

## Material Derivative.

Consider the temperature of a fluid in 3D:

$$T(x, y, z, t)$$

The total time derivative is:

$$\frac{dT}{dt} = \frac{\partial T}{\partial t} + \frac{\partial T}{\partial x} \cdot \frac{\partial x}{\partial t} \quad v_x$$

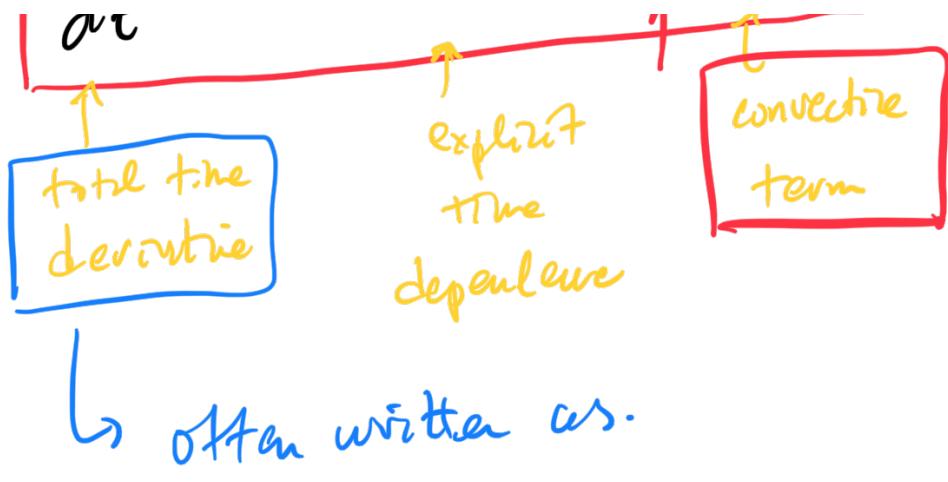
$$+ \frac{\partial T}{\partial y} \cdot \frac{\partial y}{\partial t} + \frac{\partial T}{\partial z} \cdot \frac{\partial z}{\partial t}$$

$$\frac{dT}{dt} = \frac{\partial T}{\partial t} + \left[ v_x \frac{\partial T}{\partial x} + v_y \frac{\partial T}{\partial y} \right]$$

$$\vec{v} = v_x \frac{\partial}{\partial x} + v_y \frac{\partial}{\partial y} + v_z \frac{\partial}{\partial z}$$

$$\frac{dT}{dt} = \frac{\partial T}{\partial t} + (\vec{v} \cdot \vec{\nabla}) T$$

$$\boxed{\frac{d}{dt} = \frac{\partial}{\partial t} + (\vec{v} \cdot \vec{\nabla})}$$



$$\frac{D}{Dt} \equiv \text{material derivative.}$$

What is the time-dependent acceleration field of the fluid?

$$\vec{\ddot{a}}(x, y, z, t) \equiv \frac{D\vec{v}}{Dt}$$

$$\vec{\ddot{a}}(x, y, z, t) = \frac{\partial \vec{v}}{\partial t} + (\vec{v} \cdot \vec{\nabla}) \vec{v}$$

- ... we know that

From Newton's Laws, we know that the acceleration is proportional to the net force on the fluid.

In general, the forces on the fluid come in two forms:

① pressure forces

→ gravity (body force)

→ external pressure for humans.

② frictional forces

→ viscous forces.

Gravity:

$$\vec{a}_g = -g \hat{j} = \vec{g}$$

External:

$$\vec{a}_{\text{Ext. } P} = -\frac{\nabla P(x_1, y_1, z)}{\rho}$$

Pressures

$$[\text{N/m}^2] / \text{m} / \text{kg/m}^3 = \text{N/kg} \cdot \text{m}^{-2}$$

$$( \rightarrow \vec{a} ) \quad P_1 > P_2 \quad \therefore \frac{\partial P}{\partial x} < 0$$

$$\vec{F} = \vec{P} \cdot \vec{r}$$

Viscom Fases  $\dot{\epsilon}_{\text{viscos}} = \frac{\vec{\sigma}}{\rho}$

$\vec{\sigma}$  = deviatoric stress tensor  
[ $\sigma$ ] = Pa

→ this is the nasty part!  
( $\vec{F} = m\vec{a}$  for fluids)

$$\boxed{\rho \frac{D\vec{v}}{Dt} = - \vec{\nabla} p + \vec{\nabla} \cdot \vec{\tau} + \vec{\rho g}}$$

This is known as the Cauchy momentum equation. Various hypotheses for the form of  $\vec{\tau}$  lead to the Navier-Stokes equation.

Conservation of mass:  
(no sources or sinks)

$$\frac{D}{Dt} (\rho V) = 0$$

↑ volume

$$\boxed{\frac{D\rho}{Dt} = 0}$$

⇒

$$\boxed{\frac{\partial \rho}{\partial t} + (\vec{v} \cdot \vec{\nabla}) \rho =}$$

Continuity Equation:

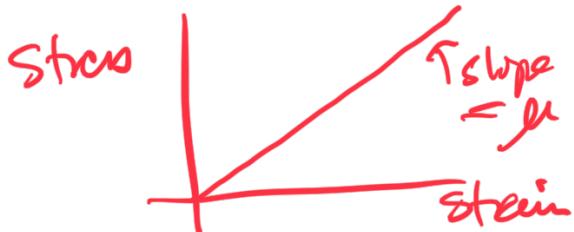
$$\cancel{\frac{\partial p}{\partial t}} + \vec{\nabla} \cdot (\rho \vec{v}) = 0$$

[ Note: for an incompressible fluid,  $\rho = \text{constant}$ ,  
and hence  $\vec{\nabla} \cdot \vec{v} = 0$  ]

## Navier-Stokes Equations:

Assumptions:

Newtonian Fluid.



① Stress tensor is a linear function of the strain rate tensor, or equivalently the velocity gradient.

$$\vec{\tau} \propto \vec{\nabla} \cdot \vec{u}$$

② The fluid is isotropic

③ for a fluid at rest,  $\vec{\nabla} \cdot \vec{\tau} = C$

(i.e. we get the hydrostatic press.)

???) ...

$$\vec{\tau} = \mu \left( \vec{\nabla} \cdot \vec{u} + (\vec{\nabla} \cdot \vec{u})^T \right) + \lambda (\vec{\nabla} \cdot \vec{u}) \mathbb{I}$$

} } } \text{ sum}

$$\boxed{\tau_{ij}} = \mu \left( \frac{\partial v_i}{\partial x_j} + \frac{\partial v_j}{\partial x_i} \right)$$

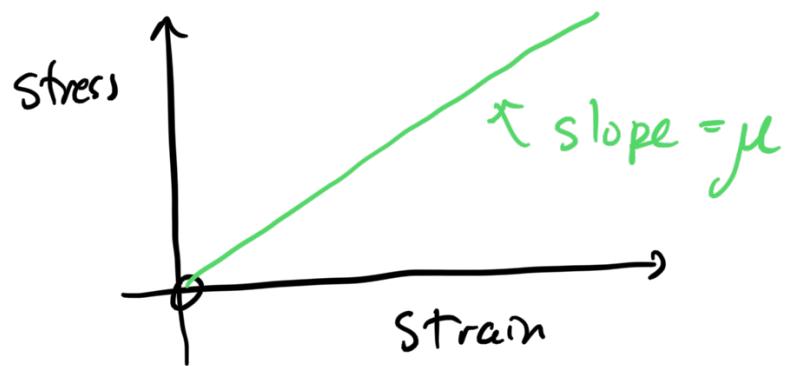
↓  
 first coefficient  
 of  
 viscosity  
 (The normal  
 one)  
 second coefficient of  
 viscosity  
 (volume or bulk  
 viscosity)

$$\begin{aligned}
 & \rho \left( \frac{\partial \vec{v}}{\partial t} + (\vec{v} \cdot \vec{\nabla}) \vec{v} \right) \\
 &= -\vec{\nabla} p + \vec{\nabla} \cdot \left[ \mu [ \nabla \vec{u} + (\nabla \vec{u})^T ] \right. \\
 &\quad \left. + \vec{\nabla} \cdot [\lambda (\vec{\nabla} \cdot \vec{u})] \right]
 \end{aligned}$$

## Navier - Stokes Equations

Example: Incompressible  
Newtonian Fluid

(i) viscosity is a constant



(ii) second viscosity =  $\lambda = 0$

(iii) continuity equation

$$\vec{\nabla} \cdot \vec{v} = 0$$

$$1 \cdot \vec{\nabla} \cdot (\vec{v} \cdot \vec{\nabla}) \vec{v}$$

$$\rho \left( \frac{\partial \vec{v}}{\partial t} + \vec{v} \cdot \nabla \vec{v} \right)$$

$$\cancel{\rho \frac{D\vec{v}}{Dt}} = -\vec{\nabla} p + \vec{\nabla} \cdot \left[ \mu \left( \vec{\nabla} v + (\vec{\nabla} v)^T \right) \right] + \rho \vec{g}$$

Let's look at the form of the viscous terms, in the  $x$ -direction for example.

$$\underline{\tau_{ij}} = \underline{-\mu} \left( \frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right) \quad (+ \cancel{\text{elsewhere}})$$

$$\underline{\tau_{11}} = \mu \left( \frac{\partial u}{\partial x} + \frac{\partial u}{\partial x} \right) \quad \begin{matrix} u, v, w \\ x, y, z \end{matrix}$$

$$\underline{\tau_{12}} = \mu \left( \frac{\partial u}{\partial y} + \frac{\partial v}{\partial x} \right)$$

$$\underline{\tau_{13}} = \mu \left( \frac{\partial u}{\partial z} + \frac{\partial w}{\partial x} \right)$$

$$\begin{aligned}
 (\vec{\nabla} \cdot \vec{v})_x &= \frac{\partial}{\partial x} \left( 2\mu \frac{\partial u}{\partial x} \right) \\
 &\quad + \frac{\partial}{\partial y} \left( \mu \left( \frac{\partial u}{\partial y} + \frac{\partial v}{\partial x} \right) \right) \\
 &\quad + \frac{\partial}{\partial z} \left( \mu \left( \frac{\partial u}{\partial z} + \frac{\partial w}{\partial x} \right) \right) \\
 &= 2\mu \frac{\partial^2 u}{\partial x^2} + \underbrace{\mu \frac{\partial^2 u}{\partial y^2}}_{+ \mu \frac{\partial^2 u}{\partial z^2}} + \underbrace{\mu \frac{\partial^2 v}{\partial x \partial y}}_{+ \mu \frac{\partial^2 w}{\partial x \partial z}} \\
 &= \boxed{\mu \nabla^2 u} + \mu \left( \frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 v}{\partial x \partial y} + \frac{\partial^2 w}{\partial x \partial z} \right)
 \end{aligned}$$

$$= \mu \nabla^2 u + \mu \frac{\partial}{\partial x} \left( \frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} \right) = \Delta$$

$$= \boxed{\mu \nabla^2 \vec{u}}$$

$$\boxed{\nabla \cdot \nabla} = \nabla^2$$

In the  $y$ - and  $z$ -directions,  
we get  $\mu \nabla^2 v$  and  $\mu \nabla^2 w$ ,  
respectively.

$$\rho \left( \frac{\partial \vec{v}}{\partial t} + (\vec{v} \cdot \vec{\nabla}) \vec{v} \right) = - \vec{\nabla} p + \mu \nabla^2 \vec{v} + \rho \vec{g}$$

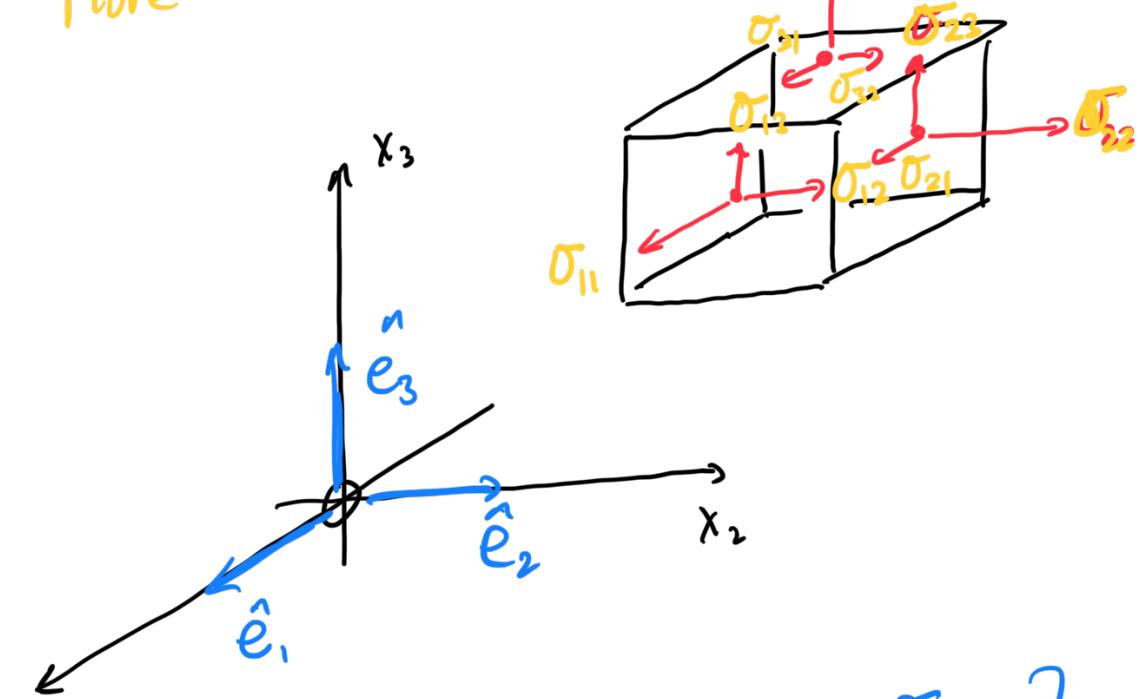
Navier - Stokes Equations

1D  
for an incompressible Newtonian  
Fluid.  $\rightarrow$  non-linear  
 $\mu = 0$   $\rightarrow$  coupled

$$\dots \text{and} \dots \vec{v} = 0$$

Inviscid Gamma i J

More on the stress tensor!



$$\boldsymbol{\sigma} = \begin{bmatrix} \sigma_{11} & \sigma_{12} & \sigma_{13} \\ \sigma_{21} & \sigma_{22} & \sigma_{23} \\ \sigma_{31} & \sigma_{32} & \sigma_{33} \end{bmatrix}$$

$$[\sigma] = \frac{N}{m^2} = P_a$$

$$\overline{\boldsymbol{\sigma}} = \boldsymbol{\sigma} \hat{n} = \begin{bmatrix} \sigma_{11} & \sigma_{12} & \sigma_{13} \\ \sigma_{21} & \sigma_{22} & \sigma_{23} \\ \sigma_{31} & \sigma_{32} & \sigma_{33} \end{bmatrix} \begin{bmatrix} \hat{e}_1 \\ \hat{e}_2 \\ \hat{e}_3 \end{bmatrix}$$

$$\rightarrow \text{Normal stresses } (\sigma_{11}, \sigma_{22}, \sigma_{33}) \equiv \delta$$

→ Shearing stress ( $\sigma_{ij}$ ,  $i \neq j$ )  $\equiv \tau_{ij}$

$$\sigma = \begin{bmatrix} \sigma_1 & \tau_{12} & \tau_{13} \\ \tau_{21} & \sigma_2 & \tau_{23} \\ \tau_{31} & \tau_{32} & \sigma_3 \end{bmatrix}$$

Because Pressure is so important, we separate that out of the diagonal elements.

$$\sigma_1 = P + \tau_{11}$$

$$\sigma_2 = P + \tau_{22}$$

$$\sigma_3 = P + \tau_{33}$$

$$\therefore \sigma = P + \begin{bmatrix} \tau_{11} & \tau_{12} & \tau_{13} \\ \tau_{21} & \tau_{22} & \tau_{23} \\ \tau_{31} & \tau_{32} & \tau_{33} \end{bmatrix}$$

$$\tilde{\sigma} = P \tilde{I} + \tilde{\tau}$$

tends to  
change the  
volume of  
the element

tends to  
distort  
the element

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