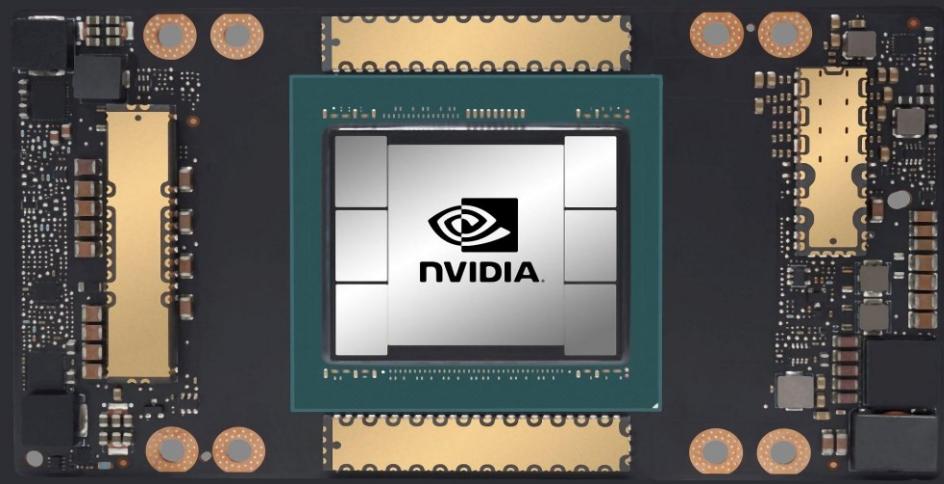


THE TECHNOLOGY OF OPTICAL HIGH PERFORMANCE PROFILERS



## parallel data processing using advances algorithms

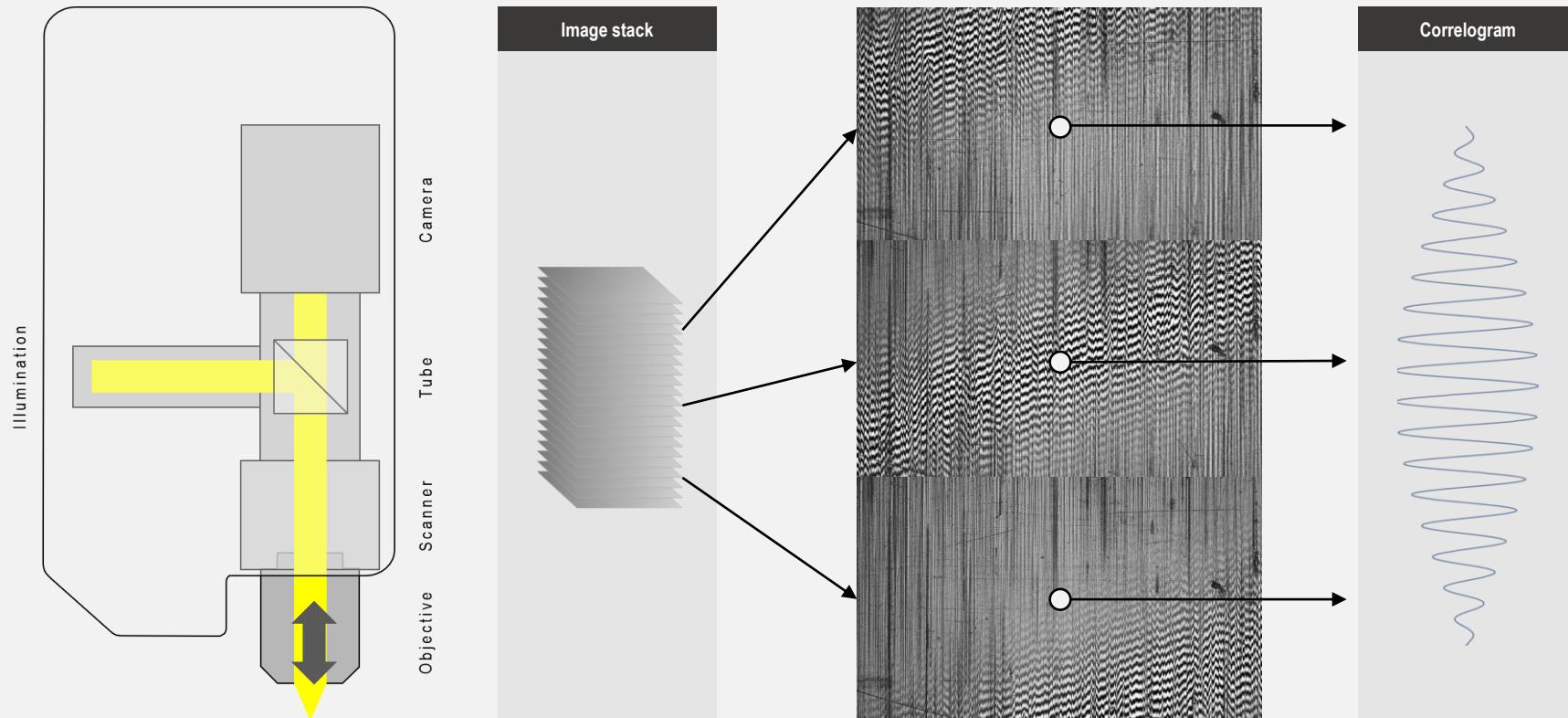
GPGPUs (General Purpose Graphic Processing Units) using thousands of processing cores which are optimized for massively parallel and ultra fast image processing. Even the best CPUs on the market can't perform at that level. The processing speed is very useful for coherence scanning interferometry because thousands of large image stacks can be evaluated in real time with the following purpose:

- higher resolution in xyz
- scanning of larger areas
- shorter measuring time
- independent from environmental conditions

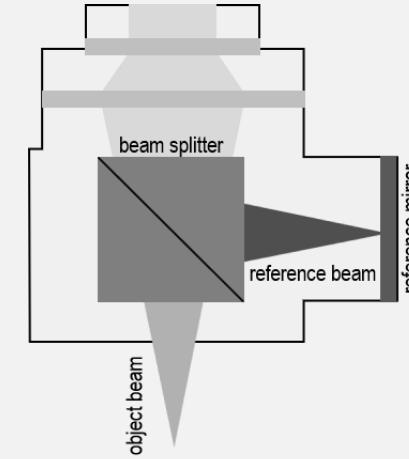
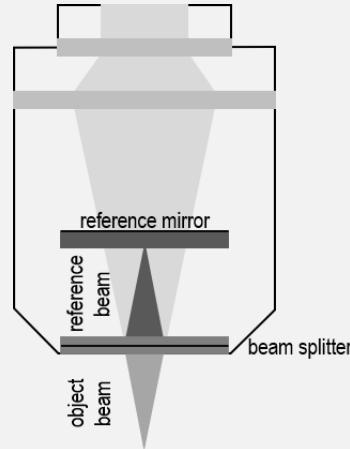
## performance comparison

|                          | Core i9 13900K | GTX 1060   | RTX 2060   | RTX 3060    | RTX 4090      |
|--------------------------|----------------|------------|------------|-------------|---------------|
| release date             | 2022           | 2018       | 2019       | 2020        | expected 2022 |
| FP32 (float) performance | 0.74 TFLOPS    | 4.4 TFLOPS | 6.4 TFLOPS | 16.2 TFLOPS | 82.6 TFLOPS   |
| process size             | 10 nm          | 16 nm      | 12 nm      | 8 nm        | 5 nm          |

GPGPUs are not only much faster than CPUs, they have shown very fast performance improvements in the past years. This unbroken trend assists the significant and continuous performance improvements of all smartWLI sensors. On the one side this calculation power is usefully to reduce the noise and analyze signals on very steep object features and on the other side it is the foundation for developing enhanced sensors using faster cameras while still processing the 3D data in real time.



The coherence scanning interferometer realizes the acquisition of an image stack while the scanner is precisely moving the interference objective. For each pixel in the image stack, the interference signal (correlogram) contains the exact height information that is physically when object and reference beam are equidistant in path length.

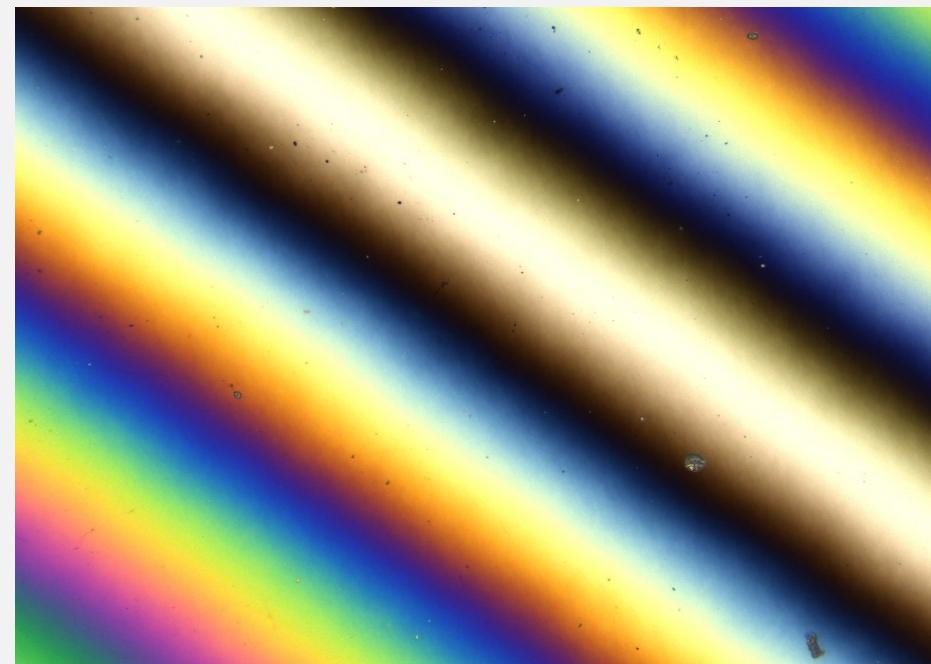


## objective type comparison

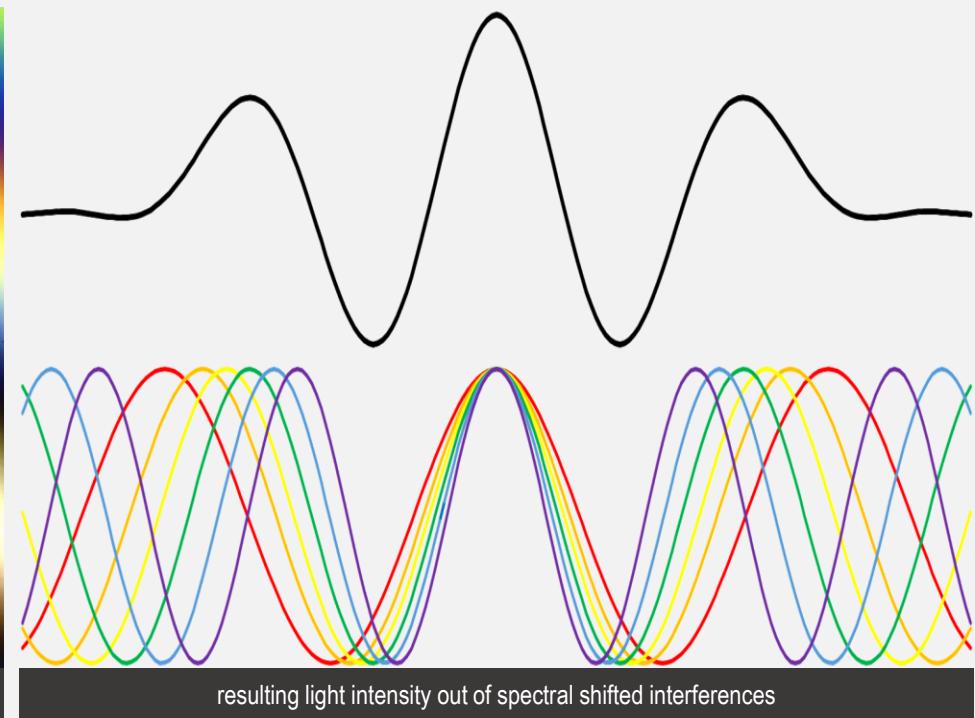
| objective type         | Mirau |      |      |     |     | Michelson |       |
|------------------------|-------|------|------|-----|-----|-----------|-------|
| magnification          | 115x  | 100x | 50x  | 20x | 10x | 5x        | 2.5x  |
| numerical aperture     | 0.8   | 0.7  | 0.55 | 0.4 | 0.3 | 0.13      | 0.075 |
| parfocal distance [mm] | 45    | 45   | 45   | 45  | 45  | 49        | 90    |
| working distance [mm]  | 0.7   | 2.0  | 3.4  | 4.7 | 7.4 | 9.4       | 10.3  |

Coherence scanning interferometers use exchangeable interference objectives that are available with various magnifications. For technical reasons, Mirau objectives are used for higher magnifications like 115x, 100x, 50x, 20x and 10x and Michelson objectives are used for lower magnifications like 5x and 2.5x.

# smartWLI interferences of white light

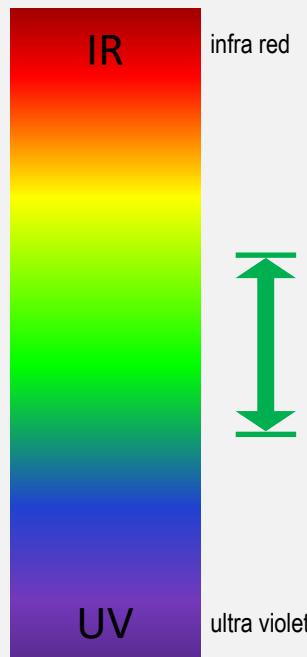


camera image of a mirror / centre of the interference zone

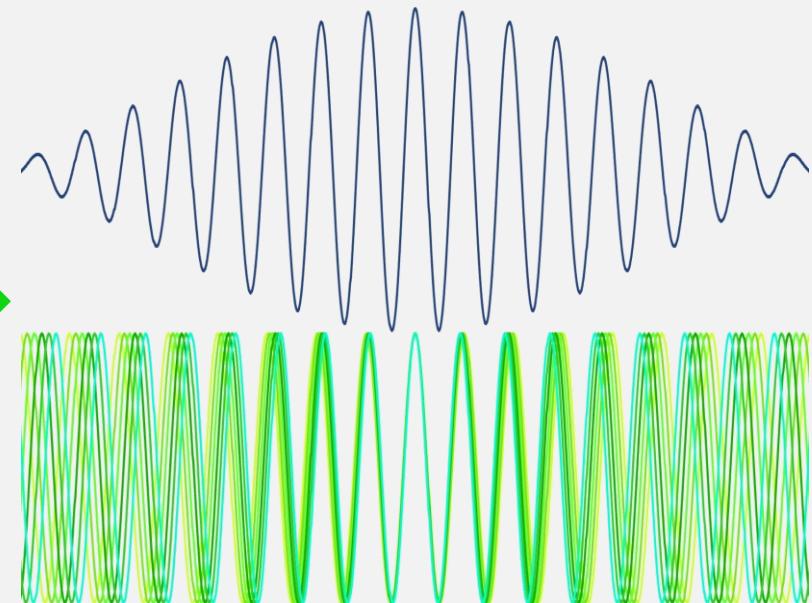


White light consist of a continuous distribution of various spectral colours. All spectral colours show interferences between reference and object beam. In the centre position where reference beam and object beam have a equal length, all spectral colours have a maximum. Because of the various wave length the second, third ... maxima have a shifted position and the resulting intensity of interference is smaller because of a very limited – so called – coherence length of white light.

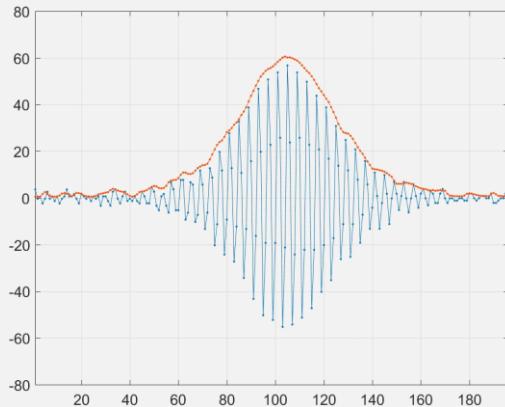
# smartWLI spectral optimization for noise reduction



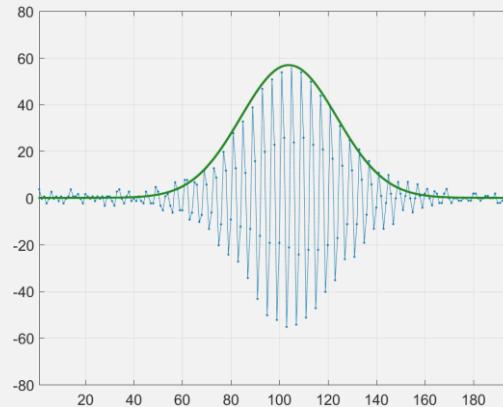
reduction of the spectral bandwidth  
and enlargement of the correlogram



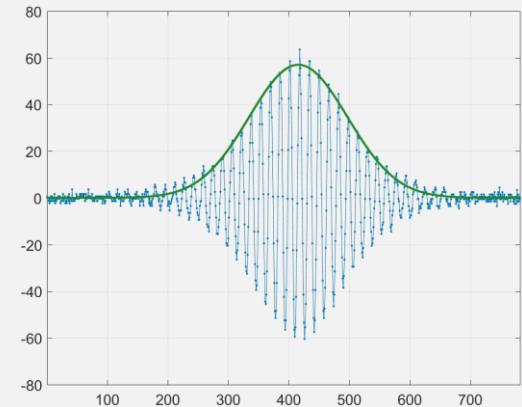
Bigger correlograms with several sinus like intensity variation enable the use of phase-shift algorithms. Such algorithms use the sinus like light intensity variations to increase the height resolution/reduce the noise. In contrary to illumination sources with a smaller coherence length, statistical positioning deviations and the camera noise are filtered more effective. Such algorithms require significant more calculation power. GBS uses its massive parallel image processing expertise for effective and extreme fast data evaluation in real time and without delays.



VSI (vertical scanning interferometry)  
intensity based evaluation of the interference signal

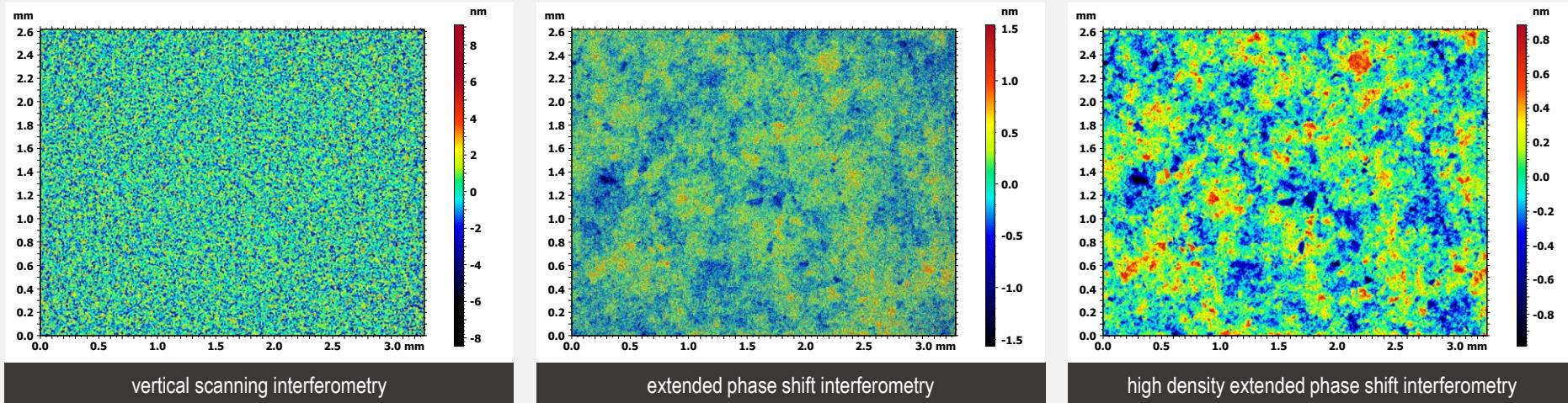


EPSI (extended phase shift interferometry)  
phase based evaluation of the interference signal

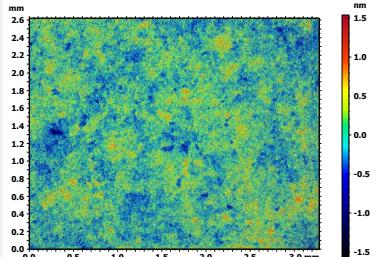
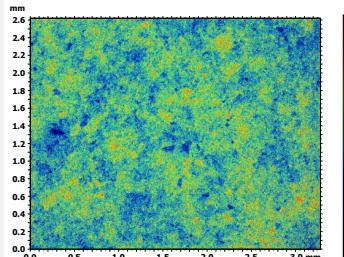
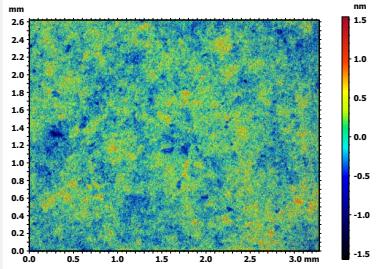
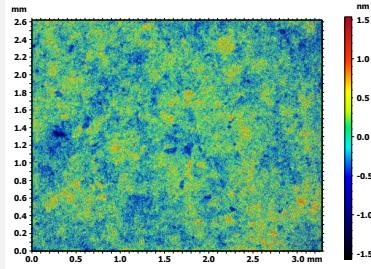


HD - EPSI (high density extended phase shift  
interferometry) phase based evaluation of the interference  
signal with a higher density

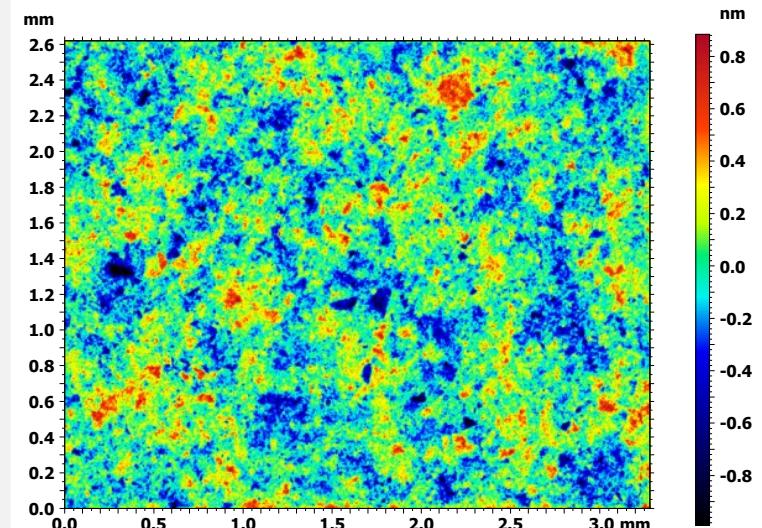
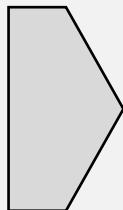
Shown are the signals and correlogram evaluations of one and the same pixel. The intensity based evaluation of the VSI method show a not ideal red curvature which cause a significant higher noise than the phase based evaluation shown in the green curvatures. Once the increment get smaller (here from  $\lambda/8 \rightarrow \lambda/32$ ) the evaluation getting better and the noise can reduced further. The advantages are useful if polished surface with a surface roughness below 1 nm should be measured (-> evaluation examples on the next pages)



The images show exactly the same area of a super polished SiC surface with a surface roughness  $S_q$  of approximately 0.3 nm. VSI (vertical scanning interferometry) doesn't provide the required height resolution to quantify the topography. EPSI with an much higher resolution and a topography reproducibility (average noise) of approximately 0.1 nm make some structures visible but still looks noise compared with a HD-EPSI scan of the same area.



4 scans using extended phase shift interferometry

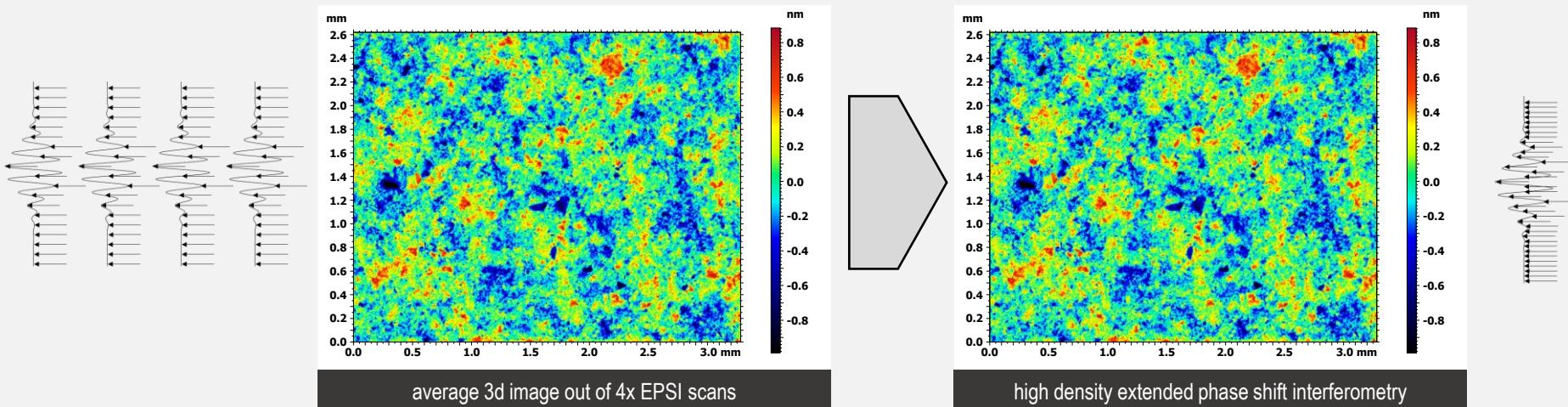


average 3d image out of 4x EPSI scans

- profile averaging is a common method for noise reduction
- random noise has an Gaussian-like distribution

$$\text{resulting noise} = \frac{\text{original noise}}{\sqrt{\text{number of scans}}}$$

- significant noise reduction through a larger number of scans
- a larger number of scans require a significantly higher measuring time
- drift effects – specifically while using higher magnification objectives – may reduce the lateral resolution
- averaging with a higher number of scans is partially used to improve the system specification and therefore meaningless without the specification of the required measuring time

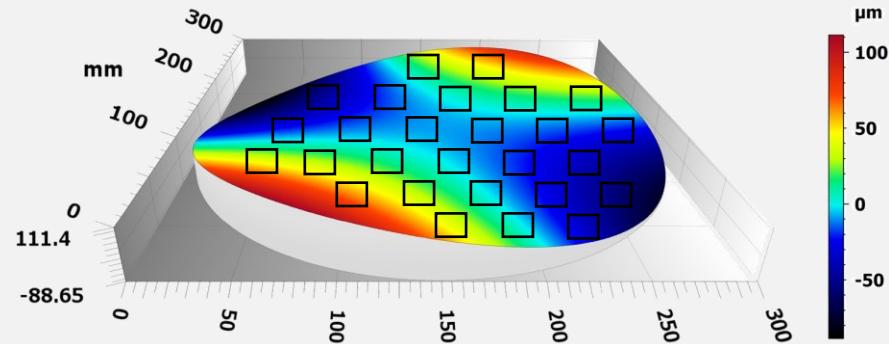


## comparison between HD-EPSI and EPSI with profile averaging

- 4x EPSI scans acquire as many images out of the interference zone as a single scan using a high density scan with 4x smaller increment between images
- both methods reduce the noise level and the result is similar under ideal environmental conditions
- on the one side the scanning speed of HD-EPSI drops down to ¼ of the scanning speed of EPSI but has the following advantages
  - scans are done against gravitation from the lowest point to the highest one and HD-EPSI doesn't require the scanner to reposition to the start point
  - it requires only 1 acceleration phase of the objective
  - scanning speed is lower and reduces motion blur, which enables longer integration times for the camera
  - averaging calculation isn't necessary
- practical tests have shown the following advantages
  - HD-EPSI scans are much faster than multiple EPSI scans with profile averaging
  - HD-EPSI shows a lower sensitivity against vibration and drift effects
- HD-EPSI requires more memory and calculation power of the GPGPU for real time evaluation of 3D data

### The challenge to measure multiple position on a super polished wafer:

- polished wafer have extreme smooth surfaces with roughness values below 1 nm – sometimes even between 0.1 and 0.3 nm but usually a much larger wafer bow
- this requires high resolution measurements using HD-EPSI scans or even HD-EPSI scans combined with profile averaging and an therefore moderate scanning speed
- the wafer bow of several 100 µm requires a longer scanning range
- higher scanning ranges with a lower scanning speed for extreme resolution could extend the measuring time
- specifically for larger wafers with multiple measuring position a dual approach with a extreme fast prescan followed from a high resolution scan with a limited scanning range can reduce the measuring time significant
- below a calculation sample for a typically situation
- the time benefit depends from the application but could be more dramatically if sensors with a lower scanning speed get used

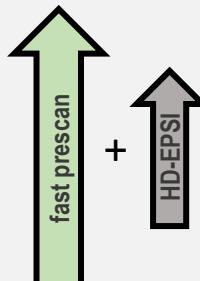


measuring task: local control of the polishing processes  
on wafer with a bow of app. 200 µm with multiple single scans



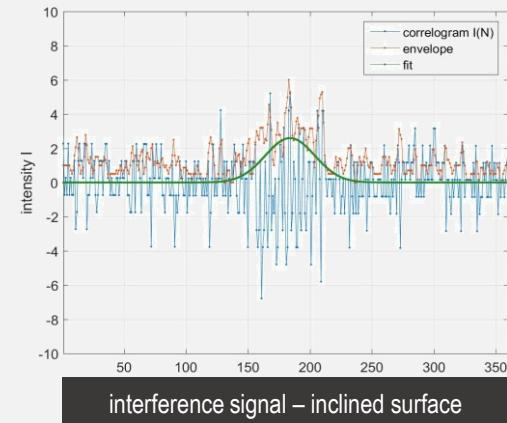
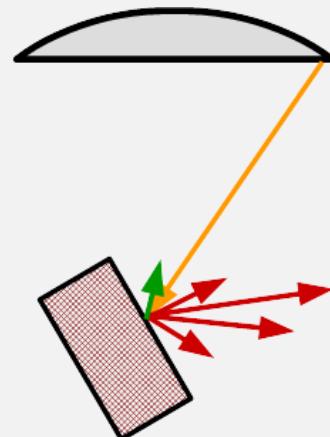
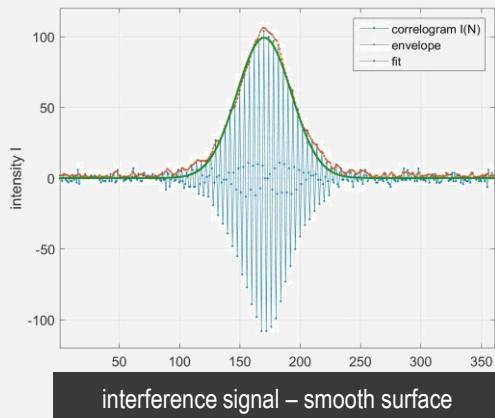
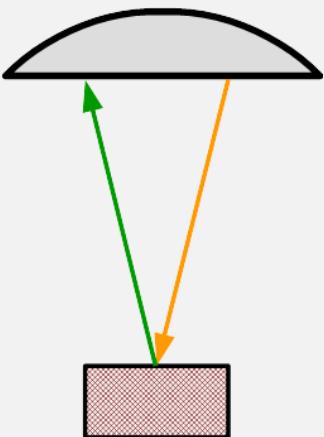
#### standard scanning time:

- scanning range 200 µm
- scanning speed HD-EPSI with 17 nm increment and full resolution = 16 µm/s
- scanning time =  $200 \mu\text{m} / 16 \mu\text{m/s} = 12.5 \text{ s}$
- scan preparation and data processing app. 0.5 s
- **complete measuring time app. 13 s**



#### accelerated scanning time using a fast prescan

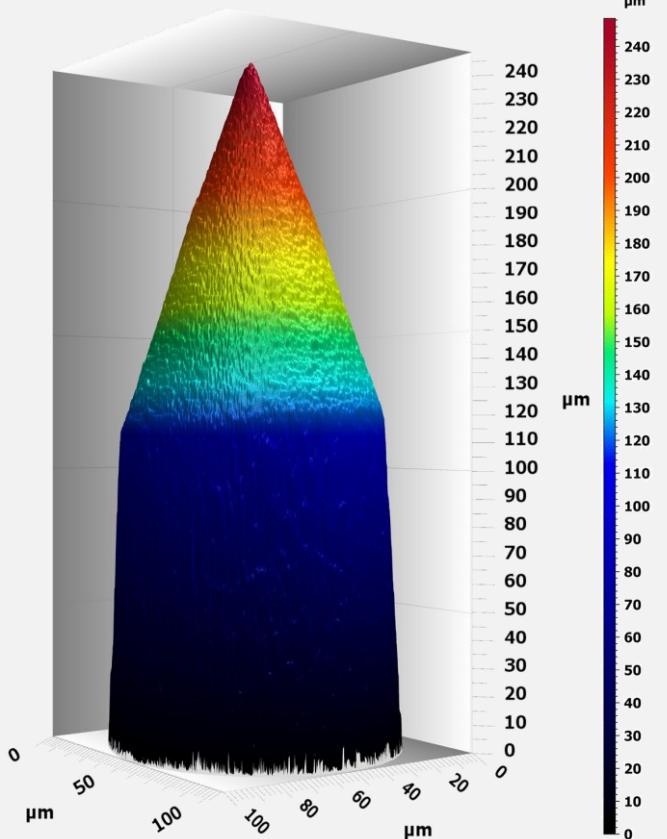
- scanning range 200 µm
- fast prescan: decimation 5 and increment 200 nm =  $1029 \mu\text{m/s}$
- fast prescan =  $200 \mu\text{m} / 1029 \mu\text{m/s} = 0.2 \text{ s}$
- scan preparation and data processing app. 0.5 s
- scanning range around the wafer = 10 µm
- scanning time =  $10 \mu\text{m} / 16 \mu\text{m/s} = 0.6 \text{ s}$
- scan preparation and data processing app. 0.5 s
- **complete measuring time app. 1.8 s**



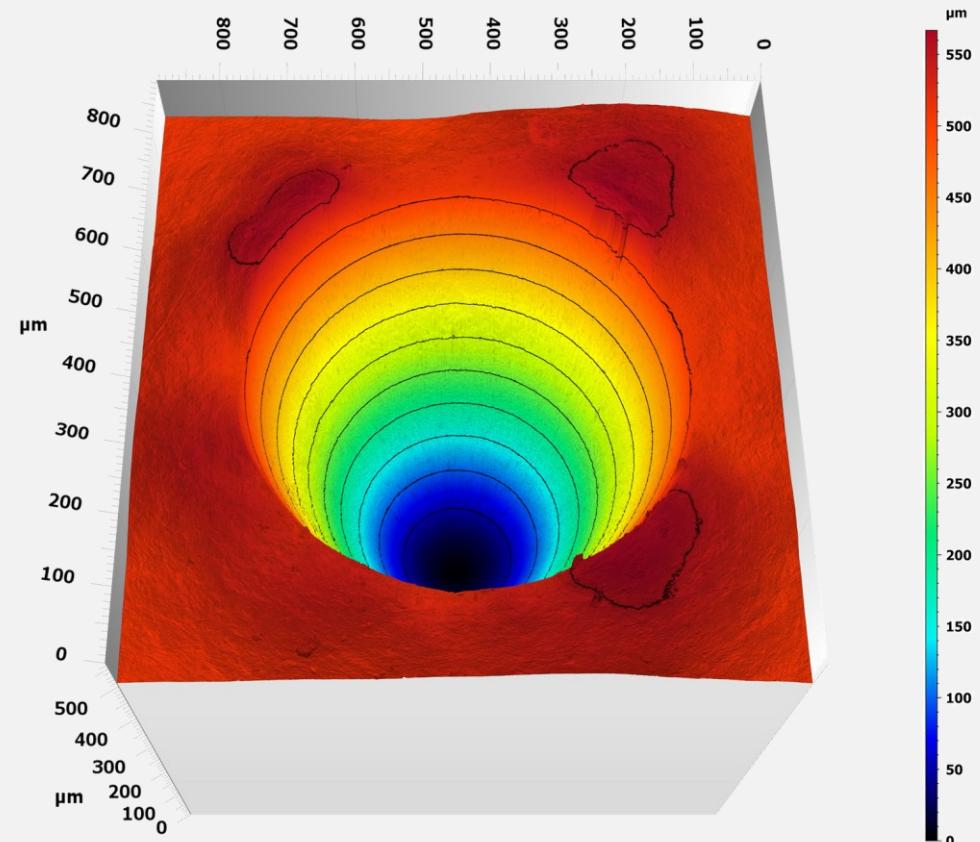
#### maximum angle for high reflective surfaces

| magnification      | 2.5x  | 5x   | 10x   | 20x   | 50x   | 100x  | 115x  |
|--------------------|-------|------|-------|-------|-------|-------|-------|
| numerical aperture | 0.075 | 0.13 | 0.3   | 0.4   | 0.55  | 0.7   | 0.8   |
| max. angle         | 4.3°  | 7.4° | 17.5° | 23.6° | 33.4° | 44.4° | 53.1° |

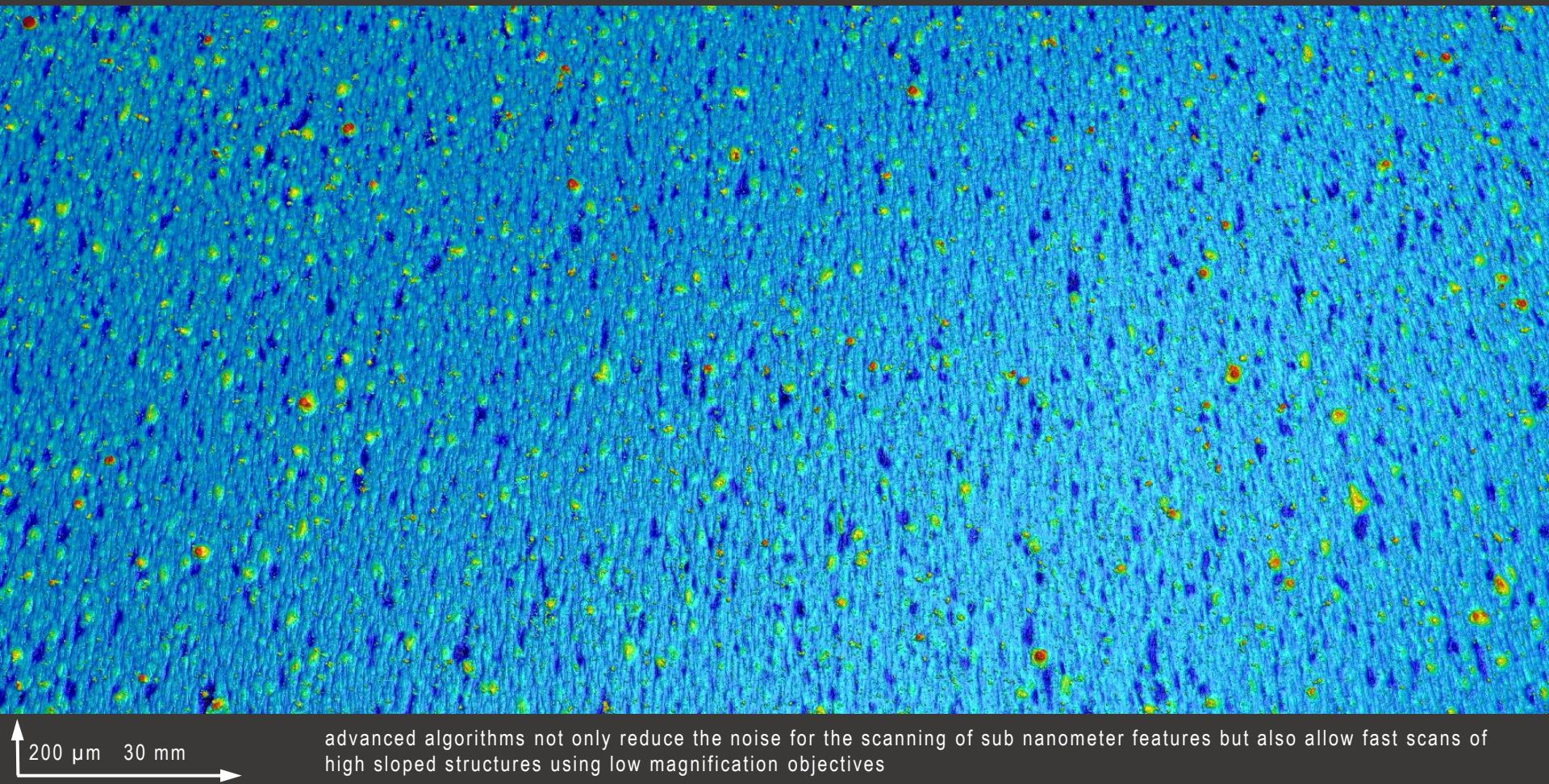
All microscopic optical area scanning devices which project and receive the light through the same objective have a limited maximum angle for high reflective surfaces. Once the angle is too big an objective with a higher aperture is necessary. However, most surfaces scatter at least a small part of the light diffuse and back into the objective. The resulting signals can be analysed but require advanced algorithms since the interference contrast goes down.



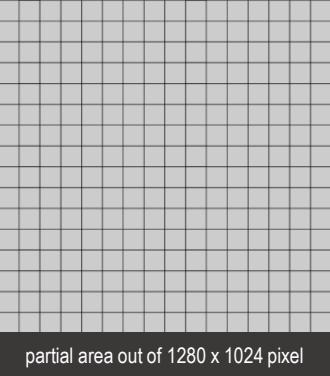
needle to manufacture spinnerets



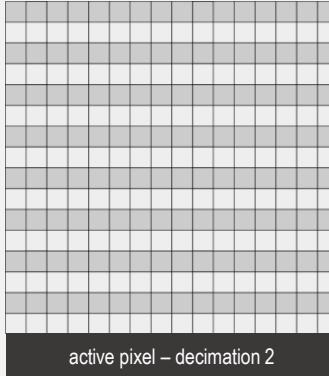
“lens” to focus x-ray beams



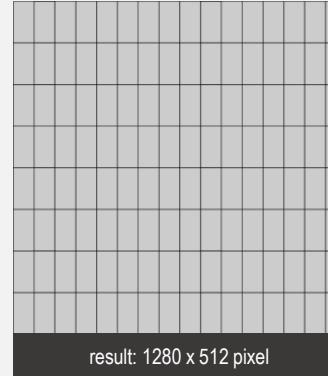
the principle of line decimation applied in firebolt



partial area out of 1280 x 1024 pixel



active pixel – decimation 2



result: 1280 x 512 pixel

**smartWLI firebolt:**

- 1.3 MP; 10 GigE interface; bandwidth of 1000 MByte/s; 935 f/s (full resolution)
- allows line decimation with a factor 2 ... 15

**smartWLI compact, extended, extended range and next with an 2.3 MP camera:**

- 2.3 MP; USB 3.0 interface; bandwidth of 400 MByte/s; 169 f/s (full resolution)
- allows area decimation with a factor 2 x 2 in x and y direction

Decimation is a method to reduce the number of used pixel/measuring points and accelerate the scanning speed. The method of decimation doesn't change the scanning area but reduce the pixel/measuring point density inside of the scanning area. Decimation has the significant advantage compared to the often used binning that the interference contrast on rough and inclined surfaces stays unchanged.

**firebolt, 1.3 MP camera - scanning speed -  $\mu\text{m}/\text{s}$** 

| decimation | increment 17 nm | increment 70 nm | increment 200 nm |
|------------|-----------------|-----------------|------------------|
| full area  | 16              | 65              | 206              |
| 2          | 32              | 131             | 411              |
| 3          | 48              | 196             | 617              |
| 4          | 64              | 262             | 823              |
| 5          | 79              | 327             | 1029             |
| 6          | 95              | 393             | 1234             |
| 7          | 111             | 458             | 1440             |
| 8          | 127             | 524             | 1646             |
| 9          | 143             | 589             | 1851             |
| 10         | 159             | 655             | 2057             |
| 11         | 175             | 720             | 2263             |
| 12         | 191             | 785             | 2468             |
| 13         | 207             | 851             | 2674             |
| 14         | 223             | 916             | 2880             |
| 15         | 238             | 982             | 3086             |

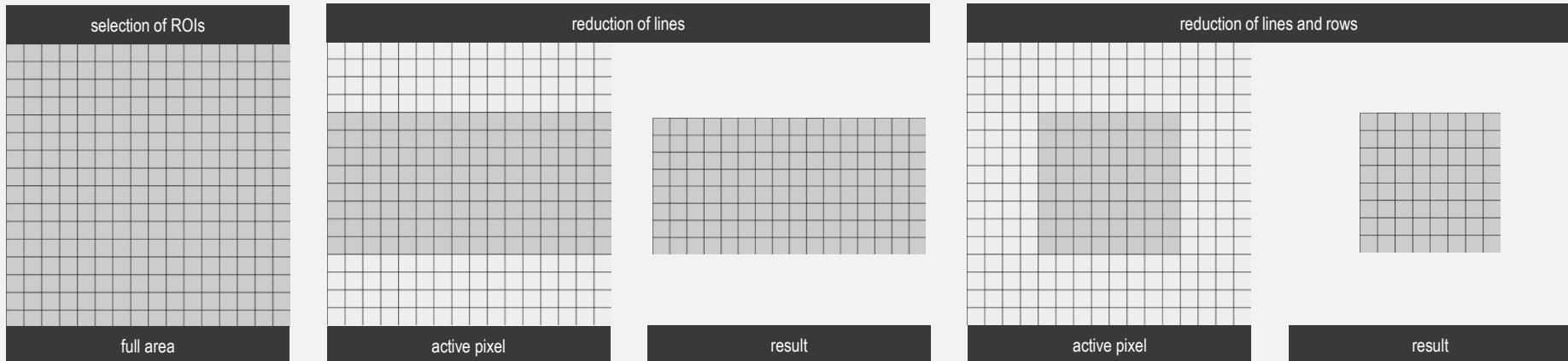
**various sensors, 2.3 MP camera - scanning speed -  $\mu\text{m}/\text{s}$** 

| decimation | increment 17 nm | increment 70 nm | increment 200 nm |
|------------|-----------------|-----------------|------------------|
| full area  | 2.8             | 11.4            | 34.2             |
| 2 x 2      | 9               | 36              | 108              |

partial area out of 1920 x 1200 pixel

active pixel – decimation 2 x 2

result: 960 x 600 pixel



| 1.3 MP camera          |                          | 2.3 MP camera                           |   | 5 MP camera              |                          |
|------------------------|--------------------------|---|---|--------------------------|--------------------------|
| smartWLI sensors       | firebolt                 | compact, extended, extended range, next | compact, extended, extended range, next, nanoscan | pixel / measuring points | speed - f/s              |
| feature                | pixel / measuring points | speed - f/s                             | pixel / measuring points                          | speed – f/s              | pixel / measuring points |
| full area              | 1280 x 1024              | 935                                     | 1920 x 1200                                       | 169                      | 2456 x 2054              |
| half lines             | 1280 x 512               | 1800                                    | 1920 x 600  | 350                      | 2456 x 1028              |
| half lines / half rows | 640 x 512                | 2100                                    | 960 x 600   | 600                      | 1228 x 1028              |
| max. speed             | 1280 x 8                 | 84000                                   | 1920 x 36   | 3200                     | 2456 x 2                 |
|                        |                          |   |   |                          | 1958                     |

ROIs are an alternative method to accelerate the sensor speed. In contrary to the decimation, it keeps the measuring point density but reduces the scanning area (field of view). This acceleration is interesting for inline measurements under vibration if partial areas include all features or several lines are suitable to evaluate 2d line roughness parameters in contrary to 3d roughness parameters.

**Advantage and limitations of optical resolution and point density to qualify optical 3d profilers:**

- The basis of the definition of the optical resolution is the ability of the optical system to separate 2 different light sources. If the optics is able to separate them, it is practically only possible if the point density is significantly higher.
- To select a fitting device with a suitable objective for your application both optical resolution and point density have to be significantly smaller than the features you want to measure.
- Once the point density drops far below the optical resolution, the practical improvements in resolution of the measured surface feature will be limited.
- Please note that there isn't a general accepted way to specify the optical resolution. Individual systems with different measuring principles, different types of data processing, utilizing noise reduction techniques as well as filtering processes can not be compared using either optical resolution or point density.

| objective and system comparison                         |       |      |      |       |      |       |      |
|---|-------|------|------|-------|------|-------|------|
| magnification   | 2.5x  | 5x   | 10x  | 20x   | 50x  | 100x  | 115x |
| aperture  | 0.075 | 0.13 | 0.3  | 0.4   | 0.55 | 0.7   | 0.8  |
|   | 4.23  | 2.44 | 1.06 | 0.79  | 0.58 | 0.45  | 0.4  |
| optical resolution Rayleigh criterion [ $\mu\text{m}$ ] | 3.78  | 2.18 | 0.95 | 0.71  | 0.52 | 0.41  | 0.35 |
|   | 3.26  | 1.9  | 0.81 | 0.61  | 0.44 | 0.35  | 0.31 |
| optical resolution Sparrow criterion [ $\mu\text{m}$ ]  | 3.10  | 1.79 | 0.78 | 0.58  | 0.42 | 0.33  | 0.29 |
|   | 5.2   | 2.6  | 1.3  | 0.65  | 0.26 | 0.13  | 0.11 |
| point density 1.3 MP camera [ $\mu\text{m}$ ]           | 3.8   | 1.9  | 0.96 | 0.48  | 0.19 | 0.1   | 0.08 |
| point density 2.3 MP camera [ $\mu\text{m}$ ]           | 2.8   | 1.4  | 0.69 | 0.35  | 0.14 | 0.07  | 0.06 |
| point density 5 MP camera / nanoscan [ $\mu\text{m}$ ]  | 1.4   | 0.7  | 0.35 | 0.175 | 0.07 | 0.035 | 0.03 |

**Rayleigh criterion:**

- light intensity has to drop to 73.5% of the max. intensity between the light sources
- standard approach for microscopic observations with the human eye

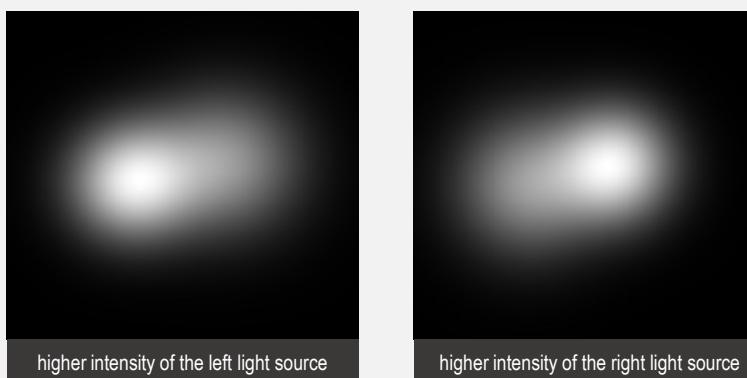
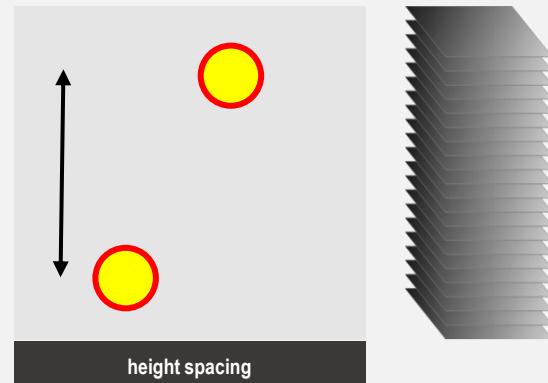
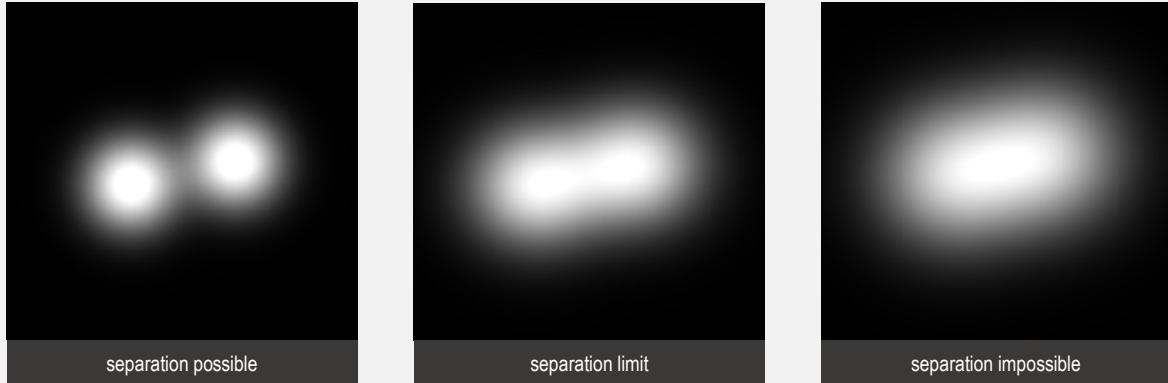
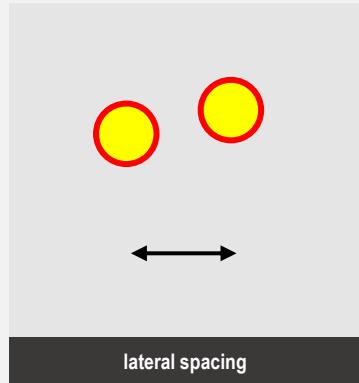
$$\text{resolution} = \frac{0.61 * \lambda}{\text{aperture}}$$

**Sparrow criterion:**

- limit where the light intensity start to drop below the light intensity of the light sources
- address the higher sensitivity of matrix cameras to visualize smaller intensity differences

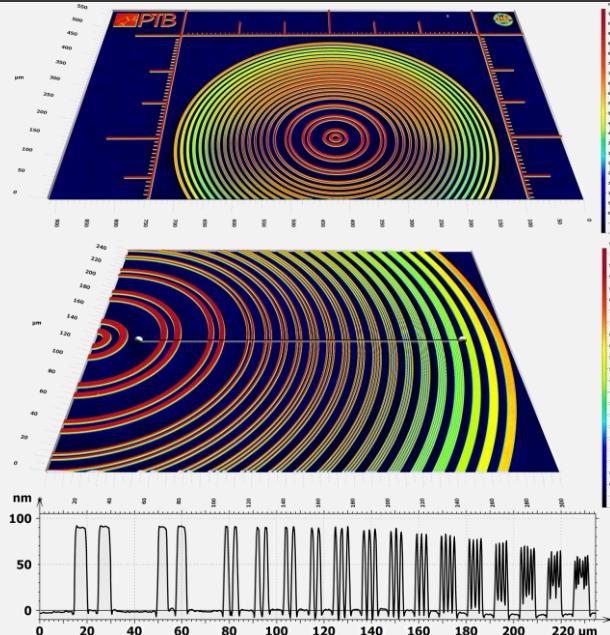
$$\text{resolution} = \frac{0.47 * \lambda}{\text{aperture}}$$

# smartWLI microscope image analysis compared to the 3d scanning

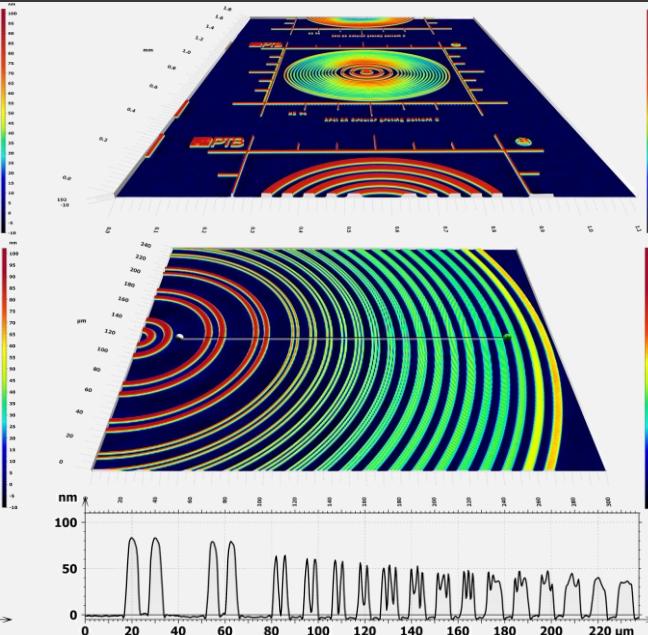


- structures which reflect light may be located on different height levels
- different height levels may enable the separation of structures below the resolution limit
- theoretical consideration based on optical resolution and point density about the lateral system resolution can be confirmed with practical tests

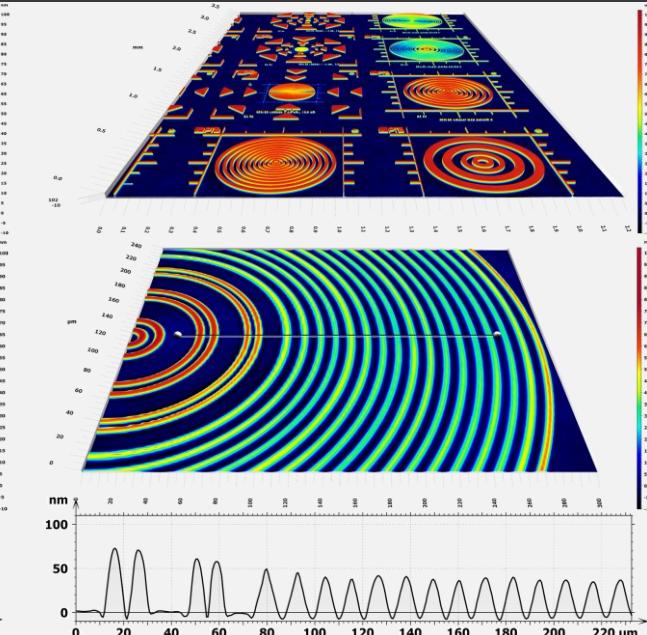
smartWLI compact, 20x objective



smartWLI compact, 10x objective

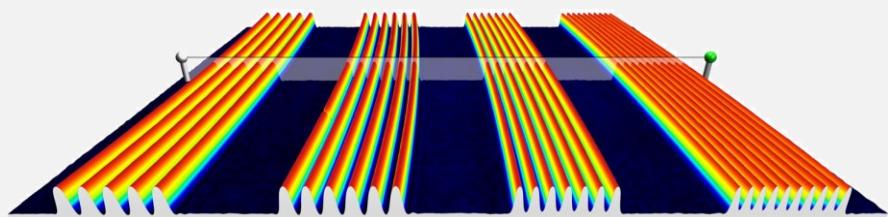


smartWLI compact, 5x objective

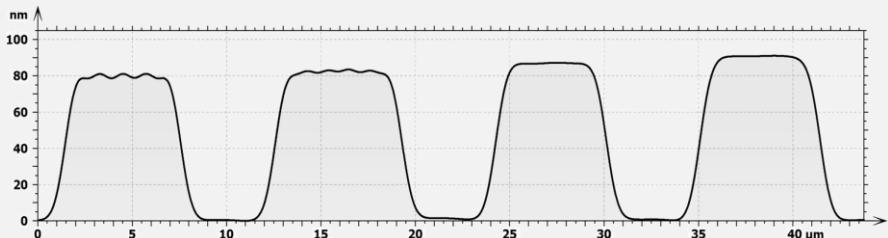


lateral period limit  $D_{LIM}$  (defined in ISO 25178-604 – drop of the measured amplitude of sinus structures as function of the wavelength to 50% ) for the smartWLI compact with 2.3 MP camera

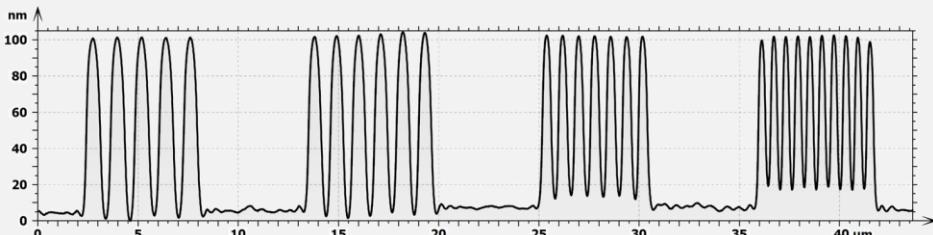
| magnification factor    | 2.5x | 5x  | 10x  | 20x  | 50x  | 100x |
|-------------------------|------|-----|------|------|------|------|
| point density [μm]      | 3.8  | 1.9 | 0.96 | 0.48 | 0.19 | 0.1  |
| $D_{LIM} / \mu\text{m}$ | 10   | 5   | 2.5  | 1.25 | 0.8  | 0.5  |



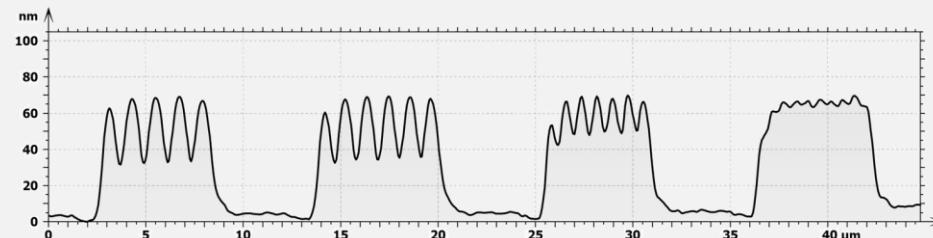
PTB resolution standard, nominal sinus height: 100 nm



tactile measurement (simulation, without system noise and tactile damages)  
tip diameter = 4 μm, high pass filter  $\lambda_s$  = 2.5 μm

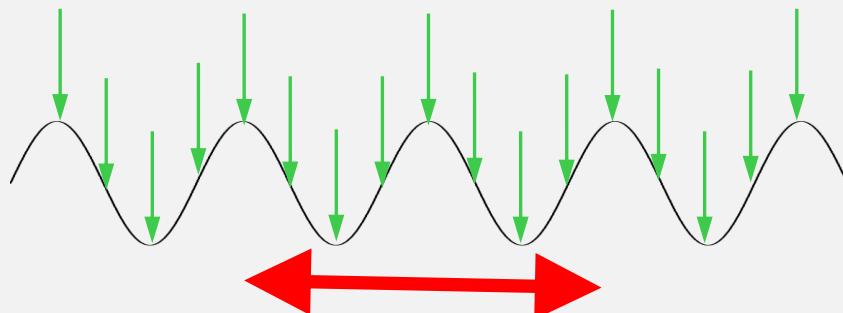


smartWLI nanoscan, 100x objective  
optical resolution = 0.27 μm, point density = 0.03 μm

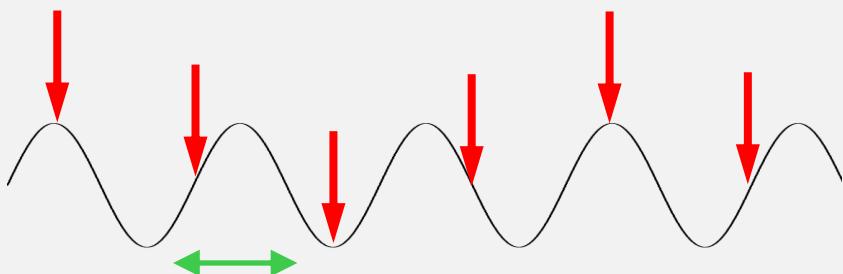


smartWLI compact, 50x objective  
optical resolution = 0.48 μm, point density = 0.2 μm

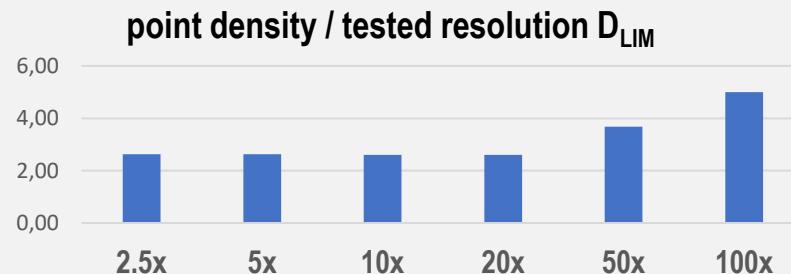
The measured structure amplitude of the sinus structures highly depends on the resolution of the measuring system and the used objective. The effect increases with decreasing structure size. Depending on the real object structures and the measuring task, the optical profiler requires to provide significantly higher resolution than the surface feature structures to be analysed. Furthermore, the observed area of interest has to be selected such that several relevant structures or waves can be evaluated.



point density good / optical resolution too bad

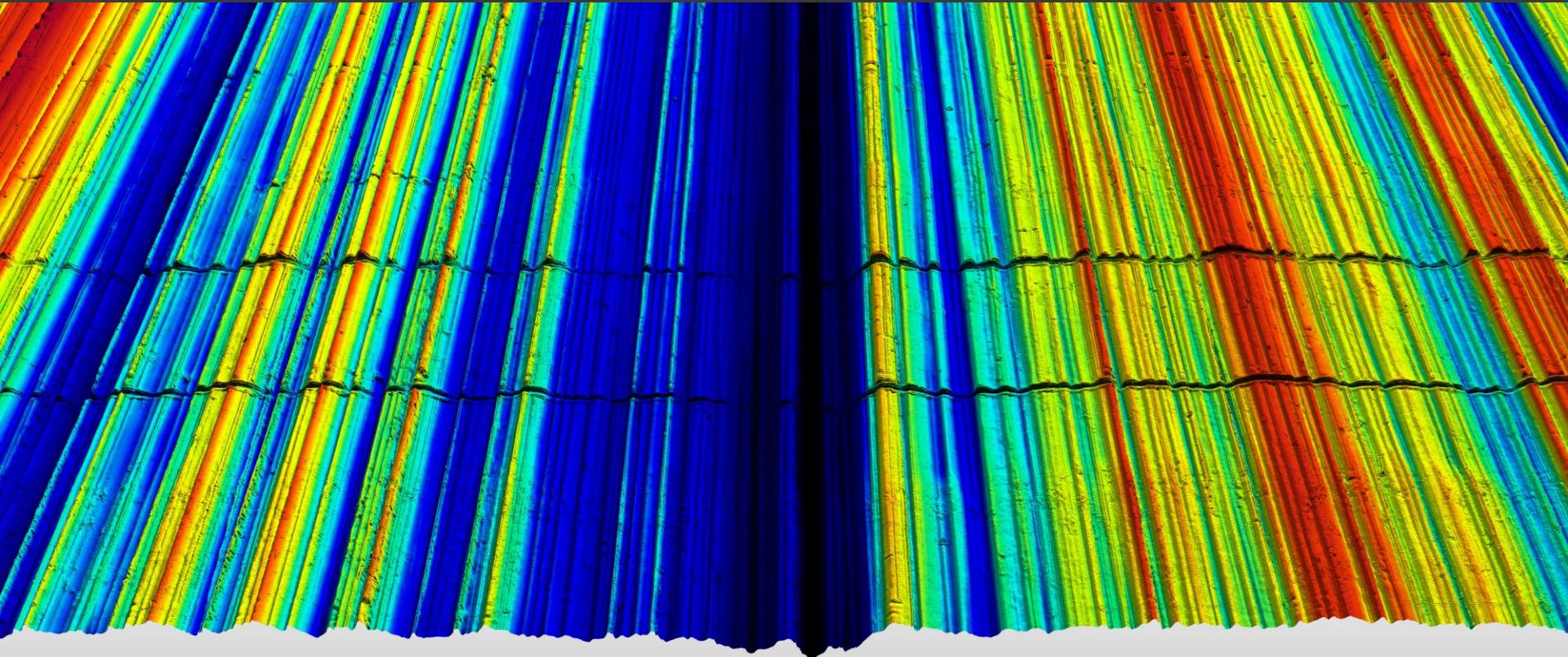


point density too bad / optical resolution ok



practical test of the smartWLI compact with 2.3 MP camera

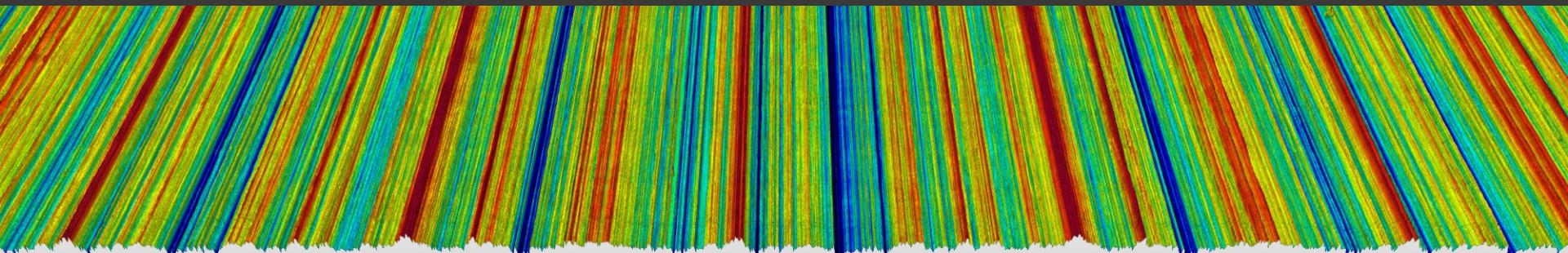
- the resolution of the optical profiler can be limited from the point density and/or the optical resolution
- for one and the same sensor the situation depends from the used objective
- the reason is the not linear relation from objective magnification and optical resolution
- while the point density getting from the 2.5x objective to the 100x objective 40 times higher the optical resolution get only 10.7 times higher



Stylus measuring instruments use a static force of 0.75 mN on the stylus tip with a radius < 2  $\mu\text{m}$  to hold the tip on the surface while performing the scanning process.

This leads to measurable scratches on the measurand. A bigger tip radius will reduce the system resolution.

Using non-tactile optical coherence scanning interferometer demonstrates the limits of tactile measurements while providing the resolution for the visualization of such small damages.



Halle – KNT 4058/01 Nr. 7413 / 2015-12  
certified surface standard

R<sub>a</sub>

0.2059 µm

R<sub>z</sub>

1.505 µm

R<sub>max</sub>

1.642 µm



Tolerance: 0.2000 µm ± 0.0180 µm



Tolerance: 1.490 µm ± 0.1300 µm



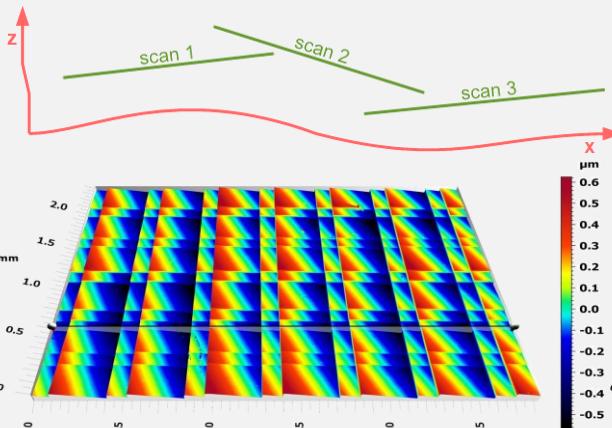
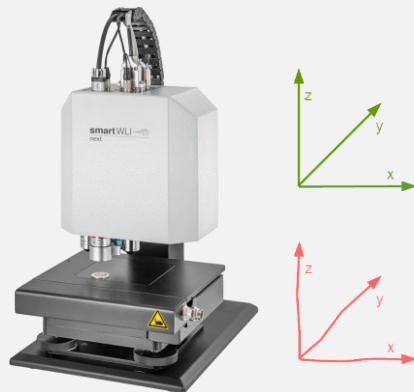
Tolerance: 1.630 µm ± 0.1500 µm

## correct measurement of surface roughness:

- profile roughness measurements are originally standardized for stylus instruments
- even using optical high performance profilers certain rules of the ISO standards have to be respected to get correct measuring results
- ISO 4288: here for nonperiodic profiles with Ra 0.1 ... 2 µm:
  - sampling length and cut off high pass filter: 0.8 mm
  - evaluation length: 4 mm
- ISO 3274: here for nonperiodic profiles with Ra 0.1 ... 2 µm:
  - max. point distance: 0.5 µm
  - stylus tip radius: 2 µm (translated for optical profilers: optical resolution should be better than 2 µm)
  - cut off low pass filter: 2.5 µm

## conclusions for optical profilers:

- the combined specification of ISO 4288 and ISO 3274 regarding point density and profile length require the generation of profiles with at least 8000 measuring points
- since smartWLI systems cannot provide 8000 measuring points in a single scan, multiple profile lines within the given AOI or multiple scans and stitching are required to fulfil the specification of ISO 4288 and ISO 3274
- one of the specific advantage of the smartWLI systems is the ability to scan larger areas with high resolution in a short measuring time

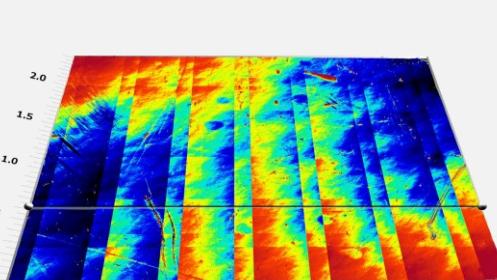


stitching without error compensation

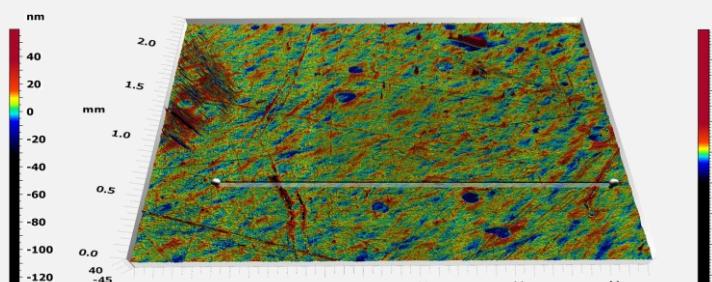
| feature            | flatness | straightness | pitch       | yaw         | technology |
|--------------------|----------|--------------|-------------|-------------|------------|
| sensor             | < 1 nm   | < 1 nm       | single μrad | single μrad | optics     |
| positioning system | >> 1 μm  | >> 1 μm      | >> 10 μrad  | >> 10 μrad  | mechanics  |

### smartSTITCH – the software for optimized stitching results on super smooth optical and semiconductor surfaces:

- mechanical positioning systems cause very small height and angle differences of the coordinate systems for every single scan
- these errors cause visible stitching artefacts
- height compensation using overlapping zones are available in many software evaluation packages like MountainsMap® to reduce the effect of errors
- for typical roughness measurements on machined surface with roughness values over 10 nm, the height compensation is in general acceptable
- even though eliminating some stitching errors, problems may stay visible:
  - using objectives with a lower magnification
  - on smooth surfaces e.g., optics, semiconductors, polished or diamond turned metal surfaces
- smartSTITCH compensates not only height but also angular errors, and provides much better results



stitching with height compensation (MountainsMap®)



smartSTITCH with height and angular compensation