

Q1:

F_{GS}

$$T = 75^\circ\text{C} = 348.15\text{K}$$

$$P = 15\text{ bar}$$

$$T_c = 318.7\text{K}; \omega = 0.286$$

$$P_c = 37.6\text{ bar}$$

$$\left. \begin{array}{l} V: ? \\ Z: ? \end{array} \right\}$$

(a) Virial EOS:

$$Z = \frac{PV}{RT} = 1 + \frac{B}{V} + \frac{C}{V^2}$$

$$\frac{PV}{RT} = 1 + \frac{B}{V} + \frac{C}{V^2} \quad (*) \quad \begin{array}{l} B = -194\text{ cm}^3/\text{mol} \\ C = 15300\text{ cm}^6/\text{mol}^2 \end{array}$$

Solving for V (calculator, using an iterative method) with the initial guess of (ideal gas equation)

$$V^{\text{GUESS}} = \frac{RT}{P} = \frac{8.314\text{ J}}{\text{molK}} \times 348.15\text{K} \times \frac{1}{15\text{ bar}}$$

$$V^{\text{GUESS}} = 1929.68\text{ cm}^3/\text{mol}$$

leads to (from *)

$$V = 1722.2698 \text{ cm}^3/\text{mol}$$

Now calculating Z ,

$$Z = \frac{PV}{RT} = 0.8925$$

(b) RK EOS:

$$P = \frac{RT}{V-b} - \frac{a}{T^{1/2}(V+b)V} \quad (*)'$$

with:

$$a = 0.42748 \frac{R^2 T_c^2}{P_c}; \quad b = 0.08664 \frac{RT_c}{P_c}$$

There are two ways to solve this problem:

(i) Calculating V from Eqn (*)' through an iterative method and

then obtain Z or;

(ii) Using the general form of the cubic EOS to obtain Z and then calculate V :

$$Z = 1 + \beta - q\beta \frac{Z - \beta}{(Z + \epsilon\beta)(Z + \sigma\beta)}$$

where: $P_r = 0.3989$; $\Omega = 0.08664$

$T_r = 1.0924$; $\Psi = 0.42748$

$$\alpha = T_r^{-1/2} = 0.9568$$

$$\beta = \Omega \frac{P_r}{T_r} = 3.1637 \times 10^{-2}$$

$$q = \frac{\Psi \alpha}{\Omega T_r} = 4.3215$$

$$\epsilon = 0 \quad ; \quad \sigma = 1$$

$$Z = 1 + \beta - q\beta \frac{Z - \beta}{Z(Z + \beta)}$$

Using
 $Z^{\text{GUESS}} = 1$

$$Z = 0.8883 \Rightarrow V = \frac{ZRT}{P} = 1714.1342 \frac{\text{cm}^3}{\text{mol}}$$

(c) SRK EOS:

Using the same procedure as in (b) with

$$P_r = 0.3989 ; \Omega = 0.08664$$

$$T_r = 1.0924 ; \Psi = 0.42748$$

$$\alpha = 0.9191 ; \beta = 3.1637 \times 10^{-2}$$

Using $Z_{\text{GUESS}} = 1$

$$q = 4.1512 ; \sigma = 1 ; \epsilon = 0$$

$$Z = 0.8949 \Rightarrow V = 1726.8701 \text{ cm}^3/\text{mol}$$

(d) PR EOS:

Using the same procedure as in (b) with

$$P_r = 0.3989 ; \Omega = 0.07780$$

$$T_r = 1.0924 ; \Psi = 0.45724$$

$$\alpha = 0.9296 ; \beta = 0.02841$$

Using $Z_{\text{GUESS}} = 1$

$$q = 5.0013 ; \sigma = 1 + \sqrt{2} ; \epsilon = 1 - \sqrt{2}$$

$$Z = 0.8818 \Rightarrow V = 1701.5913 \text{ cm}^3/\text{mol}$$

In summary :

F_6S } 348.15K
 } 15 bar

	Z	V (cm^3/mol)
Virial	0.8925	1722.27
RK	0.8883	1714.13
SRK	0.8949	1726.87
PR	0.8818	1701.59

Q2: N_2 (gas) $\left\{ \begin{array}{l} 175 \text{ K} \\ v = 3.75 \times 10^{-3} \text{ m}^3/\text{kg} \\ \text{MW} = 28 \text{ g/mol} \end{array} \right.$

$P: ?$

$P^{\text{exp}} = 10^7 \text{ kPa}$

(a) Ideal gas EOS

Transforming from specific volume to molar volume

$$P = \frac{RT}{v} = \frac{8.314 \frac{\text{J}}{\text{mol K}} \times 175 \text{ K}}{3.75 \times 10^{-3} \text{ m}^3/\text{kg} \times \frac{1000 \text{ g}}{1 \text{ kg}} \times \frac{\text{mol}}{28 \text{ g}}} \times \frac{1 \text{ N.m}}{1 \text{ J}}$$

$[Pa = N/m^2]$

$P = 1.3857 \times 10^7 \text{ Pa}$

The error

$$\epsilon = \frac{|P - P^{\text{exp}}|}{P^{\text{exp}}} \times 100 = \frac{|1.3857 \times 10^7 - 10^7|}{10^7} \times 100$$

$\epsilon = 38.57\%$

(b) vdW ($T_c = 126.2 \text{ K}$; $P_c = 34 \text{ bar}$)

$\alpha = 1$; $\Omega = 1/8$; $\Psi = 27/64$

$E = 0$; $\sigma = 0$; $T_a = 1.3867$

$P_r = P/P_c \therefore P?$

\therefore Thus we can not use the general form of

the cubic EOS, thus

$$a = \frac{27}{64} \frac{R^2 T_c^2}{P_c} = \frac{27}{64} \left[\frac{8.314 \frac{J}{mol \cdot K}}{\cancel{mol \cdot K}} \times 126.2 K \times \frac{1 Pa \cdot m^3}{15} \right]^2 \times \frac{1}{34 \cancel{bar}} \times \frac{1 \cancel{bar}}{10^5 Pa}$$

$[m^6 \cdot Pa / Kg^2]$

$$a = 0.1365 \frac{m^6 \cdot Pa}{mol^2} \times \left[\frac{1 mol}{28 g} \times \frac{1000 g}{1 kg} \right]^2$$

$$\frac{15 \times \frac{1 kg \cdot m^2 / s^2}{15}}{1 kg / (m \cdot s^2)} = \frac{1 Pa \cdot m^3}{15}$$

\hookrightarrow
 $15 = 1 Pa \cdot m^3$

$$a = 174.2347 \frac{m^6 \cdot Pa}{Kg^2}$$

$$b = \frac{RT_c}{8 P_c} = \frac{8.314 \frac{J}{mol \cdot K}}{\cancel{mol \cdot K}} \times 126.2 K \times \frac{1}{8} \times \frac{1}{34 \cancel{bar}} \times \frac{1 \cancel{bar}}{10^5 Pa} \times \frac{1 Pa \cdot m^3}{15} \times \frac{1 mol}{28 g} \times \frac{1000 g}{1 kg}$$

$[m^3 / Kg]$

$$b = 1.3777 \times 10^{-3} m^3 / Kg$$

Replacing in

$$P = \frac{RT}{v-b} - \frac{a}{v^2}$$

$[Pa]$

$$P = \left[\frac{8.314 \cancel{\text{J}}}{\cancel{\text{mol}} \cdot \cancel{\text{K}}} \times 175 \cancel{\text{K}} \times \frac{1 \text{ Pa} \cdot \text{m}^3}{15} \times \frac{1 \cancel{\text{mol}}}{28 \cancel{\text{g}}} \times \frac{1000 \cancel{\text{g}}}{1 \cancel{\text{kg}}} \right] \times$$

$$\left[3.75 \times 10^{-3} \frac{\text{m}^3}{\text{kg}} - 1.3777 \times 10^{-3} \frac{\text{m}^3}{\text{kg}} \right]^{-1} +$$

$$- \left[174.2347 \frac{\text{m}^6 \text{ Pa}}{\text{kg}^2} \right] \left[3.75 \times 10^{-3} \text{ m}^3 / \text{kg} \right]^{-2}$$

$$P = 9.5138 \times 10^6 \text{ Pa}$$

$$\mathcal{E} = \frac{|9.5138 \times 10^6 - 10^7|}{10^7} \times 100 = 4.86\%$$

Q3 : $V = 0.0283 \text{ m}^3$

$T = 0^\circ\text{C}$ (const)

$P_1 = 1 \text{ atm}$; $P_2 = 3000 \text{ atm}$

Hg

$\kappa = 3.9 \times 10^{-6} - 0.1 \times 10^{-9} P$ $[P]: \text{atm}; [\kappa]: \text{atm}^{-1}$

Assuming that the volume of liquid mercury remains constant during the compression,

$$W = - \int P dV$$

with

$$\kappa = -\frac{1}{V} \left(\frac{\partial V}{\partial P} \right)_T \therefore dV = -\kappa V dP$$

replacing in the expression for work,

$$W = - \int P [-\underbrace{(a+bP)}_{\kappa} V] dP$$

$a = 3.9 \times 10^{-6} \text{ atm}^{-1}$
 $b = -0.1 \times 10^{-9} \text{ atm}^{-2}$

$$W = \underbrace{V}_{\text{constant}} \left[\int a P dP + \int b P^2 dP \right] = V \left[\frac{a P^2}{2} \Big|_{P_1}^{P_2} + \frac{b P^3}{3} \Big|_{P_1}^{P_2} \right]$$

$W = 0.4712 \text{ m}^3 \cdot \text{atm} = 47.7438 \text{ kJ}$

Q4: Liquid water

$$T_1 = 25^\circ\text{C}$$

$$T_2 = 50^\circ\text{C}$$

$$P_1 = 1 \text{ bar}$$

$$\beta = \frac{1}{V} \left(\frac{\partial V}{\partial T} \right)_P = 36.2 \times 10^{-5} \text{ K}^{-1}$$

$$\kappa = -\frac{1}{V} \left(\frac{\partial V}{\partial P} \right)_T = 4.42 \times 10^{-5} \text{ bar}^{-1}$$

$$dV = \left(\frac{\partial V}{\partial T} \right)_P dT + \left(\frac{\partial V}{\partial P} \right)_T dP$$

$$\frac{dV}{V} = \beta dT - \kappa dP$$

Assuming β & κ are constant during the process, we can easily ~~write~~ integrate this equation

$$\ln \frac{V_2}{V_1} = \beta (T_2 - T_1) - \kappa (P_2 - P_1)$$

The vessel is rigid $\rightarrow V$ constant ($V_2 = V_1$)

$$P_2 = \frac{\beta (T_2 - T_1)}{\kappa} + P_1 = 205.75 \text{ bar}$$