



Harry Skoblenick, P. Eng
WCE Master Expert - RSC
Alstom Transport Canada Inc.
Kingston, Ontario
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Vehicle Suspension and Vehicle / Track Interaction



ALSTOM
•mobility by nature•

PRINCIPLES COURSE



August 26-28,
2025



SEATTLE, WA

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Overview



- Transit Vehicle Suspension
- Track Influence on Stability
- Wheel-to-Rail Interface Criteria
- Wheel Profile Sensitivity
- Improving Wheel Profiles
- Dynamic Modeling – Normal vs Improved
- Conclusion





Passenger Vehicles

- Large number of vehicle designs and types.
- Often custom or “one-off” designs, unique to a city or a route within a city.
- Urban and intercity from streetcars to complete trainsets. At-grade, tunnel, and elevated guideways.
- Light to heavy; low speed to very fast (90kph).
- Includes new Low-floor Light Rail Vehicles (LRV) for urban applications.



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Transit Vehicle Suspensions

Passenger vehicles are designed to provide a *comfortable and stable ride by isolating the vehicle body from track irregularities and ensuring proper wheel-rail contact.*

Instability can occur when a combination of bogie design, springing, vehicle and bogie wheelbase, and track condition may cause unstable dynamics – leading to reduced ride quality.

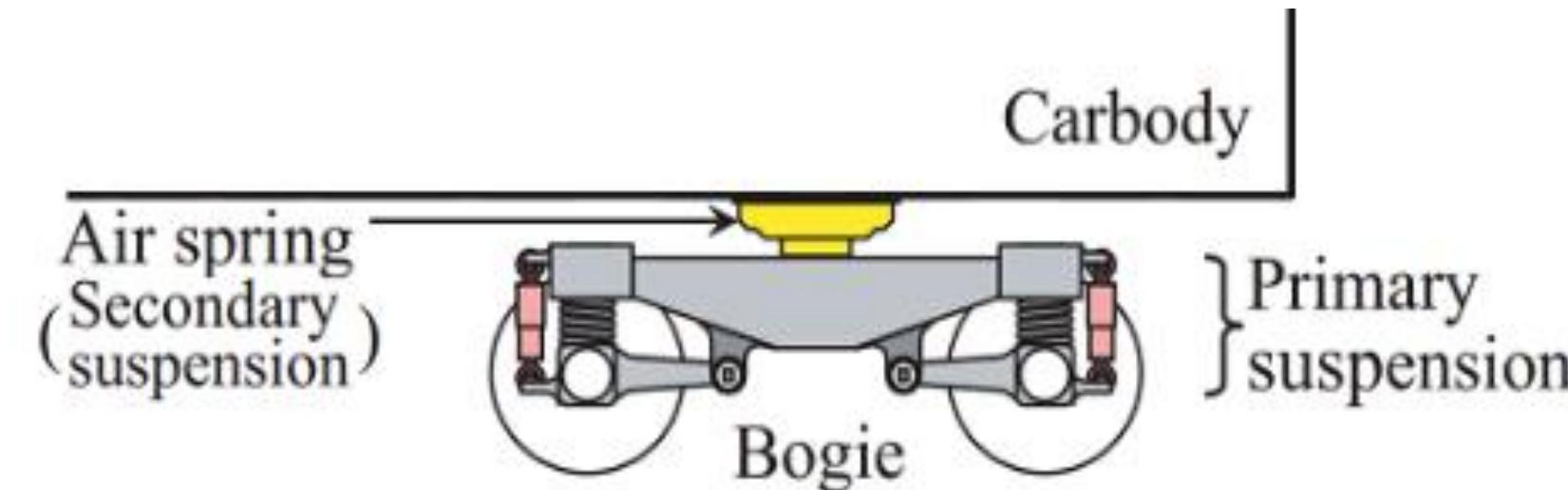


Vehicle Truck Design

Truck (Bogie) serve a number of purposes:

- supporting the body of the rail vehicle.
- running in a **stable** manner on both straight and curved track.
- improving ride quality by absorbing vibrations and minimizing the impact of centrifugal forces when the train runs in curves at high-speed.
- minimizing generation of track surface irregularities and high rail abrasion.



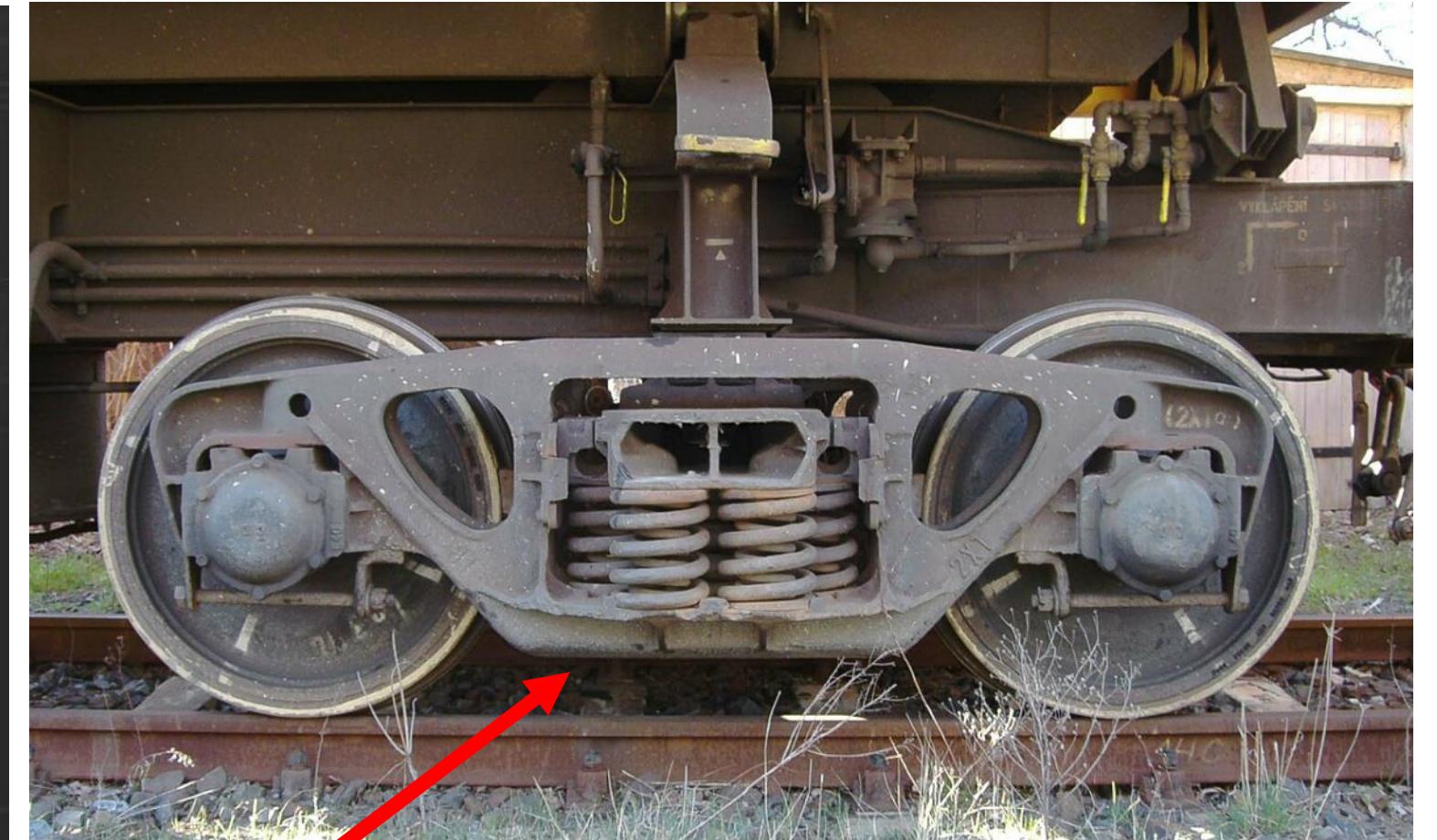
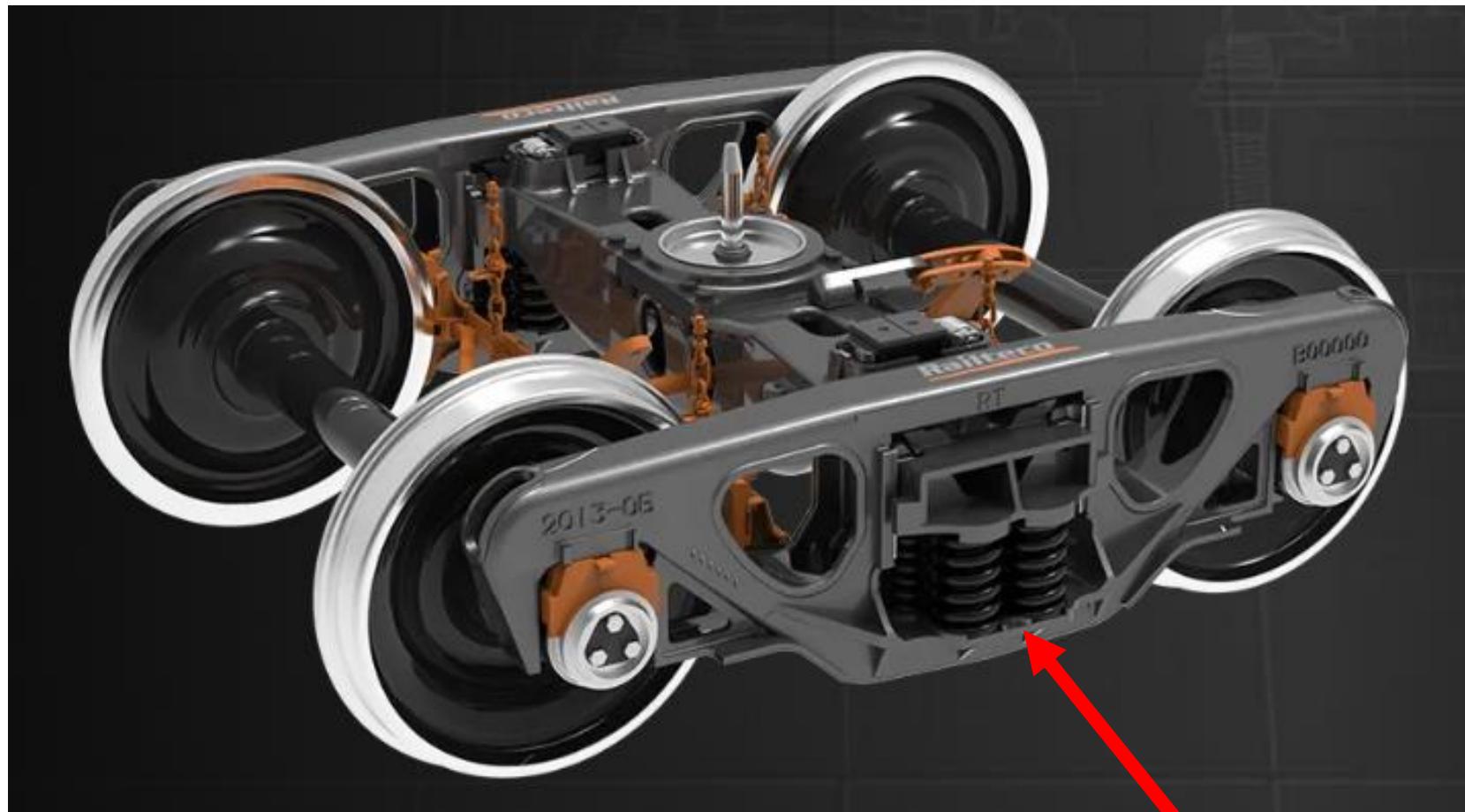


Transit vehicles typically consist of two main ride controls, primary and secondary suspension systems:

- **Primary suspension** - located between the wheelsets and bogie frame, manages higher-frequency vibrations and allows for steering on curves.
- **Secondary suspension** - positioned between the bogie and the car body, handles lower-frequency disturbances, reducing vibrations felt by passengers.



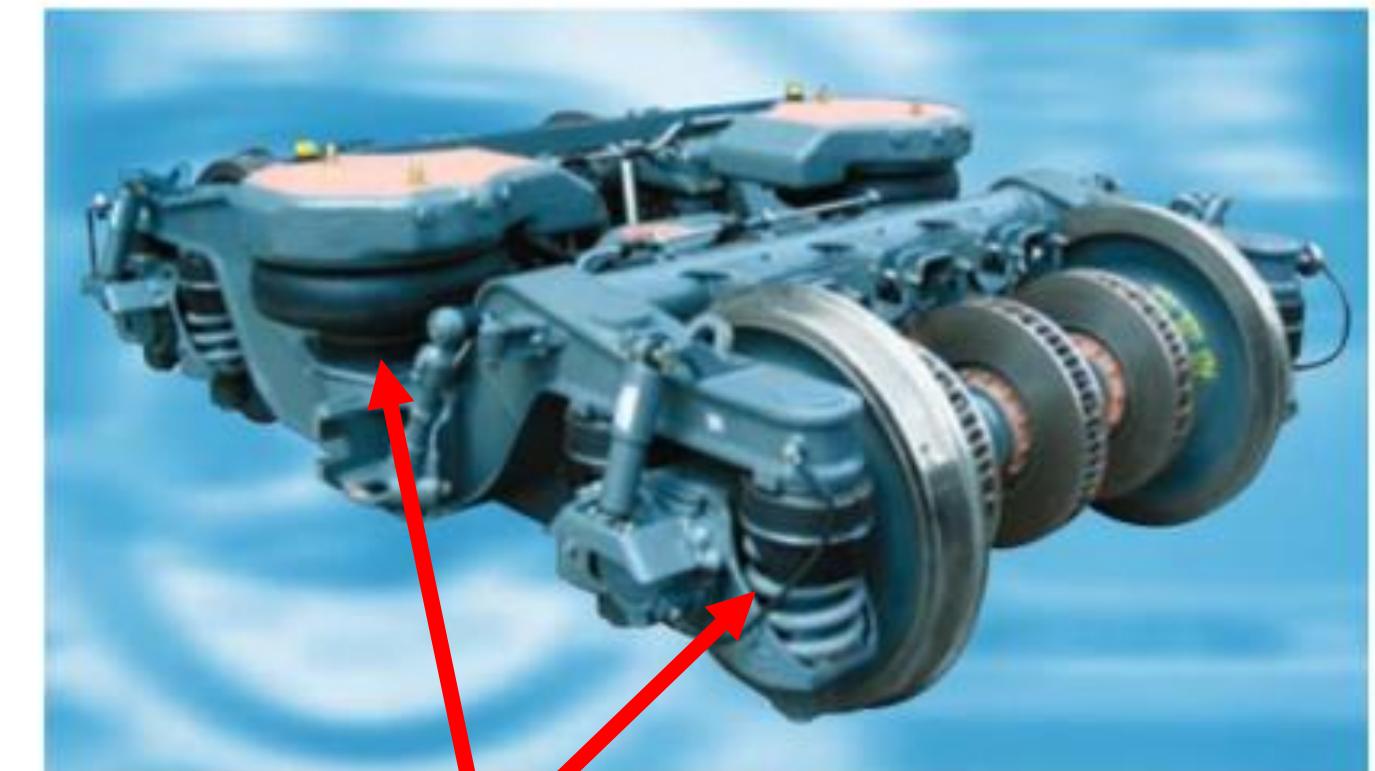
Freight Truck Suspension



'Stiff' Secondary suspension



Transit Vehicle Truck Suspension

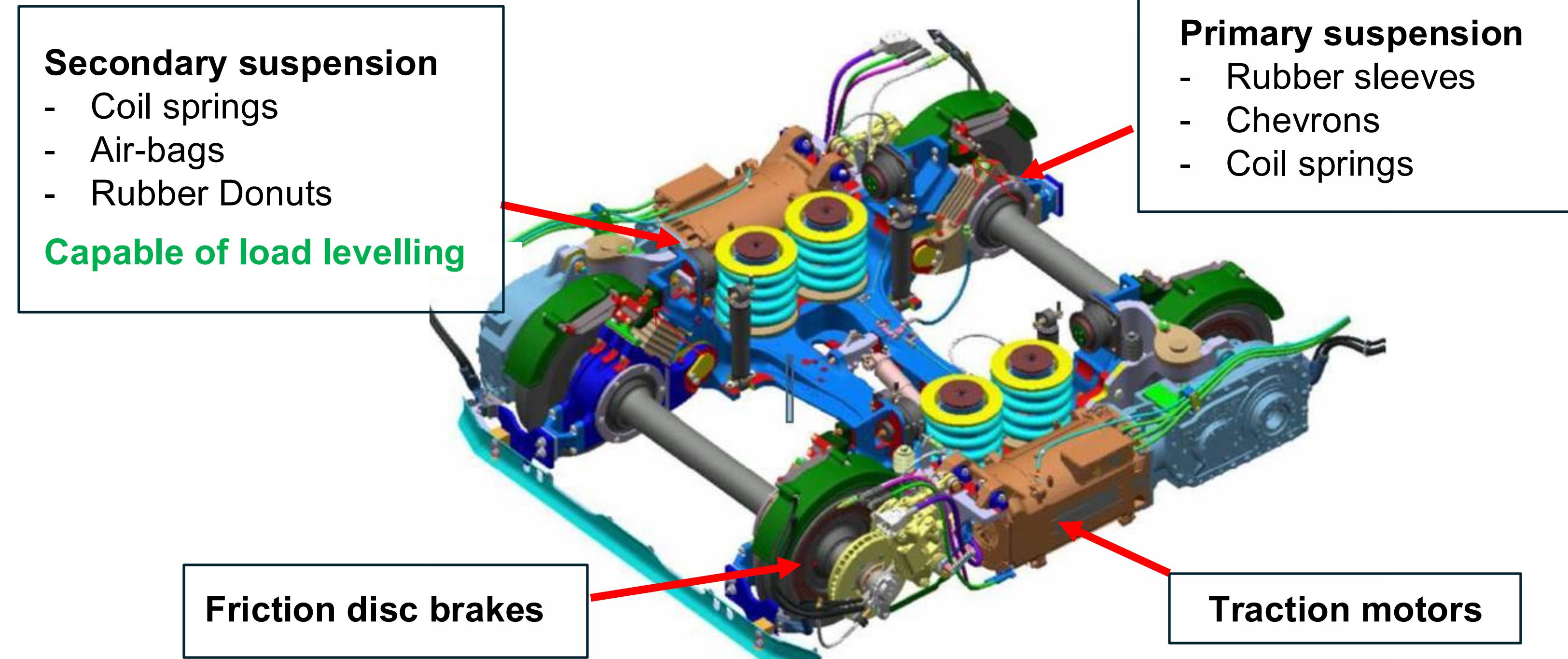


Custom Engineered - Primary and Secondary 'soft' suspensions



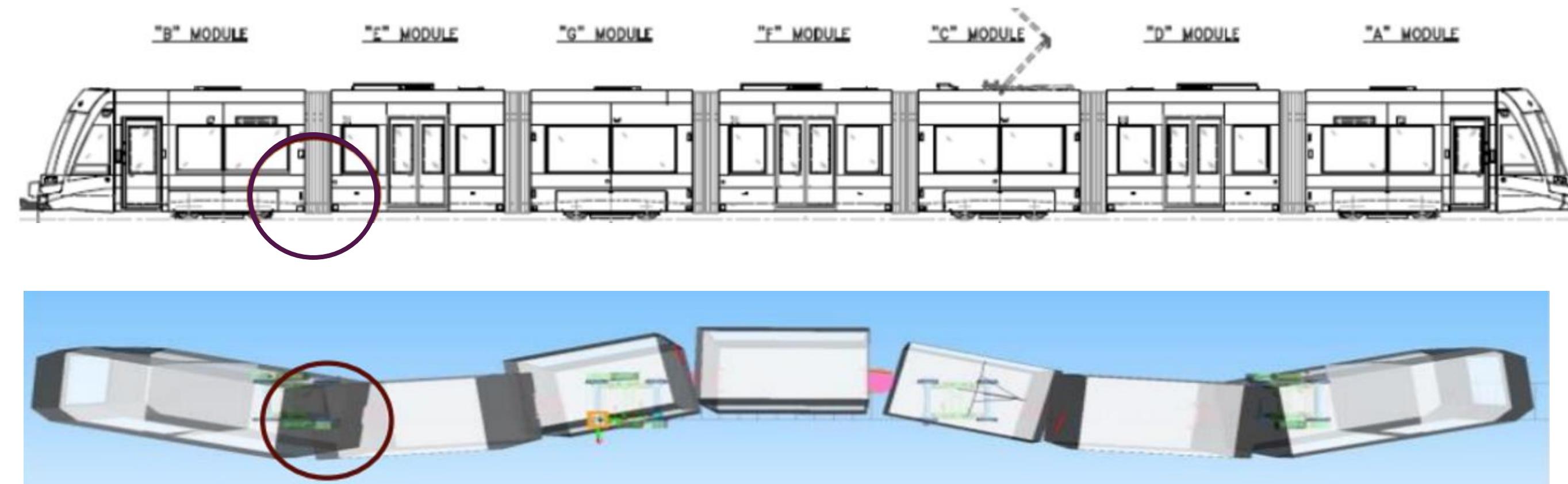


Transit Vehicle Truck Suspension (Low-floor LRV vehicle)



Low-Floor LRV Vehicle

Typical LRV vehicles require fewer bogies with articulation joints between cars.



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Track Installation - North America Requirements

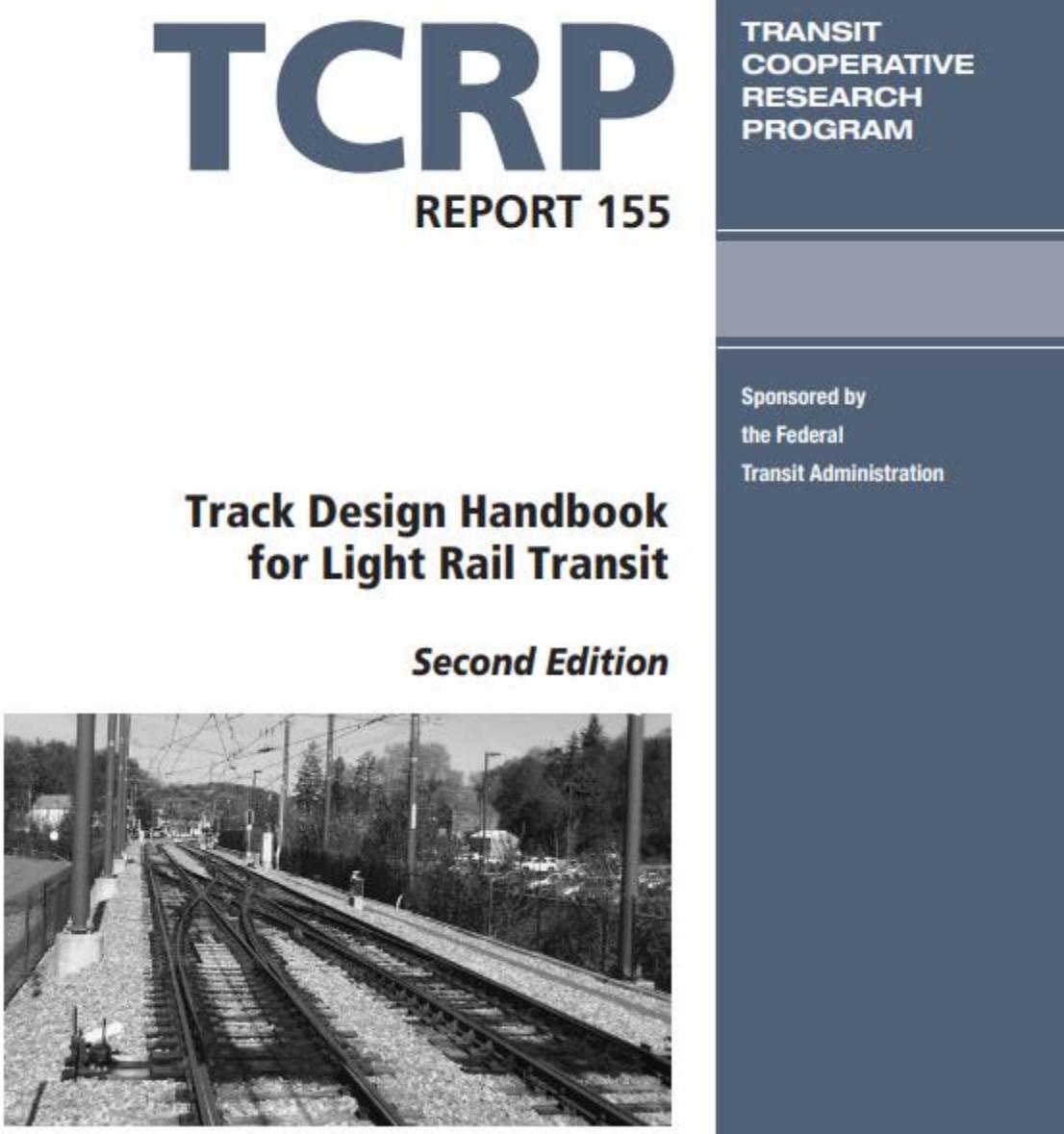


Table 4.2.1 Track construction tolerances

Type of Track	Track Gauge ⁽⁵⁾	Guard Rail Gauge ⁽⁵⁾	Cross Level ⁽⁵⁾	Construction Tolerances		Location Tolerances	
				Horizontal Alignment Deviation ^{(1) (5)}	Vertical Alignment Deviation ^{(1) (5)}	Horizontal Alignment Variable ⁽⁶⁾	Vertical Alignment Variable ⁽⁶⁾
Ballasted concrete cross ties (Main Line)	+/- 1/16" [+/- 1 mm]	+1/8", -1/16" [+3, -1 mm]	+/- 1/8" [+/- 3 mm]	1/4" [6 mm] ⁽²⁾	1/4" [6 mm] ⁽³⁾	1/2" [13 mm]	1/2" [13 mm]
Ballasted timber cross ties (Main Line)	+/- 1/8" [+/- 3 mm]						
Ballasted concrete cross ties (Yard)	+/- 1/16" [+/- 1 mm]	+1/8", -1/16" [+3, -1 mm]	+/- 3/16" [+/- 5 mm]	3/8" [9 mm]	3/8" [9 mm]	1/2" [13 mm]	1/2" [13 mm]
Ballasted timber cross ties (Yard)	+3/16", -1/16" [+5, -1 mm]						
Direct Fixation	+1/8", -1/16" [+3, -1 mm]	+1/8", -1/16" [+3, -1 mm]	+/- 1/8" [+/- 3 mm]	1/4" [6 mm] ⁽²⁾	1/4" [6 mm] ⁽³⁾	1/4" [6 mm]	1/4" [6 mm]
Embedded	+1/8", -1/16" [+3, -1 mm]	+1/8", -1/16" [+3, -1 mm]	+/- 1/8" [+/- 3 mm]	1/4" [6 mm] ⁽²⁾	1/4" [6 mm] ^{(3) (4)}	1/4" [6 mm]	1/4" [6 mm]

⁽¹⁾ Deviation is the allowable construction discrepancy between the standard theoretical designed track and the actual constructed track.



Track Installation – ROC Criteria

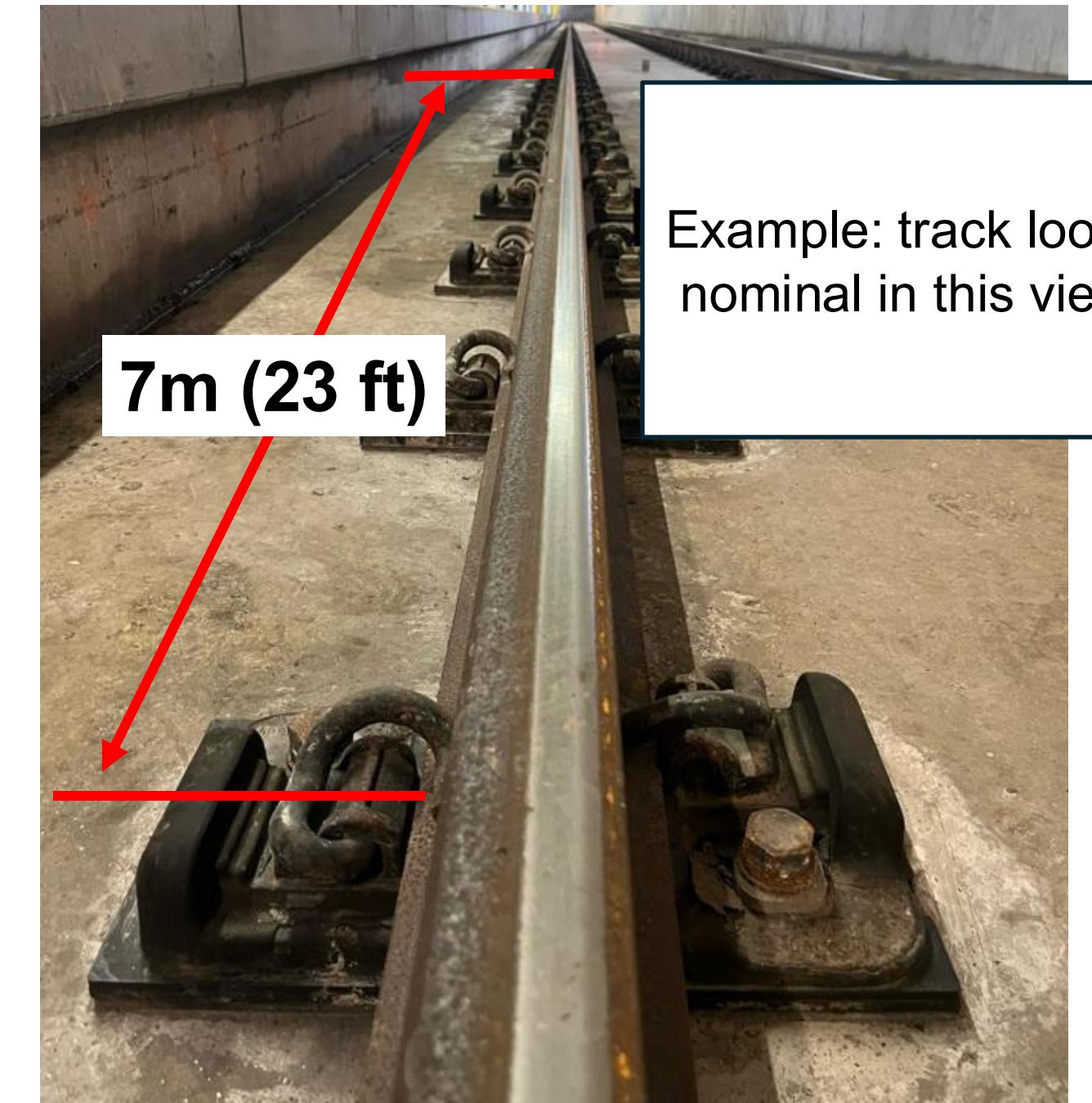
- (1) Deviation is the allowable construction discrepancy between the standard theoretical designed track and the actual constructed track.
- (2) Deviation (horizontal) in station platform areas shall be: zero inches [millimeters] toward platform, 0.125 inches [3 millimeters] away from platform.
- (3) Deviation (vertical) in station platform areas shall be: plus 0, minus 0.25 inches [6 millimeters] or in conformity with current ADAAG requirements.
- (4) Deviation at top of rail to adjacent embedment surface shall be plus 0.25 inches [6 millimeters] minus 0.
- (5) Rate of change variations in gauge, horizontal alignment, vertical alignment, cross level, and track surface shall be limited to 0.125 inches [3 millimeters] per 15 feet [4.6 meters] of track.
- (6) Variable is the allowable construction discrepancy between the theoretical mathematized and the actual as-built locations of the track. Tracks adjacent to fixed structures shall consider the as-built tolerances of the structures.





DF Rail Fasteners

Rail Fasteners @ 750mm spacing



Example: track looks nominal in this view

Case Study

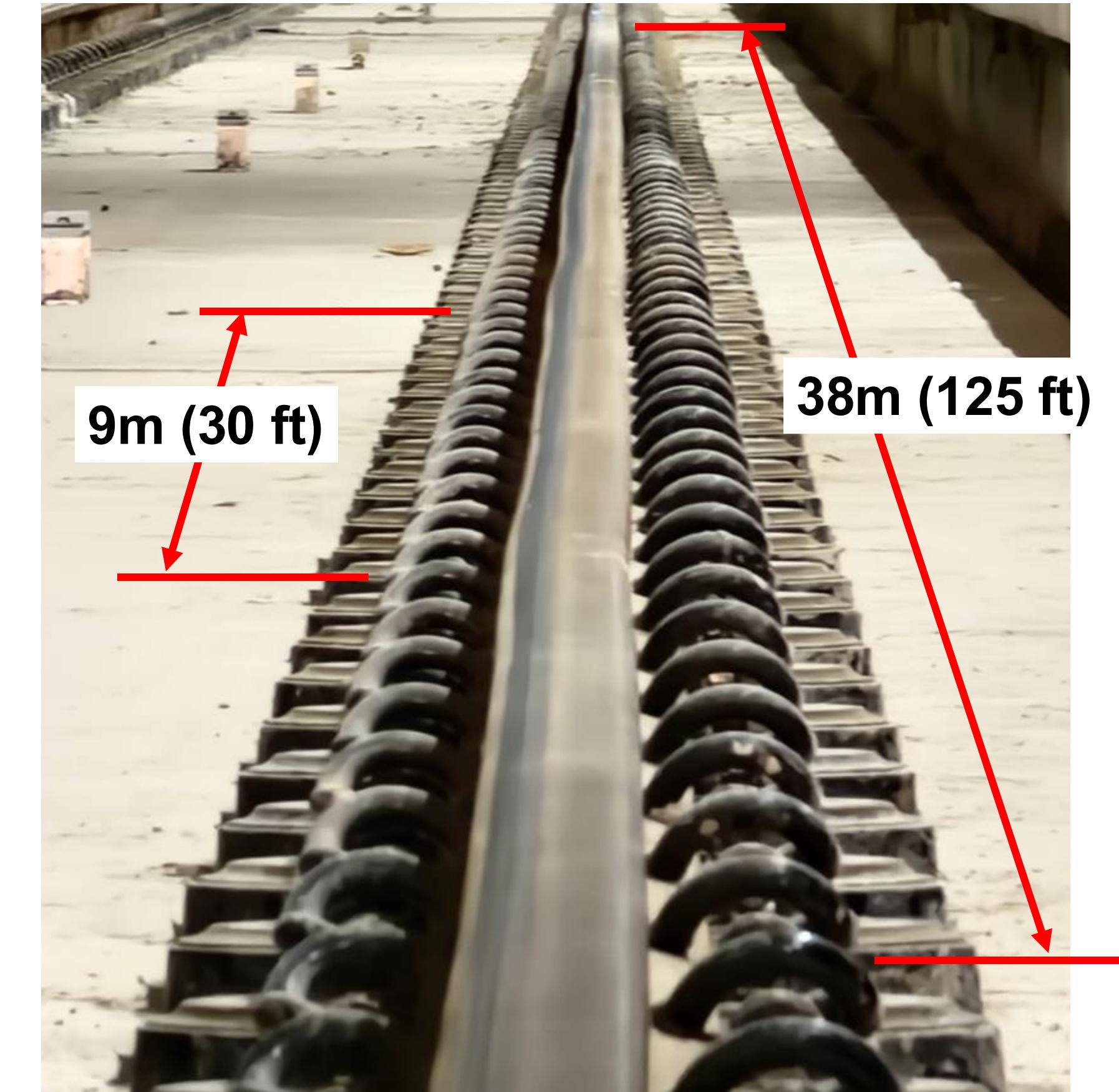
TCRP ROC Criteria - Horizontal Deviation:

3mm / 4.6m change limit (1/2 wave)

Shown - Rail Fasteners @ 750mm spacing

Shown - Embedded Track wave @ 3mm / 9m (30 ft) pitch often 150-200m length.

At 35kph, Horizontal cyclic input frequency to bogie @ >1.1 Hz impacting ride quality



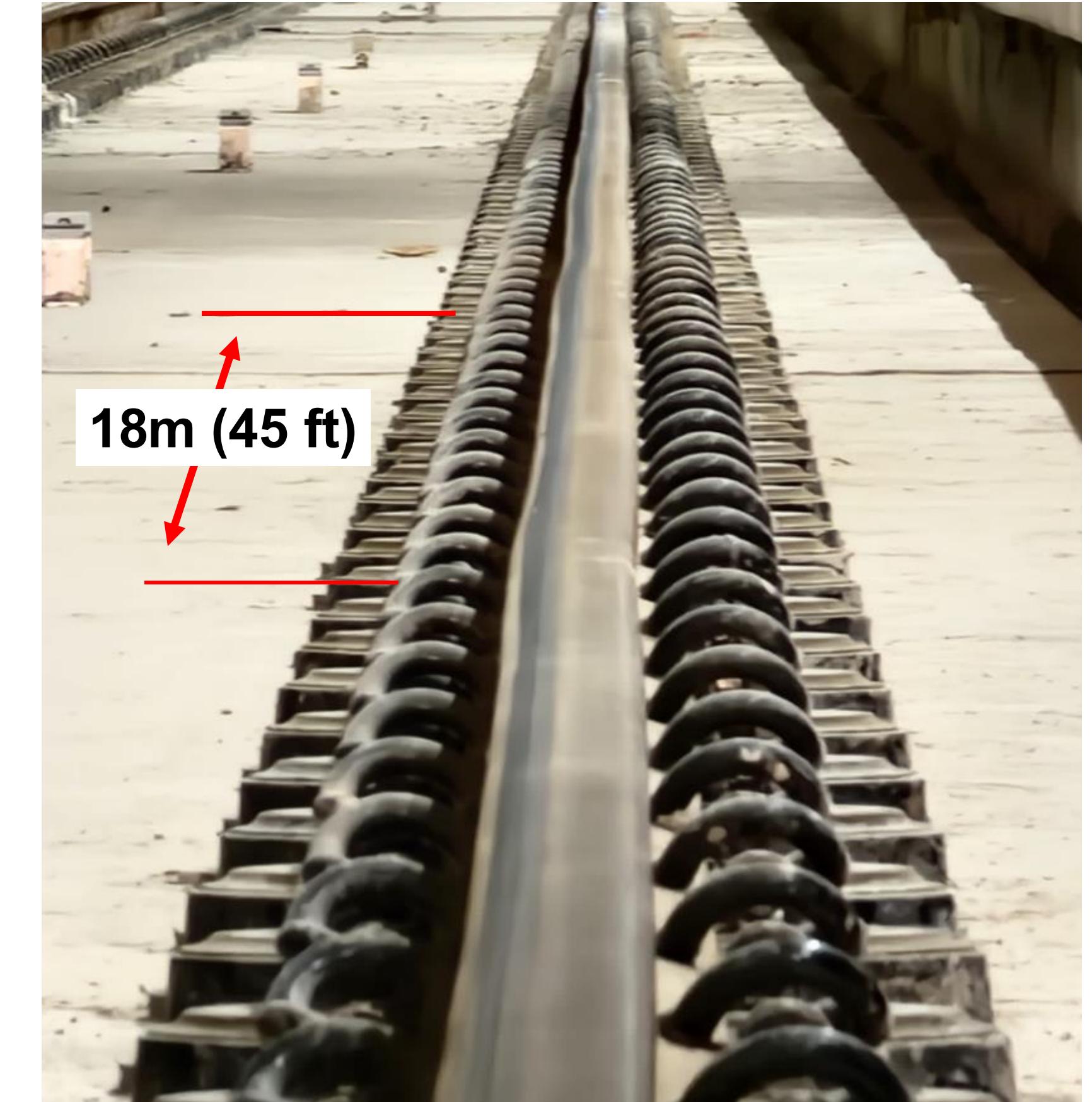
Case Study

**Class A ROC Criteria –
Horizontal Deviation:
3mm / 9m change limit (1/2 wave)**

**Example - Embedded Track
wave @ 3mm / 18m (45 ft) pitch
often 150-200m length.**

**At 35kph, Horizontal cyclic input
frequency to bogie @ >0.55Hz**

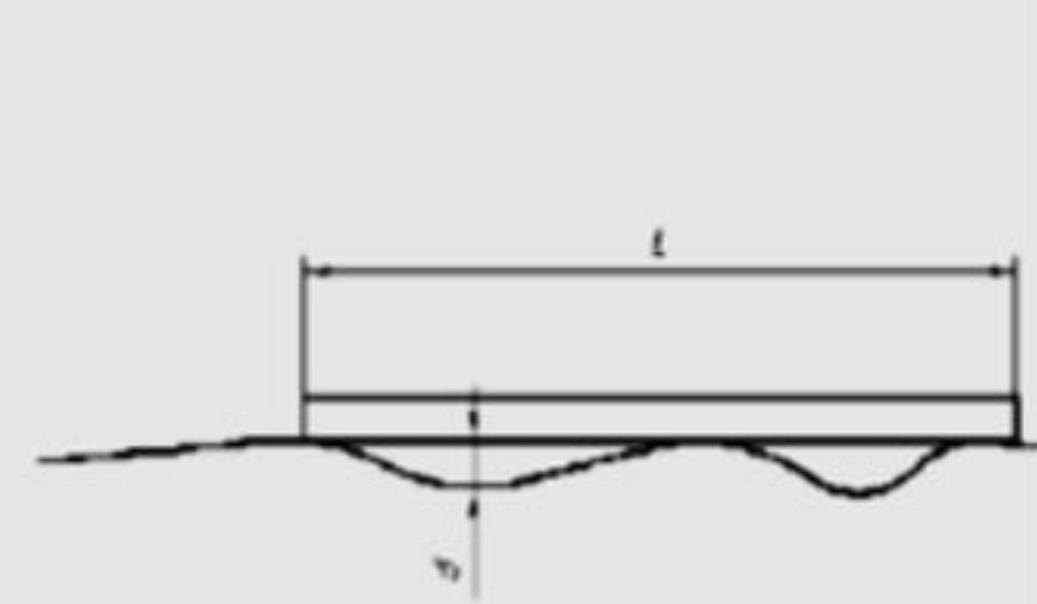
Improved ride quality



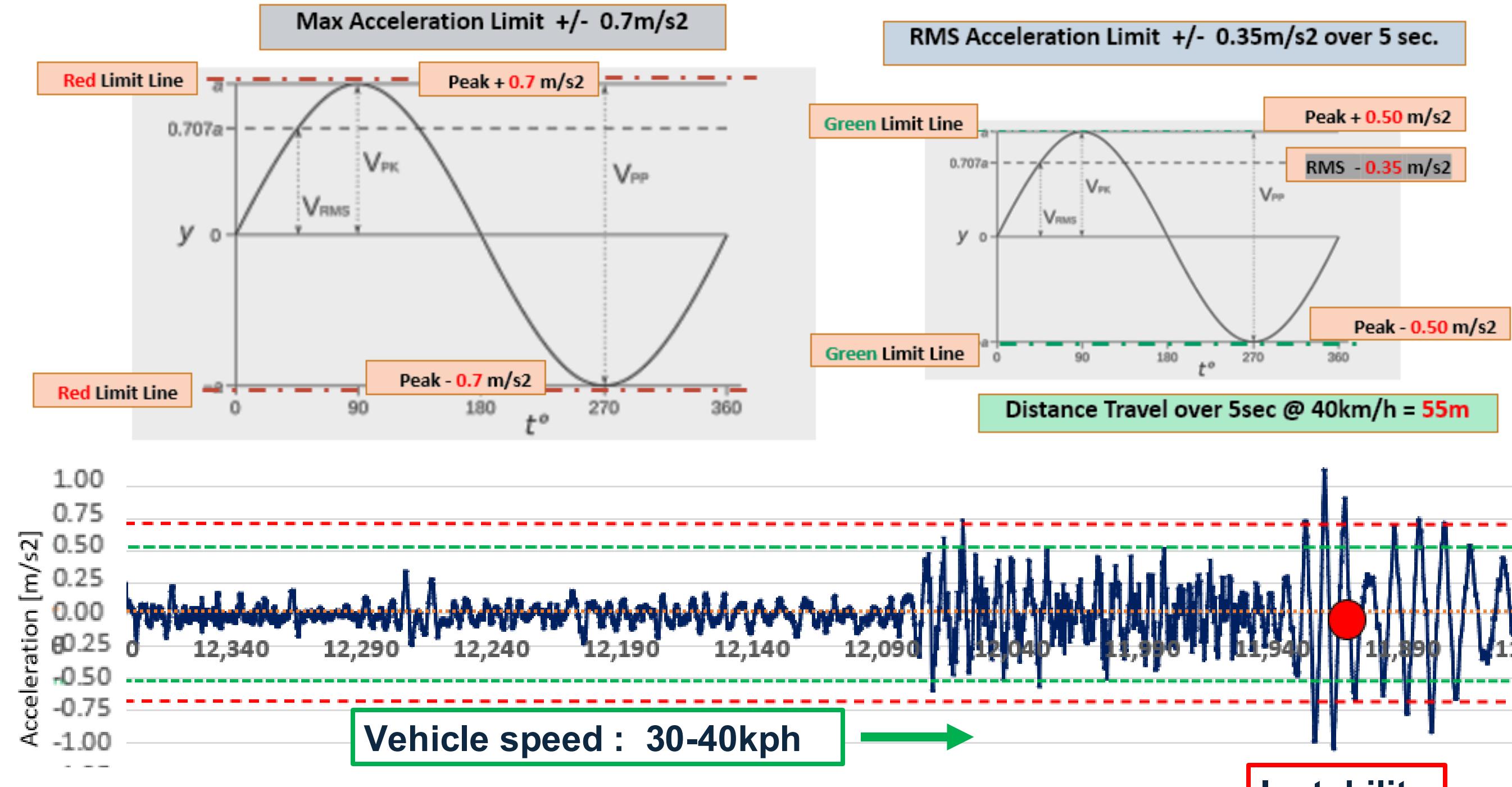
Track Straightness – Improves ROC

When specifying 115RE rails for new track installations consider **Class A** requirements for rail straightness (**3mm/10m ROC**) vs TCRP standard **Class B** with **3mm/4.6m** ROC.

	Class B		Class A	
	<i>d</i>	<i>L</i>	<i>d</i>	<i>L</i>
Vertical flatness V	$\leq 0.4 \text{ mm}$	3 m°	$\leq 0.3 \text{ mm}$	3 m°
	$\leq 0.3 \text{ mm}$	and 1 m°	$\leq 0.2 \text{ mm}$	1 m°
Horizontal flatness H	$\leq 0.6 \text{ mm}$	1.5 m°	$\leq 0.45 \text{ mm}$	1.5 m°




Case Study – Poor Ride Quality





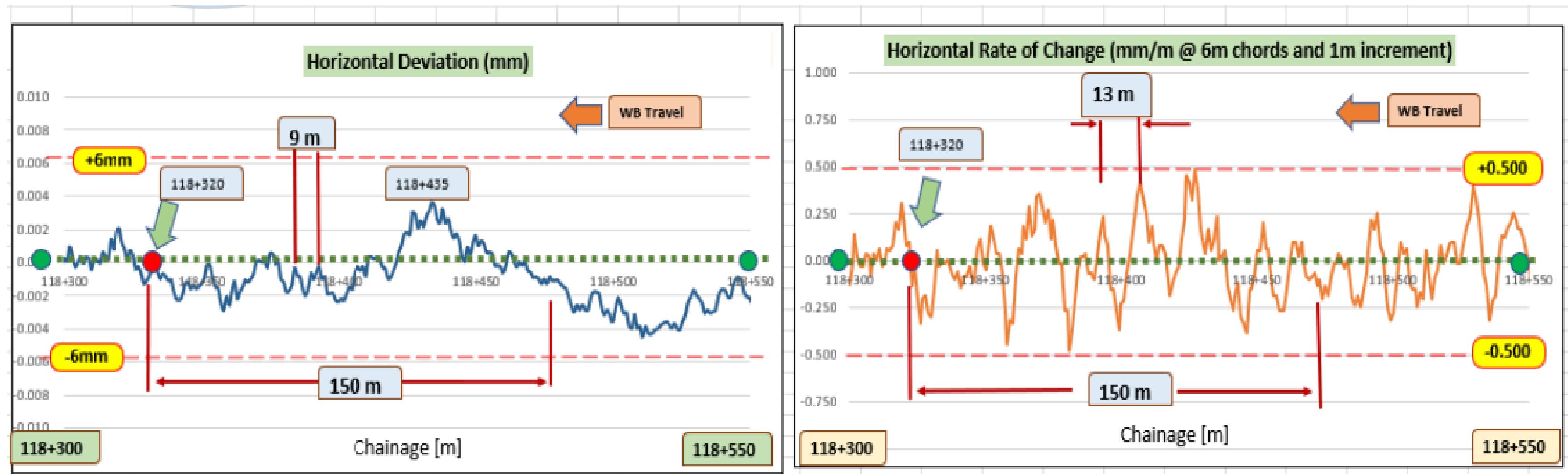
Measuring Track Survey Data – Gauge, Vertical, and Horizontal Deviations



**GEDO survey
tool identifies
each rail head
position to
within +/-1mm
accuracy**

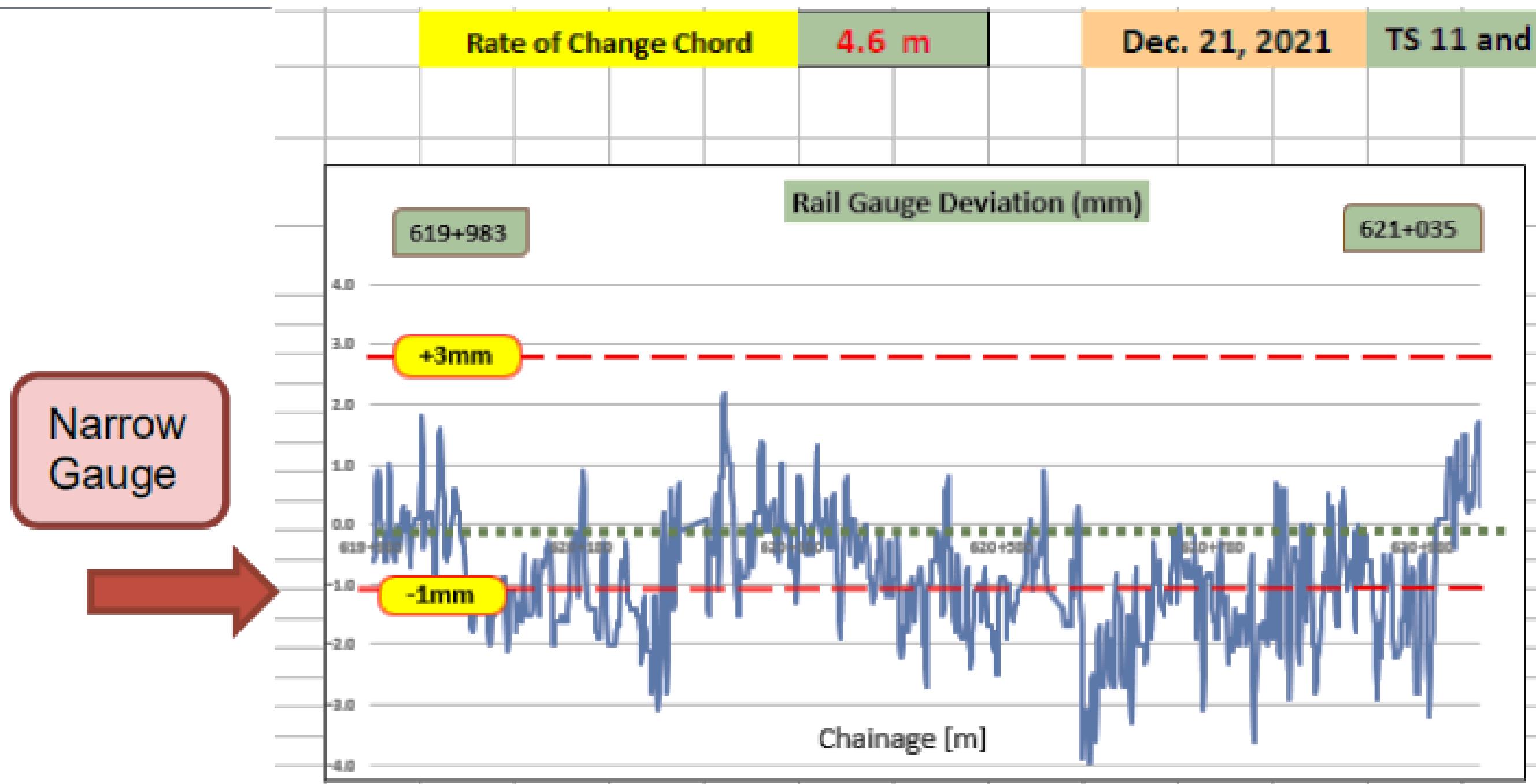
Case Study – Analysis of Horizontal Deviations and *ROC* towards identifying and correcting ride quality

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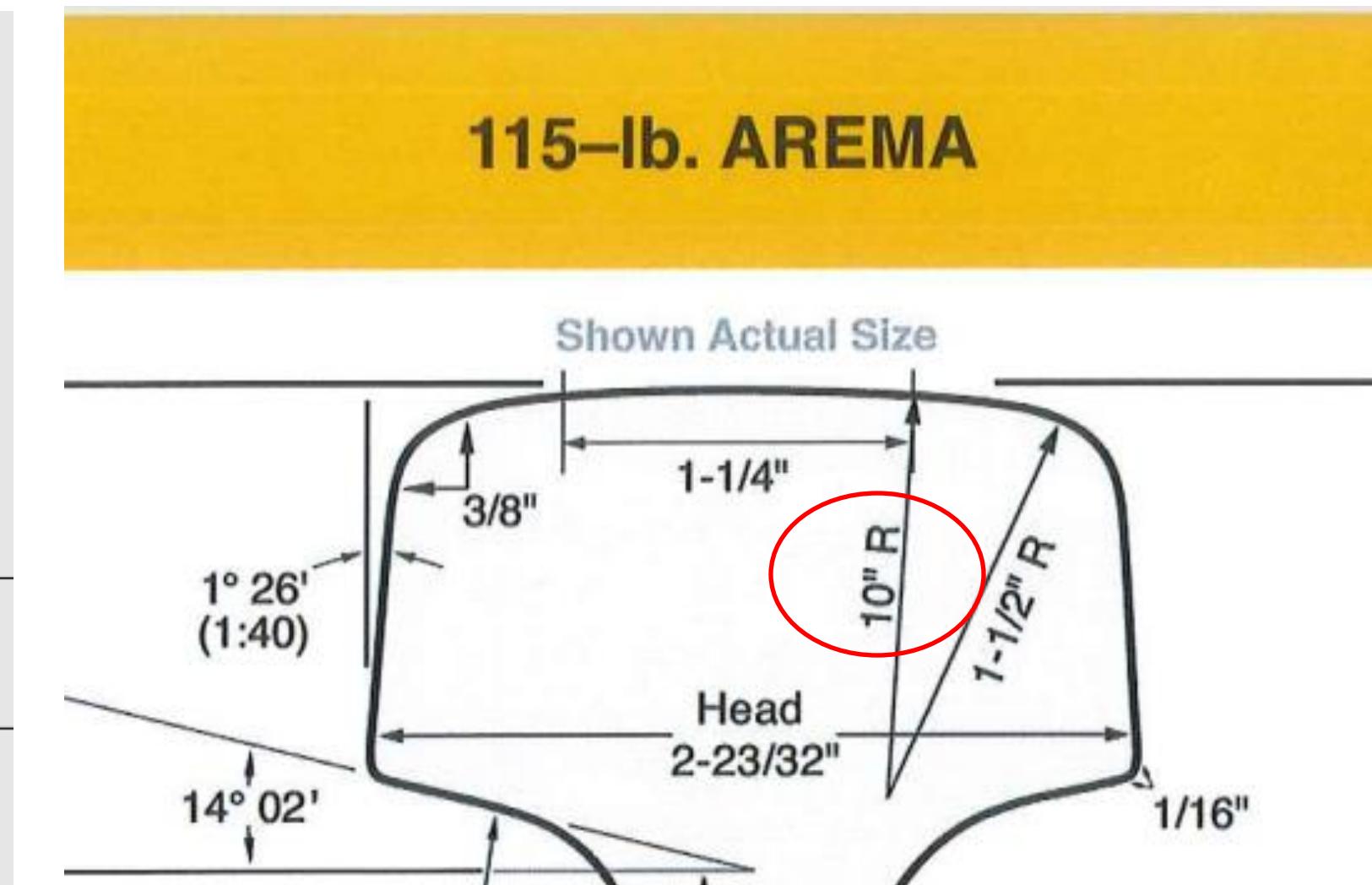
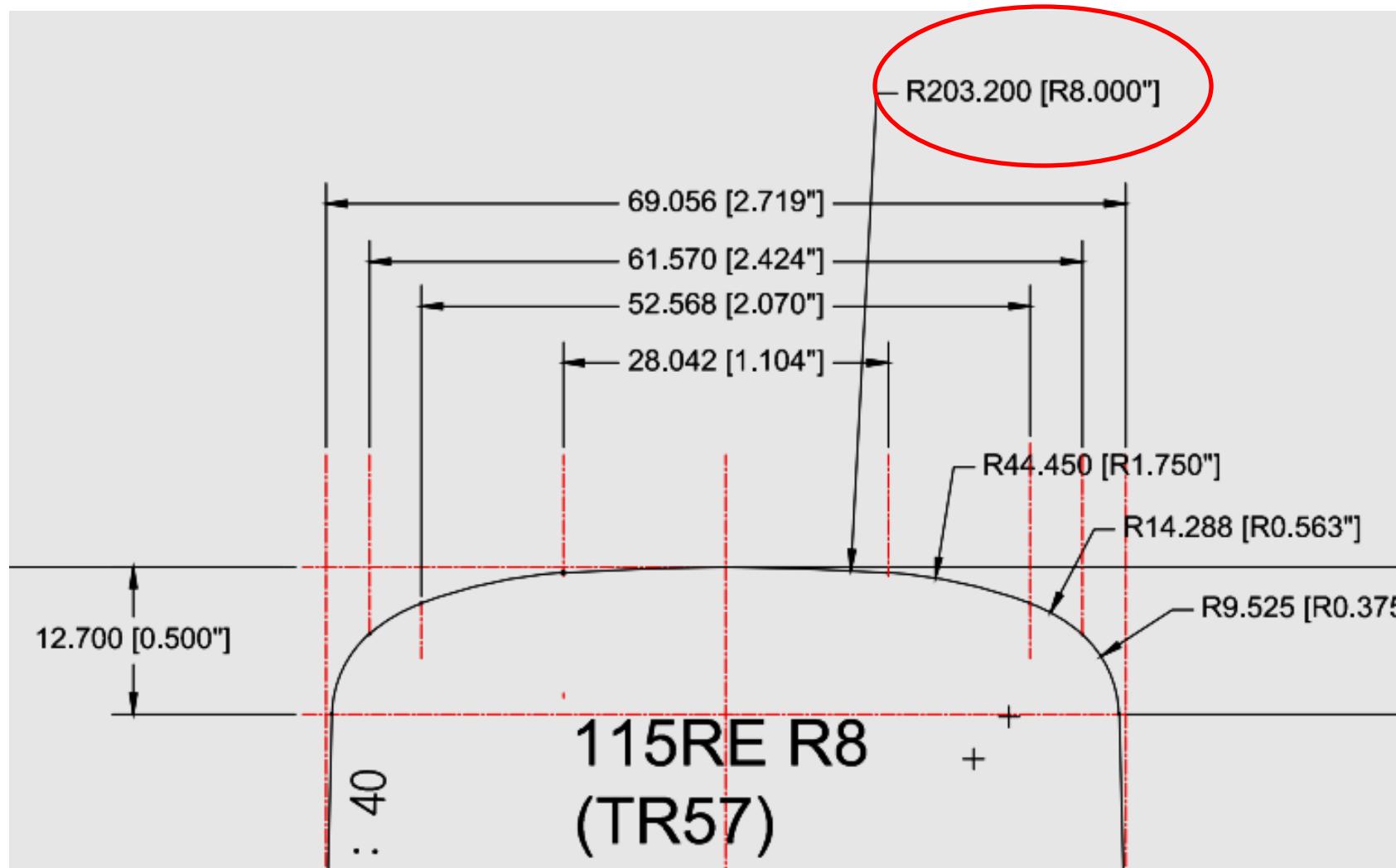


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Case Study – Analysis for locating and correcting Narrow Gauge problems



Rail Head Profile – 115RE 8" or 10" radius



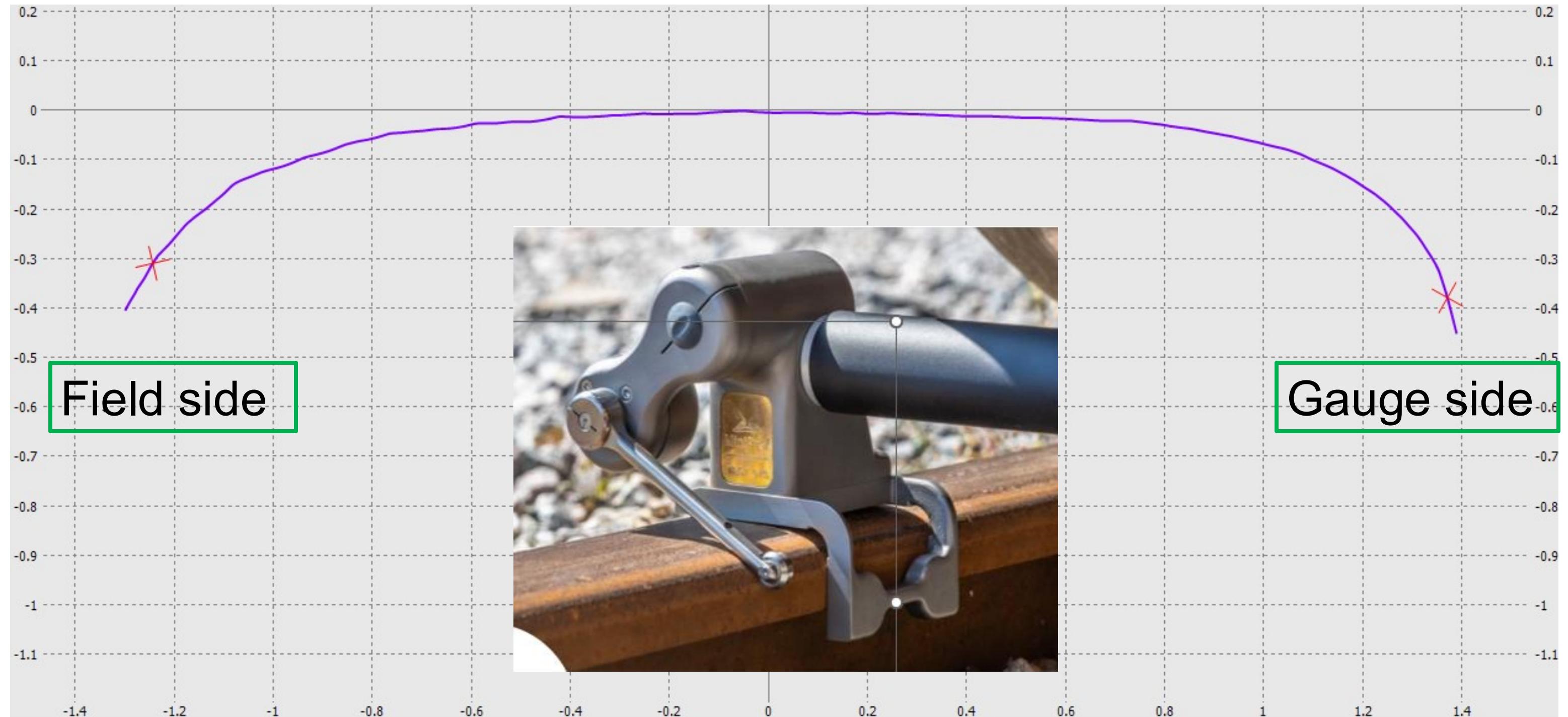
Due to improved stability, Transit wheel profiles optimized for 8" head radius

Rail head has flatter profile for freight wheels



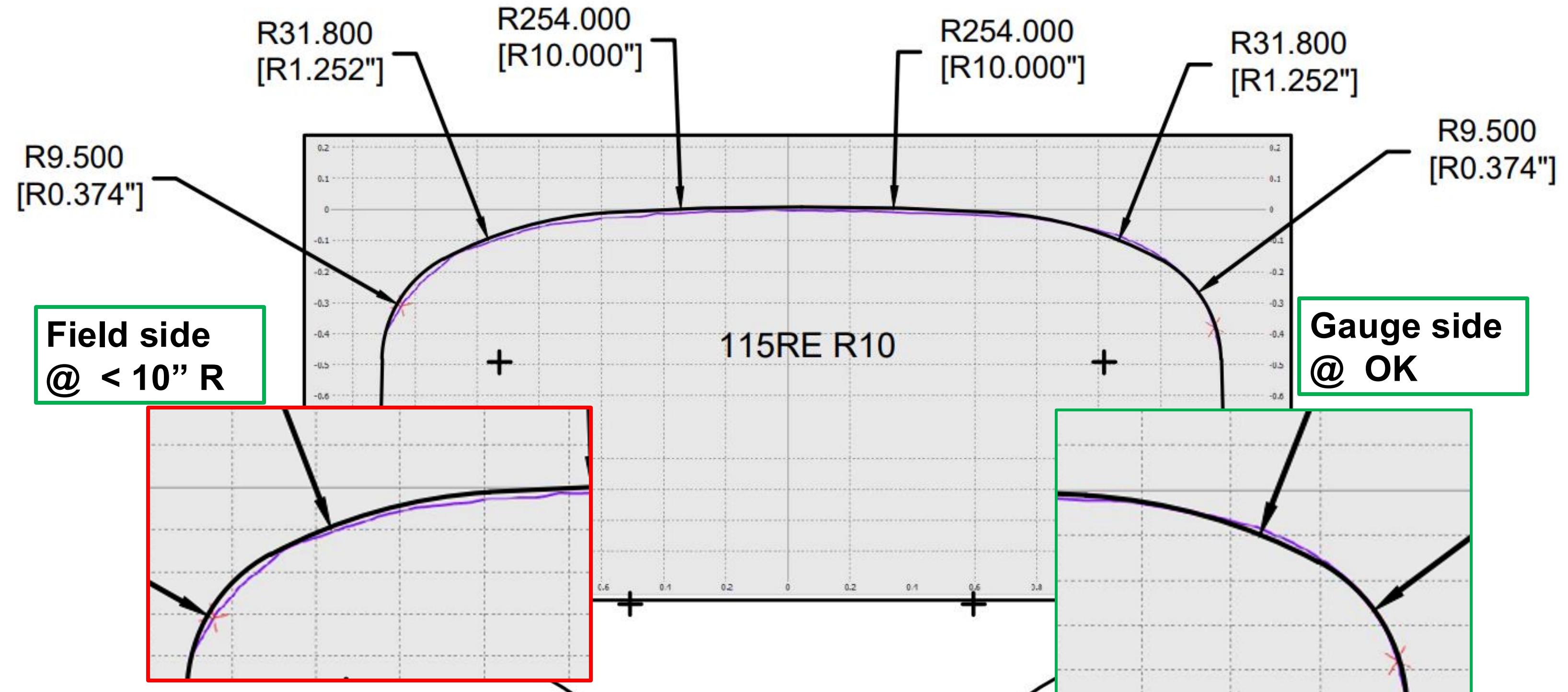


Case Study - Measuring 115RE Rail Head Profile with MiniProf Tool (*no cant*)



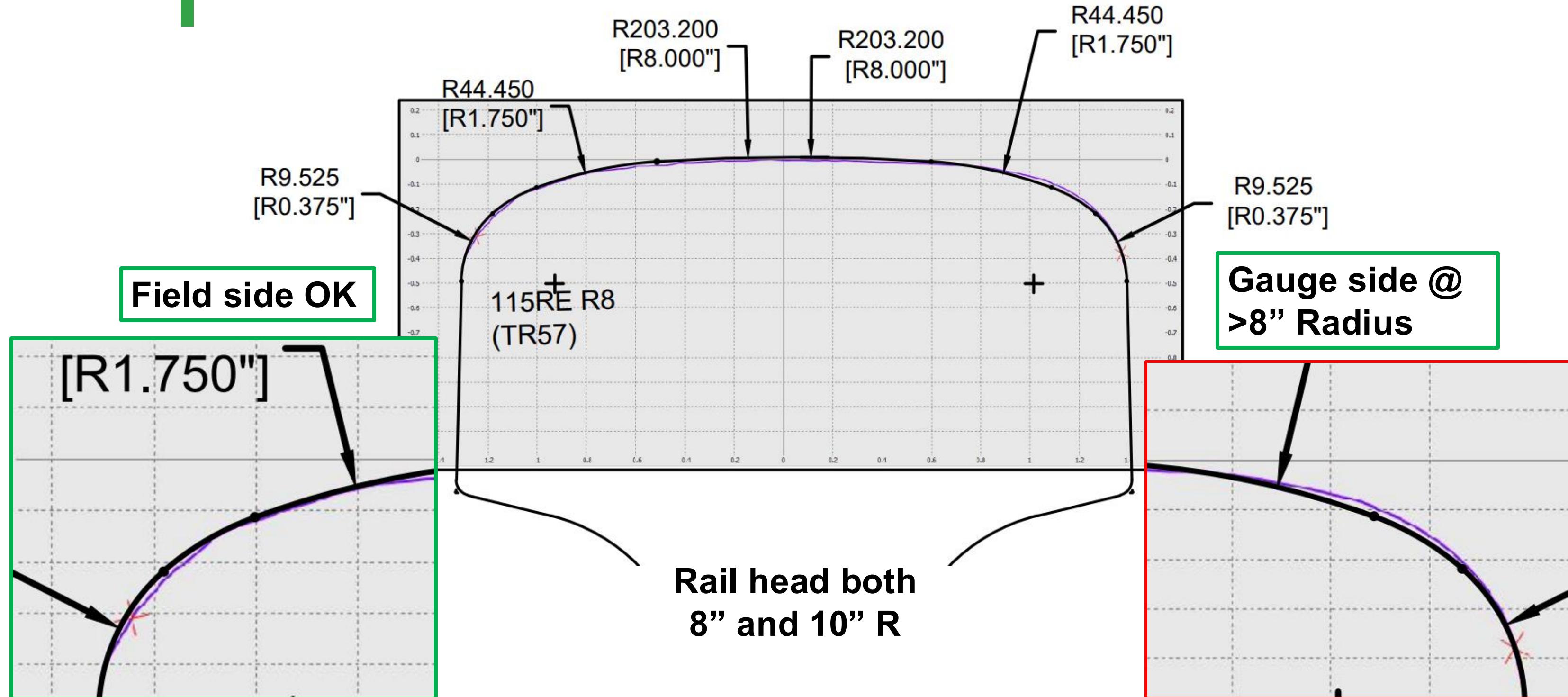


Comparative Analysis with 115RE 10" Rail Head Profile





Comparative Analysis with 115RE 8" Rail Head Profile



AREMA Tolerance - 115RE Rail Head

Table 4-2-2. Section Tolerances

Description	Tolerance, Inches			
	Rail		Trackwork Rail	
	Plus	Minus	Plus	Minus
Height of rail (measured within one foot from end)	0.030	0.015	0.030	0.015
Width of rail head (measured within one foot from end)	0.025	0.025	0.015	0.015
Thickness of web	0.040	0.020	0.040	0.020
Fishing template standout	0.060	0.000	0.030	0.000
Asymmetry of head with respect to base	0.050	0.050	0.030	0.030
Width of base	0.040	0.040	0.030	0.030
Flange height	0.025	0.015	0.015	0.015
Note 1: Base concavity shall not exceed 0.010 inch. Convexity is not permitted. Note 2: No variation will be allowed in dimensions affecting the fit of the joint bars, except that the fishing template may stand out not to exceed 0.060 inch laterally. Note 3: All four corners of the rail base shall have the radii according to the drawing $\pm 1/32$ inch. Any disputes shall be analyzed on an Optical Comparator. Note 4: The section of the rails to be used in AREMA trackwork shall conform to the design specified by the purchaser subject to the tolerances listed under trackwork rail above. Note 5: Head radius to be within (\pm) 2 inches per Figure 4-2-40 . Note 6: On up to 5% of the order, the height of the rail plus tolerance can be between 0.030 and 0.040 inches, if the purchaser's authorized representative and the manufacturer agree. This exception does not apply to trackwork rail.				

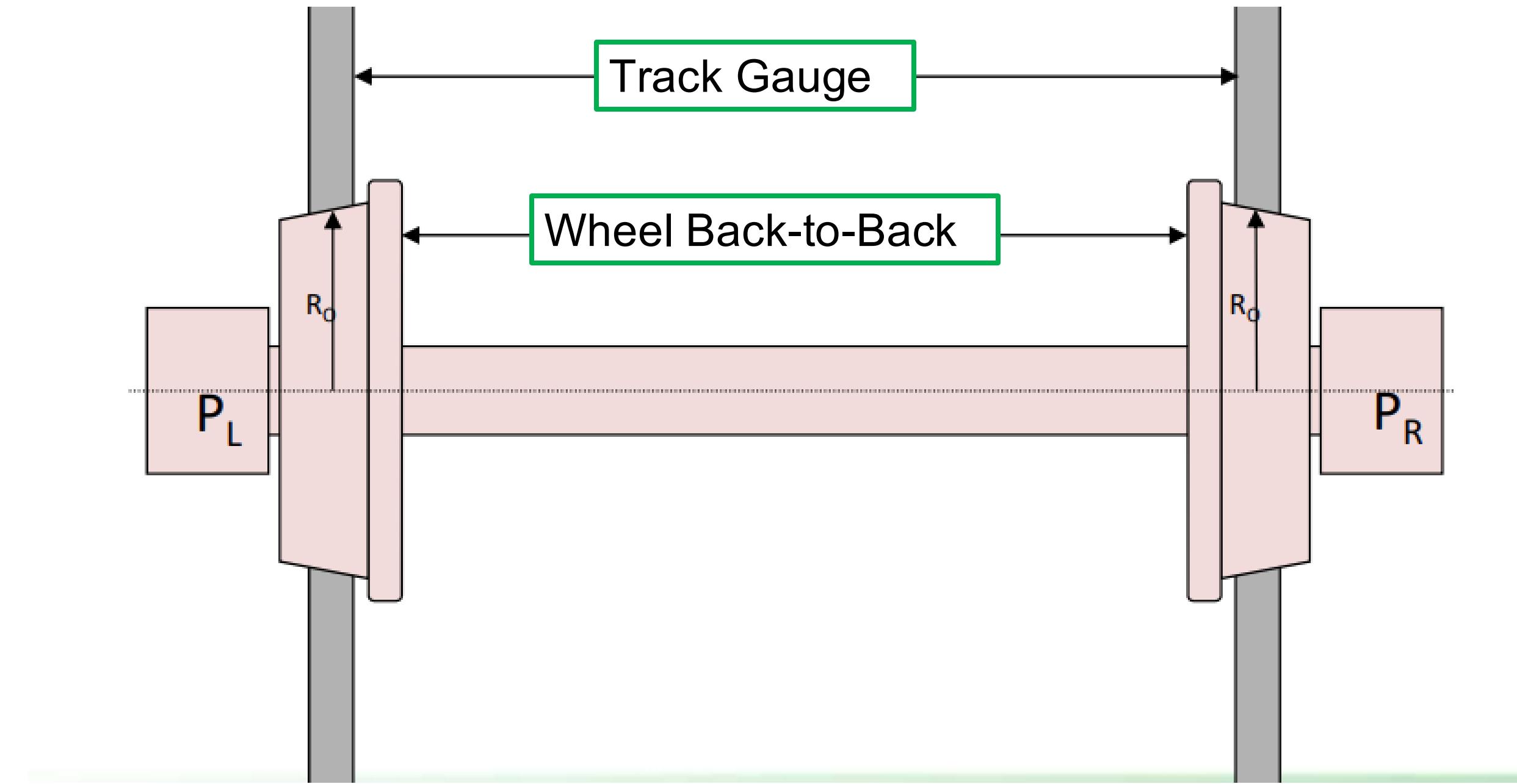


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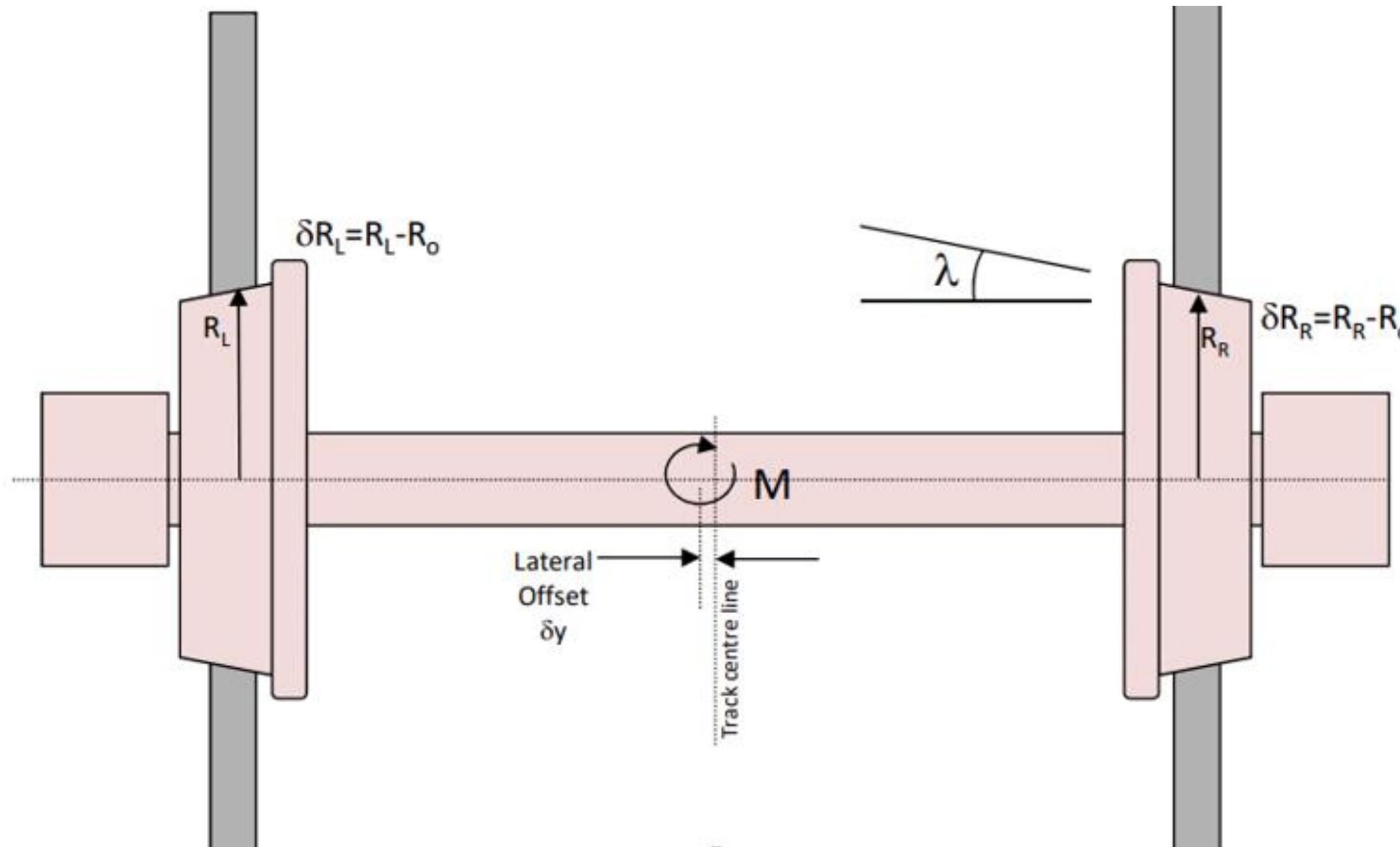




Vehicle Steering - Tangent track

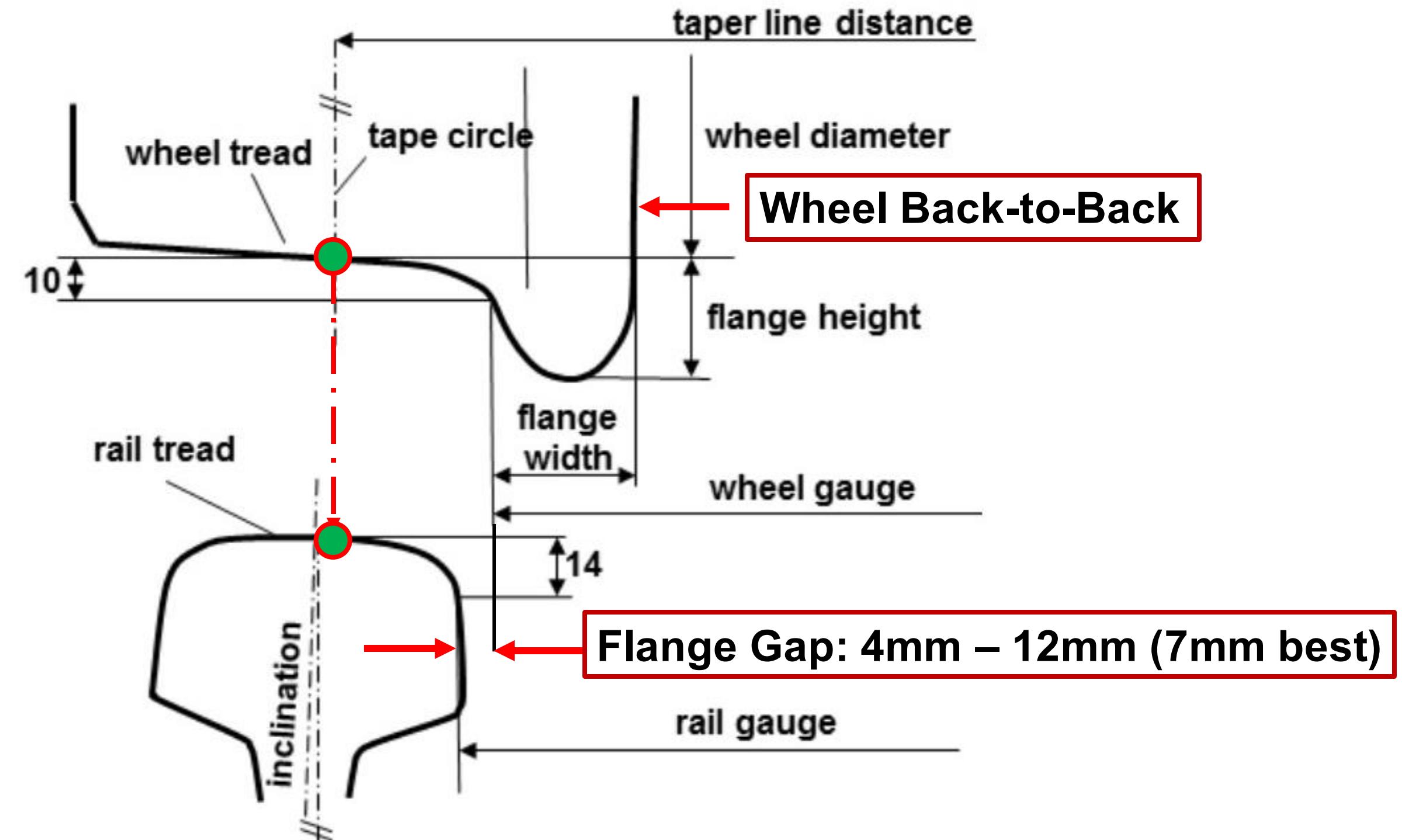


Vehicle Steering - Tangent track



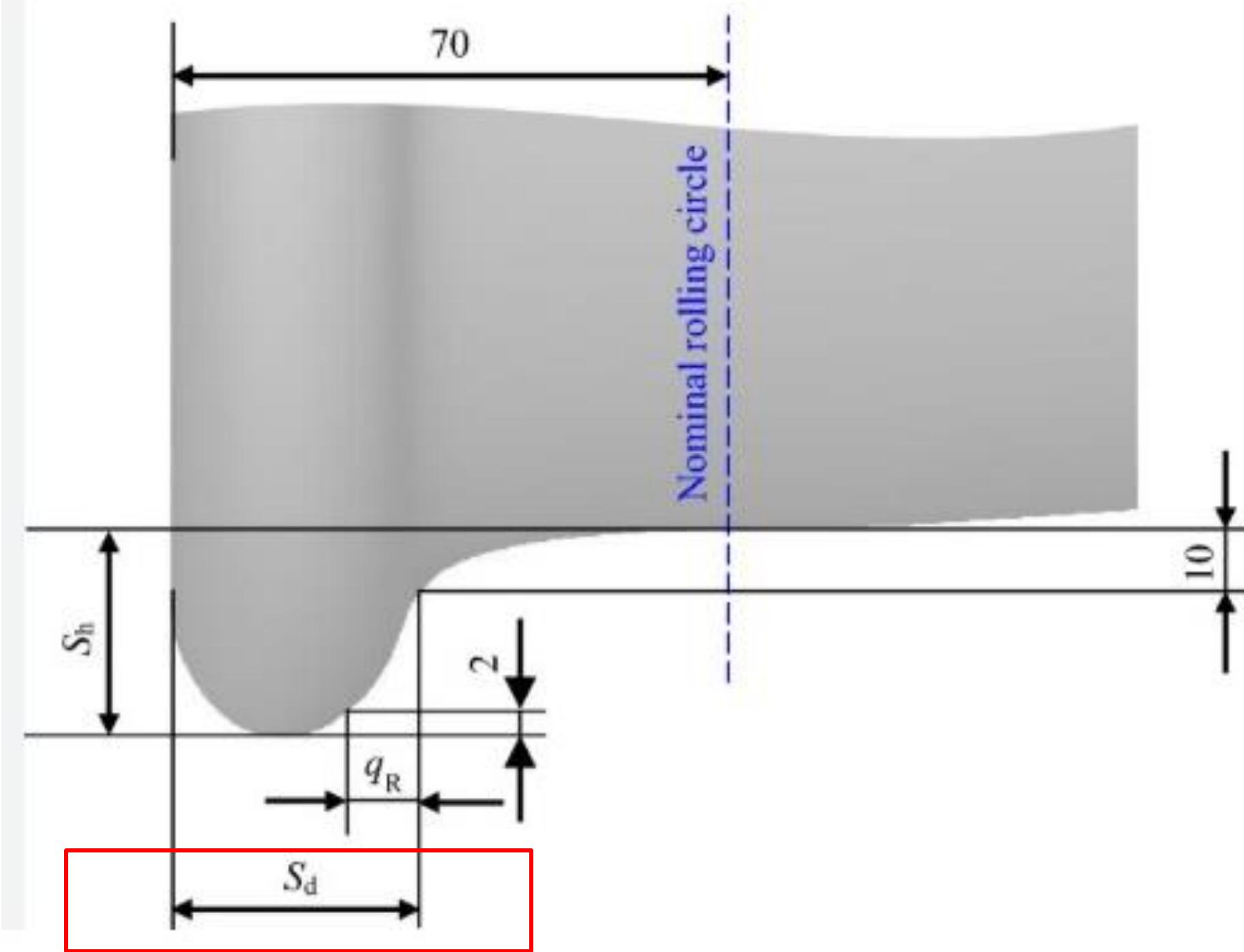


Wheel to Rail Interface Description





Typical Wheel Profile



Parameter

S_h =Flange height

S_d =Flange thickness

q_R = Flange slope quota

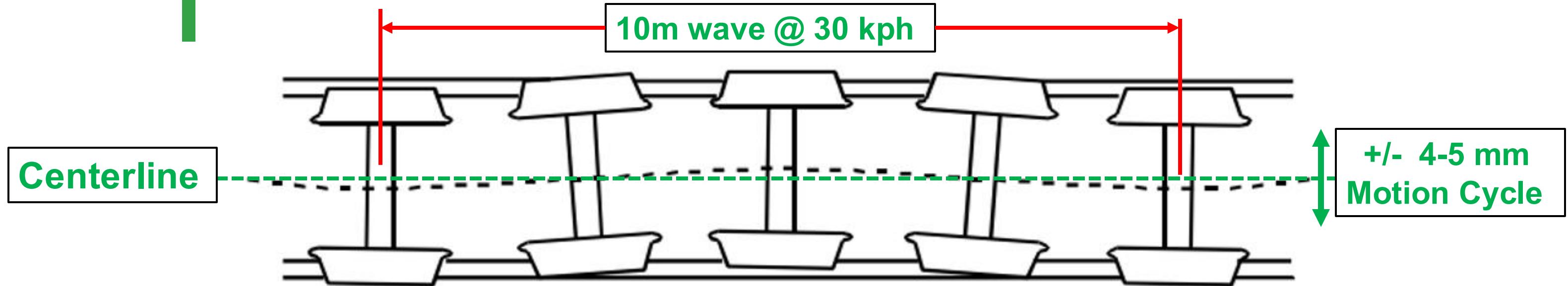
Limit value

$27.5 \text{ mm} \leq S_h \leq 36 \text{ mm}$

$22 \text{ mm} \leq S_d \leq 33 \text{ mm}$

$6.5 \text{ mm} \leq q_R$

Motion of a Free Wheelset



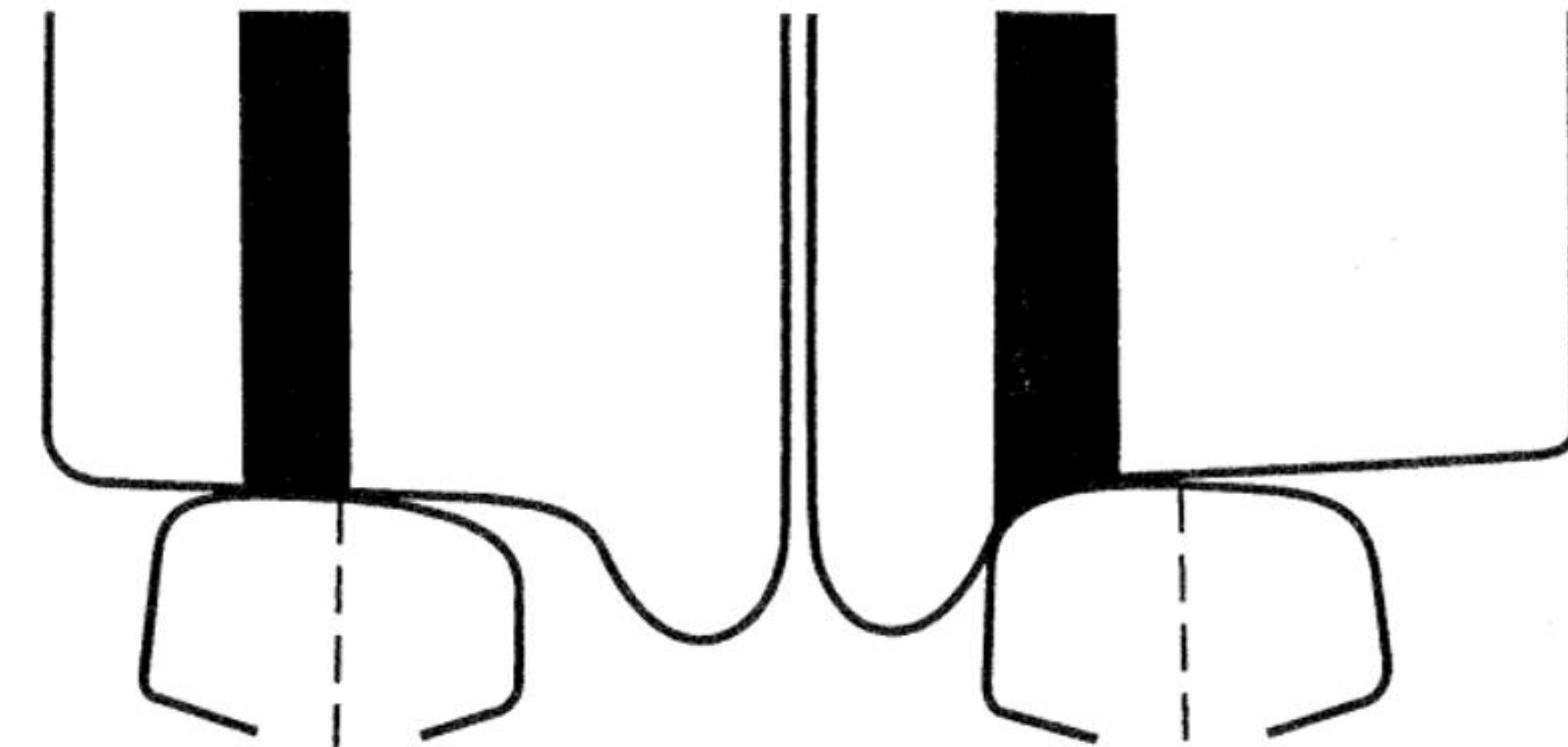
If a free wheelset is rolling along the track, starting from a displaced position, then it will initially steer itself towards the centreline of the track as a result of the rolling radius difference. As it reaches the centreline of the track it will have a yaw angle to the track, and so it will continue to roll towards the other side of the track, and so on.

This oscillatory motion along the track is known as the wheelset kinematic motion, and depends only on the geometry of the system, in particular the effective conicity of the wheelset, the wheel radius and the track gauge.

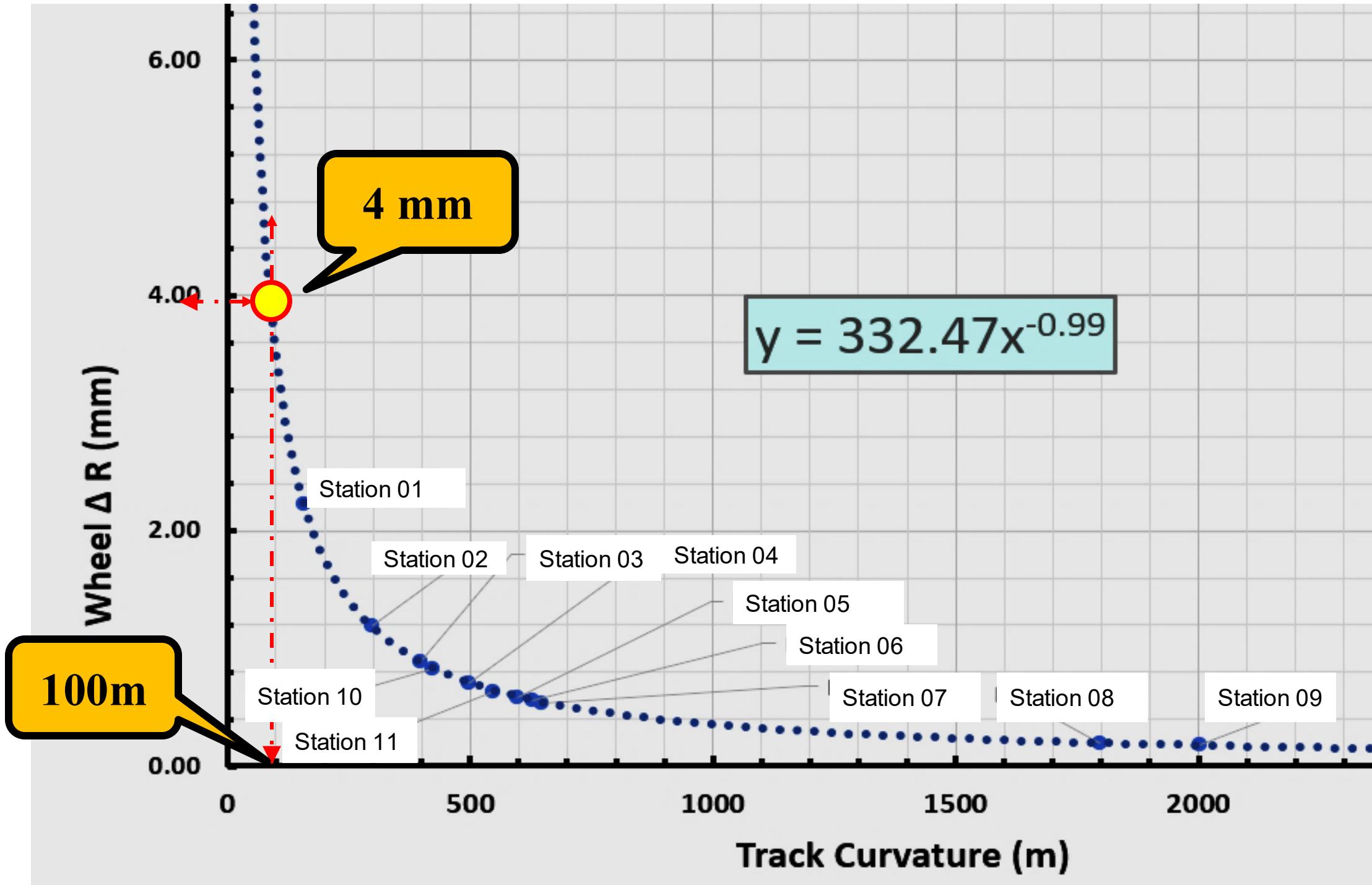


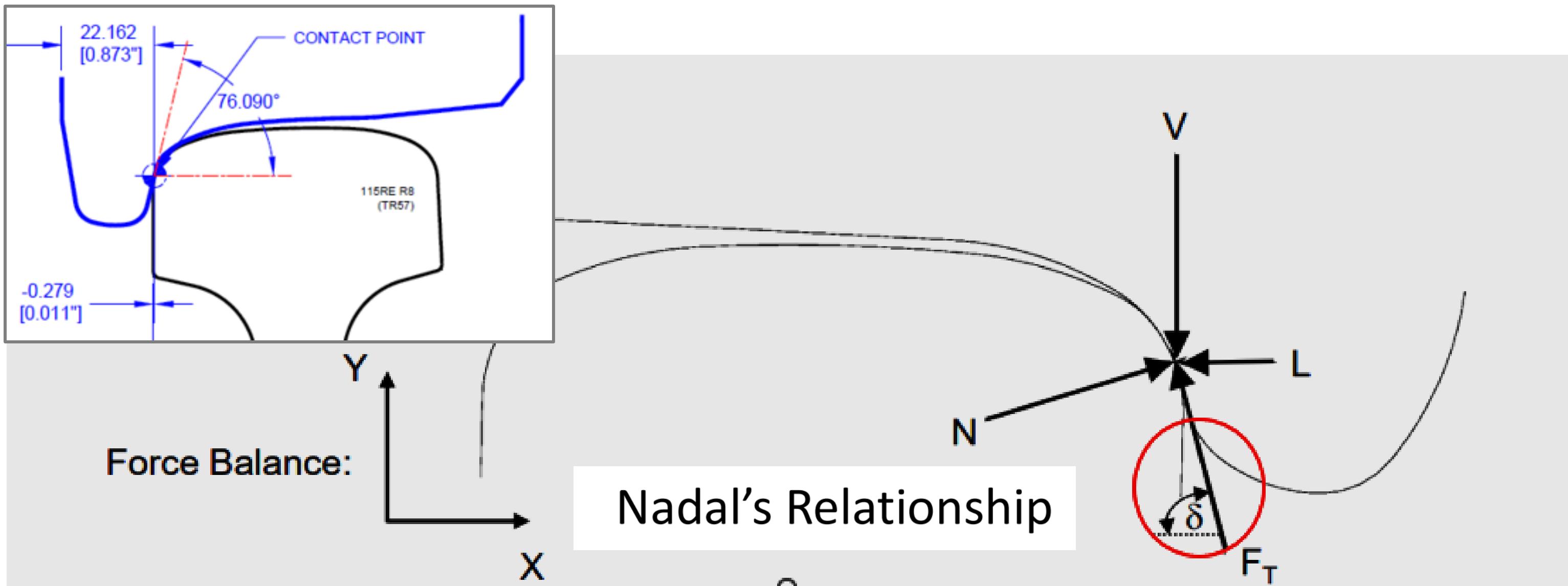


Asymmetric profiling - improves developing rolling radius difference (ΔR) for steering on tangent and curved track



Case Study - Typical ΔR for Curves





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Wheel Profile Sensitivity

The optimization of the wheel profile requires unique target requirements for each of the following design parameters:

- Effective conicity
- One-point contact
- Continuous increasing rate for wheelset Delta R
- Evenly distributed contact patch

Result, smooth wheelset steering on tangent and curves.

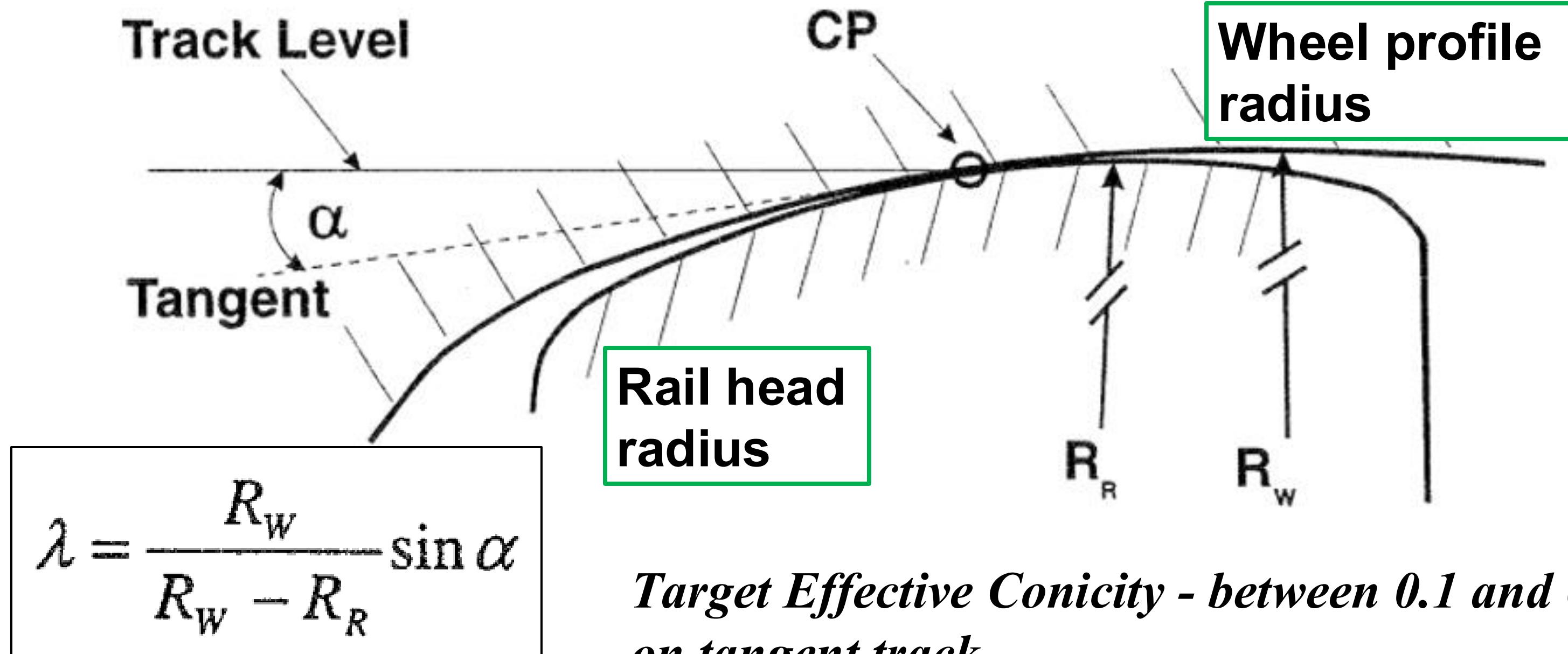


Effective Conicity (λ)

- When the rolling wheelset is offset on tangent rails, self-centering (steering) forces should normally act on the wheelset to ***maintain central position*** on the rail head.
- If the steering force is too low, or too high, the wheelset will overshoot and go too far to the other side where a new set of steering forces turn it back the other way.
- The wheelset is said to be ***hunting*** for the center position causing sinusoidal rail wear and rail corrugation. The hunting force is governed by a parameter known as the effective conicity.



Single Point Contact (CP) - critical for Effective Conicity to govern stability and producing lower wheel / rail wear rates



Delta Radius on Tangent track (ΔR)

- Stability is achieved by optimizing the surface contact angle and Delta R * between the two axle wheels relative to track level.
- Too small, or too large, the resulting contact angle and radius difference starts instability along with increases in surface contact stress and higher wear rates.

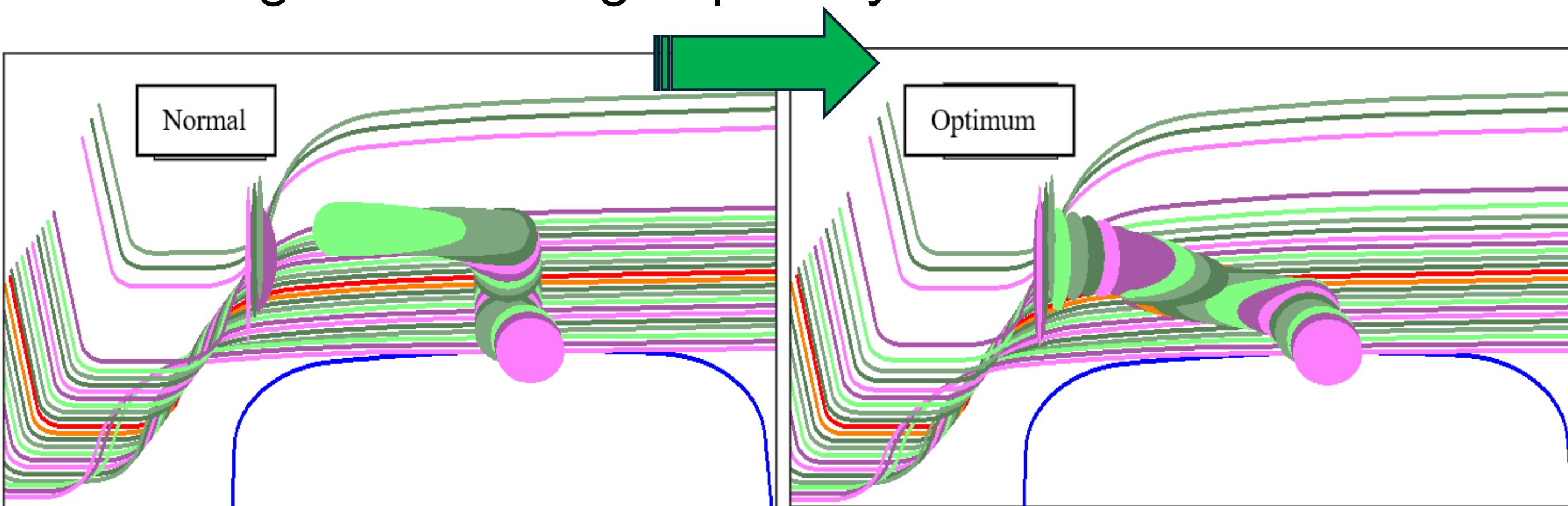
**Target ΔR : between 0.75 – 1.00 during 3–4mm offset*





Evenly Distributed Contact Patch

A uniformly distributed movement of the contact patch during lateral offset of the wheelset throughout the alignment equalizes wear and provides a more stable steering and tracking capability for the life of the wheelset.



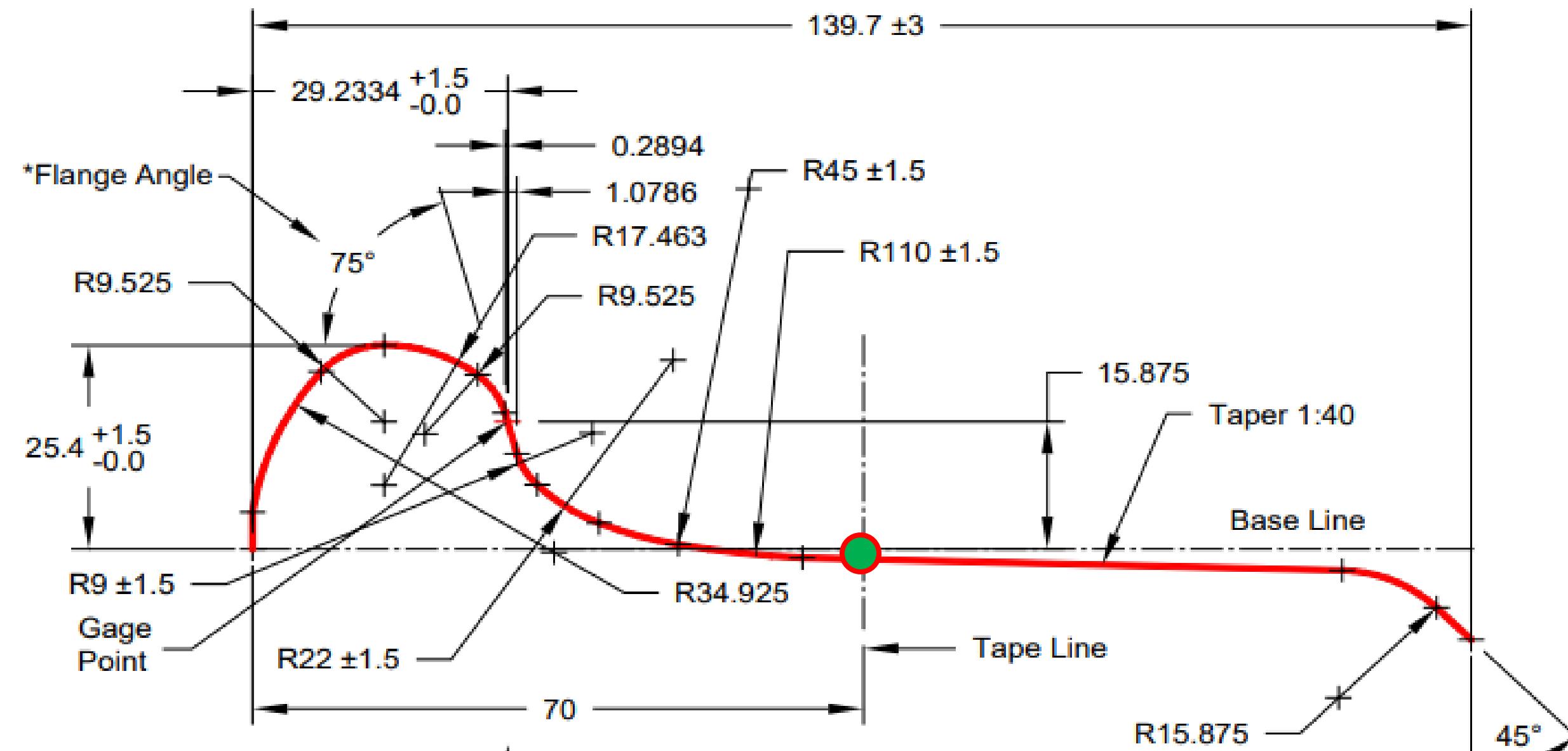
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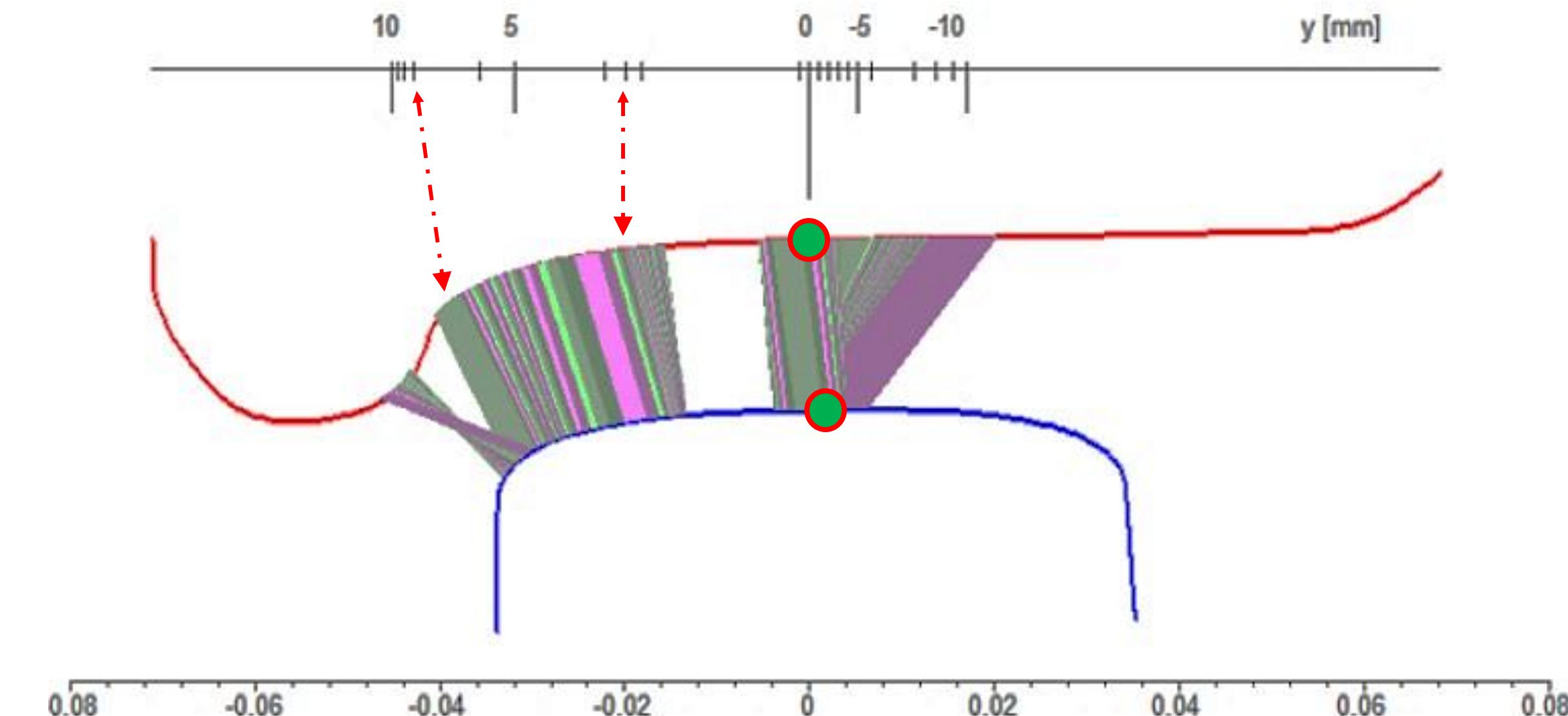


Case Study - APTA 340 wheel Profile (115RE_1:40 cant)



Case Study – Normal Wheel/Rail Contact Points (115RE_10" radius, 1:40 cant)

For comparison, the plot below shows the modeling of the Contact Point distribution for the APTA 340 profile.



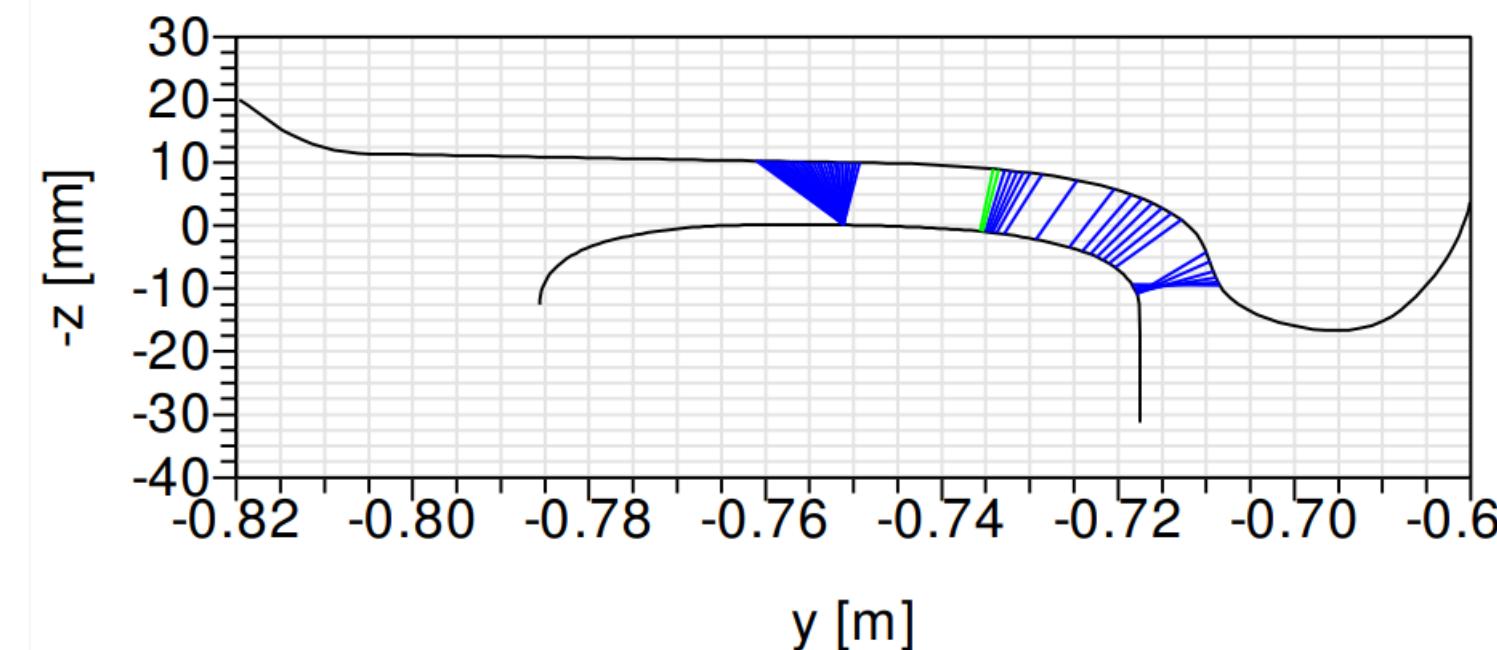


Normal – Wheel/Rail Contact Points

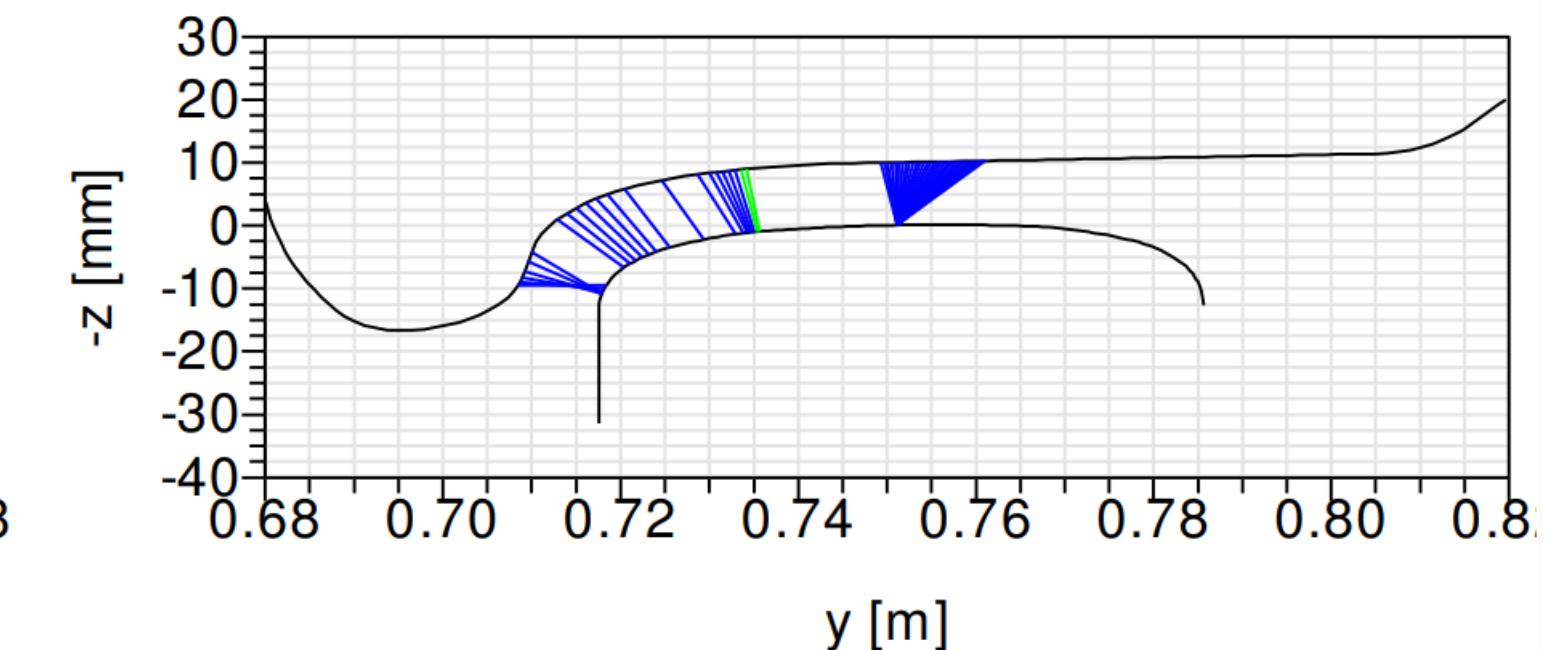
(115RE_1:40 cant)

The jump in the contact patch for the APTA 340 profile can be seen at a 1.5mm lateral offset of the wheelset. This jump in the contact patch, and the associated change in rolling radius difference, will cause high longitudinal forces in the contact patches, giving higher wear as well as initiating corrugation.

Contact connections (left)



Contact connections (right)



Improved – Even Distributed Contact Path

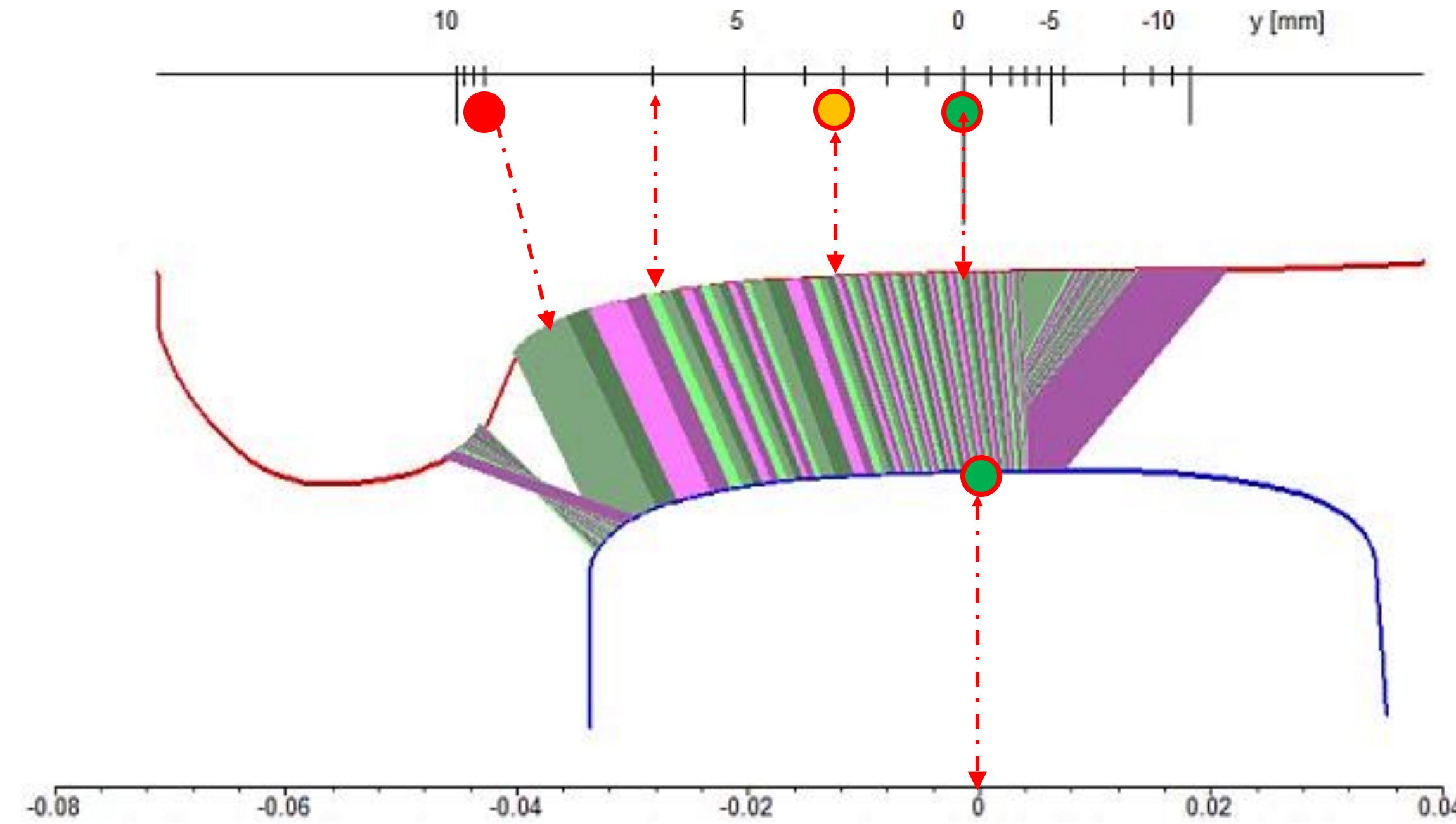
Recent developments towards a **wheel profile generation tool** allows creation of the profile directly based upon the shape and inclinations of the rail head. Once the rail head profile and cant are defined (example: standard or thru MiniProf, new or partially worn) an enhanced progressive profile can be automatically detailed for final confirmation studies.

The improved process allows wheel manipulation to give lower effective conicity values, good for running on straight tracks (>1200m radius curves), or higher conicity profiles that reduce guiding forces (flanging) in narrower curves, ideal for curvy metro networks.



Improved - Wheel/Rail Contact Points

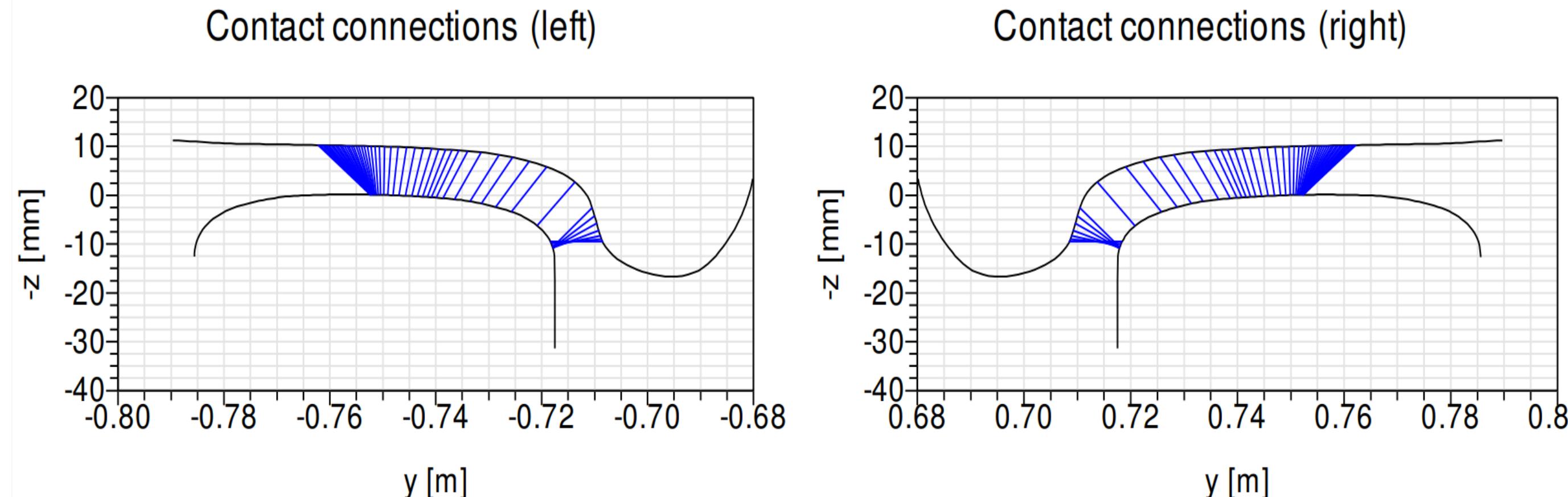
(115RE_ 10" radius , 1:40 cant)



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Improved Wheel Profile (115RE_1:40 cant)

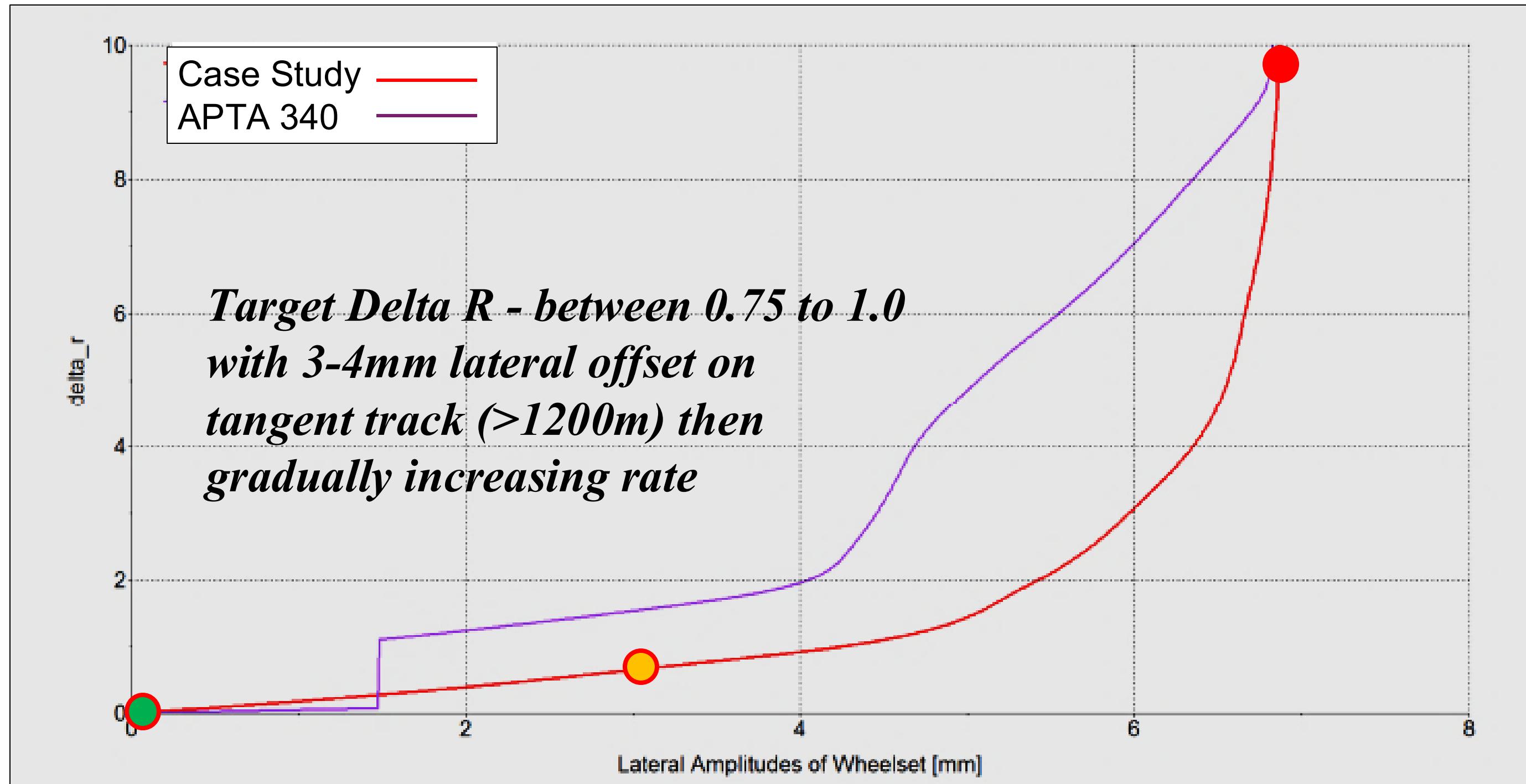
The Case Study profile is continuous throughout the 7mm lateral amplitude cycle. This demonstrates that there is single point contact along with smooth steering transitions at all lateral displacements thus achieving low-wear capability.





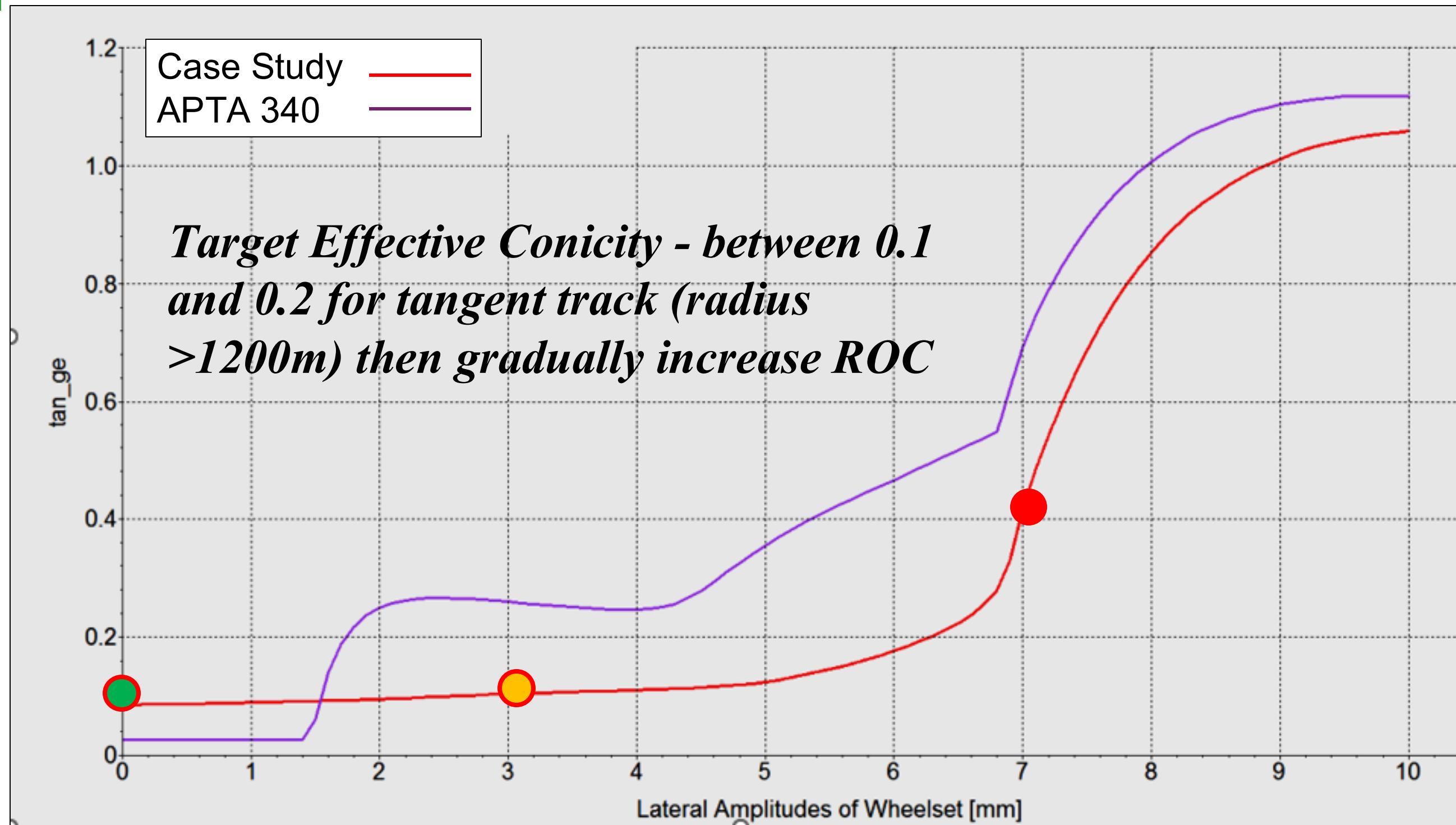
Comparing Wheel Profiles for Delta R

(115RE_1:40 cant)



Comparing Effective Conicity

(115RE_1:40 cant)



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Dynamic Modeling – Manipulating ΔR

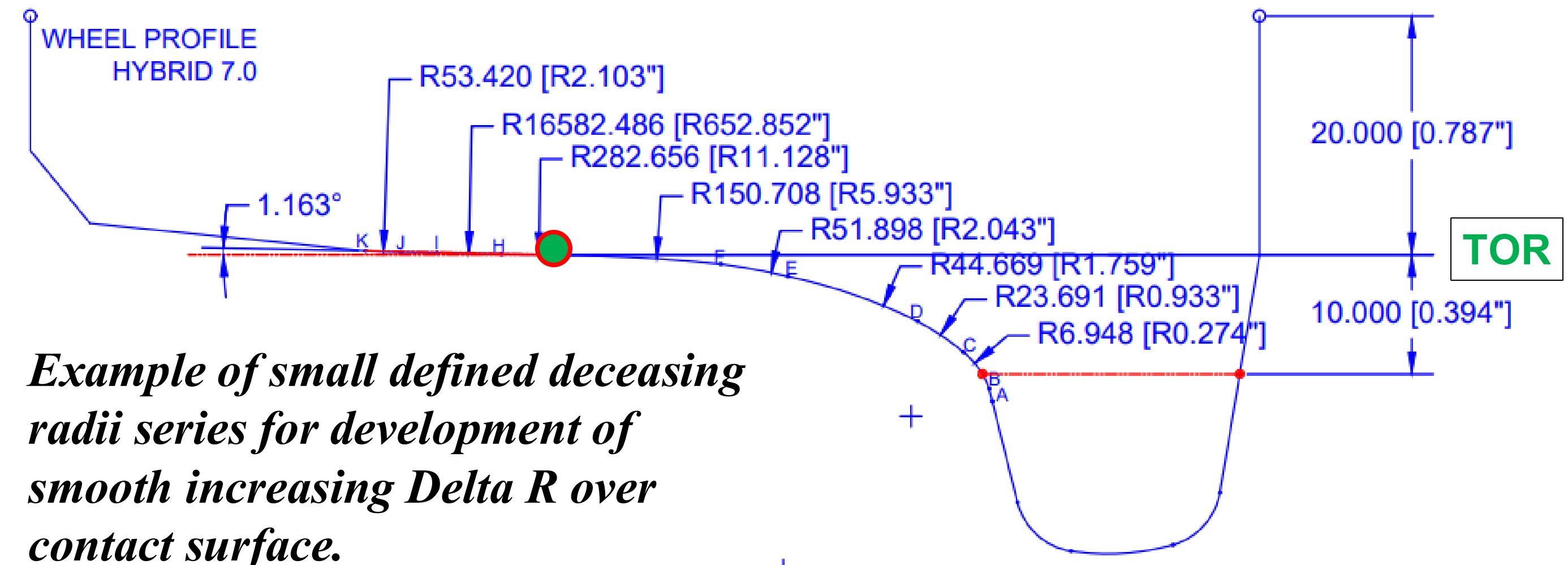
Key design criteria for defining an improved wheel profile is the precise selection of the defined **wheelset Delta R** during lateral amplitude movements over the rail head.

To accomplish this, small evenly spaced series of radius are defined along a continuous path from initial Point of Contact to the maximum movement. These small radii replaces the standard large radii or slopes of the standard profile.

An engineering **AutoCAD** analysis tool was developed for local examination and manipulation of a wheel profile for trial visualization of actual motion of the wheelset over the rail profile.

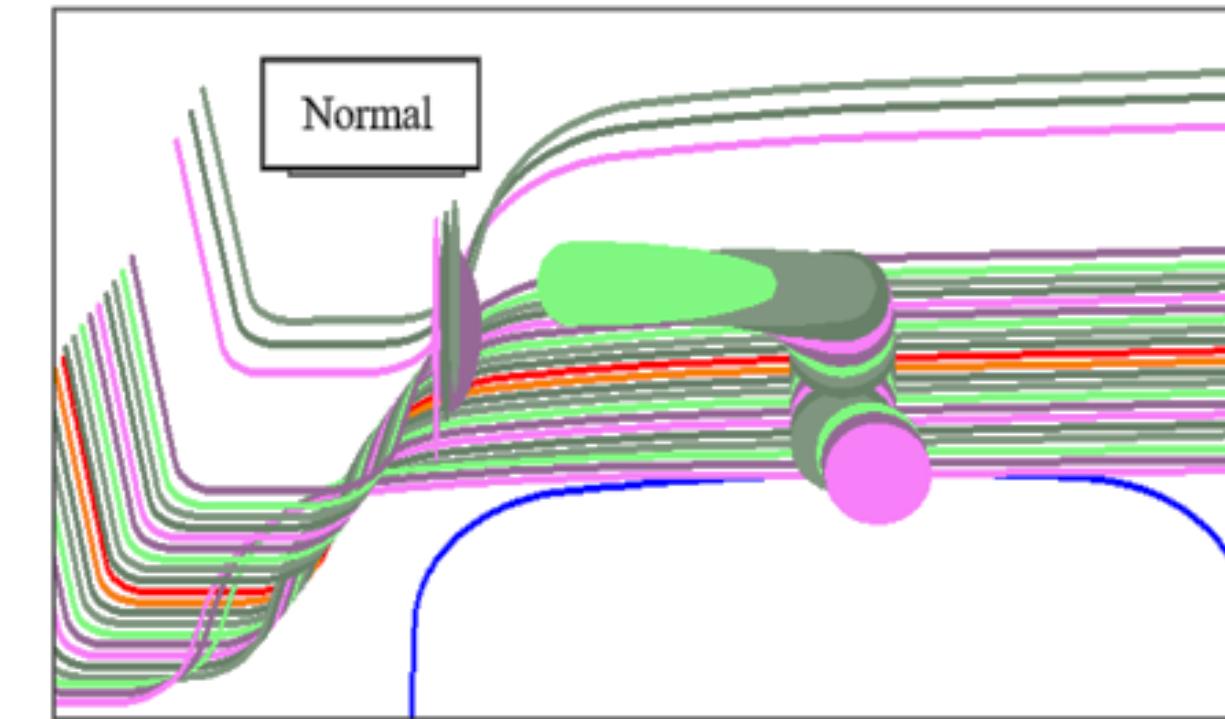


Dynamic Modeling - Manipulating ΔR



Dynamic Modeling - Normal Profile (115RE 8" _ 1:40 cant)

Uneven contact transitions



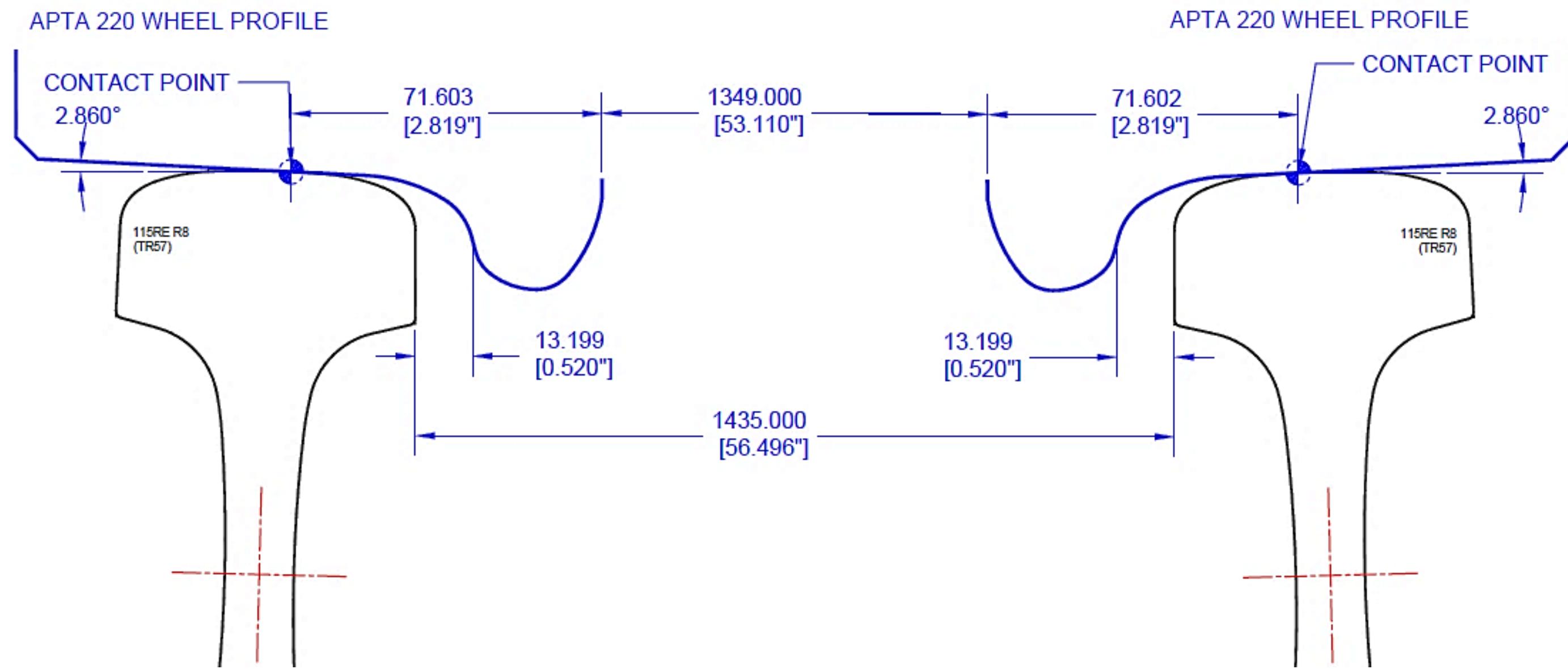
Dynamic Modeling - Normal Profile

(115RE 8" _ 1:40 cant)

1

WHEEL AXLE 0 TO LEFT
CANT: 1:40
Delta R =0.0mm

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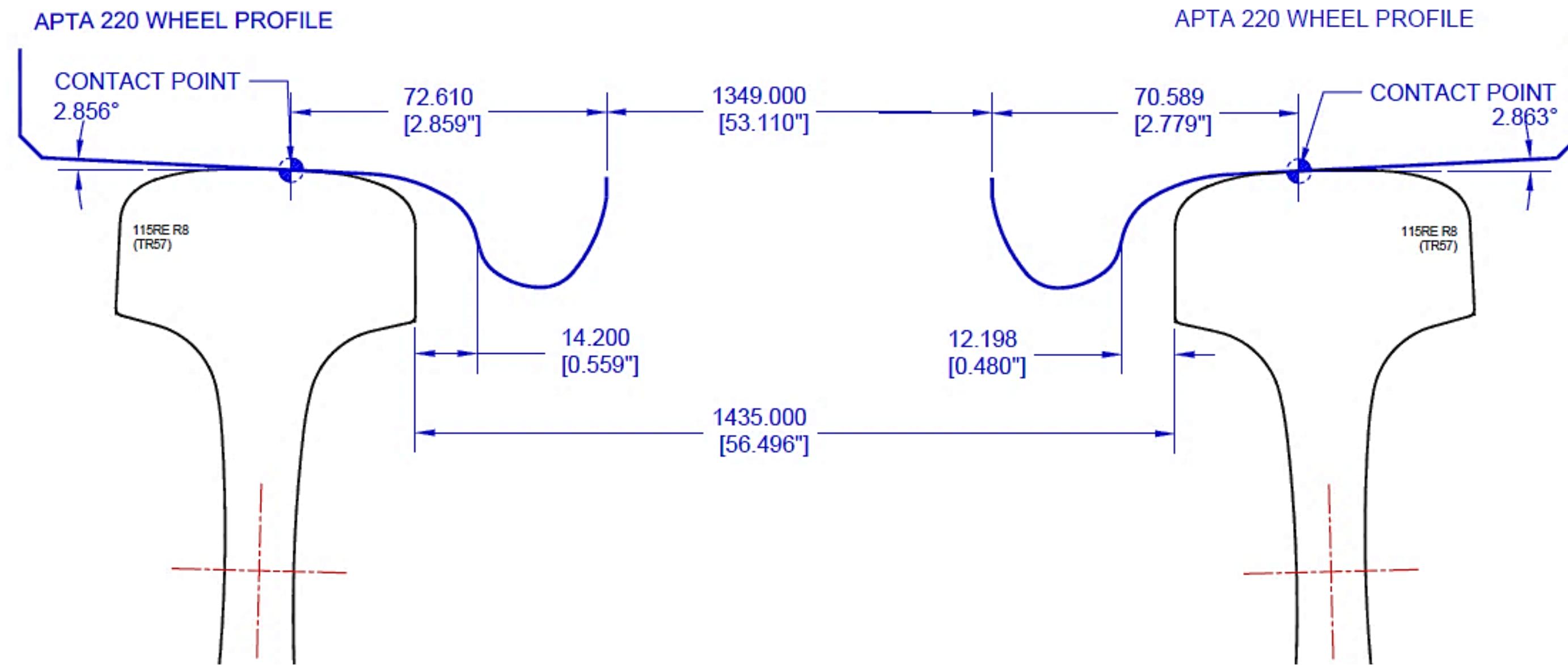
Dynamic Modeling - Normal Profile

(115RE 8" _ 1:40 cant)

2

WHEEL AXLE 1.0 TO LEFT
CANT: 1:40
Delta R = 0.046mm

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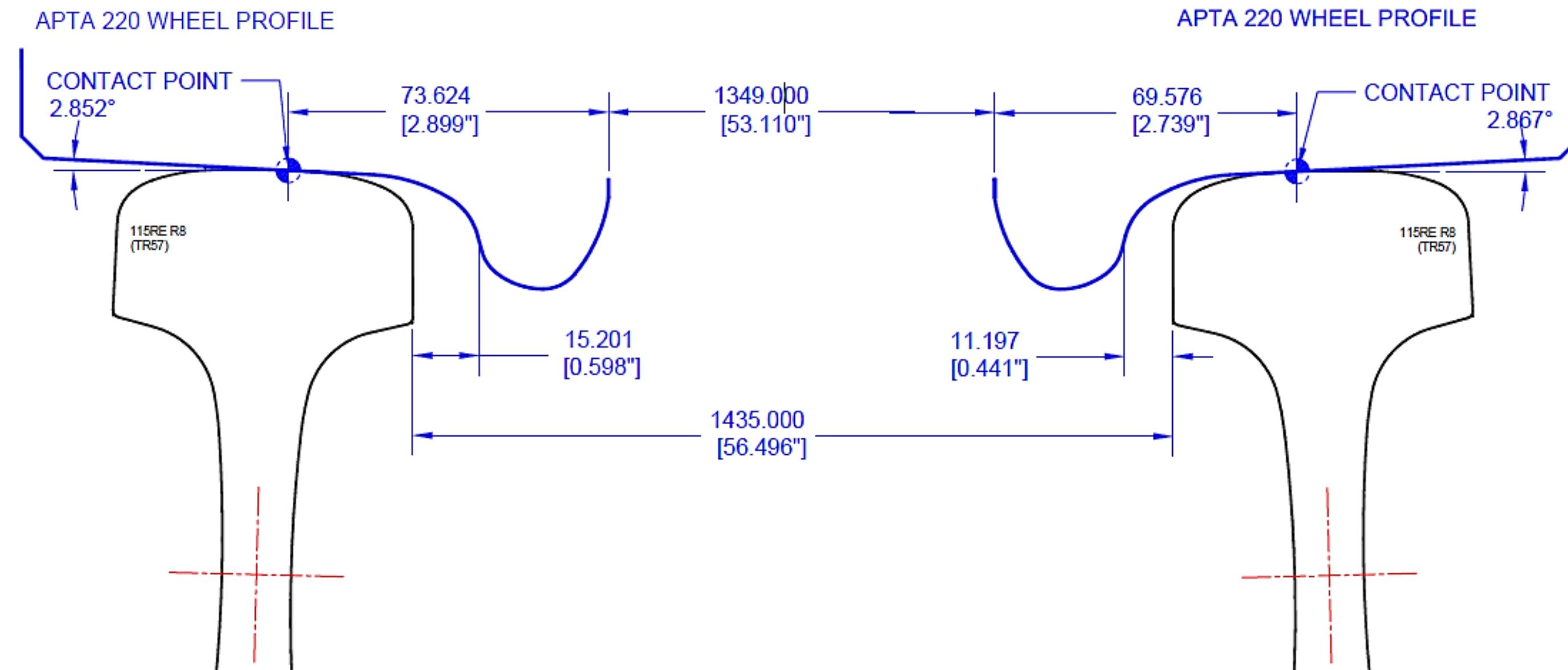
Dynamic Modeling - Normal Profile

(115RE 8" _1:40 cant)

3

WHEEL AXLE 2.0 TO LEFT
CANT: 1:40
Delta R =0.182mm

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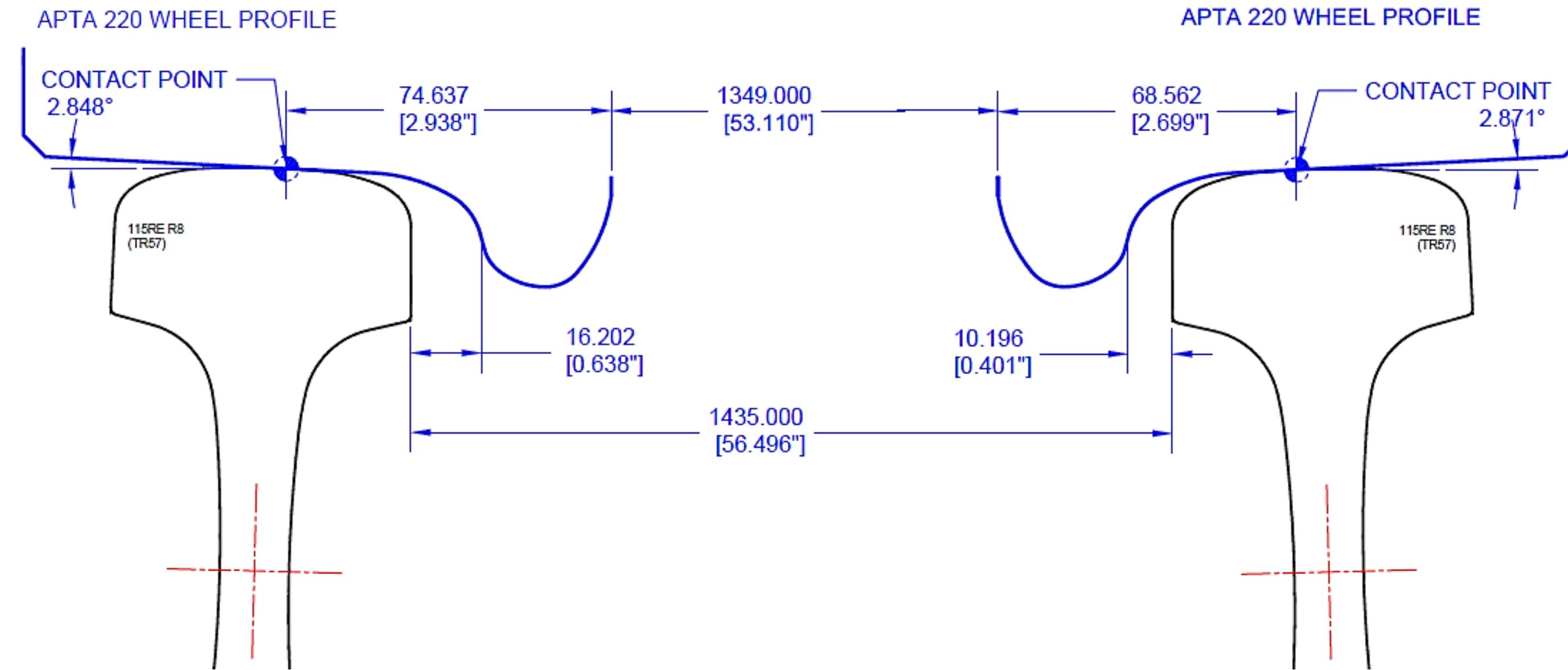
Dynamic Modeling - Normal Profile

(115RE 8" - 1:40 cant)

4

WHEEL AXLE 3.0 TO LEFT
CANT: 1:40
Delta R = 0.274mm

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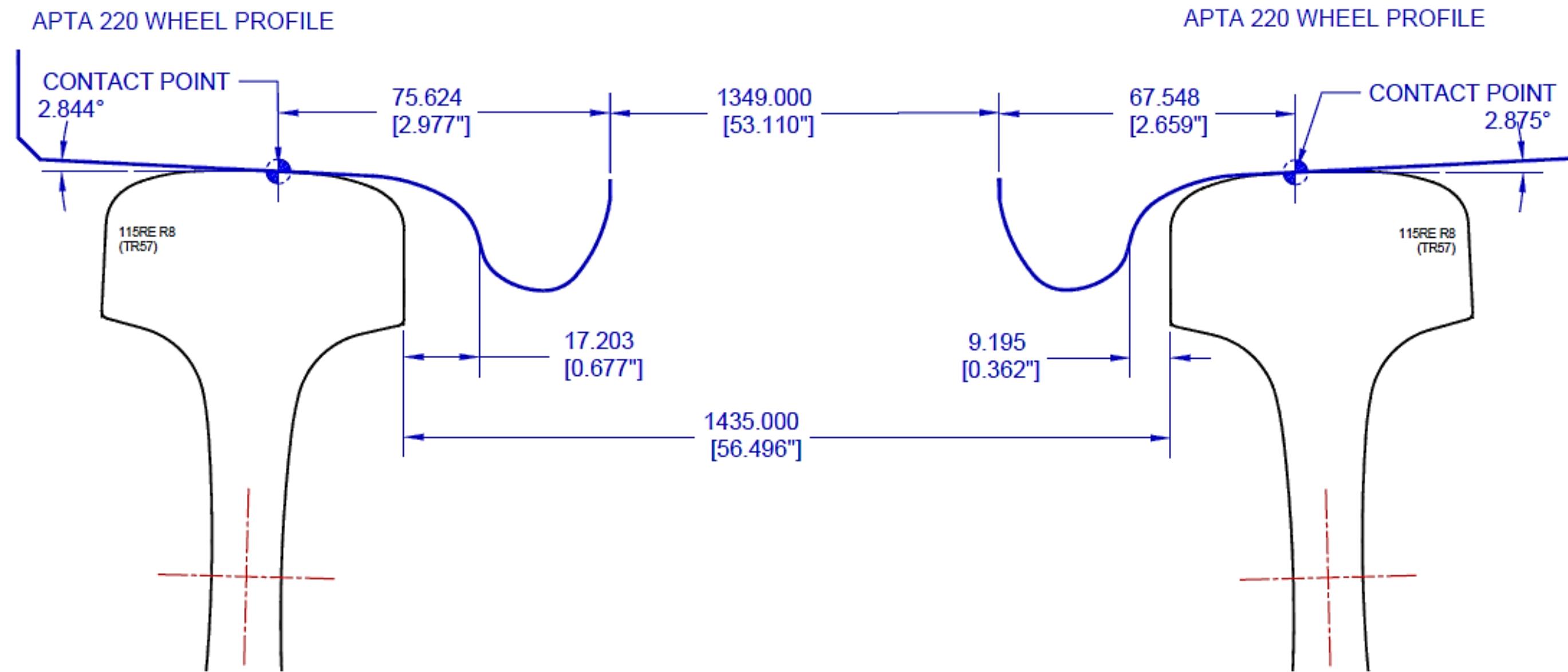


Dynamic Modeling - Normal Profile

(115RE 8" _ 1:40 cant)

WHEEL AXLE 4.0 TO LEFT
CANT: 1:40
Delta R = 0.344mm

PRINCIPLES COURSE



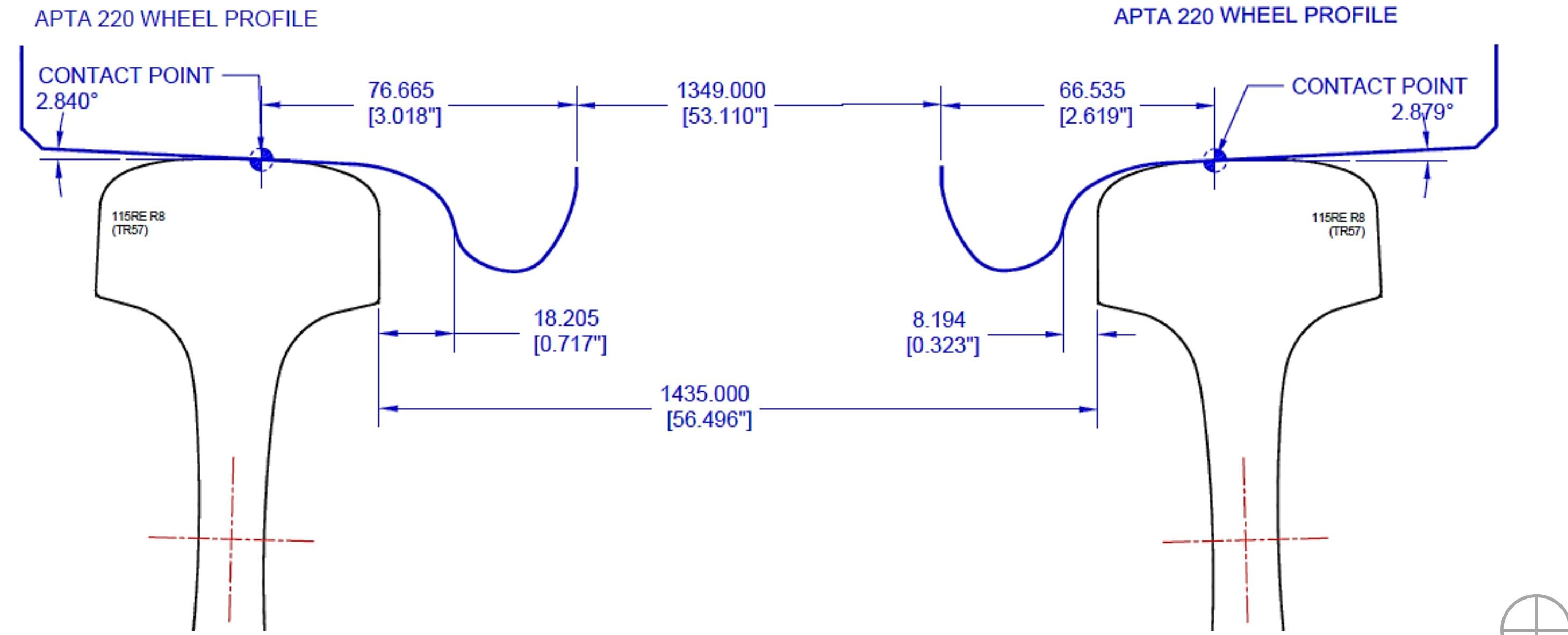
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2025

Dynamic Modeling - Normal Profile

(115RE 8" _ 1:40 cant)

WHEEL AXLE 5.0 TO LEFT
CANT: 1:40
Delta R = 0.458mm

PRINCIPLES COURSE

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2025

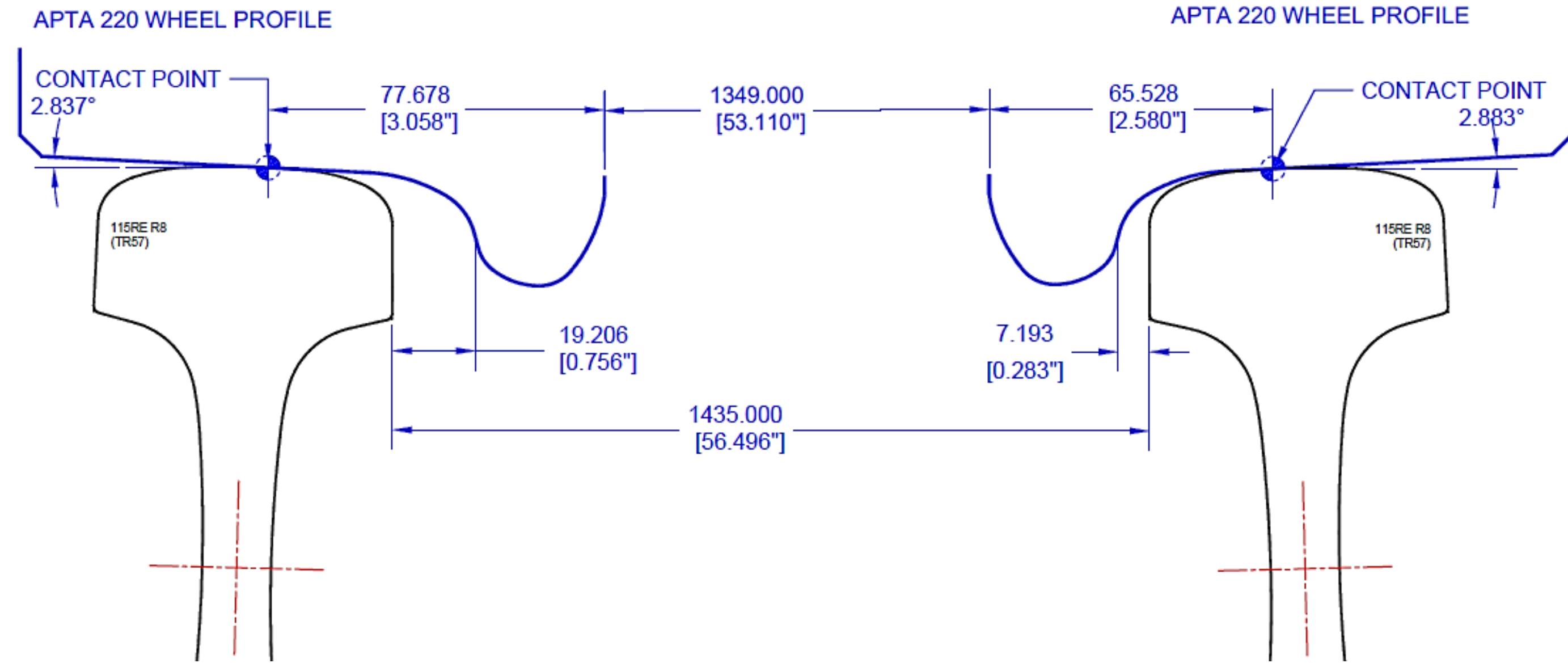
Dynamic Modeling - Normal Profile

(115RE 8" _ 1:40 cant)

7

WHEEL AXLE 6.0 TO LEFT
CANT: 1:40
Delta R = 0.549mm

PRINCIPLES COURSE

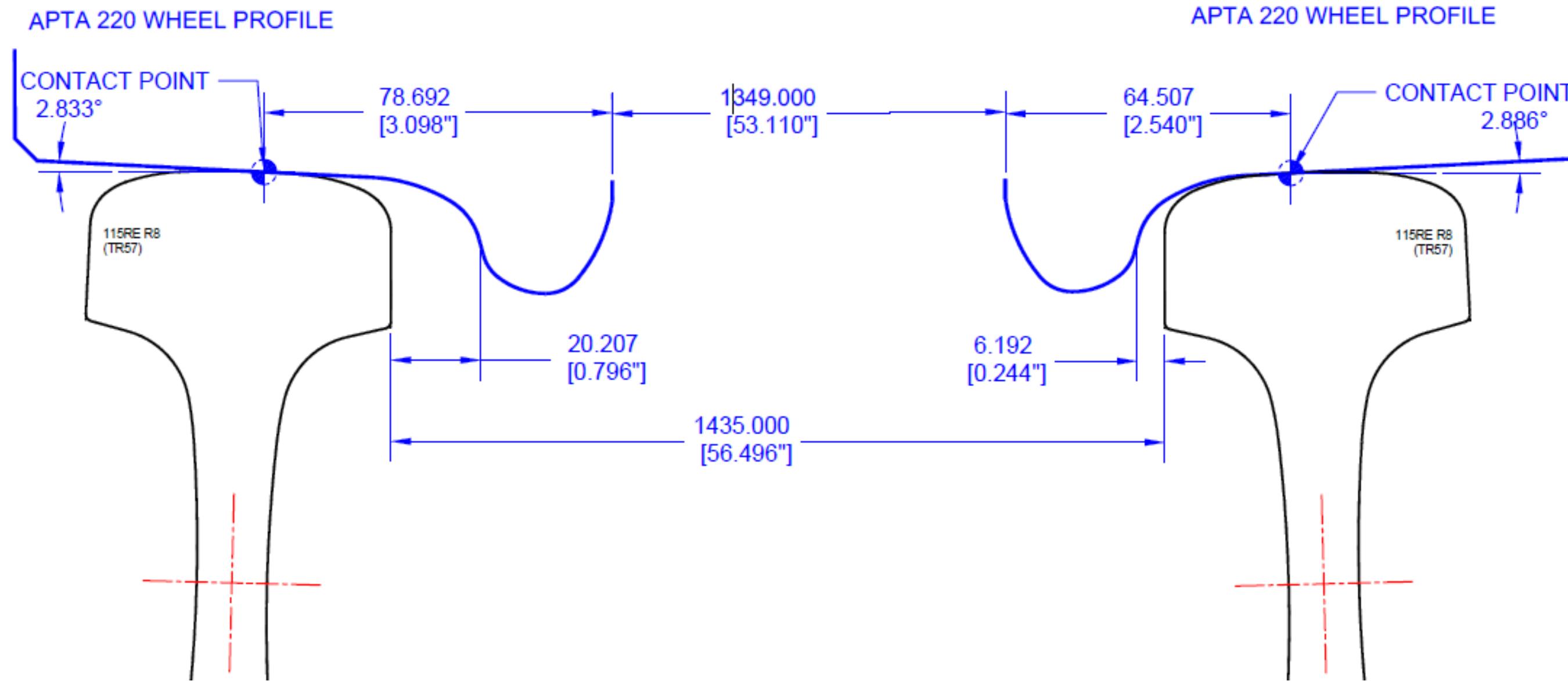


Dynamic Modeling - Normal Profile

(115RE 8" _ 1:40 cant)

WHEEL AXLE 7.0 TO LEFT
CANT: 1:40
Delta R = 0.642mm

PRINCIPLES COURSE



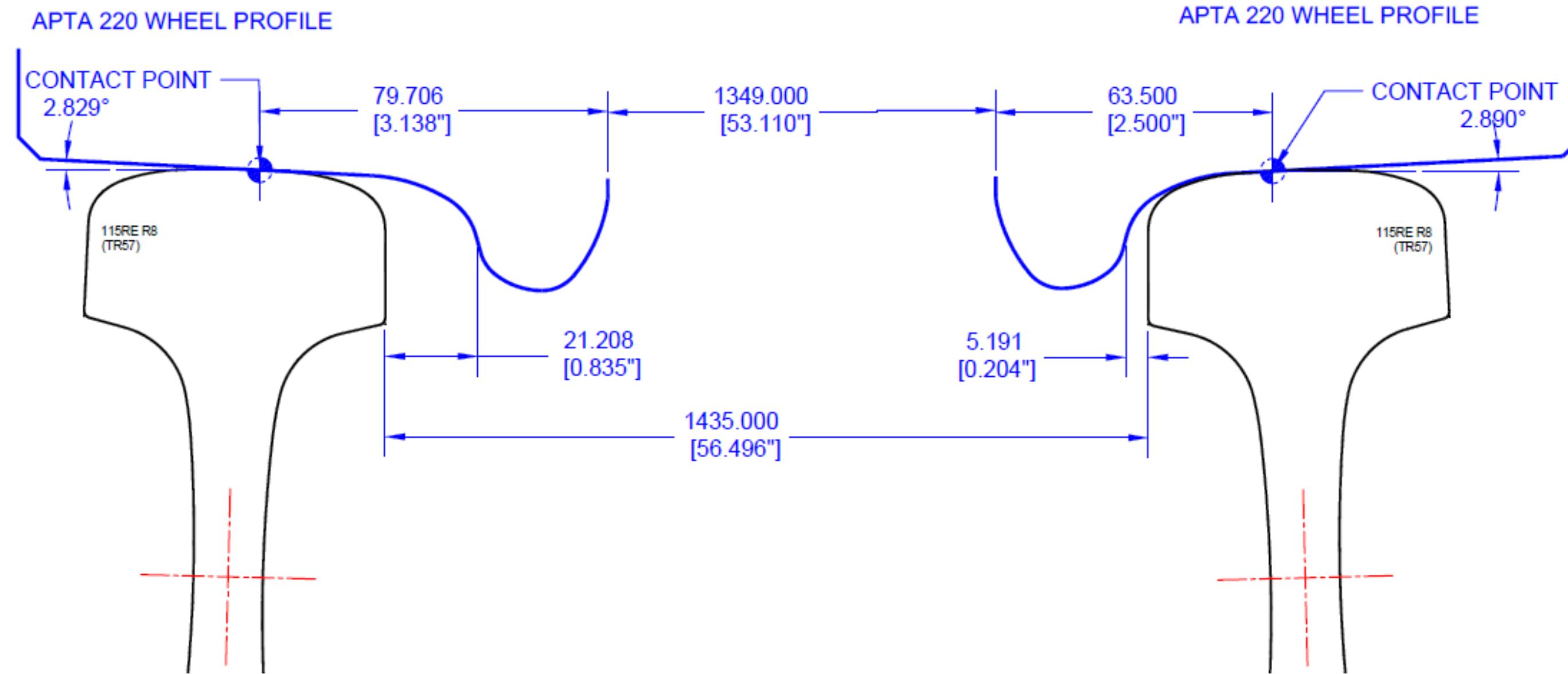
Dynamic Modeling - Normal Profile

(115RE 8" _ 1:40 cant)

9

WHEEL AXLE 8.0 TO LEFT
CANT: 1:40
Delta R = 0.733mm

PRINCIPLES COURSE

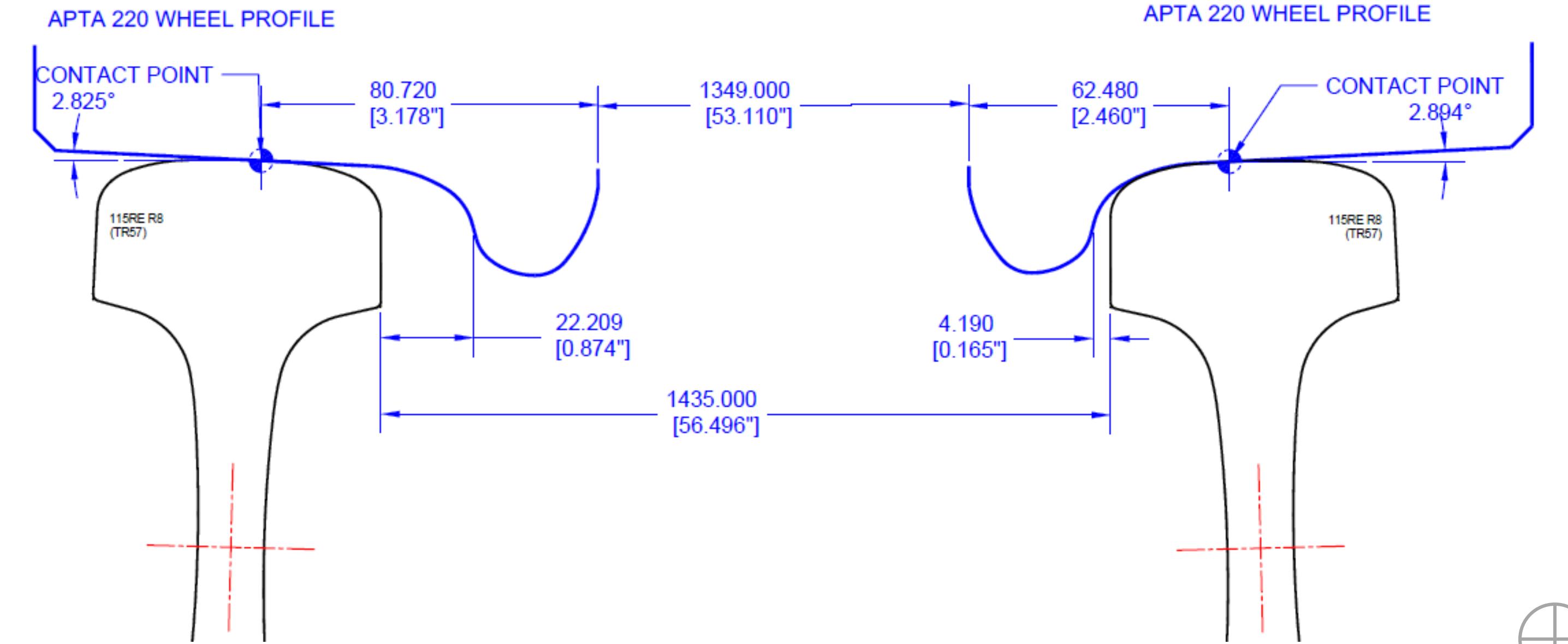


Dynamic Modeling - Normal Profile

(115RE 8" - 1:40 cant)

WHEEL AXLE 9.0 TO LEFT
CANT: 1:40
Delta R = 0.824mm

PRINCIPLES COURSE

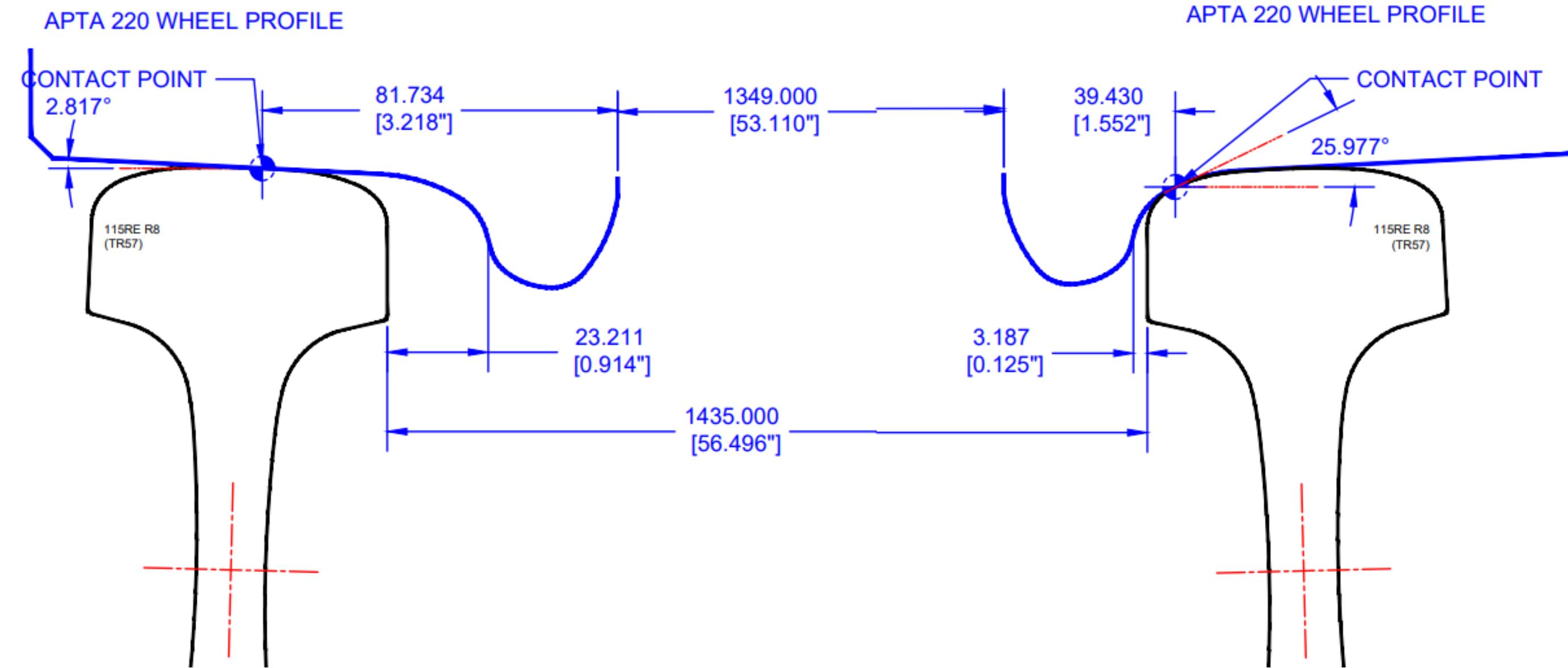
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Dynamic Modeling - Normal Profile

(115RE 8" - 1:40 cant)

WHEEL AXLE 10.0 TO LEFT
CANT: 1:40
Delta R = 5.076mm

PRINCIPLES COURSE

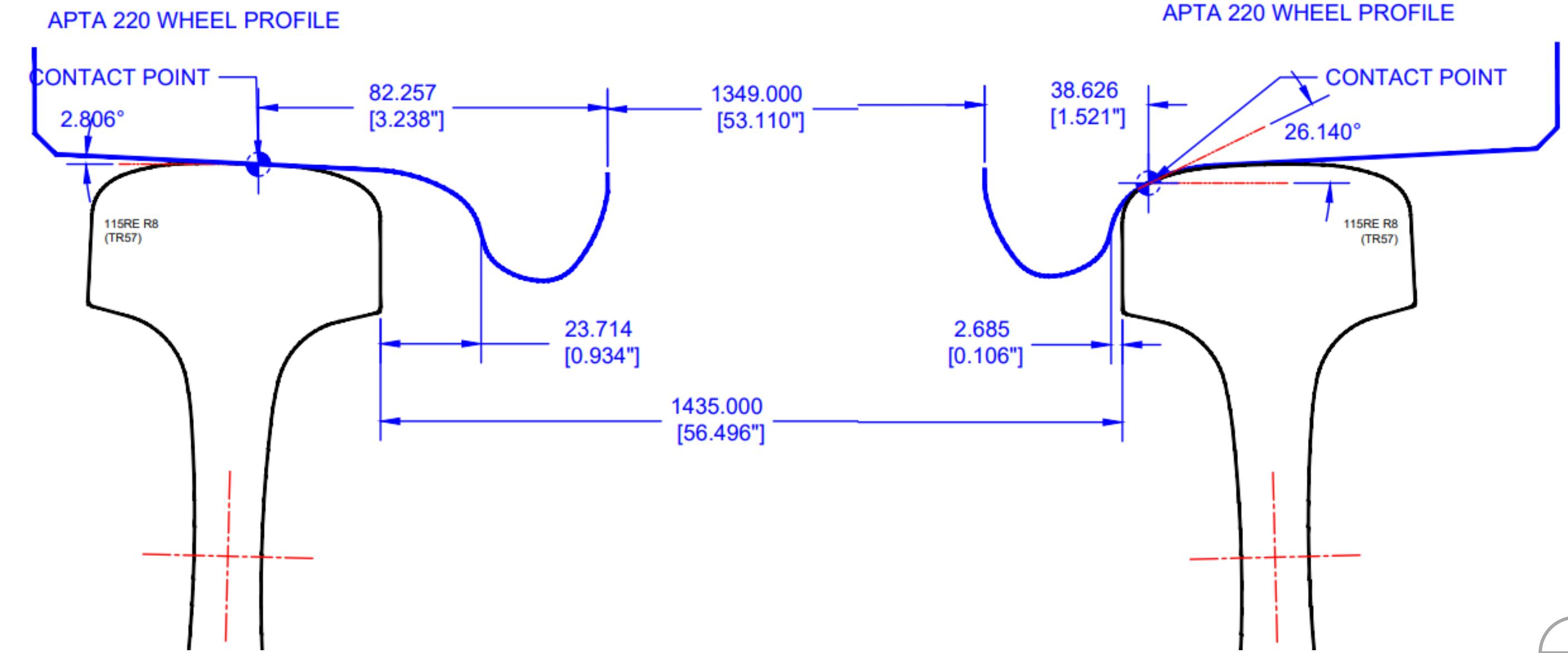


Dynamic Modeling - Normal Profile

(115RE 8" - 1:40 cant)

WHEEL AXLE 10.5 TO LEFT
CANT: 1:40
Delta R = 5.484mm

PRINCIPLES COURSE



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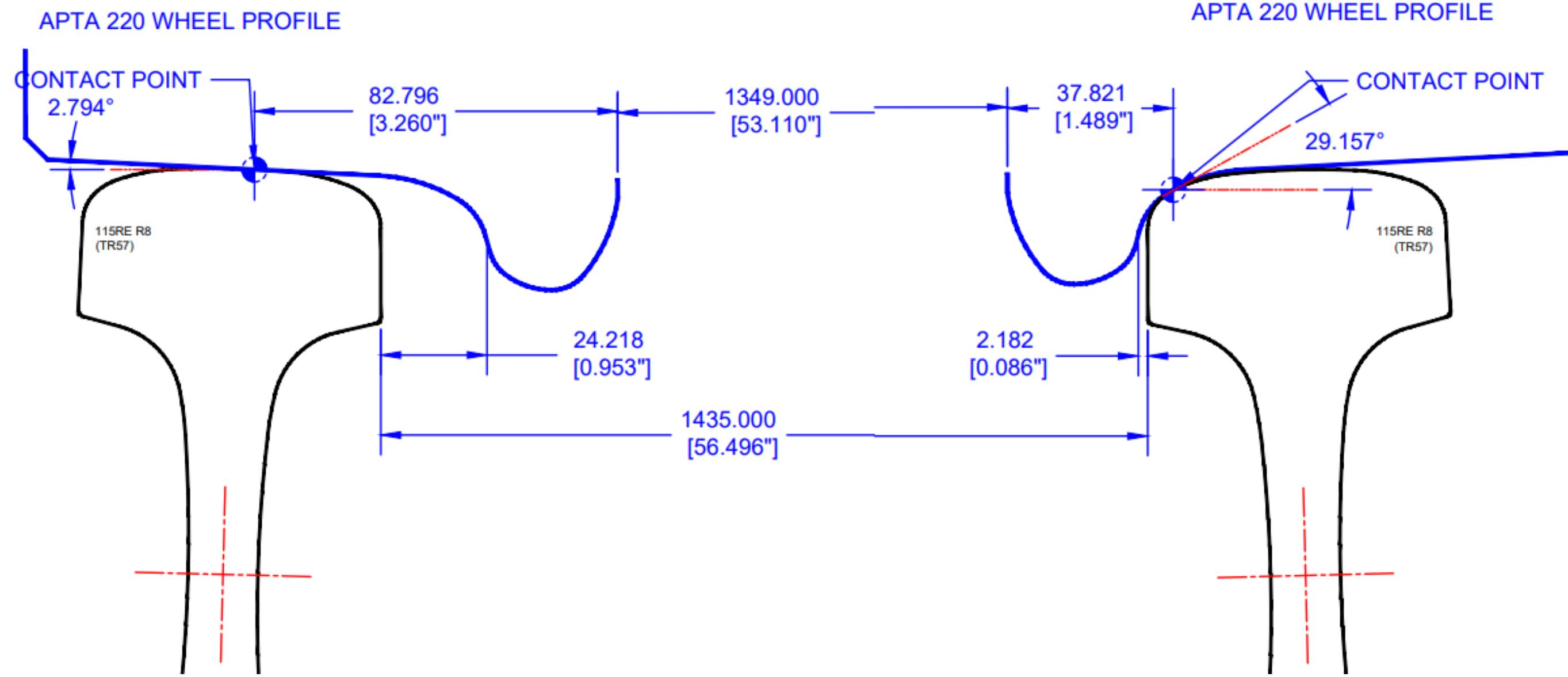


Dynamic Modeling - Normal Profile

(115RE 8"-1:40 cant)

WHEEL AXLE 11.0 TO LEFT
CANT: 1:40
Delta R = 5.915mm

PRINCIPLES COURSE

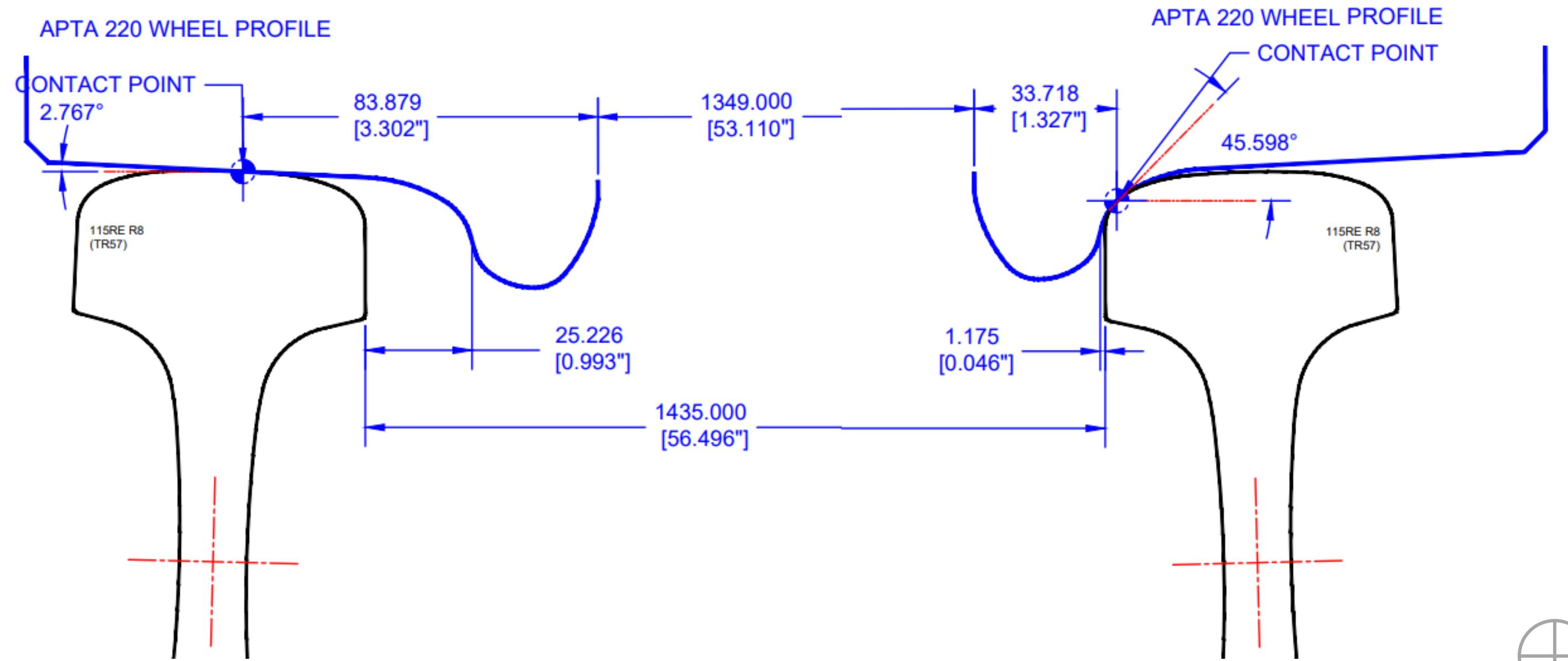


Dynamic Modeling - Normal Profile

(115RE 8" - 1:40 cant)

WHEEL AXLE 12.0 TO LEFT
CANT: 1:40
Delta R = 8.879mm

PRINCIPLES COURSE

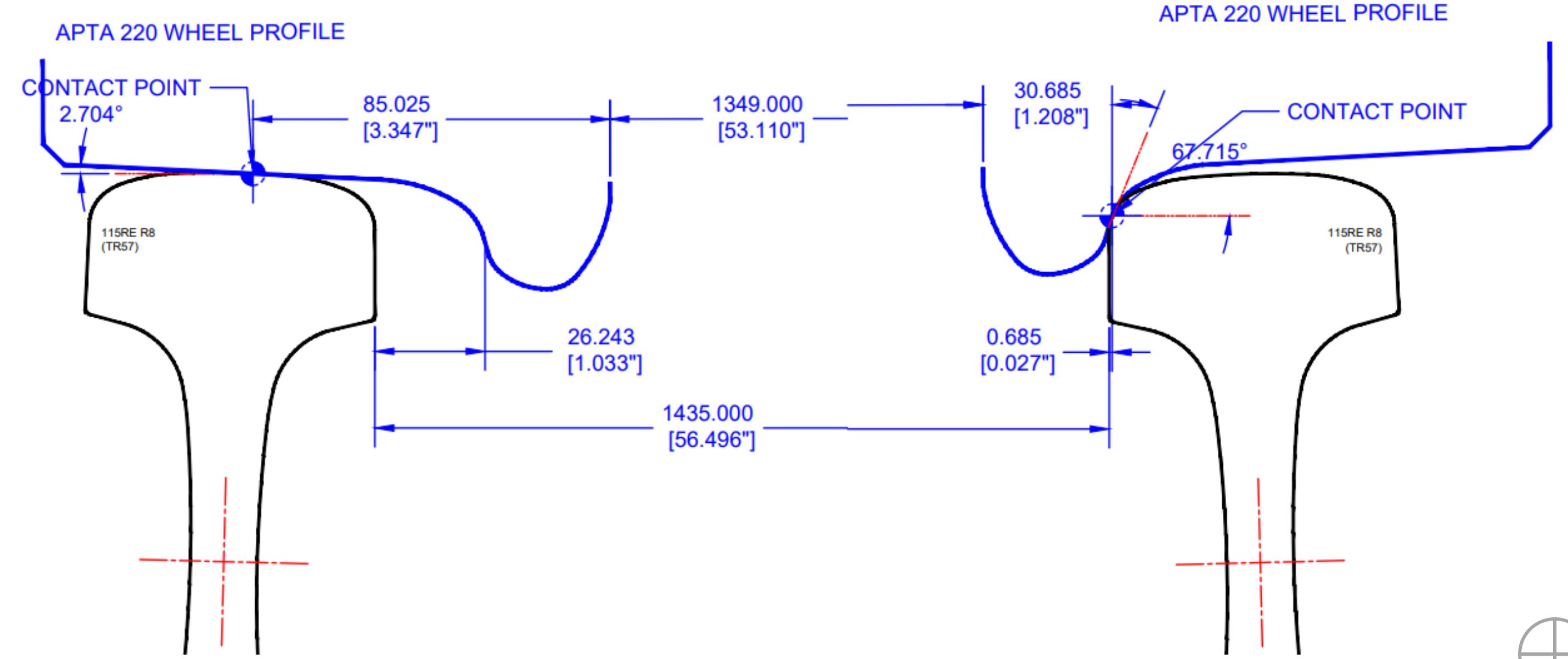


Dynamic Modeling - Normal Profile

(115RE 8" - 1:40 cant)

WHEEL AXLE 13.0 TO LEFT
CANT: 1:40
Delta R = 13.47mm

PRINCIPLES COURSE



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Dynamic Modeling - Normal Profile

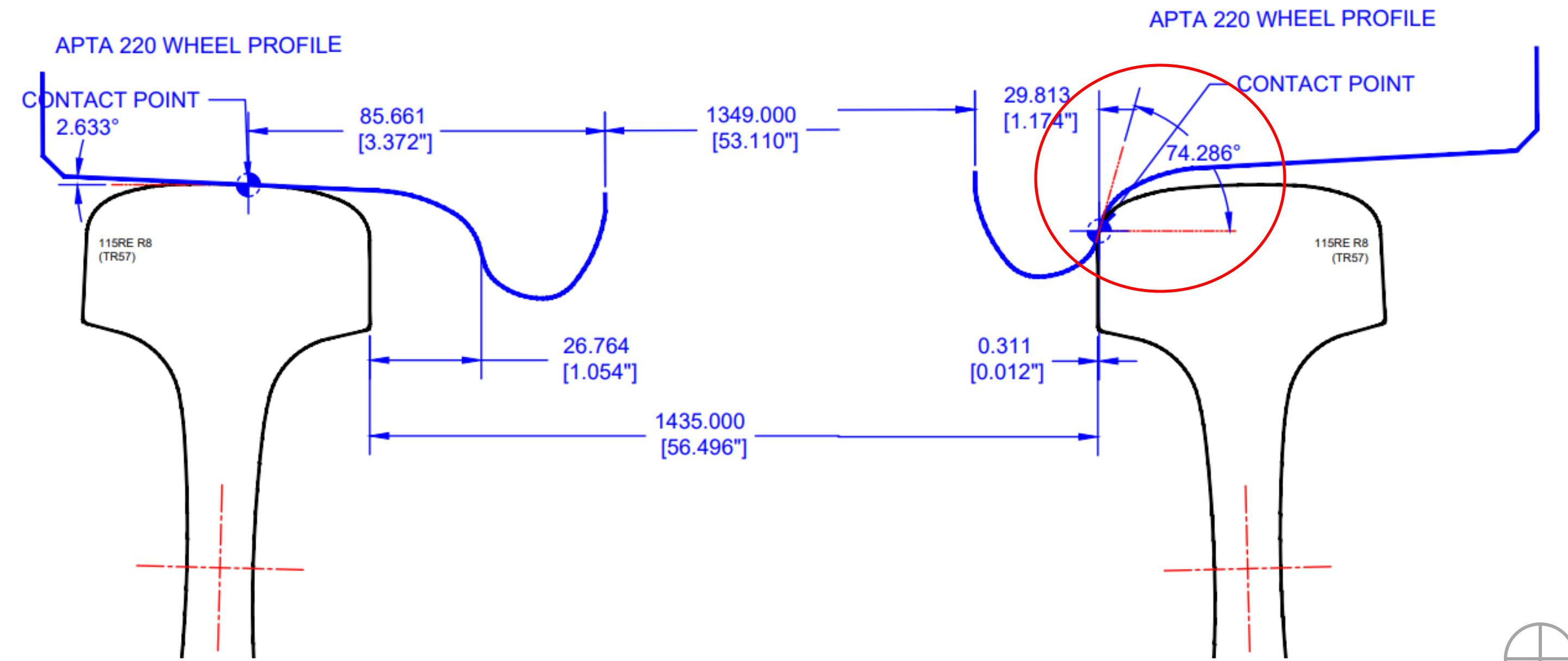
(115RE 8" - 1:40 cant)

WHEEL AXLE 13.5 TO LEFT

CANT: 1:40

$\Delta R = 16.286\text{mm}$

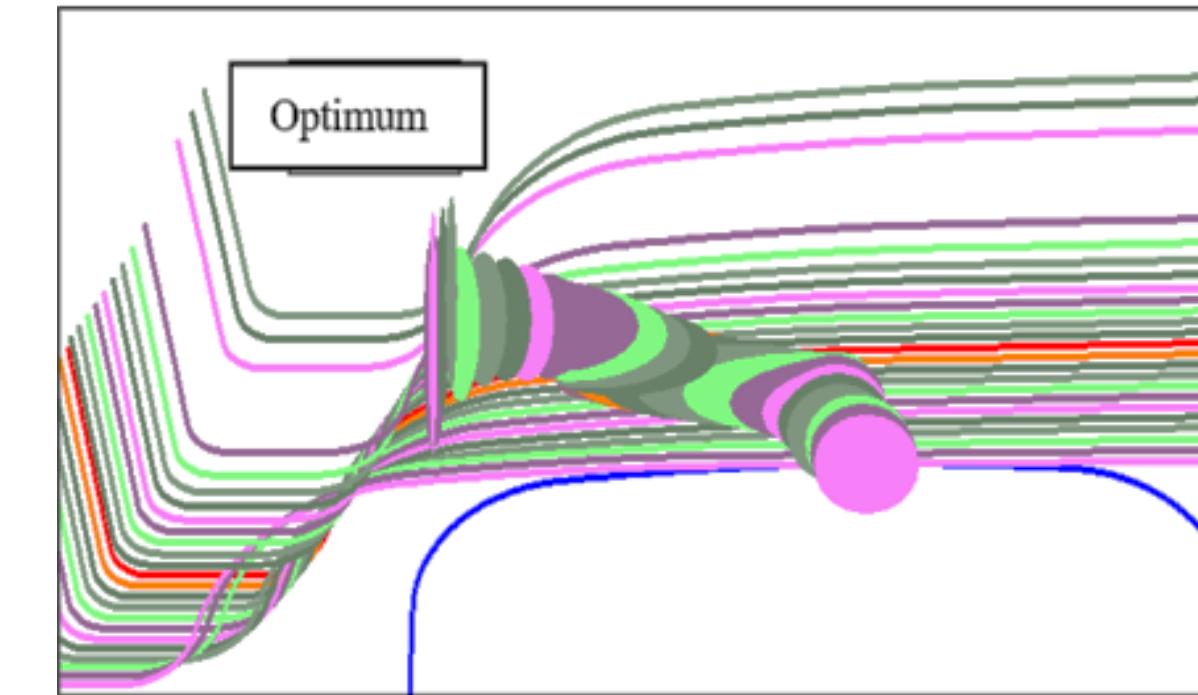
PRINCIPLES COURSE





Dynamic Modeling - Improved Profile (115RE 8" _ 1:40 cant)

Smooth steering transitions



Dynamic Modeling - Improved Profile

(115RE 8" _ 1:40 cant)

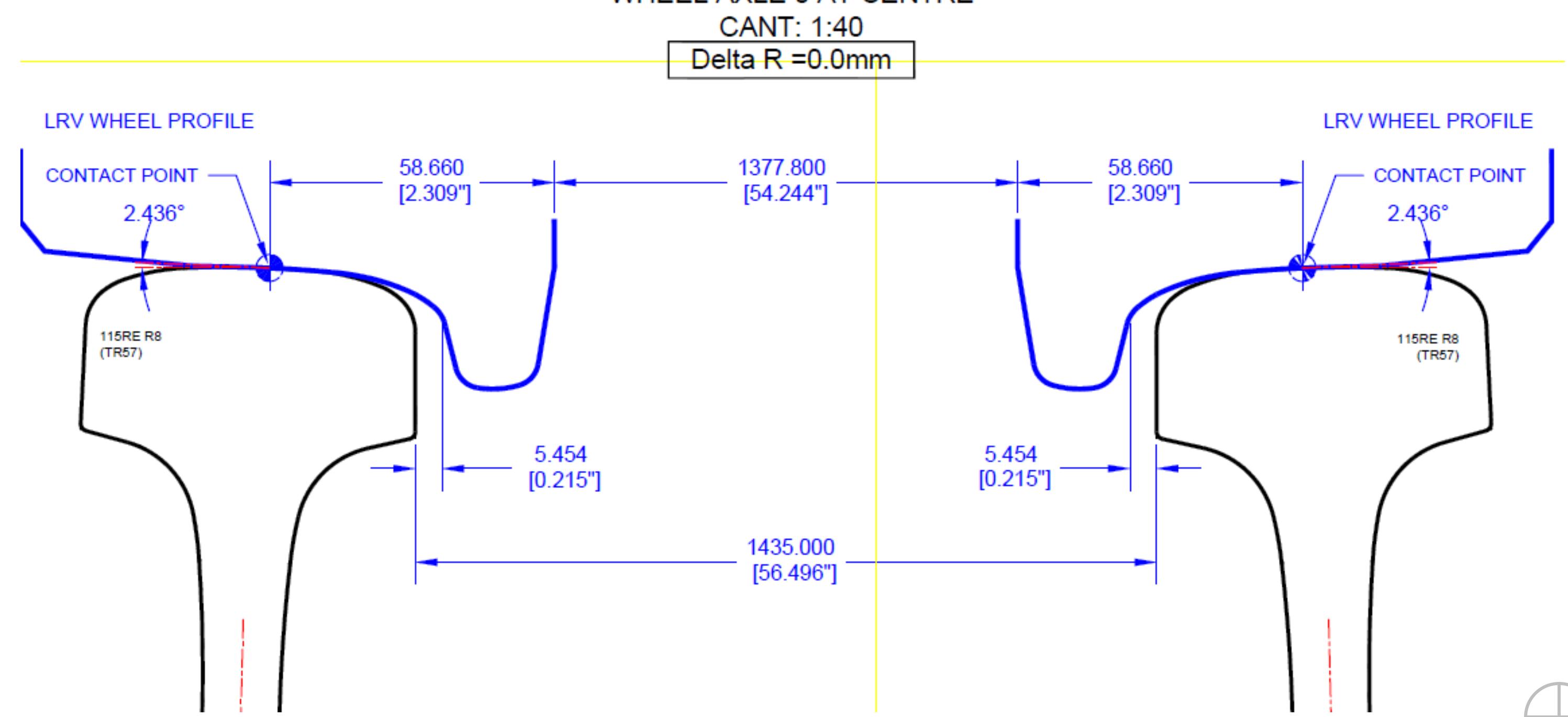
1

WHEEL AXLE 0 AT CENTRE

CANT: 1:40

Delta R = 0.0mm

PRINCIPLES COURSE

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Dynamic Modeling - Improved Profile

(115RE 8" _1:40 cant)

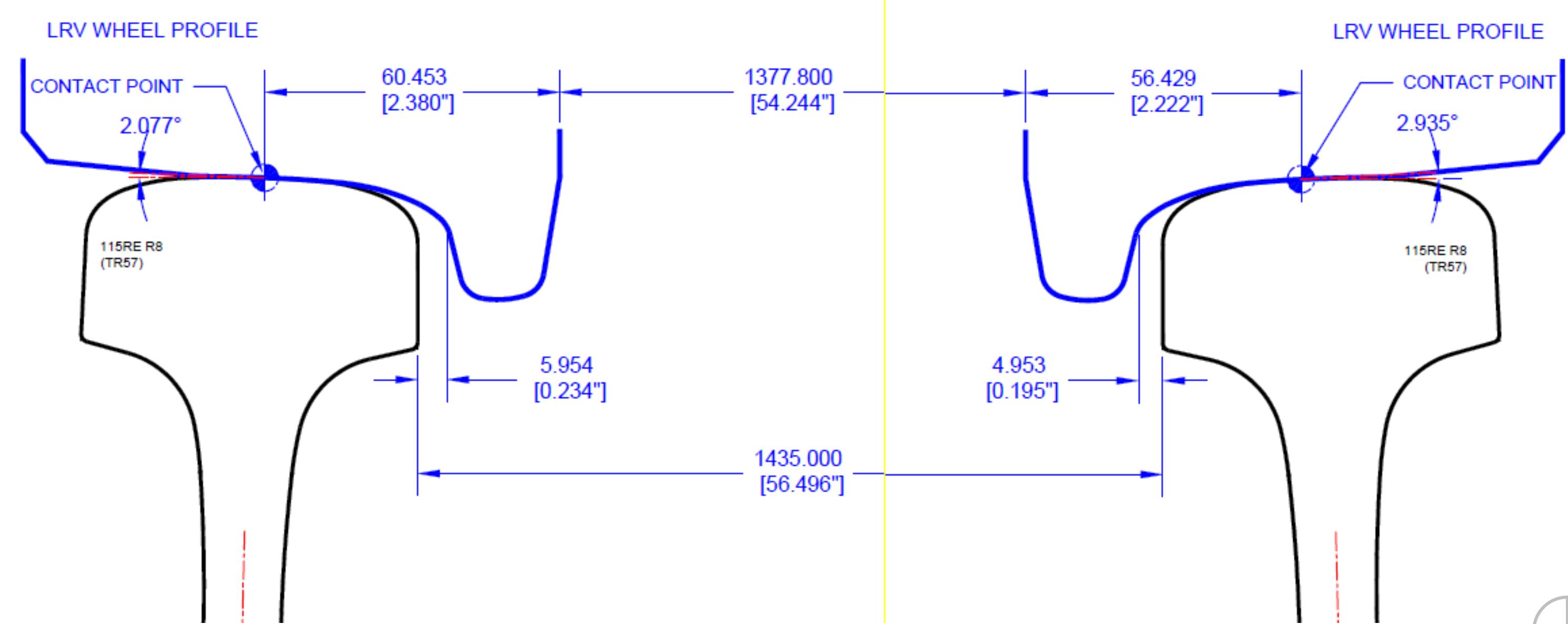
2

WHEEL AXLE 0.5 TO RIGHT

CANT: 1:40

Delta R = 0.176mm

PRINCIPLES COURSE

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Dynamic Modeling - Improved Profile

(115RE 8" _ 1:40 cant)

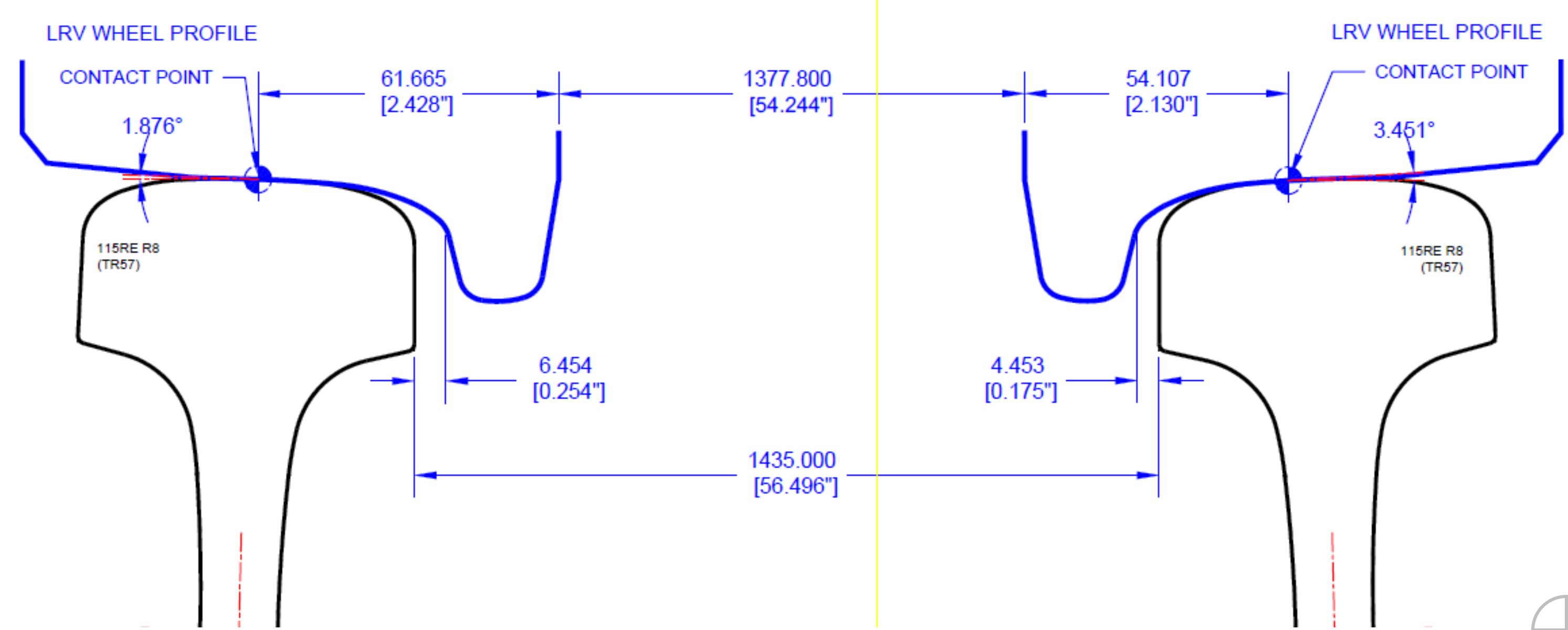
3

WHEEL AXLE 1.0 TO RIGHT

CANT: 1:40

Delta R = 0.346mm

PRINCIPLES COURSE

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Dynamic Modeling - Improved Profile

(115RE 8" _ 1:40 cant)

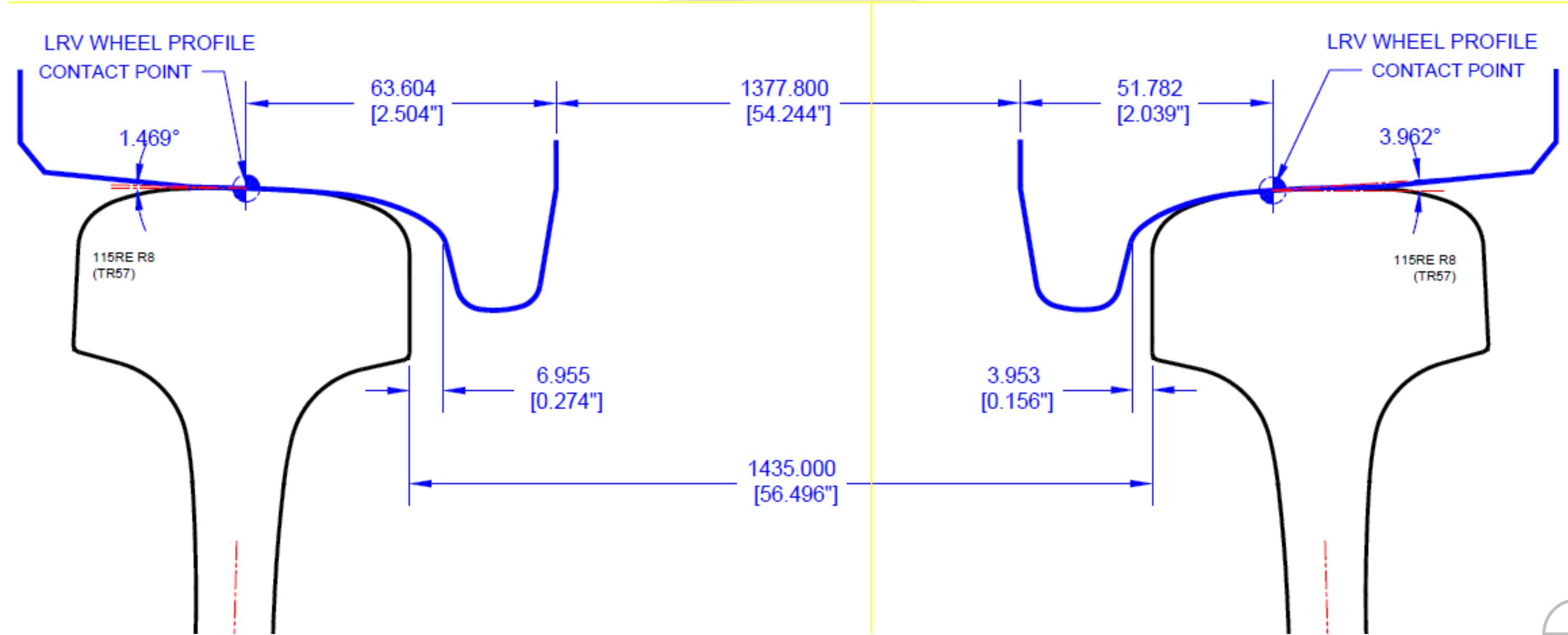
4

WHEEL AXLE 1.5 TO RIGHT

CANT: 1:40

Delta R = 0.553mm

PRINCIPLES COURSE

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Dynamic Modeling - Improved Profile

(115RE 8" _ 1:40 cant)

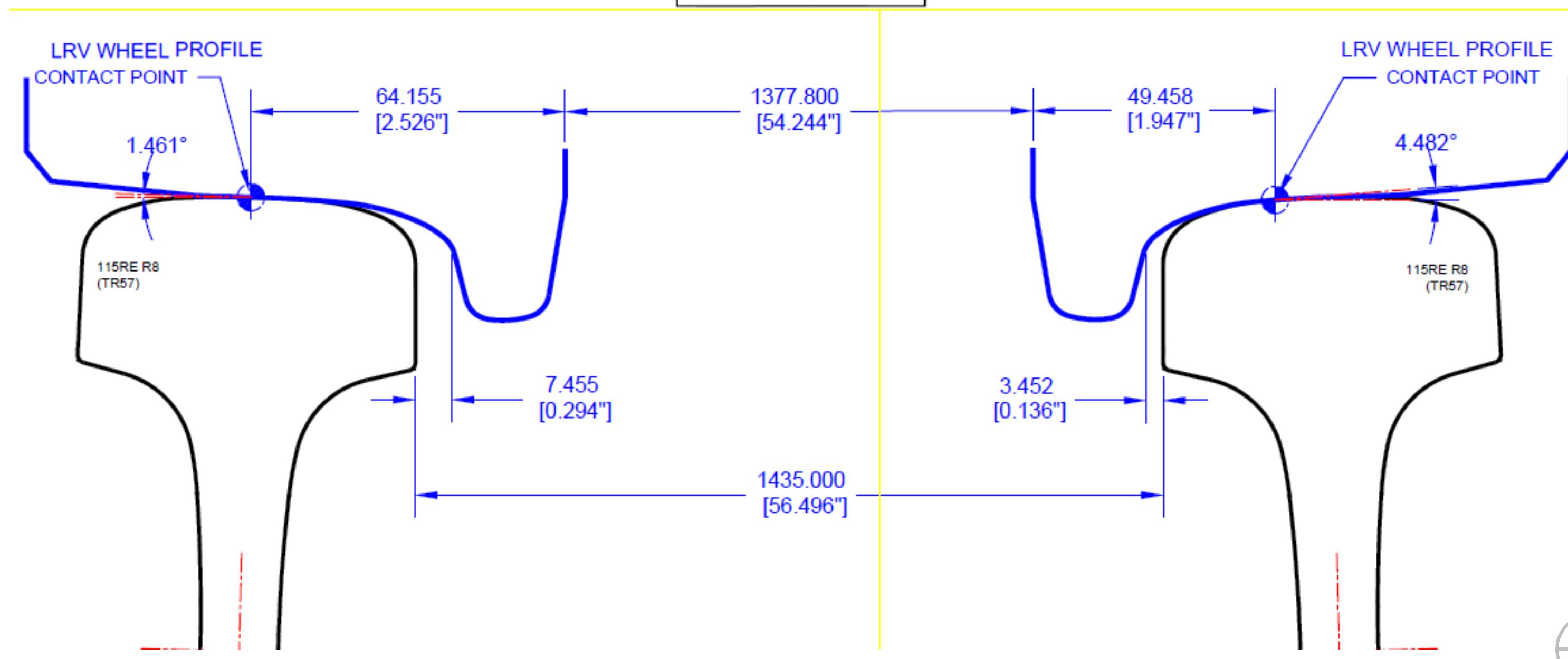
5

WHEEL AXLE 2.0 TO RIGHT

CANT: 1:40

Delta R = 0.739mm

PRINCIPLES COURSE

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Dynamic Modeling - Improved Profile

(115RE 8" _ 1:40 cant)

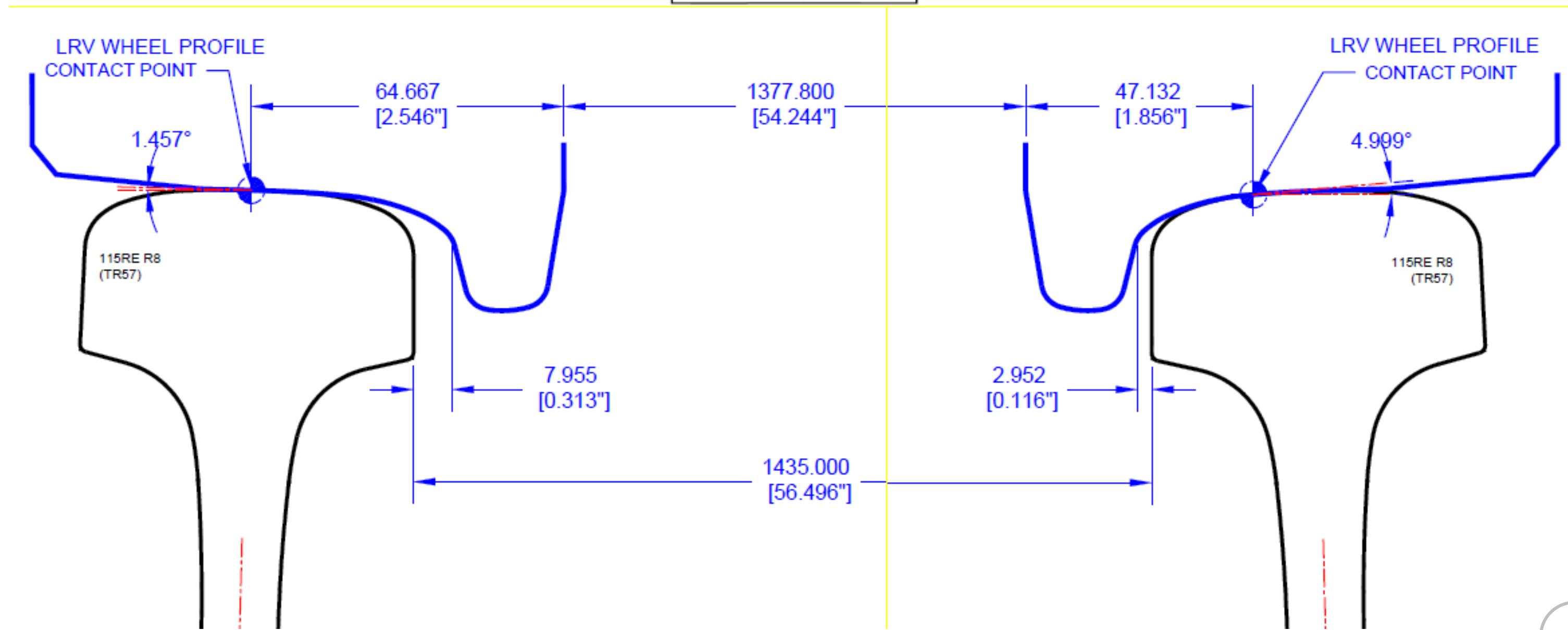
6

WHEEL AXLE 2.5 TO RIGHT

CANT: 1:40

Delta R = 0.944mm

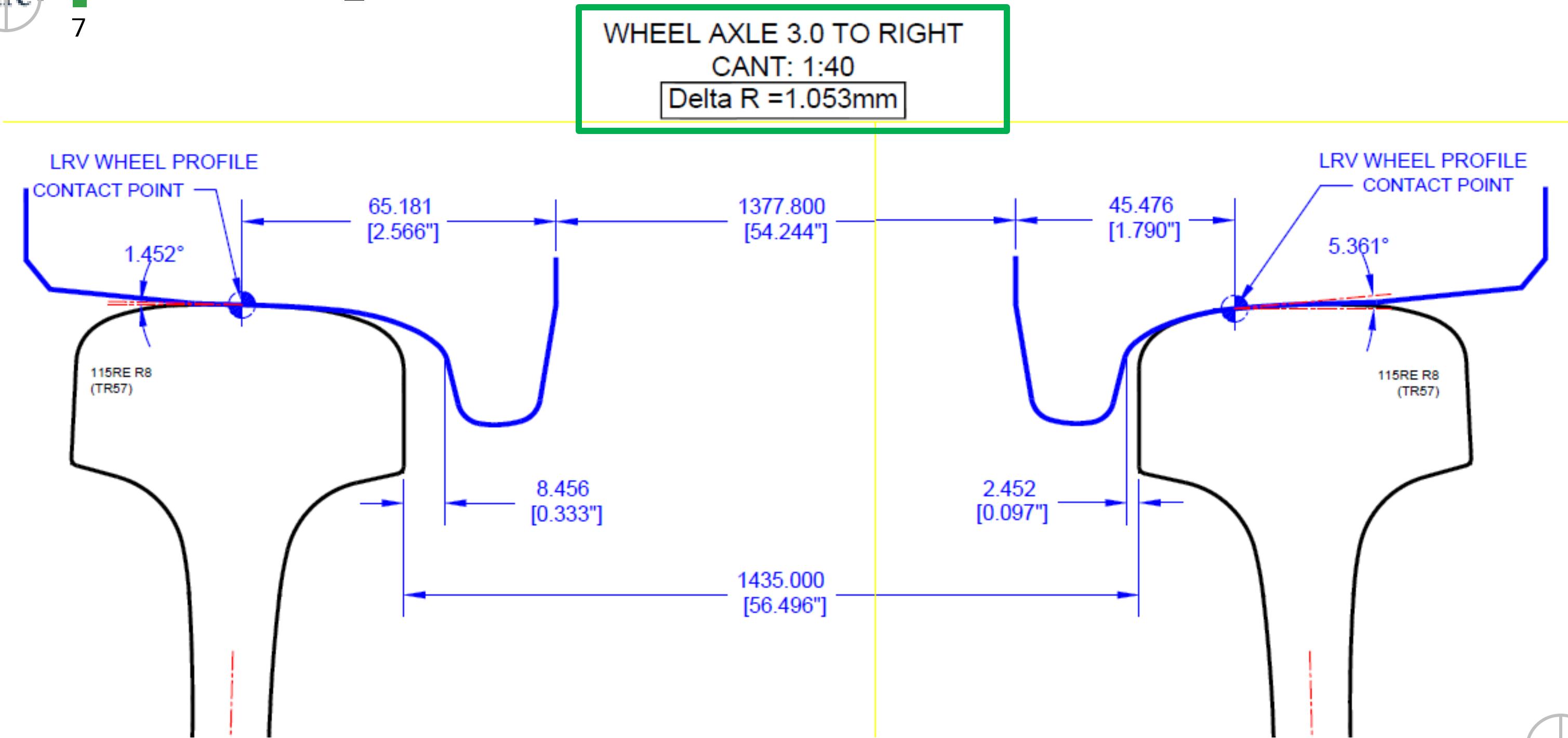
PRINCIPLES COURSE

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Dynamic Modeling - Improved Profile

(115RE 8" _ 1:40 cant)

7

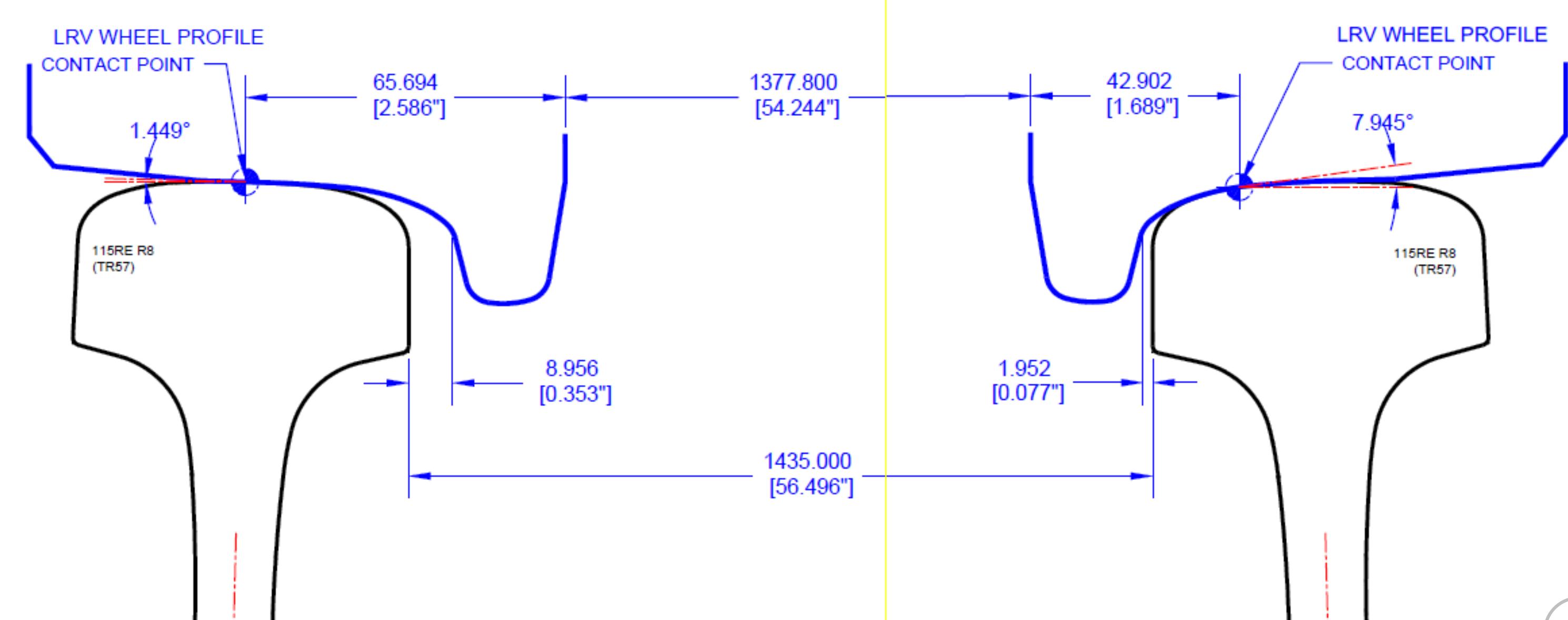


Dynamic Modeling - Improved Profile

(115RE 8" _ 1:40 cant)

8

WHEEL AXLE 3.5 TO RIGHT
CANT: 1:40
Delta R = 1.411mm



PRINCIPLES COURSE

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Dynamic Modeling - Improved Profile

(115RE 8" _ 1:40 cant)

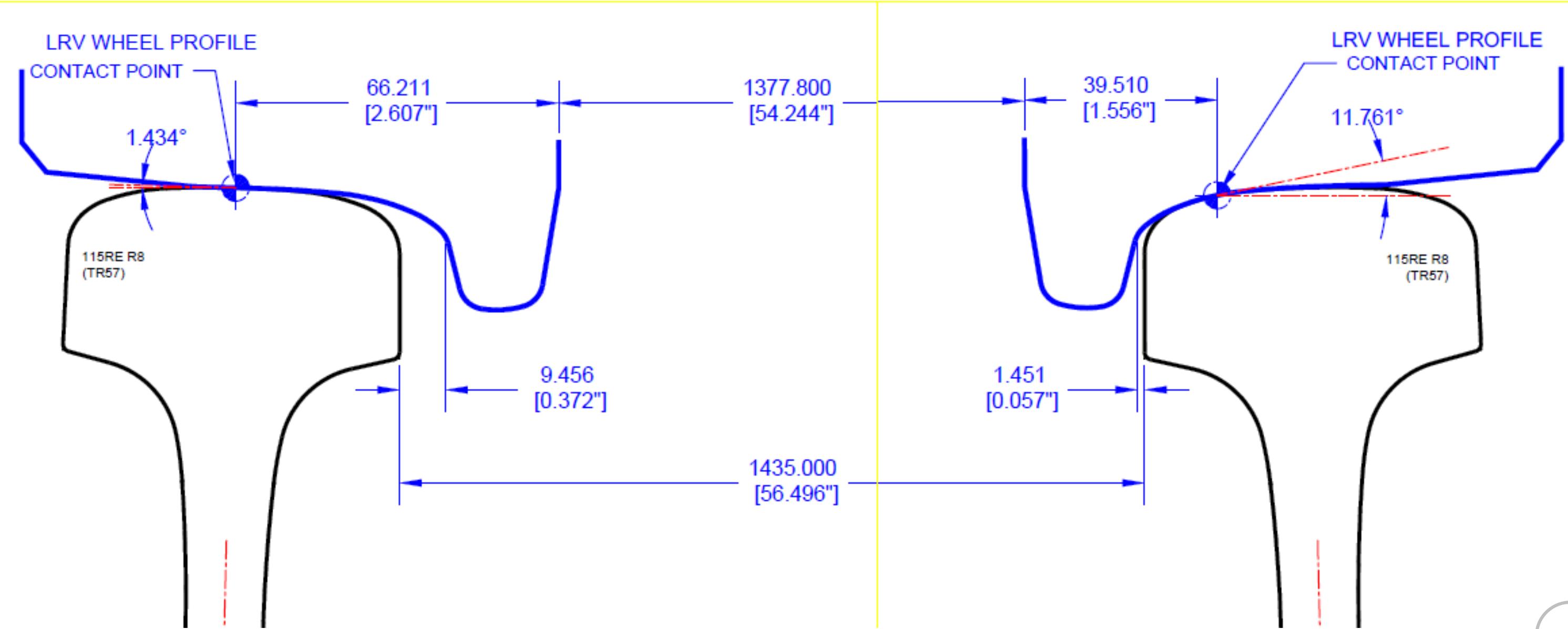
9

WHEEL AXLE 4.0 TO RIGHT

CANT: 1:40

Delta R = 2.024mm

PRINCIPLES COURSE

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Dynamic Modeling - Improved Profile

(115RE 8" _ 1:40 cant)

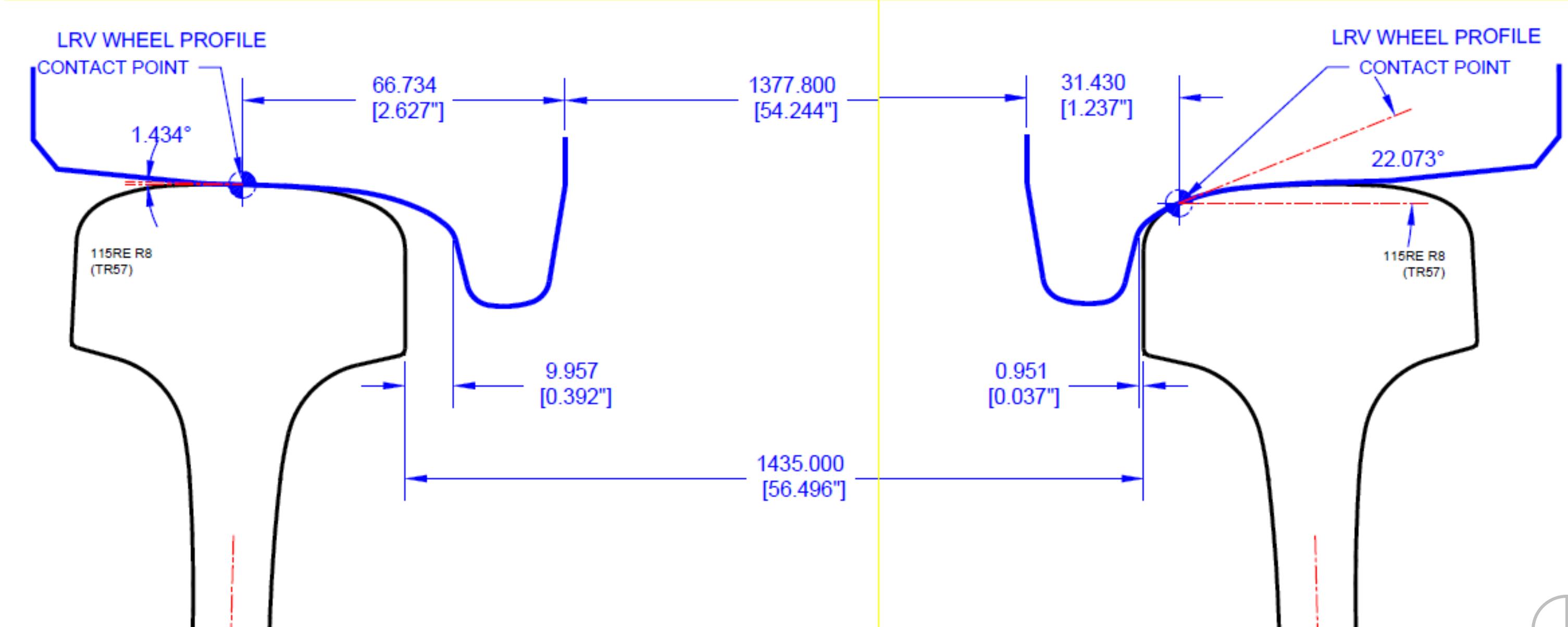
10

WHEEL AXLE 4.5 TO RIGHT

CANT: 1:40

Delta R = 4.447mm

PRINCIPLES COURSE

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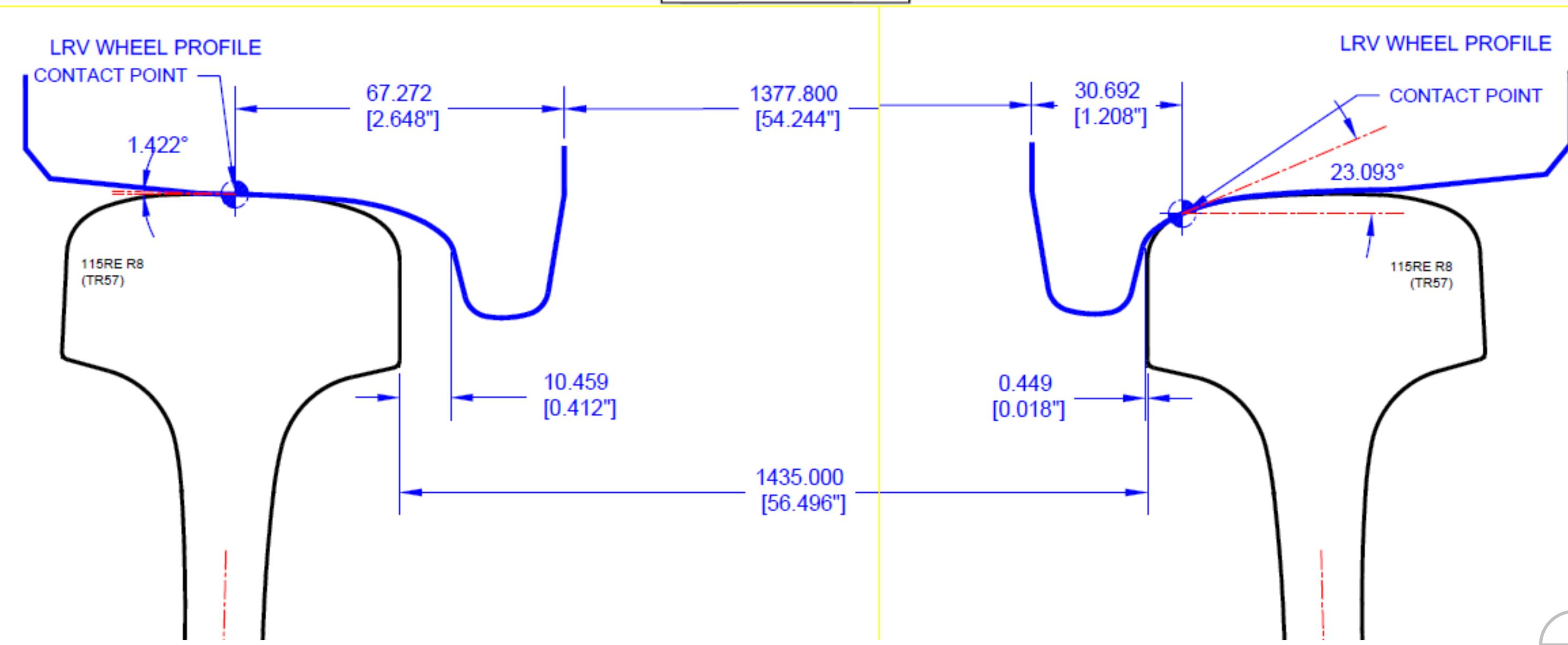
Dynamic Modeling - Improved Profile

(115RE 8" _ 1:40 cant)

11

WHEEL AXLE 5.0 TO RIGHT
CANT: 1:40
Delta R = 4.769mm

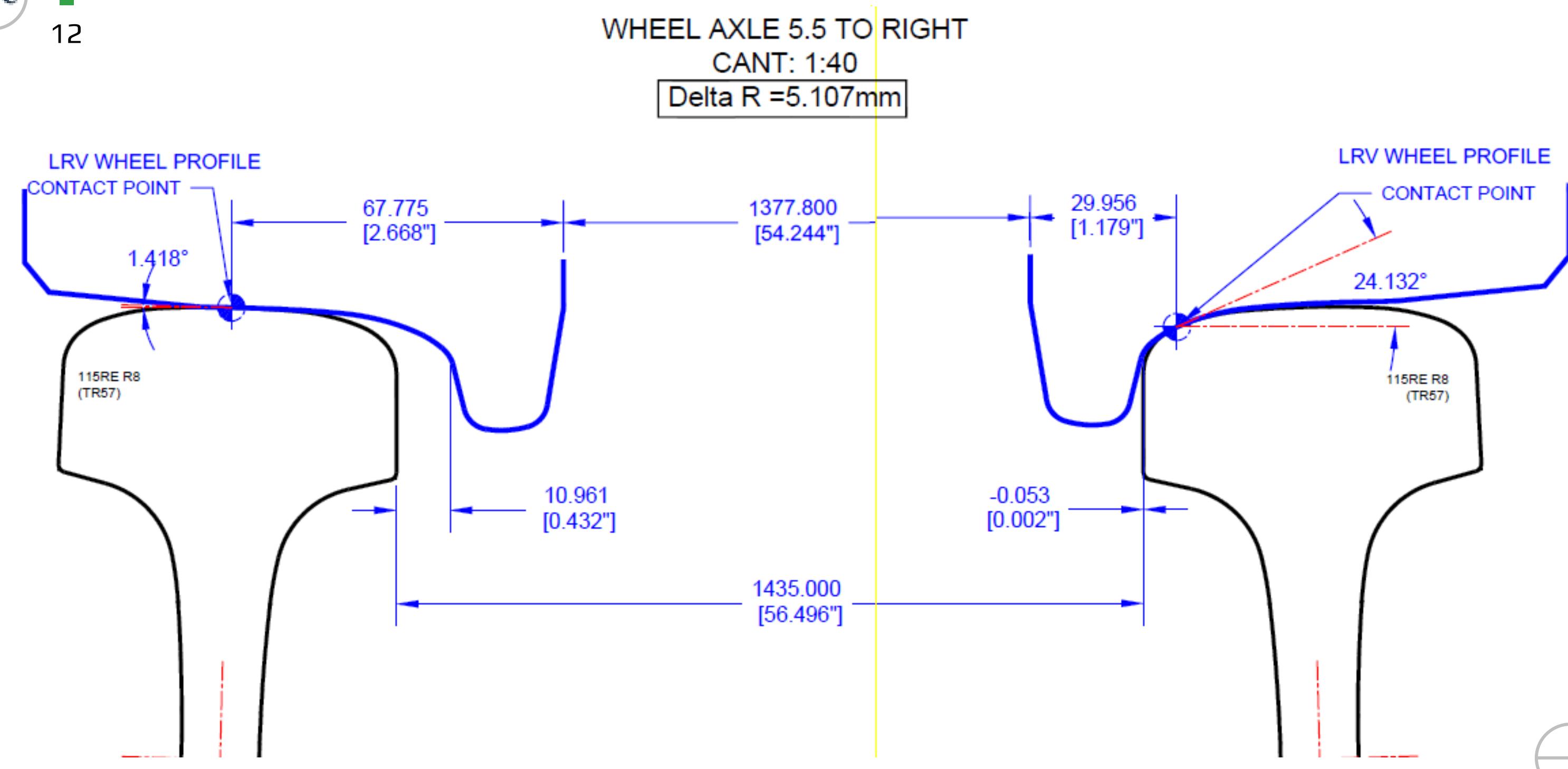
PRINCIPLES COURSE

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Dynamic Modeling - Improved Profile

(115RE 8" _ 1:40 cant)

12



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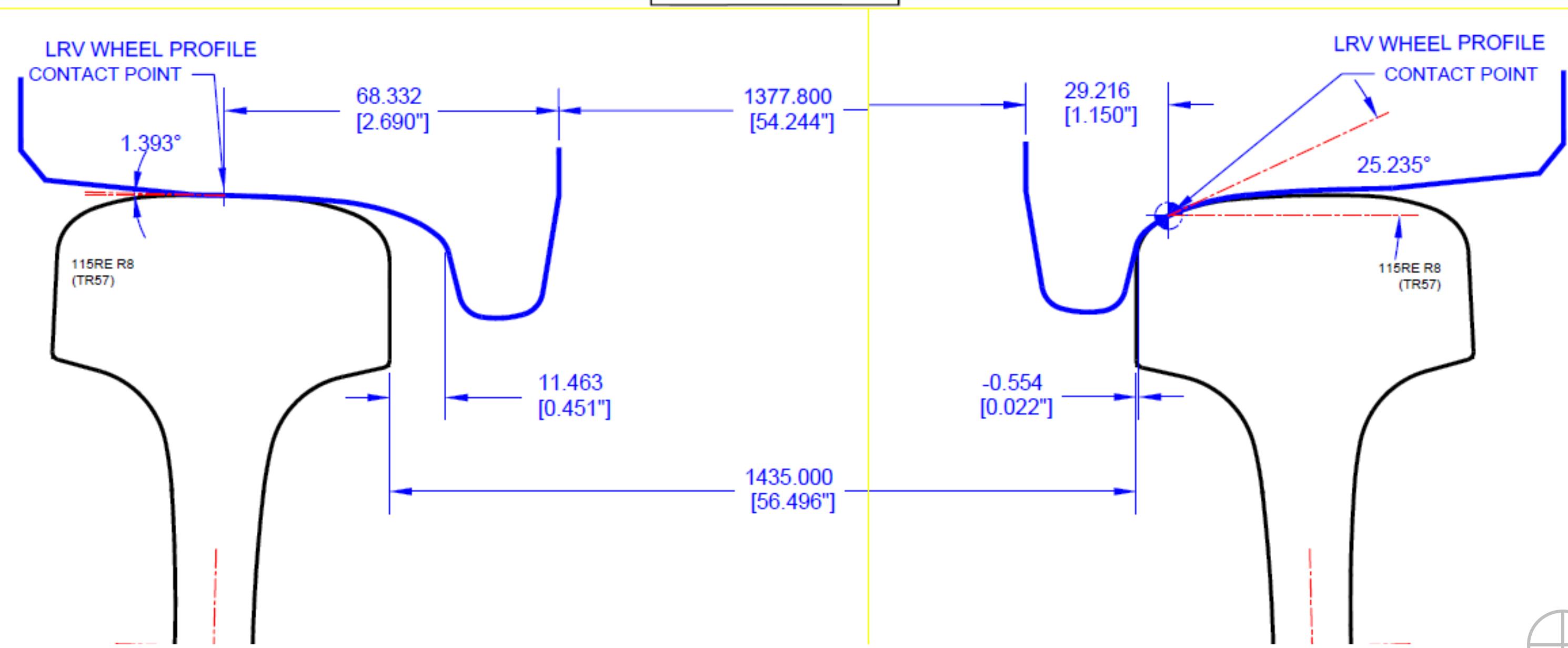


Dynamic Modeling - Improved Profile

(115RE 8" _ 1:40 cant)

13

WHEEL AXLE 6.0 TO RIGHT
CANT: 1:40
Delta R = 5.461mm



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Dynamic Modeling - Improved Profile

(115RE 8" _ 1:40 cant)

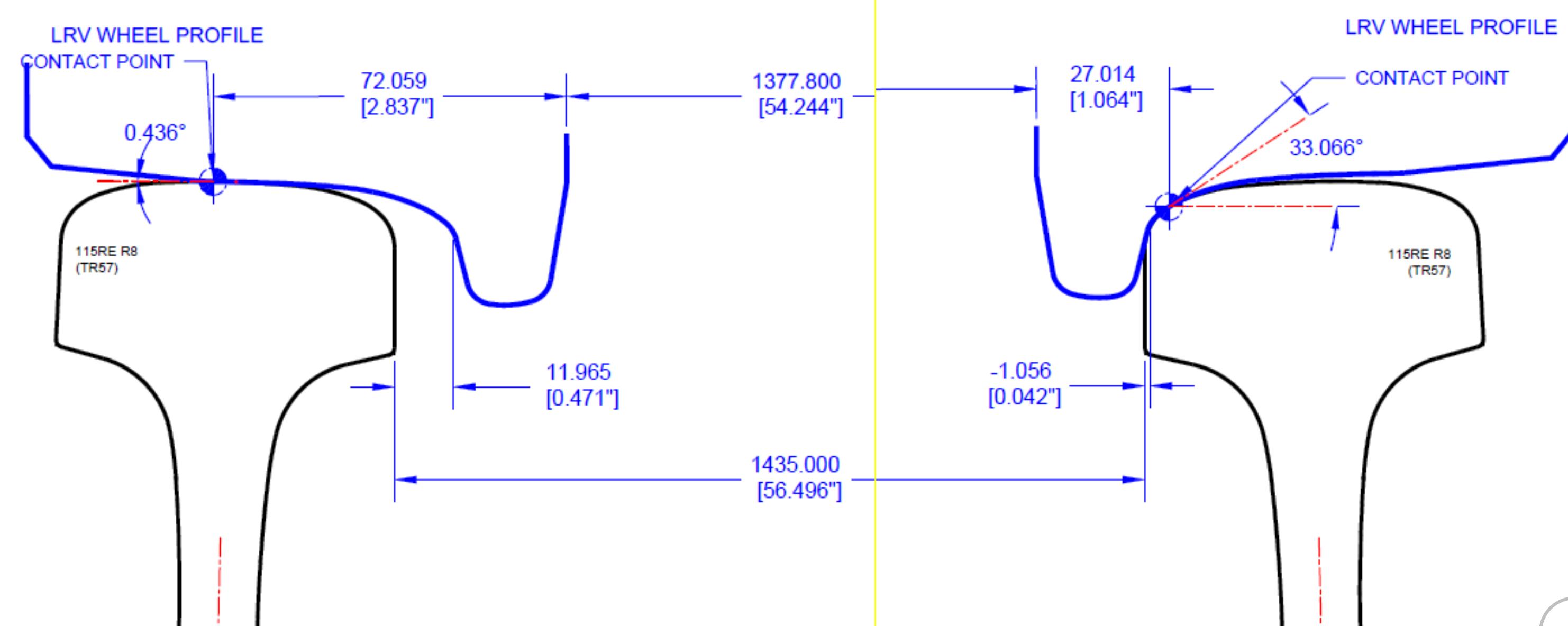
14

WHEEL AXLE 6.5 TO RIGHT

CANT: 1:40

$\Delta R = 6.772\text{mm}$

PRINCIPLES COURSE



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Dynamic Modeling - Improved Profile

(115RE 8" _ 1:40 cant)

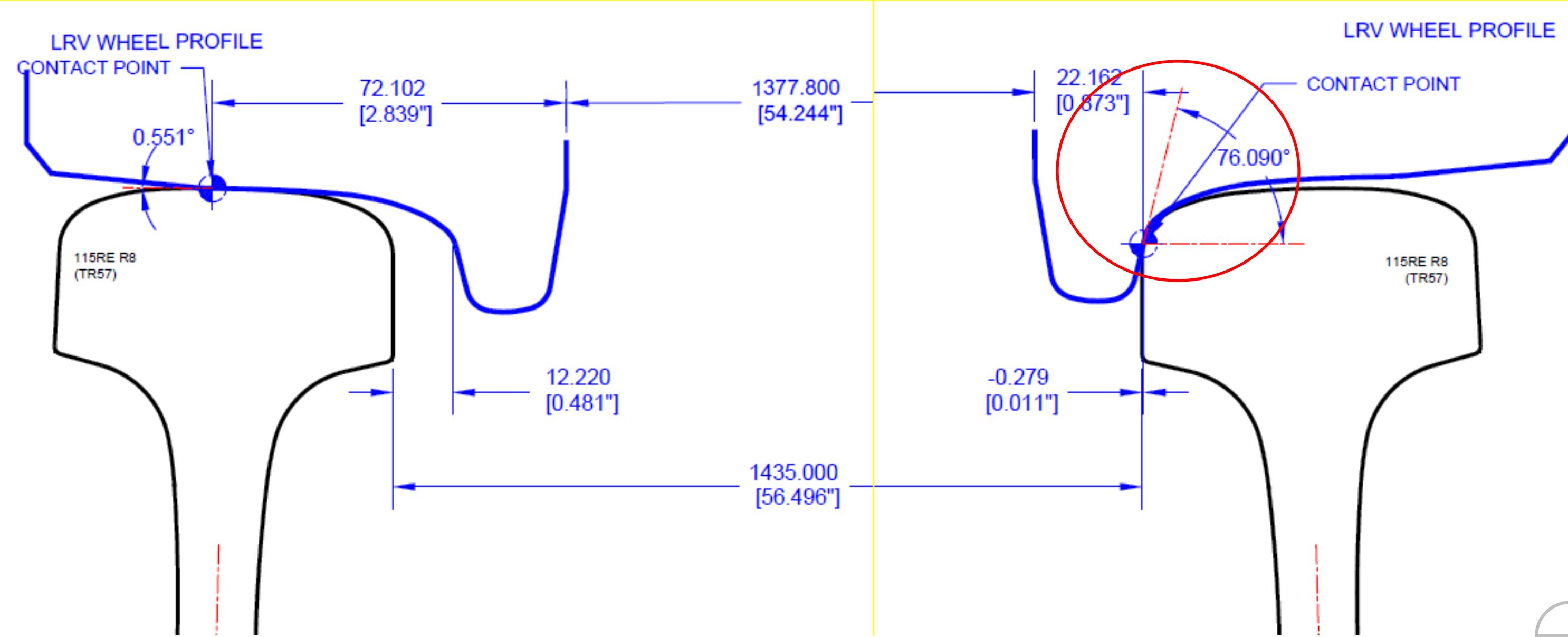
15

WHEEL AXLE 6.75 TO RIGHT

CANT: 1:40

Delta R = 13.612mm

PRINCIPLES COURSE

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- Transit Vehicle Suspension
- Track Influence on Stability
- Wheel-to-Rail Interface Criteria
- Wheel Profile Sensitivity
- Improving Wheel Profiles
- Dynamic Modeling – Normal vs Improved
- **Conclusion**





Benefits of Improved Profile

- Enhances self-centering running stability thereby
Improving ride quality.
- Reduction of rail gauge face to achieve 0.3mm per year.
- Reduction of wheel flange wear to achieve 0.03mm per 1000 kilometre (km).
- Increased wheel mileage up to 220 Tonne-kilometre (tkm).
- Avoiding hollow wear and increase the reprofiling interval for up to 150tkm without re-occurring instability problems.

Conclusion



When a uniformly distributed movement of the contact patch during lateral offset of the wheelset is achieved throughout the track network, the transit vehicle and rails will exhibit reduced wear and provide a safer and more stable steering and tracking capability.





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