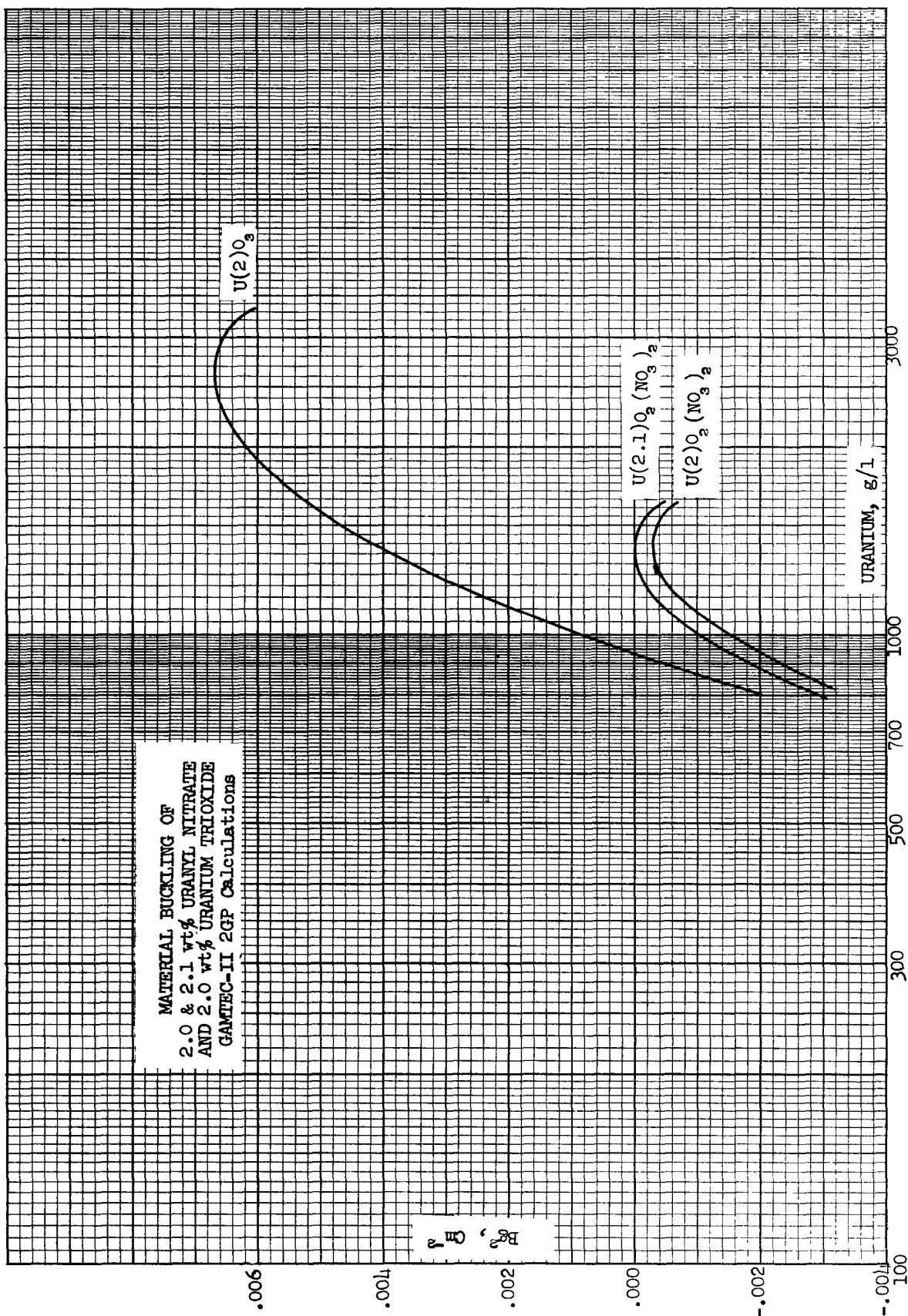
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III.B.10(1.5)-1

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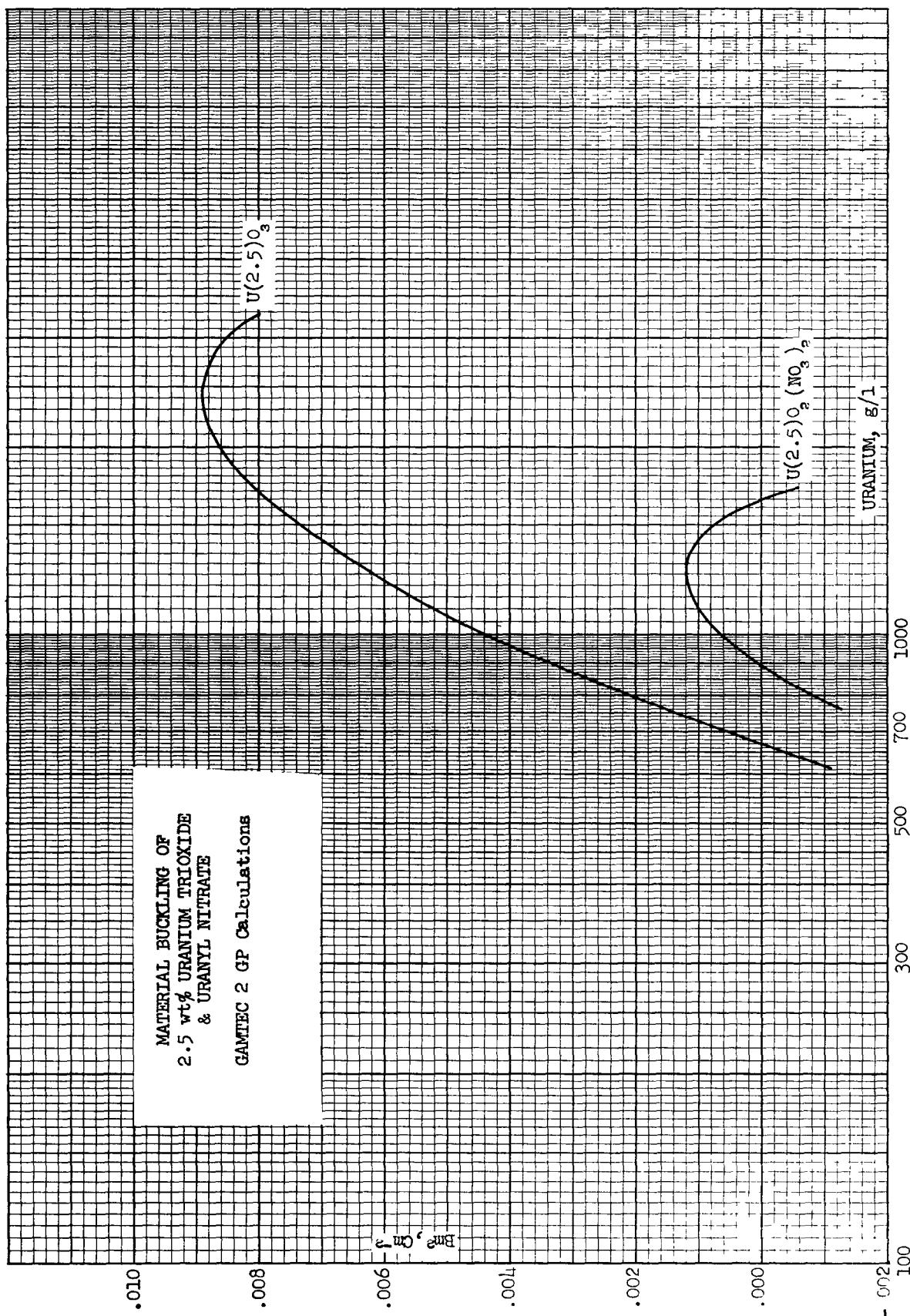
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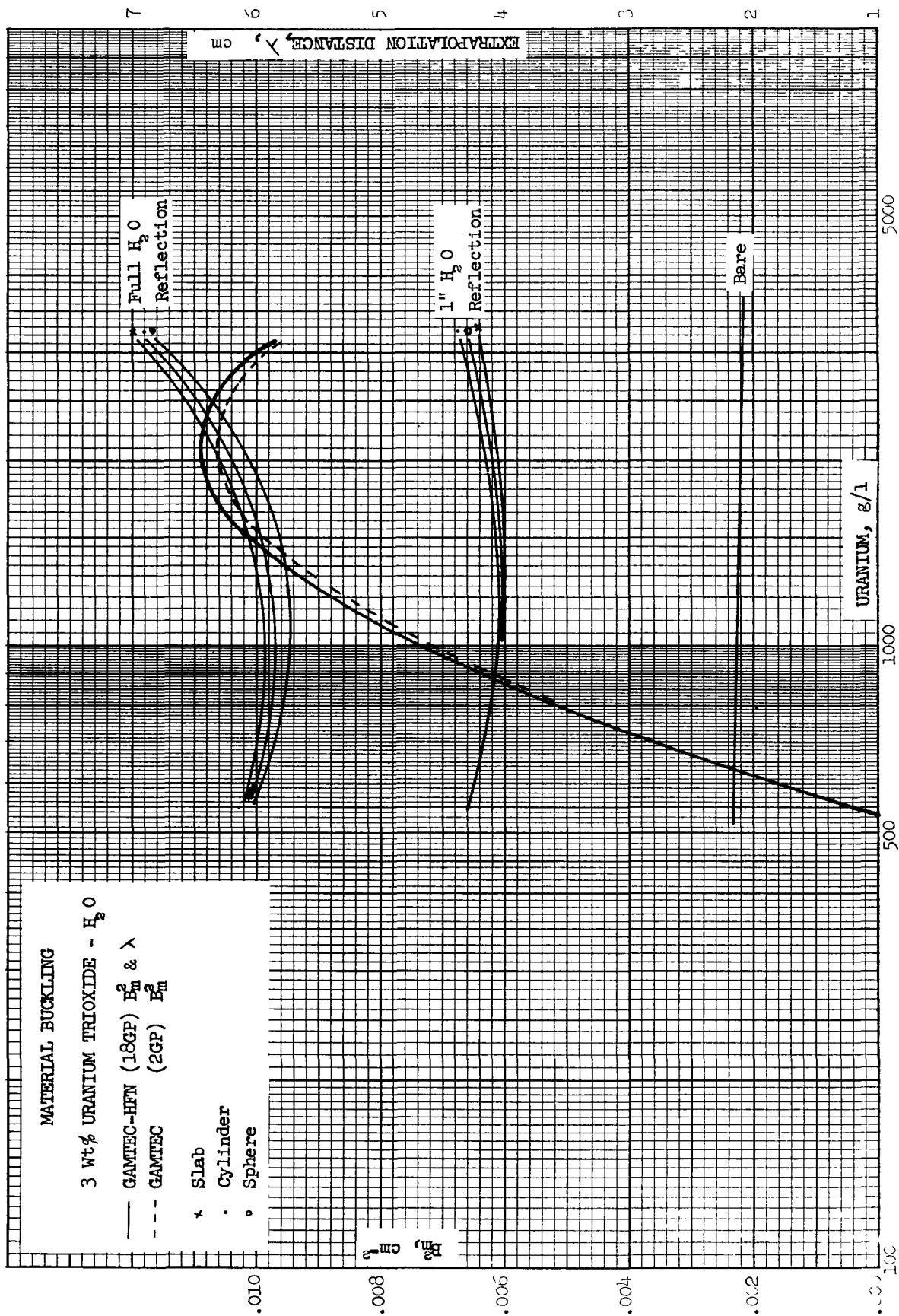
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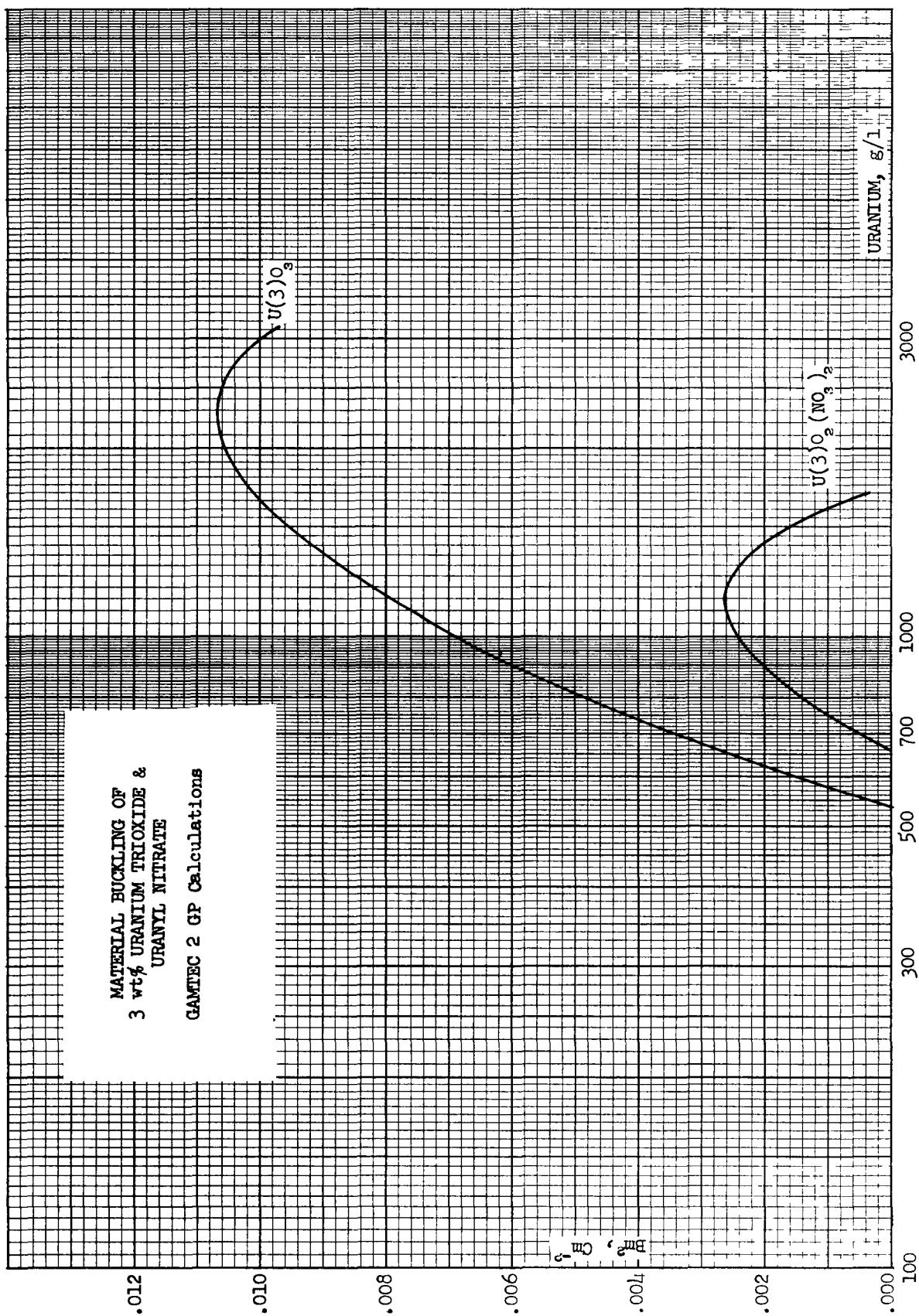
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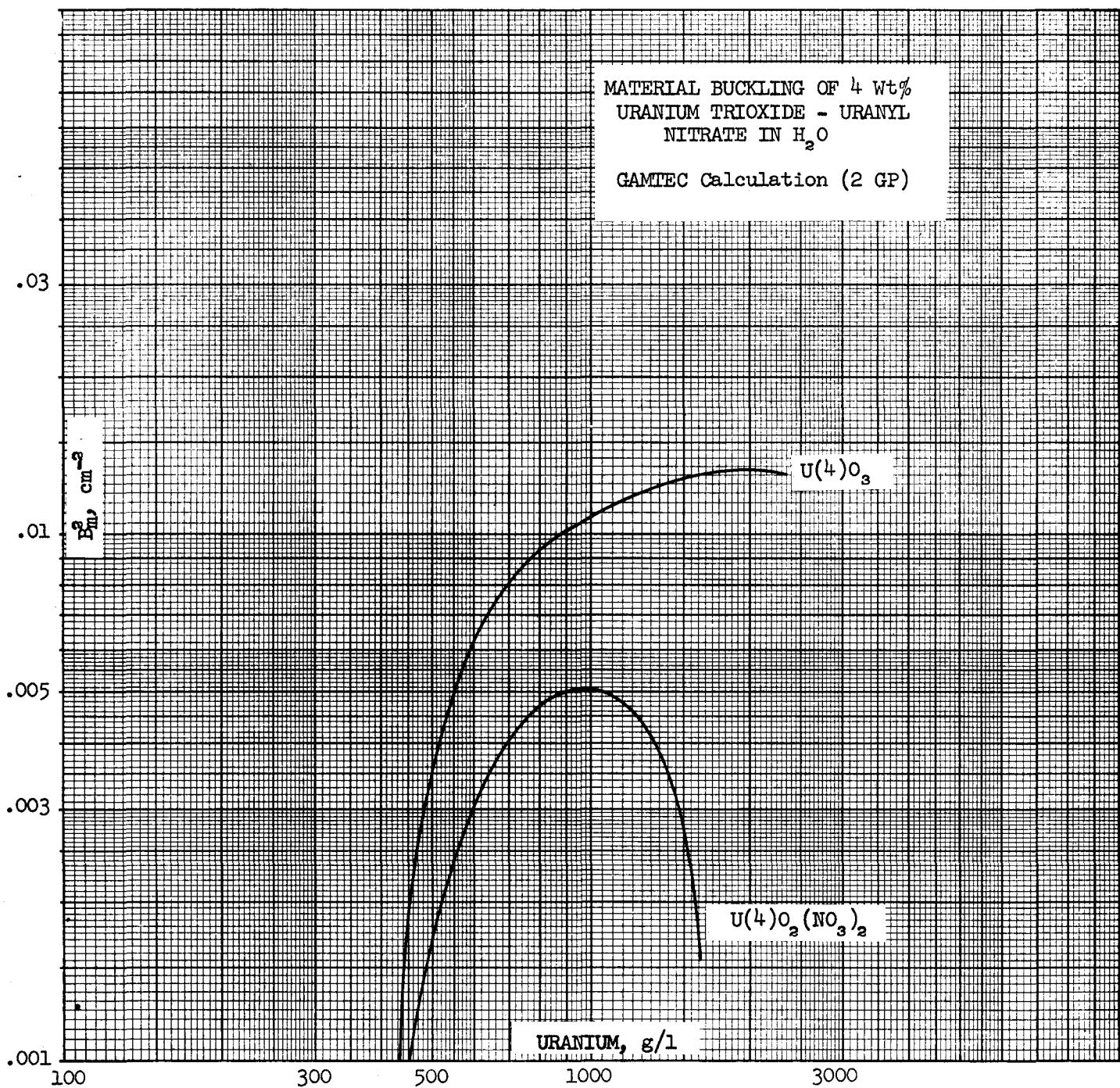
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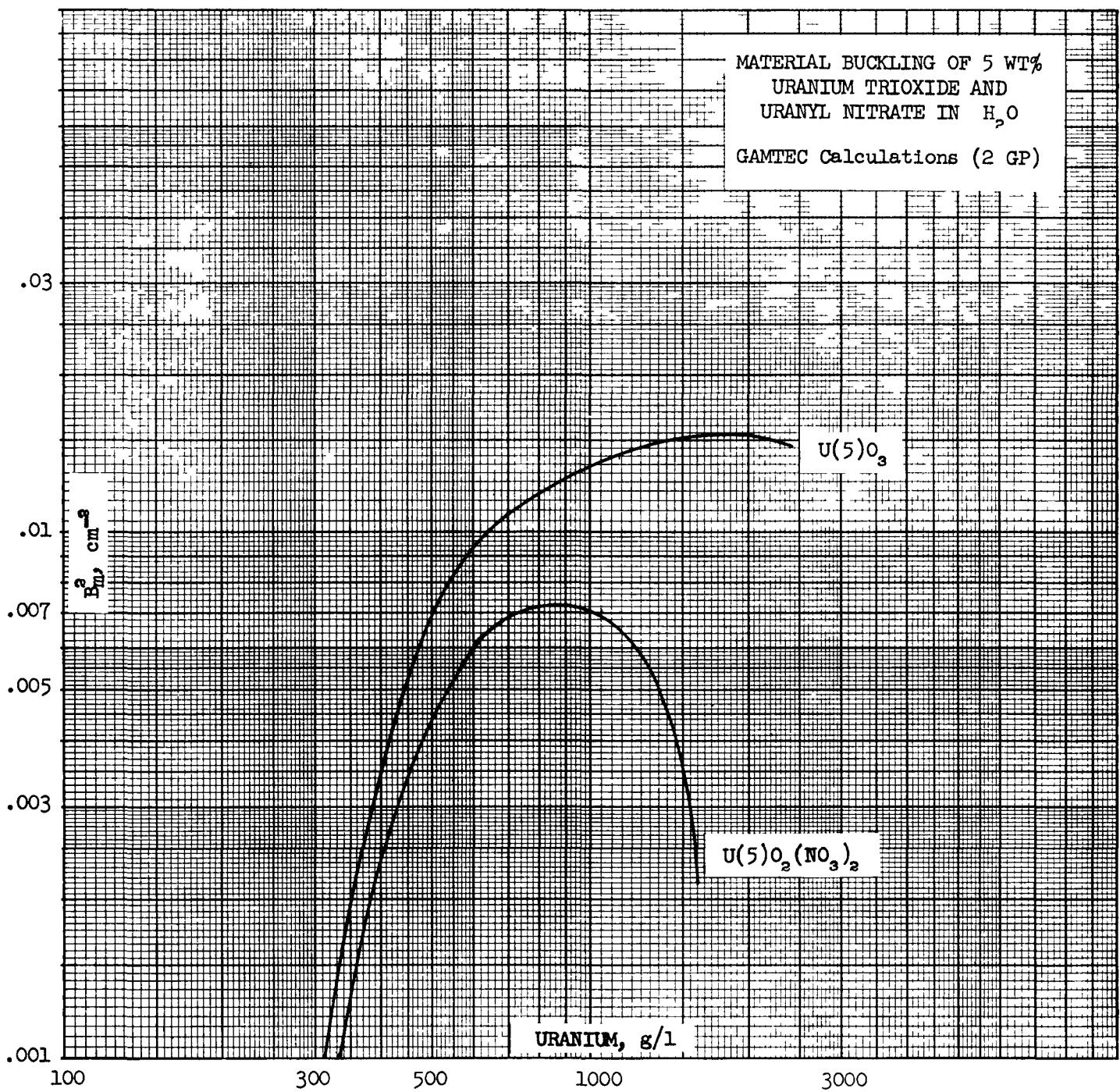


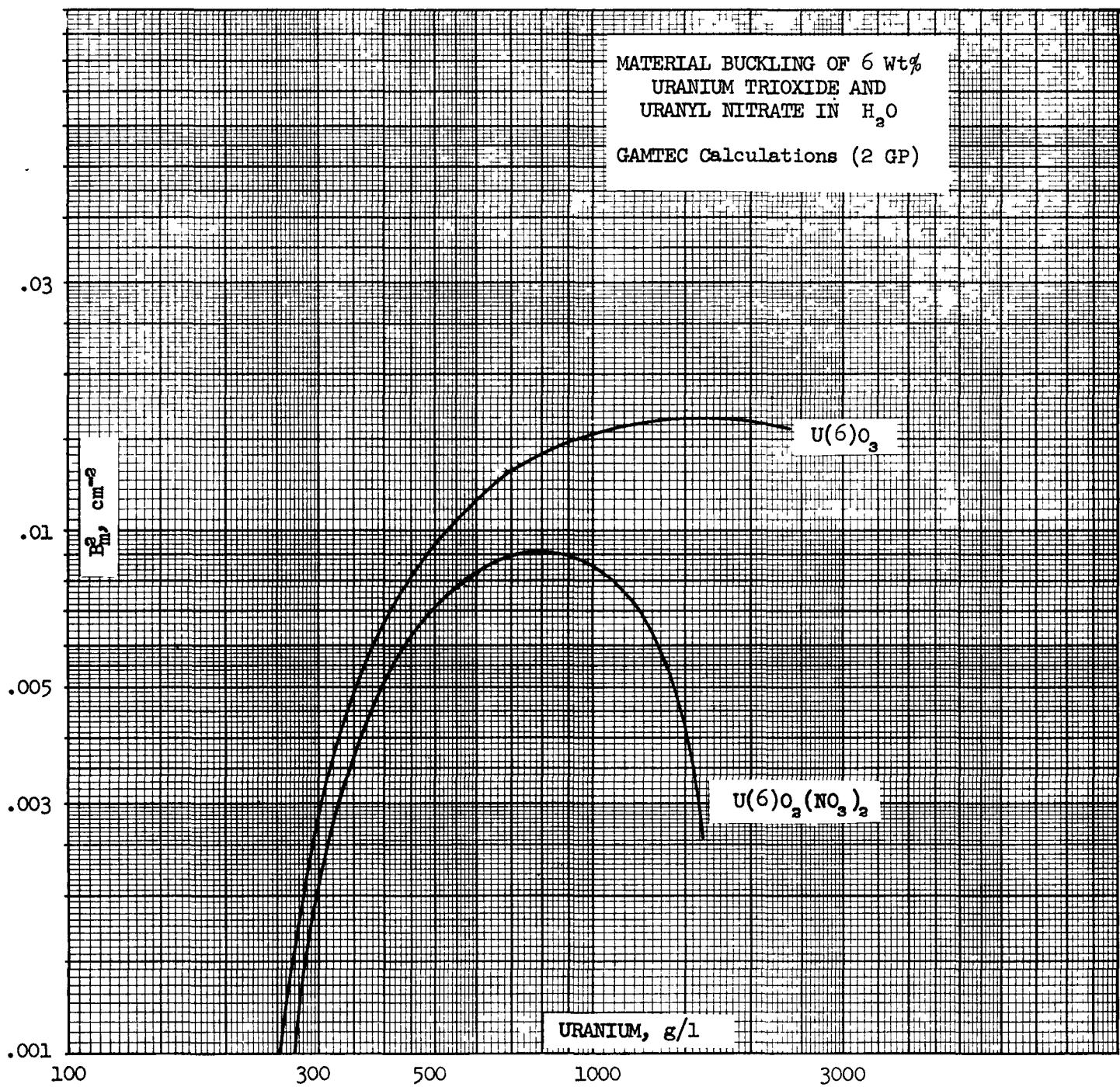
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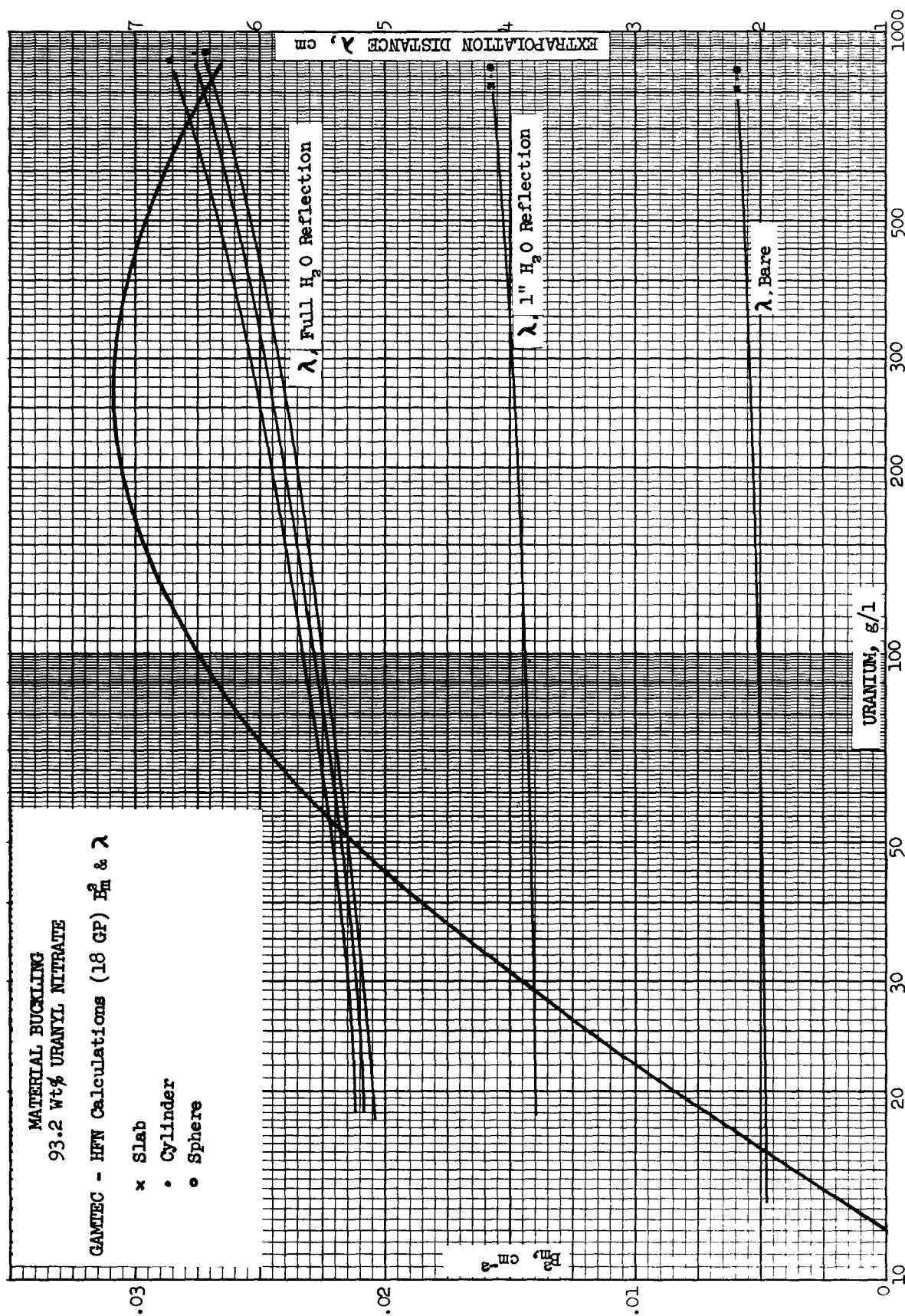




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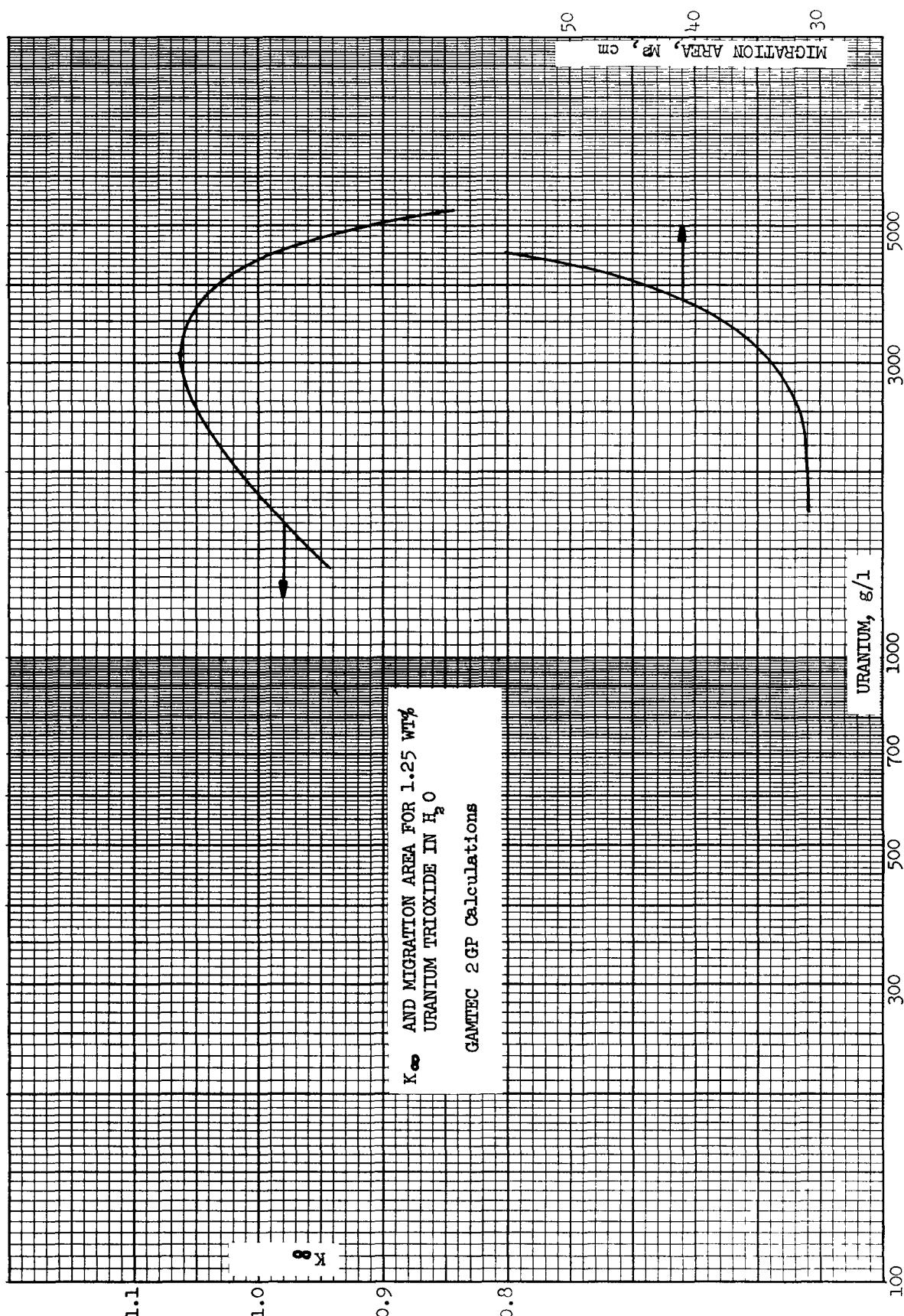


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III.B.11(1.25)-1

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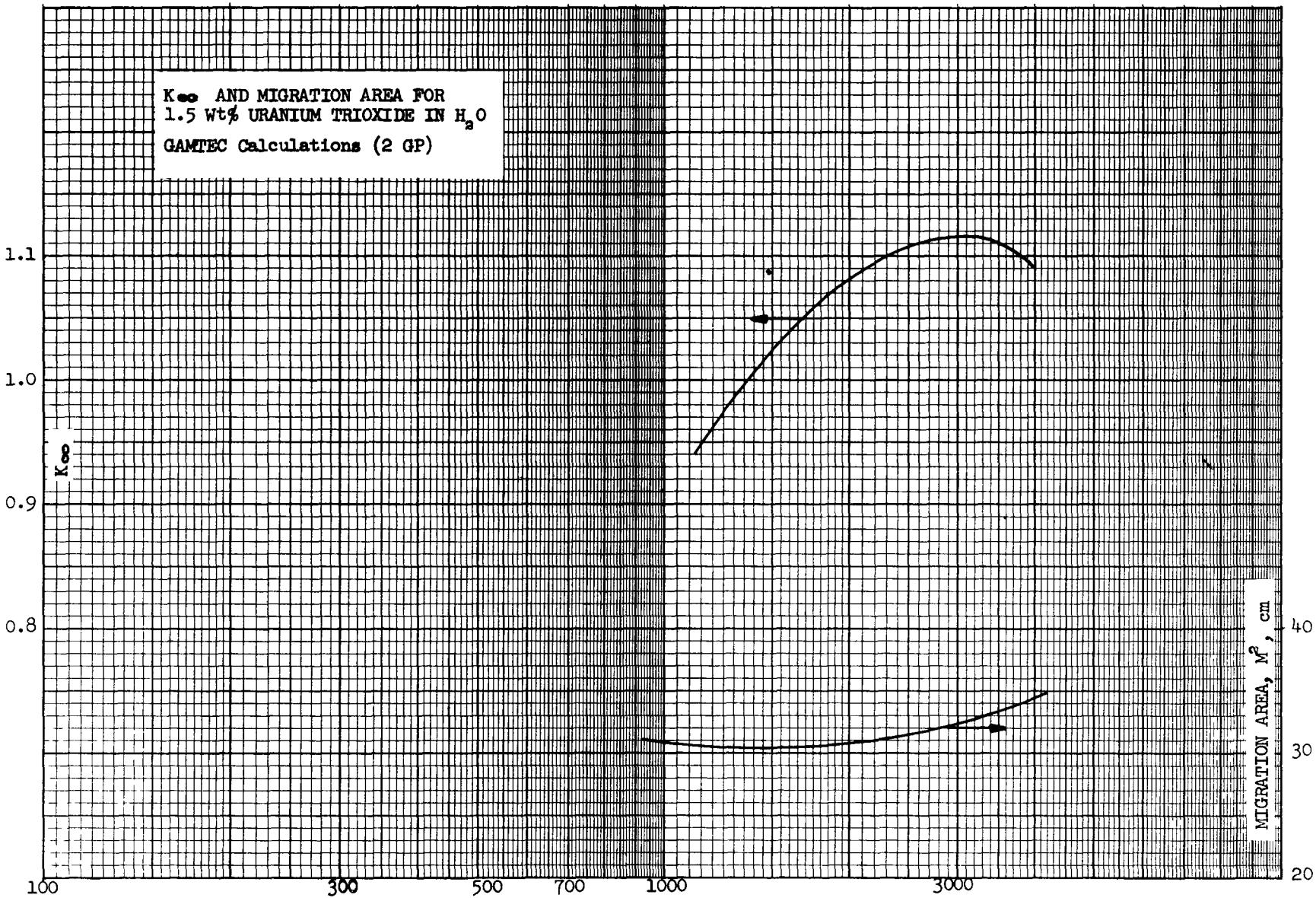


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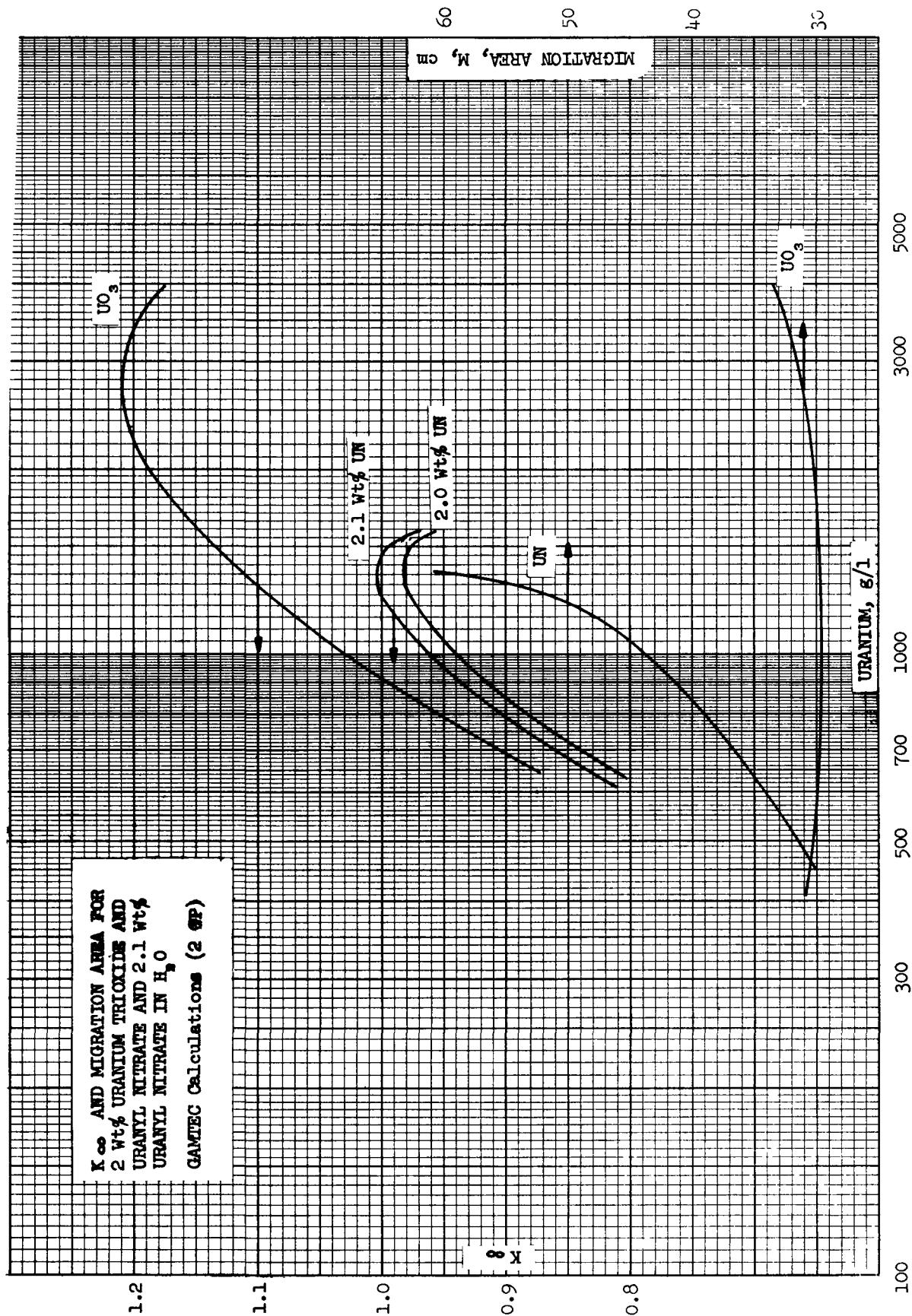
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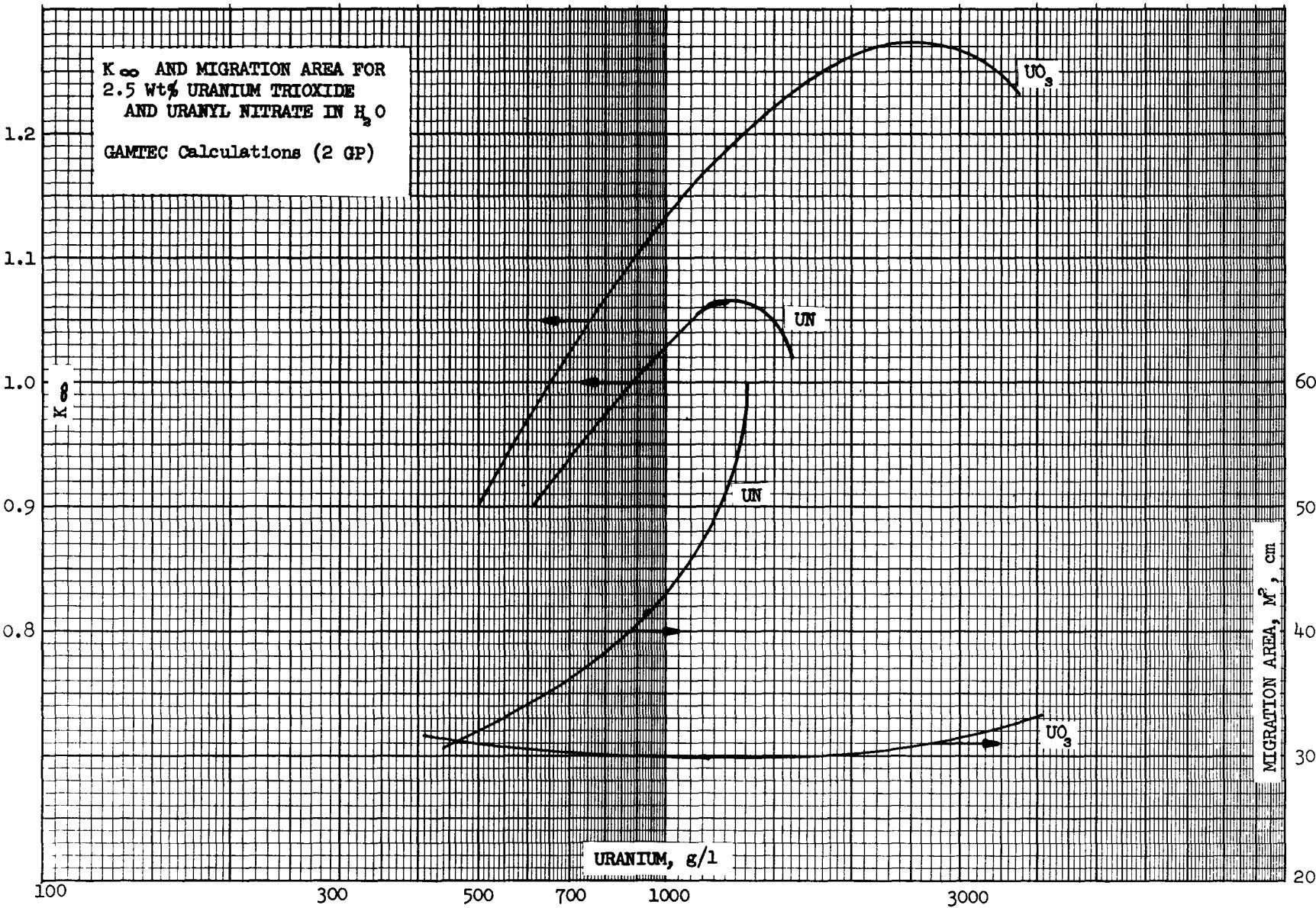
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III.B.11(2.5)-1

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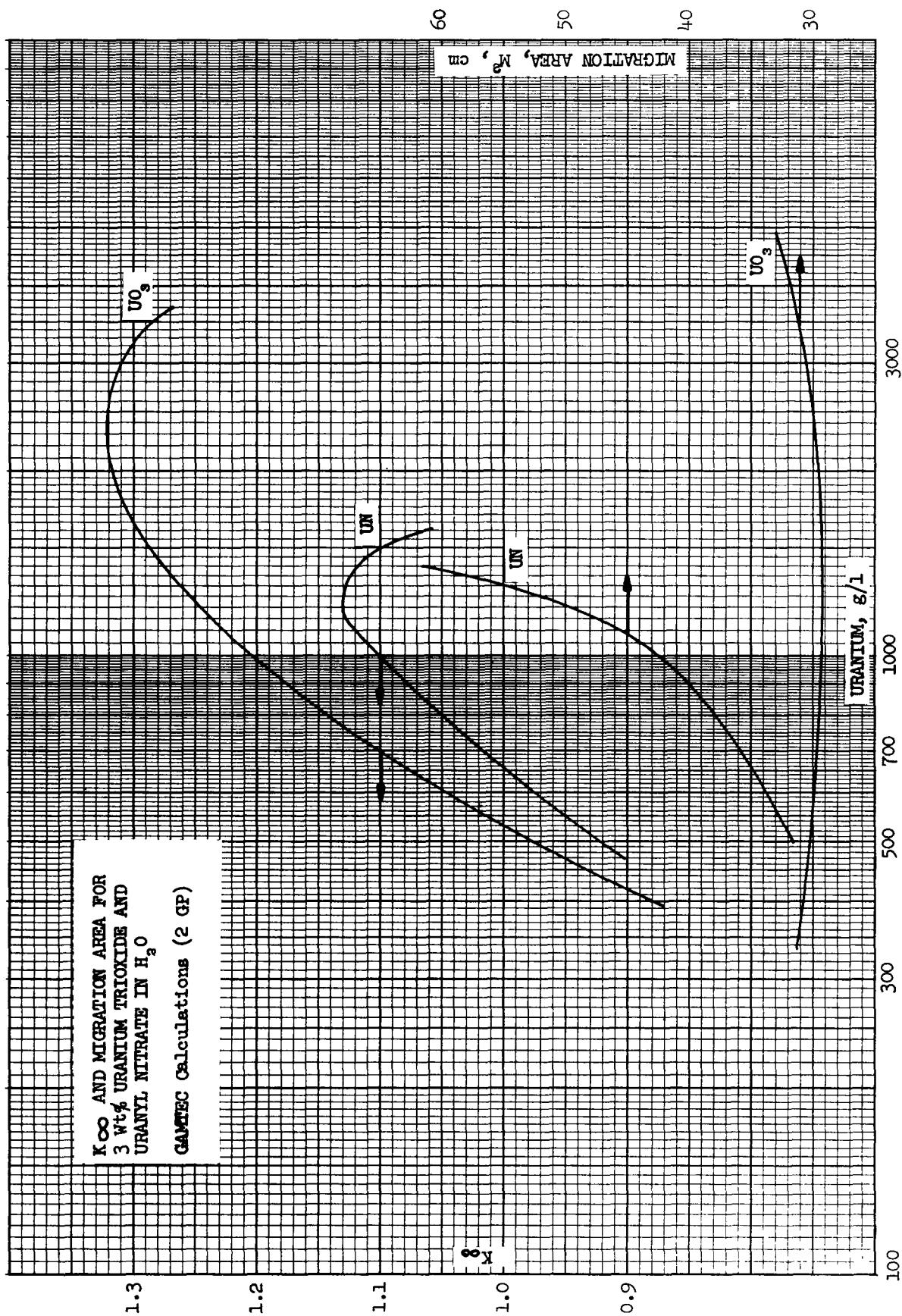


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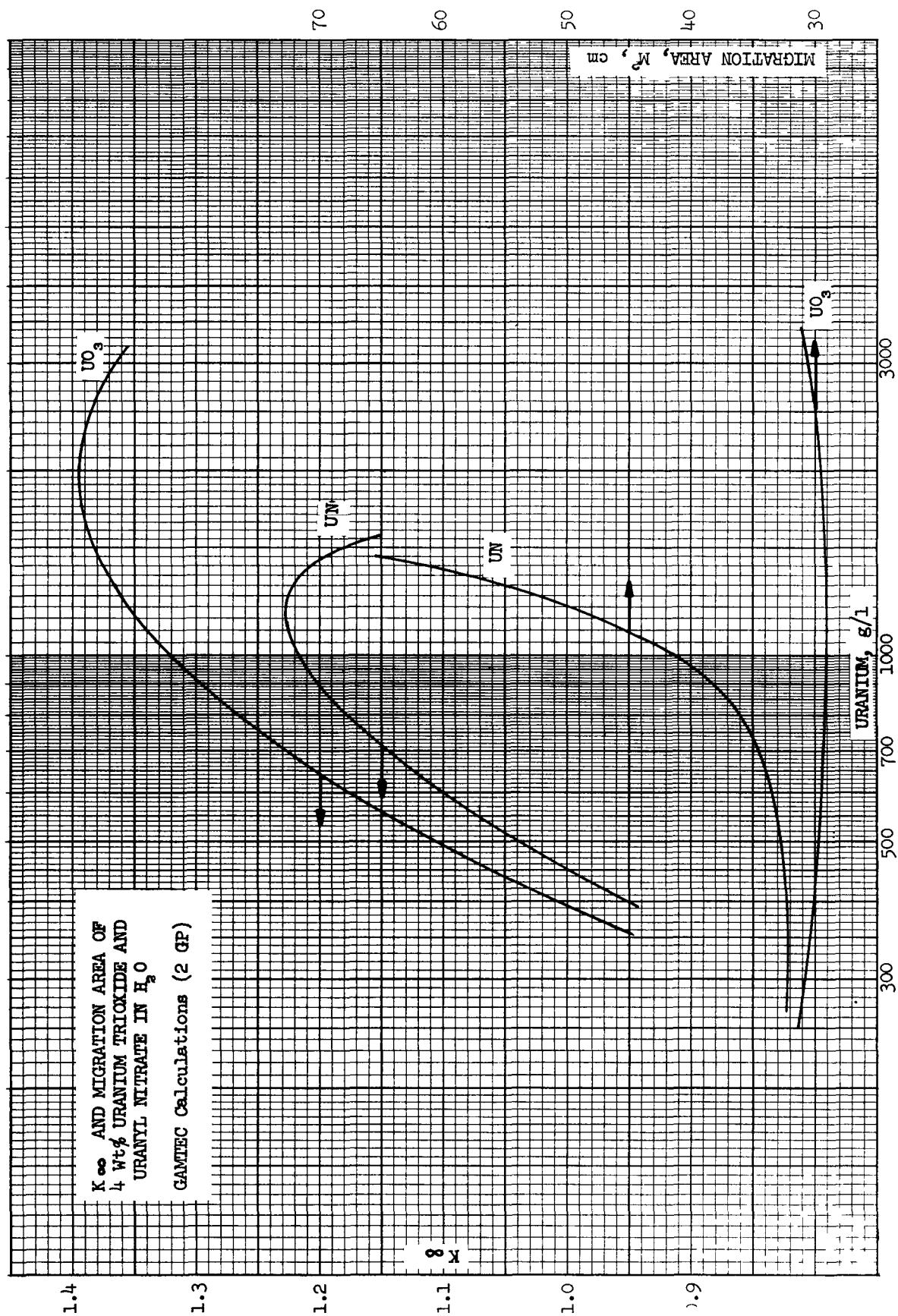
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III.B.11(3)-1

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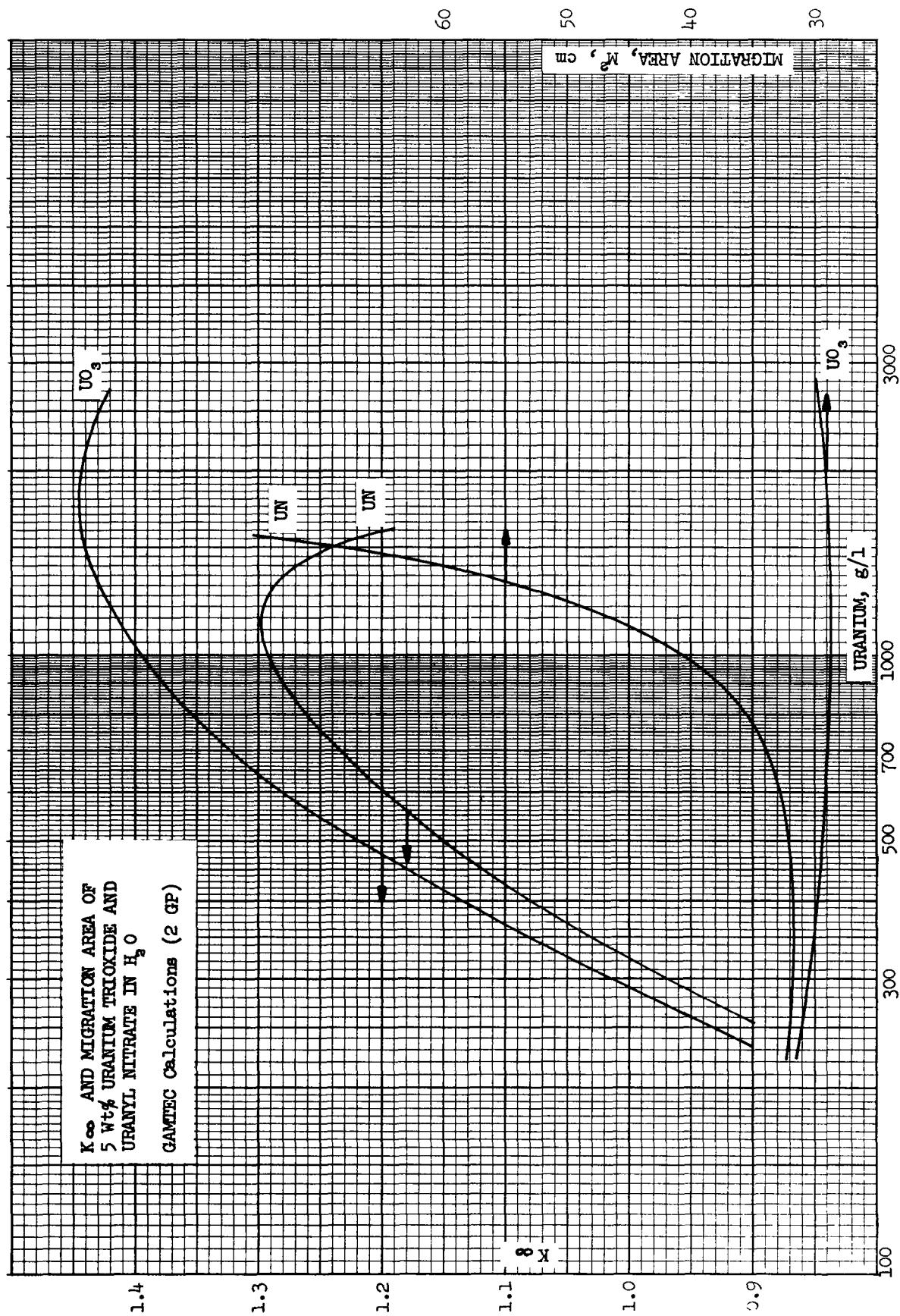
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III.B.11(5)-1

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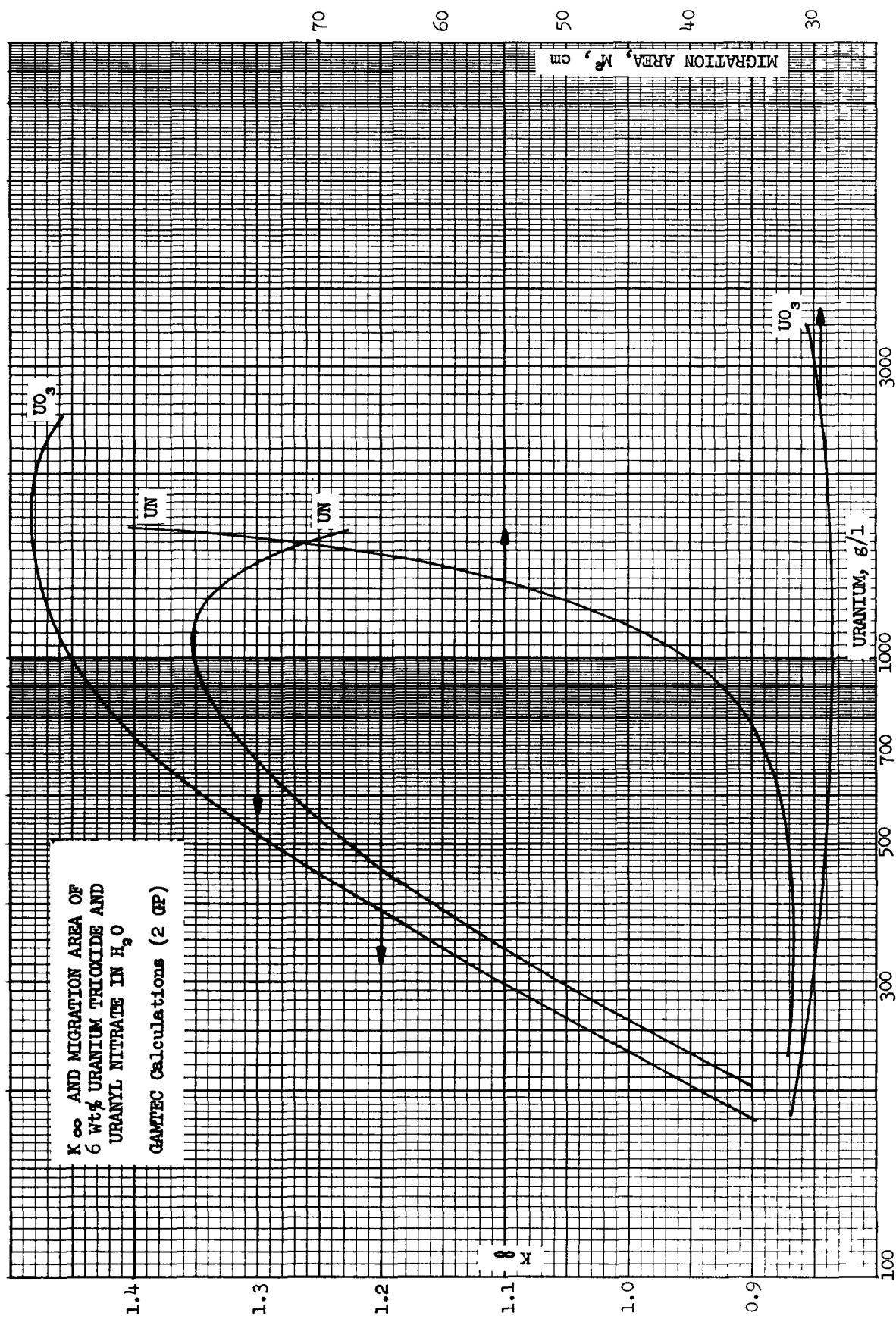


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III.B.11(6)-1

ARH-600

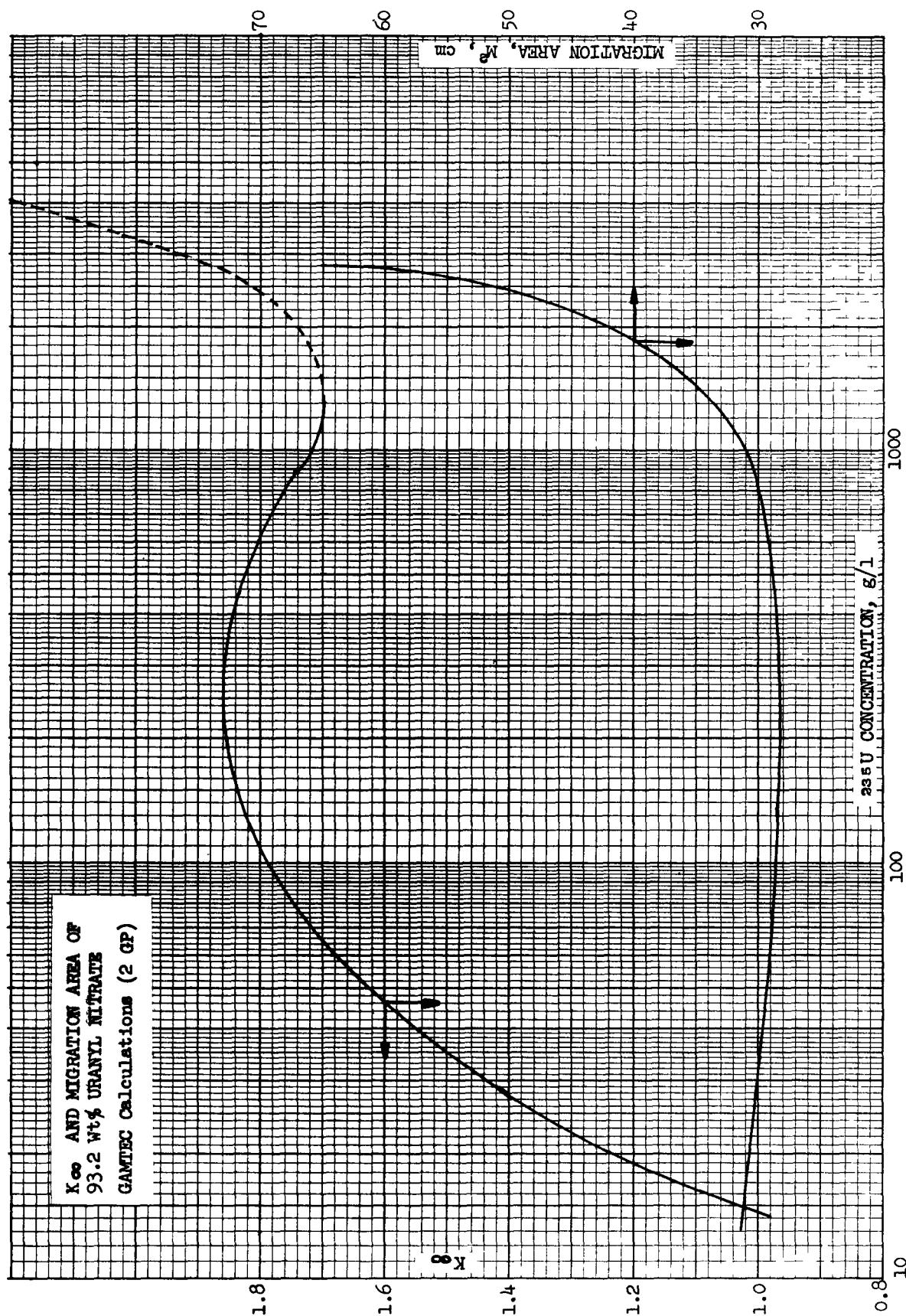


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III.B.11(93)-1

ARH-600



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