## **Inverse Differential Kinematics**

- Joint space variables <--(highly nonlinear)--> operational space variables
- · J is time variant

#### J invertible -- Numerical Solution

when  ${f J}$  is square matrix and of full rank --> invertible. use Newton-Euler Integration Method for IK.

$$\mathbf{q}(t)=\int_0^t \dot{\mathbf{q}}(t)dt+\mathbf{q}(0)$$

# Geometric Jacobian ${f J}$ Analytical Jacobian ${f J}_A$

$$egin{aligned} \dot{\mathbf{q}} &= \mathbf{J}^{-1}(\mathbf{q})\mathbf{v}_e \ \Rightarrow \mathbf{q}(t_{k+1}) &= \mathbf{q}(t_k) + \dot{\mathbf{q}}(t_k)\Delta t \ &= \mathbf{q}(t_k) + \mathbf{J}^{-1}(\mathbf{q}(t_k))\mathbf{v}_e(t_k)\Delta t \end{aligned}$$

$$egin{aligned} \dot{\mathbf{q}} &= \mathbf{J}_A^{-1}(\mathbf{q})\dot{\mathbf{x}}_e \ \Rightarrow \mathbf{q}(t_{k+1}) &= \mathbf{q}(t_k) + \dot{\mathbf{q}}(t_k)\Delta t \ &= \mathbf{q}(t_k) + \mathbf{J}_A^{-1}(\mathbf{q}(t_k))\dot{\mathbf{x}}_e(t_k)\Delta t \end{aligned}$$

当然可以用其他数值积分方法, 以达到更高的精度.

#### 1.st Order Numerical Solution

 ${f J}$  square, and of full rank, choose  $\dot{{f q}}={f J}^{-1}({f v}_e+{f K}e)$ 

## **Redundant Manipulators**

**Problem**:  $r < n, \mathbf{J}$  not square 不可逆. given  $\mathbf{v}_e, \mathbf{J}$ , find  $\dot{\mathbf{q}}$  and minimize the quadratic cost function of joint velocities  $g(\dot{\mathbf{q}}) = \frac{1}{2}\dot{\mathbf{q}}^T\mathbf{W}\dot{\mathbf{q}}, \mathbf{W}$  is a suitable  $(n \times n)$  symmetric positive definite weighting matrix.

Solving: Using Lagrange Methods:

modify cost function:

$$g(\dot{\mathbf{q}},\lambda) = rac{1}{2}\dot{\mathbf{q}}^T\mathbf{W}\dot{\mathbf{q}} + \lambda^T(\mathbf{v}_e - \mathbf{J}\dot{\mathbf{q}})$$

where  $\lambda$  is an  $r \times 1$  vector of unknown lagrange multipliers that allows the incorporation of the constraints to minimize.

· neccessary conditions:

$$\left(rac{\partial g}{\partial \dot{\mathbf{q}}}
ight)^T = \mathbf{0}, \left(rac{\partial g}{\partial \lambda}
ight)^T = \mathbf{0}$$

the ??? leads to

$$\mathbf{W}\dot{\mathbf{q}} - \mathbf{J}^T \lambda = 0 \rightarrow \dot{\mathbf{q}} = \mathbf{W}^{-1} \mathbf{J}^T \lambda$$

• Notice that solution is minimum, since  $\frac{\partial^2 g}{\partial^2 \dot{\mathbf{q}}} = \mathbf{W}$  is positive definite.

ullet under the assumption that  $oldsymbol{J}$  has full rank:

$$\mathbf{v}_e = \mathbf{J}\dot{\mathbf{q}} = \mathbf{J}\mathbf{W}^{-1}\mathbf{J}^T\lambda$$

where  $\mathbf{J}\mathbf{W}^{-1}\mathbf{J}^T$  is an r imes r square matrix of rank r and can be inverted.

$$egin{aligned} \dot{oldsymbol{\lambda}} &= (\mathbf{J}\mathbf{W}^{-1}\mathbf{J}^T)^{-1}\mathbf{v}_e \ \dot{\mathbf{q}} &= \mathbf{W}^{-1}\mathbf{J}^T(\mathbf{J}\mathbf{W}^{-1}\mathbf{J}^T)^{-1}\mathbf{v}_e, 
ightarrow \mathbf{J} \cdot \ \mathbf{J}\dot{\mathbf{q}} &= \mathbf{J}\mathbf{W}^{-1}\mathbf{J}^T(\mathbf{J}\mathbf{W}^{-1}\mathbf{J}^T)^{-1}\mathbf{v}_e = \mathbf{v}_e \end{aligned}$$

以上计算显示,  $\mathbf{W}^{-1}\mathbf{J}^T(\mathbf{J}\mathbf{W}^{-1}\mathbf{J}^T)^{-1}$  可以充当  $\mathbf{J}$  的逆.

Solution: Right Pseudo-Inverse of Jacobian

$$egin{aligned} \mathbf{J}^\dagger &= \mathbf{W}^{-1} \mathbf{J}^T (\mathbf{J} \mathbf{W}^{-1} \mathbf{J}^T)^{-1} \ \mathbf{J}^\dagger &= \mathbf{J}^T (\mathbf{J} \mathbf{J}^T)^{-1}, ext{ when } \mathbf{W} = \mathbf{I} \ \dot{\mathbf{q}} &= \mathbf{J}^\dagger \mathbf{v}_e \end{aligned}$$

same for Analytical Jacobian  $\mathbf{J}_A$  with  $\mathbf{\dot{x}}_e$ 

## **Null space IK**

## Null Space solutions of IK:

if  $\dot{\mathbf{q}}^*$  is a solution, the  $\dot{\mathbf{q}}^* + \mathbf{P}\dot{\mathbf{q}}_0$  is also a solution, where  $\dot{\mathbf{q}}_0$  is a vector of arbitrary joint velocities and P is a projector in the null space of  $\mathbf{J}$ .

• Reconstruct the cost function: and minimize the norm of  $\dot{\bf q}-\dot{\bf q}_0$ , 也就是, 解 $\dot{\bf q}$  要满足<u>???</u> 的同时, 尽可能的靠近 ${\bf q}_0$ 

$$g'(\dot{\mathbf{q}}) = rac{1}{2}(\dot{\mathbf{q}} - \dot{\mathbf{q}}_0)^T(\dot{\mathbf{q}} - \dot{\mathbf{q}}_0) + \lambda^T(\mathbf{v}_e - \mathbf{J}\dot{\mathbf{q}})$$

??? leads to:

$$egin{aligned} \dot{\mathbf{q}} &= \dot{\mathbf{q}}_0 + \mathbf{J}^T \lambda \ \lambda &= (\mathbf{J}\mathbf{J}^T)^{-1}(\mathbf{v}_e - \mathbf{J}\dot{\mathbf{q}}) \ \dot{\mathbf{q}} &= \dot{\mathbf{q}}_0 + \mathbf{J}^T (\mathbf{J}\mathbf{J}^T)^{-1}(\mathbf{v}_e - \mathbf{J}\dot{\mathbf{q}}) = \mathbf{J}^\dagger \mathbf{v}_e + (\mathbf{I} - \mathbf{J}^\dagger \mathbf{J}) \dot{\mathbf{q}}_0 \end{aligned}$$

first term: minimum norm joint velocities second term: Homogeneous solution, the null space projector is  ${f P}={f I}-{f J}^\dagger{f J}$ 

in the case  ${\bf v}_e={\bf 0}$ , it is possible to generate **internal motion** described by  $({\bf I}-{\bf J}^\dagger{\bf J})\dot{\bf q}_0$  that reconfigure the manipulator structure without changing the EEF pose.

## **Null Space control**

## **IK with Kinematic Singularities**

- ${f J}$  does not have full rank.  ${f v}_e-{f J}\dot{{f q}}$  has linearly dependent equations ,  ${f J}$  has linearly dependent rows or columns.
- if **J** is square (not redundant): at singularity or in its neighborhood,

$$\mathbf{J} o ext{singular}, \det(\mathbf{J}) o 0, \mathbf{J}^{-1} o \infty, \Rightarrow \dot{\mathbf{q}} = \mathbf{J}^{-1} \mathbf{v}_e$$

即, small  $\mathbf{v}_e$  leads to large joint velocities.

#### Solution

- 1. SVD: singular value decomposition of Matrix  ${f J}\Rightarrow {f J}^\dagger$  , (在矩阵不满秩的情况下, 计算pseudo inverse)
- 2. DLS: damped least-squares inverse

$$\mathbf{J}^* = \mathbf{J}^T (\mathbf{J} \mathbf{J}^T + k^2 \mathbf{I})^{-1}$$

where k is a damping factor that renders the inversion better conditioned from a numerical point of view. Reconstruct the cost function

$$g''(\dot{\mathbf{q}}) = rac{1}{2}(\mathbf{v}_e - \mathbf{J}\dot{\mathbf{q}})^T(\mathbf{v}_e - \mathbf{J}\dot{\mathbf{q}}) + rac{1}{2}k^2\dot{\mathbf{q}}^T\dot{\mathbf{q}}^T$$

where the first term allows a finite inversion error to be tolerated, with the advantage of norm-bounded velocities. The factor k establishes the relative weight between the two objectives.

### Multi-task

## With Equal Priority

Stack of Jacobian method:

$$\dot{\mathbf{q}} = egin{bmatrix} \mathbf{J}_1 \ dots \ \mathbf{J}_k \end{bmatrix}^\dagger \cdot egin{bmatrix} \mathbf{v}_1 \ dots \ \mathbf{v}_k \end{bmatrix} = ar{\mathbf{J}} \cdot ar{\mathbf{w}}$$

In case the row-rank of the stacked Jacobian matrix  ${f J}$  is larger than the column rank,the tasks are only fulfilled in a least square optimal sense  $\|{f ar w}-{f J}{\dot {f q}}\|_2$ .

we can use weighted pseudo-inv to weight each tasks. then we have  $\|\mathbf{W}^{\frac{1}{2}}(\bar{\mathbf{w}}-\bar{\mathbf{J}}\dot{\mathbf{q}})\|_2$ . Since  $\mathbf{W}$  is diagonal, the Cholesky factor  $\frac{1}{2}$  corresponds to element-wise square root.

#### With Prioritization

we use consecutive null-space projection. For task with decreasing priority  $T_1 > T_2 > \cdots > T_k$ 

task 1

$$\dot{\mathbf{q}} = \mathbf{J}_1^\dagger \mathbf{w}_1 + \mathbf{P}_1 \dot{\mathbf{q}}_0$$

• task 2 must be achieved in the nullspace of task 1 and don't violate the above

$$egin{aligned} \mathbf{w}_2 &= \mathbf{J}_2 \dot{\mathbf{q}} = \mathbf{J}_2 (\mathbf{J}_1^\dagger \mathbf{w}_1 + \mathbf{P}_1 \dot{\mathbf{q}}_0) \ &\Rightarrow \dot{\mathbf{q}}_0 = (\mathbf{J}_2 \mathbf{P}_1)^\dagger (\mathbf{w}_2 - \mathbf{J}_2 \mathbf{J}_1^\dagger \mathbf{w}_1) \ &\Rightarrow \dot{\mathbf{q}} = \mathbf{J}_1^\dagger \mathbf{w}_1 + \mathbf{P}_1 (\mathbf{J}_2 \mathbf{P}_1)^\dagger (\mathbf{w}_2 - \mathbf{J}_2 \mathbf{J}_1^\dagger \mathbf{w}_1) \end{aligned}$$

task n can be written in a recursive way

$$egin{aligned} \dot{\mathbf{q}} &= \sum_{i=1}^k ar{P}_i \dot{\mathbf{q}}_i \ \dot{\mathbf{q}}_i &= (\mathbf{J}_i ar{\mathbf{P}}_i)^\dagger \left( \mathbf{w}_i - \mathbf{J}_i \sum_{j=1}^{i-1} ar{\mathbf{P}}_j \dot{\mathbf{q}}_j 
ight) \ ar{\mathbf{P}}_i &= Nullspace(ar{\mathbf{J}}_i) = Nullspace\left( egin{bmatrix} \mathbf{J}_1^T & \dots & \mathbf{J}_{i-1}^T \end{bmatrix}^T 
ight) \end{aligned}$$

# 6-DOF Manipulator with spherical wrist

- a 6-DOF kinematic structure has closed form IK solutions, IF:
  - three consecutive revolute joint axes intersect at a common point, like the spherical wrist.
  - three consecutive revolute joint axes are parallel
- Articulating the IK problem into 2 subproblems, since solution for position is decoupled from that for orientation:
  - compute the wrist position  $\mathbf{p}_{wrist} = \mathbf{p}_e d_6 \mathbf{a}_e$
  - solve inverse kinematics for  $q_1,q_2,q_3$
  - compute  $\mathbf{R}_{o,3}(q_1,q_2,q_3)$
  - compute  $\mathbf{R}_{3,6}(q_4,q_5,q_6) = ackslash \mathbf{BT}_{o,3} \mathbf{R}_e$
  - solve inverse kinematics for  $q_4,q_5,q_6$

## **Numerical IK**

- $\mathbf{q} \leftarrow \mathbf{q}_0$
- while  $\|\mathbf{x}_d \mathbf{x}(\mathbf{q})\| > \epsilon\|$  do:
  - $\mathbf{J} \leftarrow \mathbf{J}(\mathbf{q}) = rac{\partial \mathbf{x}}{\partial \mathbf{q}}(\mathbf{q})$
  - $ullet \Delta \mathbf{x} \leftarrow \mathbf{x}_d \mathbf{x}(\mathbf{q})$
  - $\mathbf{q} \leftarrow \mathbf{q} + \alpha \mathbf{J}^{\dagger} \Delta \mathbf{x}$
- end while

Note that:  $0 < \alpha < 1$  is the step size to cope with the divergence problem when the error  $\Delta \mathbf{x}$  is very big. However, small  $\alpha$  could lead to slow convergence.

Another problem is when the target is close to the singularity, the Jacobian inversion is ill-conditioned. One could use damped solution. Another approach is to use Jacobian transpose instead of inverse  $\mathbf{q} \leftarrow \mathbf{q} + \alpha \mathbf{J}^T \Delta \mathbf{x}$  and choose  $\alpha$  small enogh.

# **Statics**

manipulator at equilibrium configuration, the relationship between

- the generalized forces  $\pmb{\gamma}_e$  applied to EEF [Forces/Moments] and
- the generalized forces au applied to the joints, [Torques]

### principle of virtual work:

elementary work by joint torques τ:

$$dW_{oldsymbol{ au}} = oldsymbol{ au}^T d\mathbf{q}$$

- EEF forces  $oldsymbol{\gamma}_e$ , with force contribution  $\mathbf{f}_e$  and moment contribution  $\mu_e$ :

$$dW_{oldsymbol{\gamma}_e} = (\mathbf{f}_e^T d\mathbf{p}_e + \mu_e^T \mathbf{w}_e)dt = \mathbf{f}_e^T \mathbf{J}_P(\mathbf{q}) d\mathbf{q} + \mu_e^T \mathbf{J}_O(\mathbf{q}) d\mathbf{q} = oldsymbol{\gamma}_e^T \mathbf{J}(\mathbf{q}) d\mathbf{q}$$

since virtual and elementar displacement coincide, with  $\delta$  the symbol for virtual quantities

$$egin{aligned} \delta W_{oldsymbol{ au}} &= oldsymbol{ au}^T \delta \mathbf{q} \ \delta W_{oldsymbol{\gamma}_e} &= oldsymbol{\gamma}_e^T \mathbf{J}(\mathbf{q}) \delta \mathbf{q} \ \delta W_{oldsymbol{ au}} &= \delta W_{oldsymbol{\gamma}_e} \Rightarrow \ oldsymbol{ au} &= \mathbf{J}^T(\mathbf{q}) oldsymbol{\gamma}_e \end{aligned}$$

Note that: EEF力的数值是表达在World Frame里的

# **Kineto-Statics Duality**

- the range space of  $\mathbf{J}^T$  is the subspace  $\mathscr{R}(\mathbf{J}^{\mathscr{T}})$  in  $\mathbb{R}^n$  of the joint torques that can balance the EEF forces, in the given manipulator posture.
- the **null space** of  $\mathbf{J}^T$  is the subspace  $\mathcal{N}(\mathbf{J}^T)$  in  $\mathbb{R}^{\tau}$  of the EEF forces that do not require any balancing joint torques, in the given manipulator posture.

$$\mathcal{N}(\mathbf{J}) \equiv \mathcal{R}^{\perp}(\mathbf{J}^T), \mathcal{R}(\mathbf{J}) \equiv \mathcal{N}^{\perp}(\mathbf{J}^T)$$

