

Notebook for tornado thesis

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Chapter 1

ANSYS Fluent

1.1 Solver Theory

1. pressure-based solver
2. density-based solver

1.1.1 Discretization

Spatial Discretization

Discrete values of ϕ at cell centers \rightarrow Face values ϕ_f

First-Order Upwind Scheme The face value ϕ_f is set to equal to cell-center value of ϕ in the upstream cell.

Power-Law Scheme

$$\frac{\phi(x) - \phi_0}{\phi_L - \phi_0} = \frac{\exp\left(Pe \frac{x}{L}\right) - 1}{\exp(Pe) - 1}$$
$$Pe = \frac{\rho u L}{\Gamma}$$

Second-Order Upwind Scheme

$$\phi_f = \phi + \nabla \phi \cdot \mathbf{r}$$

Central-Differencing Scheme

$$\phi_f = \frac{1}{2}(\phi_0 + \phi_1) + \frac{1}{2}(\nabla \phi_0 \cdot \mathbf{r}_0 + \nabla \phi_1 \cdot \mathbf{r}_1)$$

QUICK Scheme

$$\phi_e = \theta \left[\frac{S_d}{S_c + S_d} \phi_P + \frac{S_c}{S_c + S_d} \phi_E \right] + (1 - \theta) \left[\frac{S_u + 2S_c}{S_u + S_c} \phi_P - \frac{S_c}{S_u + S_c} \phi_W \right]$$

Evaluation of Gradients and Derivatives

Green-Gauss Cell-Based Gradient Evaluation

$$\bar{\phi}_f = \frac{\phi_{c0} + \phi_{c1}}{2}$$

Green-Gauss Node-Based Gradient Evaluation

$$\bar{\phi}_f = \frac{1}{N_f} \sum_n^{N_f} \bar{\phi}_n$$

The node-based gradient is known to be more accurate than the cell-based gradient particularly on irregular (skewed and distorted) unstructured meshes.

Least Squares Cell-Based Gradient Evaluation

$$(\nabla)_{c0} \cdot \Delta r_i = (\phi_{ci} - \phi_{c0})$$

$$\mathbf{J}(\nabla\phi)_{c0} = \Delta\phi$$

Chapter 2

Definitions

2.1 Swirl Ratio

Chapter 3

Wind-Driven Rain

3.1 Overview

Euler-Euler frame in WDR simulation[1]: rain is regarded as a continuum similar to wind rather than as a single raindrop as it is treated in the existing WDR simulation methods. A similar group of conservation equations with wind, including the mass conservation and momentum conservation equations, were established for rain based on the concept of phase and phasic volume fraction in the same Euler coordinates as wind. Then, the equations for rain can be solved in the same way as for wind.

Continuum hypothesis for raindrops[2]: Continuum hypothesis is valid mathematically in consideration of the relatively small mean inter-particle distance with an order of 0.1 m in most cases, as compared with the macroscopic size of a concerned WDR field (usually in the order of 10 m).

3.2 Governing equations for WDR with Eulerian multiphase model

Phase in multiphase flow regime[2]: In a multiphase flow regime, *phase* does not only refer to the physical phase of material, such as gas, liquid and solid, but also it has been defined in a broader sense as an identifiable class of material that has a particular inertial response to and interaction with the flow and the potential field in which it is immersed. Specifically in the WDR description, in addition to wind (air) phase (gas phase in physics), different-sized raindrops can be regarded as different phases because each collection of raindrops with the same size will have a similar dynamical response to the wind field.

Phasic volume fraction a_q : represents the space occupied by each phase, which is regarded as a continuous function in space and time.

Rain is divided into N phases according to the diameter sizes of raindrops, with each phase representing the raindrops' diameter being in the range of $[D_k - (dD/2), D_k + (dD/2)]$, where dD is the differential diameter range and $k = 1, 2, \dots, N$. The volume fraction of the k th phase, denoted by a_k , represents the volume fraction of raindrops belonging to the same diameter range $[D_k - (dD/2), D_k + (dD/2)]$.

Mass conservation equation and Momentum conservation equation for the phase k :

$$\frac{\partial \rho_l a_k}{\partial t} + \frac{\partial (\rho_l a_k u_{kj})}{\partial x_j} = 0 \quad (3.1)$$

$$\frac{\partial \rho_l a_k u_{ki}}{\partial t} + \frac{\partial (\rho_l a_k u_{ki} u_{kj})}{\partial x_j} = \rho_l a_k g_i + \rho_l a_k \frac{18\mu C_D Re_p}{24\rho_l D_k^2} (u_i - u_{ki}) \quad (3.2)$$

ρ_l : the physical density of rain

u_{ki} : the absolute velocity component of the k th phase of rain

The first term in the right hand side of Eq. 3.2: the source of gravitational force, where g_i represents the gravity in the i th direction

The second term in the right hand side of Eq. 3.2: denotes the source of drag force between the rain and the wind phases, in which Re_p is the relative Reynolds number (referring to the wind around the raindrop); C_D is the raindrop drag coefficient which is usually determined by fitting measurements, using a polynomial formula. μ and μ_i are the viscosity coefficient and velocity component of wind, respectively.

For *wind flow*, RANS equations, in combination with the realizable $k - \epsilon$ turbulence model:

Chapter 4

Wind-driven debris

4.1 Introduction

Classification of wind borne debris:

Compact debris: whose three spatial dimensions are approximately the same includes near-spherical objects such as gravel.

Sheet/Plate debris: with one of the spatial dimensions much smaller than the other two includes roof tiles, roofing sheets and other cladding elements.

Rod debris: with one of the spatial dimensions much larger compared to the other two includes objects such as timber pieces and bamboo rods.

Debris damage chain

Debris damage models and risk assessment models

1. The source and aerodynamic properties of the various debris types,
2. The debris flight behaviour, trajectory and impact velocities,
3. The damage resulting from debris impact.