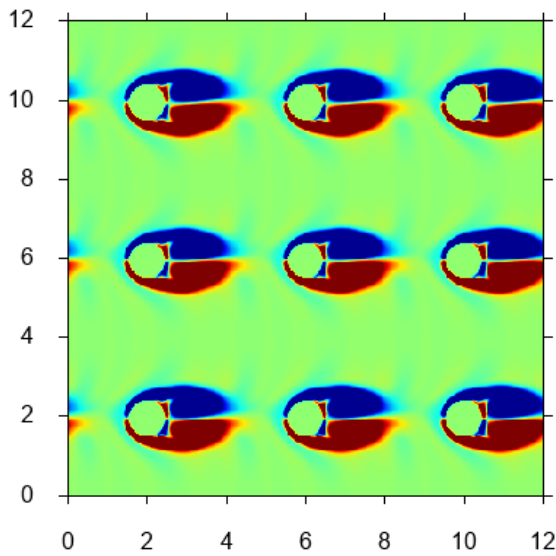
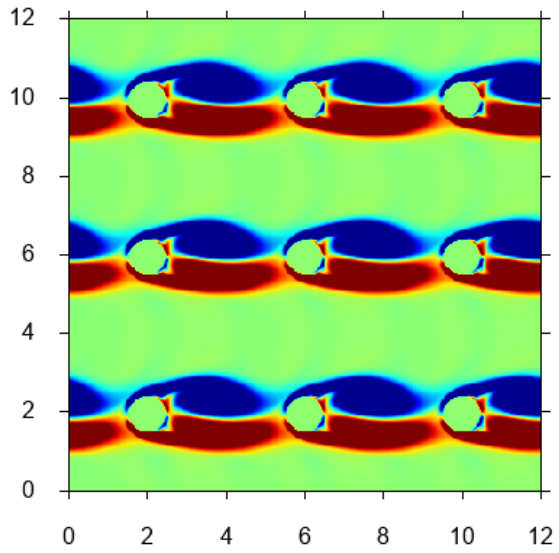
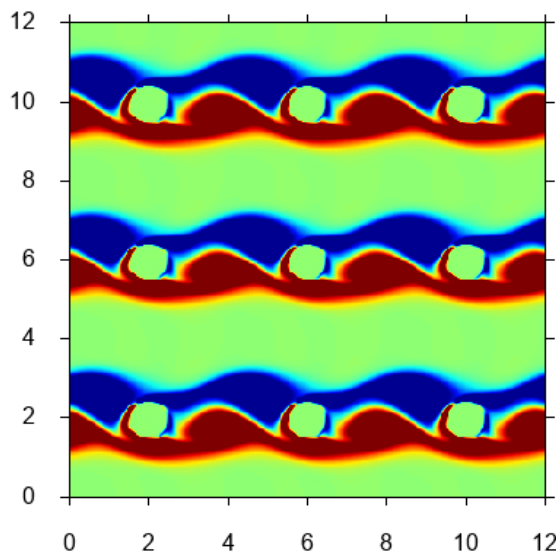
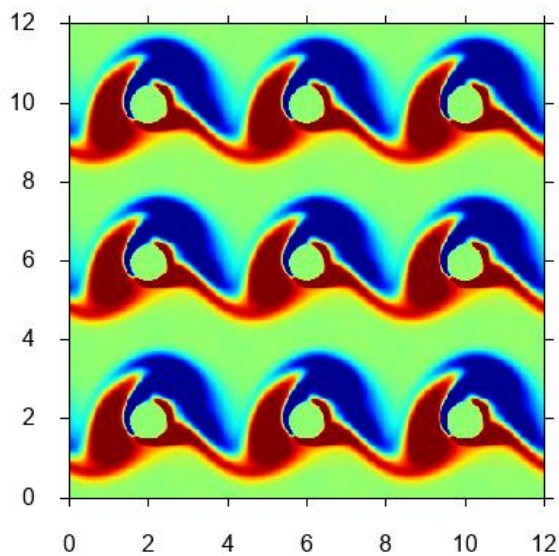


Computing assignment: AEM-ADV19 Computational Fluid Dynamics

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1. The figures below show the simulation result of 2D heat exchanger which was based on circular cylinders using a second-order Adams-Bashforth time scheme with $CFL = 0.25$ and $Re = 0.25$. Different colour represents different vorticity intensity, the green colour implies null vorticity, red and blue colour represent positive and negative vorticity respectively. The area above the cylinder tends to have negative vorticity and the area below tends to have negative vorticity. Since a periodic boundary condition has been imposed on the boundaries, it can be seen from the figures, the vorticity field has a repeating pattern around nine cylinders.

Figure 1. Vorticity field at $nt=2500$.Figure 2. Vorticity field at $nt=5000$.Figure 3. Vorticity field at $nt=7500$.Figure 4. Vorticity field at $nt=10000$.

2. In this question, CFL number was changed from 0.25 to 0.75, as a result, the simulation was not able to run. It gave a non-convergent solution. Simulation failed because of the use of inappropriate CFL number. Increasing the CFL number exceeds the stable limit of CFL condition for the Adams-Bashforth time scheme. When CFL number is 0.75, the scheme became unstable since the domain of dependence of physical solution was not contained in the domain of dependence of numerical scheme. CFL condition is a necessary condition to produce a convergent solution according to Lax Equivalent Theorem.

3. Simulation was run using 3rd Runge-Kutta time scheme with a CFL number equals to 0.75, the results are shown in figures below. By using Runge-Kutta scheme, simulation is able to produce a stable and convergent result with higher CFL number. In RK scheme, the numerical solution updated in one time step, which has three sub-steps, is equivalent to the solution update in three time steps in AB scheme. This is demonstrated by comparing the results from two different schemes, the results in RK scheme at $nt=2500$ is equal to those in AB scheme at $nt=7500$.

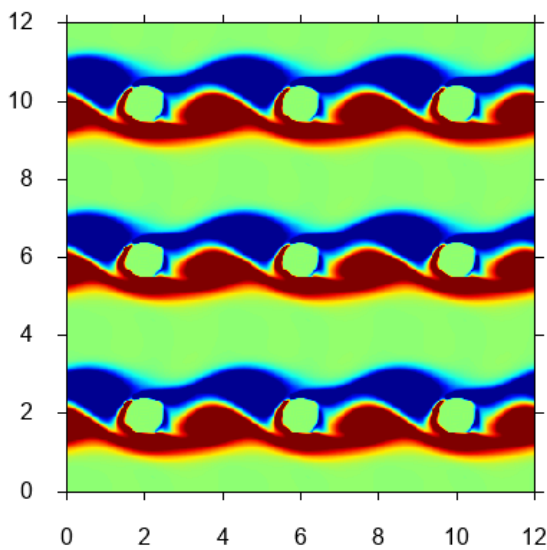


Figure 5. Vorticity filed at $nt=2500$.

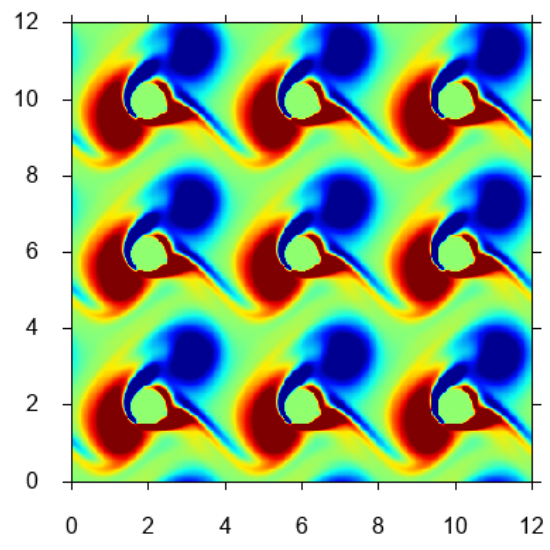


Figure 6. Vorticity filed at $nt=5000$.

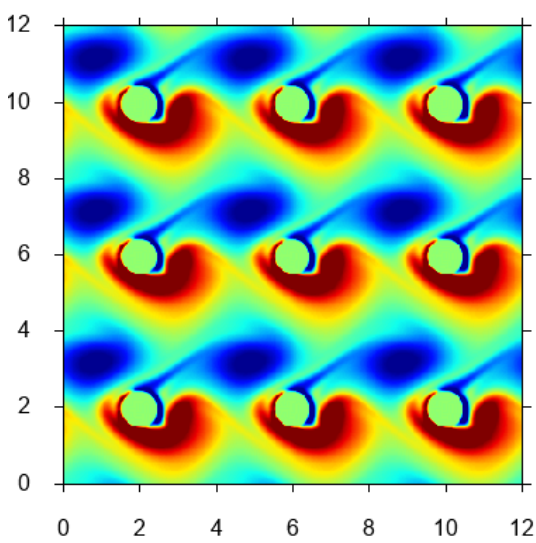


Figure 7. Vorticity filed at $nt=7500$.

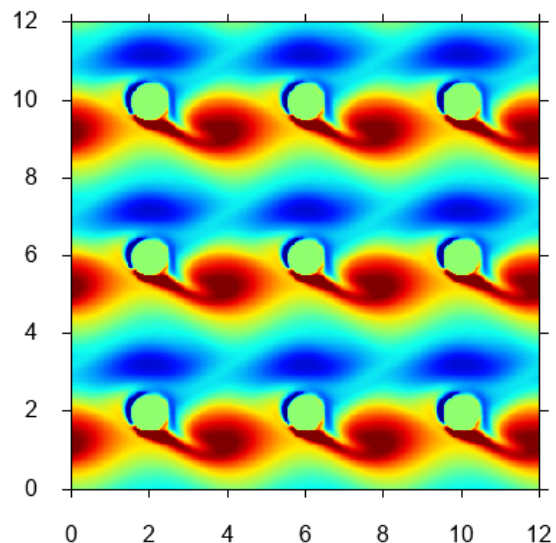


Figure 8. Vorticity filed at $nt=10000$.

```

!#####
!
subroutine rkutta(rho,rou,rov,roe,fro,gro,fru,gru,frv,grv,&
  fre,gre,ftp,gtp,nx,ny,ns,dlt,coef,scp,k)
!
!#####

implicit none
!
real(8),dimension(nx,ny) :: rho,rou,rov,roe,fro,gro,fru,gru,frv
real(8),dimension(nx,ny) :: grv,fre,gre,scp,ftp,gtp
real(8),dimension(2,ns) :: coef
real(8) :: dlt
integer :: i,j,nx,ny,ns,k
!
!coefficient for RK sub-time steps
  coef(1,1)=(8./15.)*(dlt)
  coef(1,2)=(5./12.)*(dlt)
  coef(1,3)=(3./4.)*(dlt)
  coef(2,1)=0.
  coef(2,2)=(-17./60.)*(dlt)
  coef(2,3)=(-5./12.)*(dlt)

  do j=1,ny
    do i=1,nx
      rho(i,j)=rho(i,j)+coef(1,k)*fro(i,j)+coef(2,k)*gro(i,j)
      gro(i,j)=fro(i,j)

      rou(i,j)=rou(i,j)+coef(1,k)*fru(i,j)+coef(2,k)*gru(i,j)
      gru(i,j)=fru(i,j)

      rov(i,j)=rov(i,j)+coef(1,k)*frv(i,j)+coef(2,k)*grv(i,j)
      grv(i,j)=frv(i,j)

      roe(i,j)=roe(i,j)+coef(1,k)*fre(i,j)+coef(2,k)*gre(i,j)
      gre(i,j)=fre(i,j)

      scp(i,j)=scp(i,j)+coef(1,k)*ftp(i,j)+coef(2,k)*gtp(i,j)
      gtp(i,j)=ftp(i,j)
    enddo
  enddo

  return
end subroutine rkutta
!#####

```

4. Fourth-order centred schemes for the first and second order derivatives in two spatial directions were coded in the simulation. The results are shown in the figures below. Higher order derivatives schemes give more accurate results. However, by comparing the results of 4th order scheme with the results of 2nd order scheme, no significant difference was found between them. The main reason for this is that the mesh size was not changed, when changing to higher order schemes, finer mesh should be used in order to unleash the effect of higher order schemes.

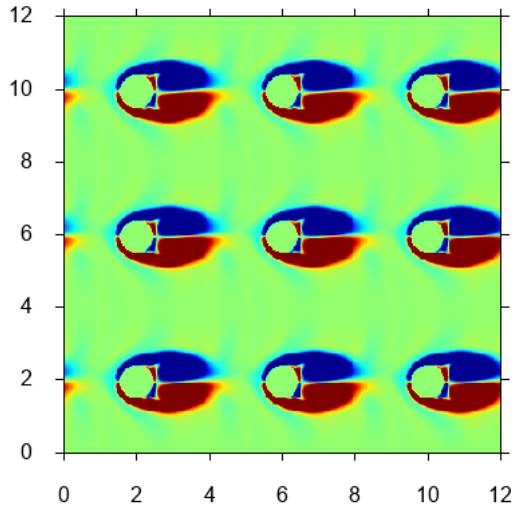


Figure 9. Vorticity field at $nt=2500$ (fourth order).

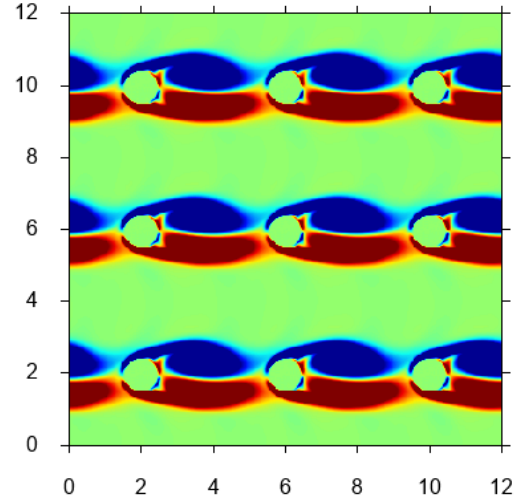


Figure 10. Vorticity field at $nt=5000$ (fourth order).

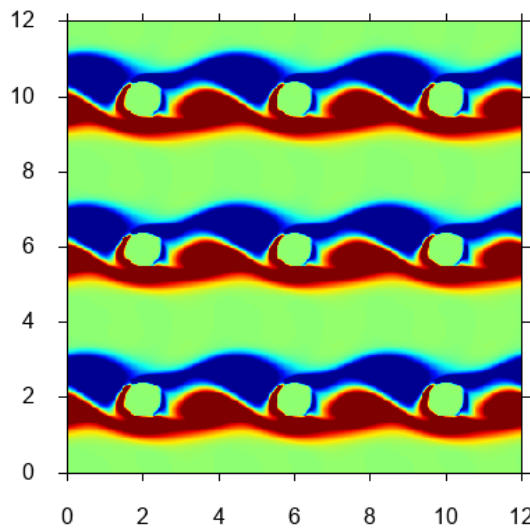


Figure 11. Vorticity field at $nt=7500$ (fourth order).

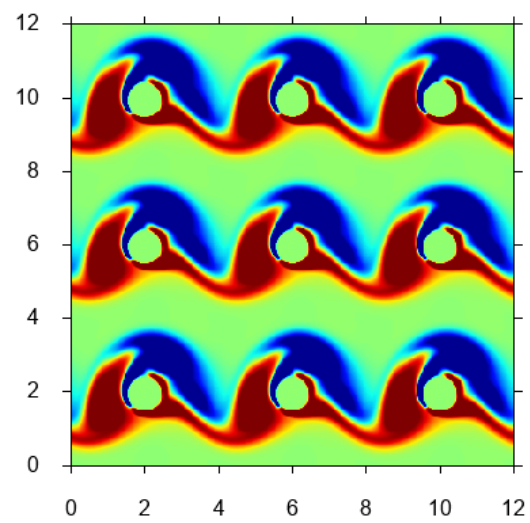


Figure 12. Vorticity field at $nt=10000$ (fourth order).

```

!#####
!
subroutine derix4(phi,nx,ny,dfi,xlx)
!
!Fourth-order first derivative in the x direction
!#####

implicit none

real(8),dimension(nx,ny) :: phi,dfi
real(8) :: dlx,xlx,udx
integer :: i,j,nx,ny

dlx=xlx/nx
udx=1./(12.*dlx)
do j=1,ny
  dfi(1,j)=udx*(-phi(3,j)+8.*phi(2,j)-8.*phi(nx,j)+phi(nx-1,j))
  dfi(2,j)=udx*(-phi(4,j)+8.*phi(3,j)-8.*phi(1,j)+phi(nx,j))
  do i=3,nx-2
    dfi(i,j)=udx*(-phi(i+2,j)+8.*phi(i+1,j)-8.*phi(i-1,j)+phi(i-2,j))
  enddo
  dfi(nx,j)=udx*(-phi(2,j)+8.*phi(1,j)-8.*phi(nx-1,j)+phi(nx-2,j))
  dfi(nx-1,j)=udx*(-phi(1,j)+8.*phi(nx,j)-8.*phi(nx-2,j)+phi(nx-3,j))
enddo

return
end subroutine derix4
!#####

!#####
!
subroutine deriy4(phi,nx,ny,dfi,yly)
!
!Fourth-order first derivative in the y direction
!#####

implicit none

real(8),dimension(nx,ny) :: phi,dfi
real(8) :: dly,yly,udy
integer :: i,j,nx,ny

dly=yly/ny
udy=1./(12.*dly)
do j=3,ny-2
  do i=1,nx
    dfi(i,j)=udy*(-phi(i,j+2)+8.*phi(i,j+1)-8.*phi(i,j-1)+phi(i,j-2))
  enddo
enddo
  do i=1,nx
    dfi(i,1)=udy*(-phi(i,3)+8.*phi(i,2)-8.*phi(i,ny)+phi(i,nx-1))
    dfi(i,2)=udy*(-phi(i,4)+8.*phi(i,3)-8.*phi(i,1)+phi(i,ny))
    dfi(i,ny)=udy*(-phi(i,2)+8.*phi(i,1)-8.*phi(i,ny-1)+phi(i,ny-2))
    dfi(i,ny-1)=udy*(-phi(i,1)+8.*phi(i,ny)-8.*phi(i,ny-2)+phi(i,ny-3))
  enddo

return
end subroutine deriy4

```

```

#####

#####
!
subroutine derxx4(phi,nx,ny,dfi,xlx)
!
!Fourth-order second derivative in y direction
#####

implicit none
real(8),dimension(nx,ny) :: phi,dfi
real(8) :: dlx,xlx,udx
integer :: i,j,nx,ny

dlx=xlx/nx
udx=1./(12.*dlx*dlx)
do j=1,ny
  dfi(1,j)=udx*(-phi(3,j)+16.*phi(2,j)-30.*phi(1,j)+16.*phi(nx,j)-phi(nx-1,j))
  dfi(2,j)=udx*(-phi(4,j)+16.*phi(3,j)-30.*phi(2,j)+16.*phi(1,j)-phi(nx,j))
  do i=3,nx-2
    dfi(i,j)=udx*(-phi(i+2,j)+16.*phi(i+1,j)-30.*phi(i,j)+16.*phi(i-1,j)-phi(i-2,j))
  enddo
  dfi(nx,j)=udx*(-phi(2,j)+16.*phi(1,j)-30.*phi(nx,j)+16.*phi(nx-1,j)-phi(nx-2,j))
  dfi(nx-1,j)=udx*(-phi(1,j)+16.*phi(nx,j)-30.*phi(nx-1,j)+16.*phi(nx-2,j)-phi(nx-3,j))
enddo

return
end subroutine derxx4
#####

#####
!
subroutine deryy4(phi,nx,ny,dfi,yly)
!
!Fourth-order second derivative in the y direction
#####

implicit none
real(8),dimension(nx,ny) :: phi,dfi
real(8) :: dly,yly,udy
integer :: i,j,nx,ny

dly=yly/ny
udy=1./(12.*dly*dly)
do j=3,ny-2
  do i=1,nx
    dfi(i,j)=udy*(-phi(i,j+2)+16.*phi(i,j+1)-30.*phi(i,j)+16.*phi(i,j-1)-phi(i,j-2))
  enddo
enddo
  do i=1,nx
    dfi(i,1)=udy*(-phi(i,3)+16.*phi(i,2)-30.*phi(i,1)+16.*phi(i,ny)-phi(i,nx-1))
    dfi(i,2)=udy*(-phi(i,4)+16.*phi(i,3)-30.*phi(i,2)+16.*phi(i,1)-phi(i,ny))
    dfi(i,ny)=udy*(-phi(i,2)+16.*phi(i,1)-30.*phi(i,ny)+16.*phi(i,ny-1)-phi(i,ny-2))
    dfi(i,ny-1)=udy*(-phi(i,1)+16.*phi(i,ny)-30.*phi(i,ny-1)+16.*phi(i,ny-2)-phi(i,ny-3))
  enddo
return
end subroutine deryy4
#####

```


5. A simulation with the same conditions as those in question 1 has been run for 100000 time-step and visualization of results has been made at each 10000 time-step. As can be observed from the figure 13 to 21, when time-step reached 6000, the vorticity field remains the same. This implies that running the simulation for a very long time will lead to a steady vorticity field. The field becomes independent of the time, in other words, there is no more changes in the vorticity over time.

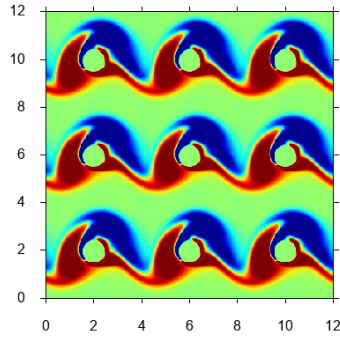


Figure 13. Vorticity at nt= 10000.

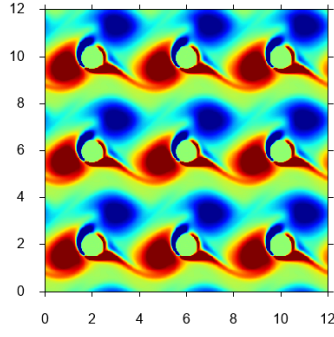


Figure 14. Vorticity at nt= 20000.

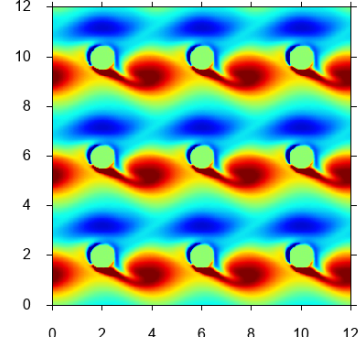


Figure 15. Vorticity at nt= 30000.

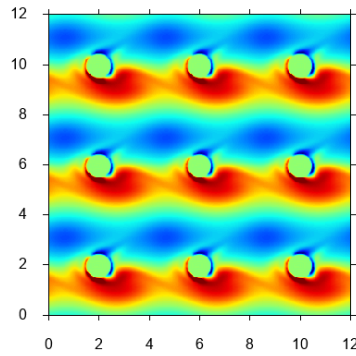


Figure 16. Vorticity at nt= 40000.

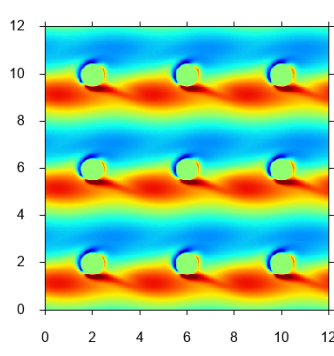


Figure 17. Vorticity at nt= 50000.

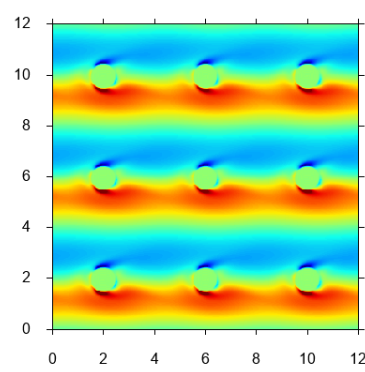


Figure 18. Vorticity at nt= 60000.

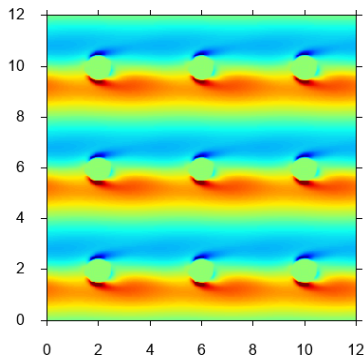


Figure 19. Vorticity at nt= 70000.

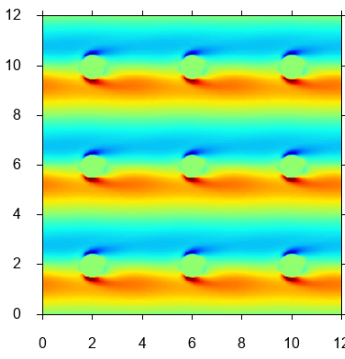


Figure 20. Vorticity at nt= 80000.

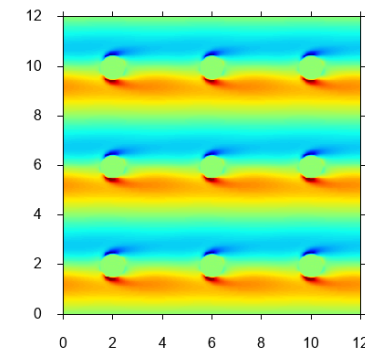


Figure 21. Vorticity at nt= 90000.

6. Code for to simulate a single cylinder.

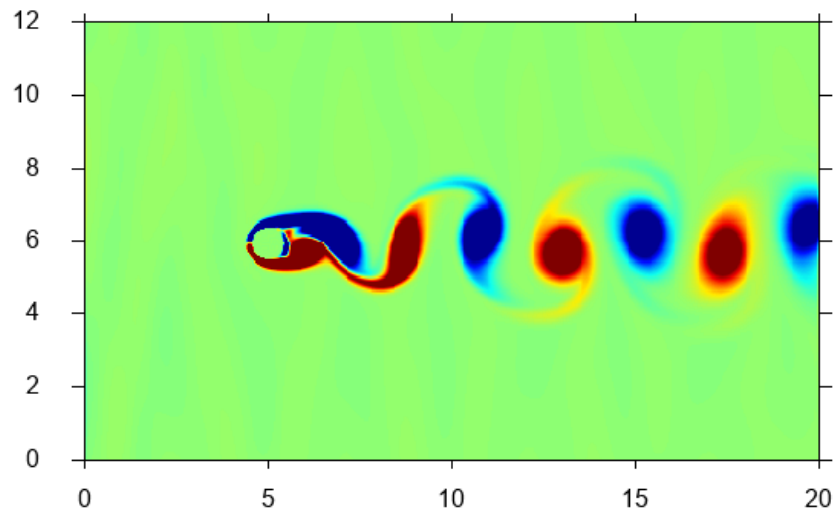


Figure 22: Flow around a single cylinder at $nt = 32500$

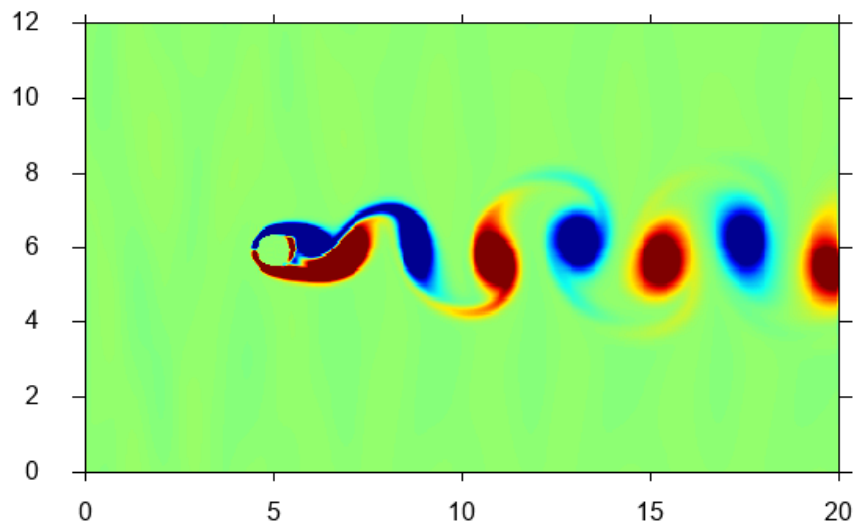


Figure 23: Flow around a single cylinder at $nt = 45000$

```

!#####
!
subroutine boundary(uuu,vvv,rho,eee,rou,rov,roe,nx,ny,&
  xlx,ylx,xmu,xba,gma,chp,dlx,scp,dlt)
!#####
implicit none
real(8),dimension(nx,ny) :: uuu,vvv,rho,eee,rou,rov,roe,scp
real(8) :: xlx,ylx,xmu,xba,gma,chp,roi,cci,d,tpi,chv,uu0
real(8) :: dlt,dlx
integer :: nx,ny,i,j
!#####
call param(xlx,ylx,xmu,xba,gma,chp,roi,cci,d,tpi,chv,uu0)

!inlet boundary condition
do j=1,ny
  rho(1,j)=roi
  rou(1,j)=rho(1,j)*uuu(1,j)
  rov(1,j)=rho(1,j)*vvv(1,j)

```

```

roe(1,j)=rho(1,j)*eee(1,j)
scp(1,j)=1.
enddo
!outlet boundary condition
do j=1,ny
rho(nx,j)=rho(nx,j)-uu0*(dlt/dlx)*(rho(nx,j)-rho(nx-1,j))
rou(nx,j)=rou(nx,j)-uu0*(dlt/dlx)*(rou(nx,j)-rou(nx-1,j))
rov(nx,j)=rov(nx,j)-uu0*(dlt/dlx)*(rov(nx,j)-rov(nx-1,j))
roe(nx,j)=roe(nx,j)-uu0*(dlt/dlx)*(roe(nx,j)-roe(nx-1,j))
scp(nx,j)=scp(nx,j)-uu0*(dlt/dlx)*(scp(nx,j)-scp(nx-1,j))
enddo
return
end subroutine boundary
!#####

!#####
subroutine derix(phi,nx,ny,dfi,xlx)
!First derivative in the x direction
!#####

implicit none
real(8),dimension(nx,ny) :: phi,dfi
real(8) :: dlx,xlx,udx
integer :: i,j,nx,ny
dlx=xlx/nx
udx=1./(dlx+dlx)
do j=1,ny
dfi(1,j)=(1./dlx)*(phi(2,j)-phi(1,j))
do i=2,nx-1
dfi(i,j)=udx*(phi(i+1,j)-phi(i-1,j))
enddo
dfi(nx,j)=(1./dlx)*(phi(nx,j)-phi(nx-1,j))
enddo
return
end subroutine derix
!#####

!#####
subroutine derxx(phi,nx,ny,dfi,xlx)
!Second derivative in y direction
!#####

implicit none
real(8),dimension(nx,ny) :: phi,dfi
real(8) :: dlx,xlx,udx
integer :: i,j,nx,ny
dlx=xlx/nx
udx=1./(dlx*dlx)
do j=1,ny
dfi(1,j)=udx*(phi(3,j)-(phi(2,j)+phi(2,j))+phi(1,j))
do i=2,nx-1
dfi(i,j)=udx*(phi(i+1,j)-(phi(i,j)+phi(i,j))&
+phi(i-1,j))
enddo
dfi(nx,j)=udx*(phi(nx,j)-(phi(nx-1,j)+phi(nx-1,j))+phi(nx-2,j))
enddo

return
end subroutine derxx
!#####

```