XC9128/XC9129 Series

ETR0411-004

1A Driver Transistor Built-In, Step-Up DC/DC Converters

GENERAL DESCRIPTION

The XC9128/XC9129 series are synchronous step-up DC/DC converters with a 0.2Ω (TYP.) N-channel driver transistor and a synchronous 0.2Ω (TYP.) P-channel switching transistor built-in. A highly efficient and stable current can be supplied up to 1.0A by reducing ON resistance of the built-in transistors. With a high switching frequency of 1.2MHz, a small inductor is selectable making the series ideally suited for applications requiring low profile or space saving solutions. With the MODE pin, the series provides mode selection of PWM control or PFM/PWM automatic switching control. In the PWM/PFM automatic switching mode, the series switches from PWM to PFM to reduce switching loss when load current is small. When load current is large, the series switches automatically to the PWM mode so that high efficiency is achievable over a wide range of load conditions. The series also provides small output ripple from light to large loads by using the built-in circuit which enables the smooth transition between PWM and PFM. When a voltage higher than the input voltage is applied to the output during shut-down, the input and the output become isolated making it possible for the IC to work in parallel with the likes of an AC adaptor.

APPLICATIONS

Digital audio equipment

Digital cameras, Video equipment

Computer Mice

Various multi-function power supplies using alkali cells (1 to 3 cells), nickel hydride batteries, or single lithium cells

FEATURES

High Efficiency, Large Current Step-Up Converter

Output Current : 150mA@ V_{OUT} =3.3V, V_{IN} =0.9V

 $500mA@V_{OUT}=3.3V, V_{IN}=1.8V$

Input Voltage Range : 0.8V~6.0V

: 1.8V~5.3V (Externally set) **Output Voltage Setting**

Range Set up freely with a reference voltage

supply of 0.45V (± 0.01V) & external

components

: 1.2MHz (Fixed oscillation frequency Oscillation Frequency

accuracy ±15%)

Input Current : 1.0A

Maximum Current Limit : 1.2A (MIN.), 2.0A (MAX.) Control : PWM, PWM/PFM control externally selectable

:100mV @ V_{OUT}=3.3V,

 V_{IN} =1.8V, I_{OUT} =10mA \rightarrow 100mA Transient Response

Protection Circuits : Thermal shutdown

: Integral latch method (Over current limit)

Soft-Start Time : 5ms (TYP.) internally set

Ceramic Capacitor Compatible Adaptor Enable Function

High Speed

Packages : MSOP-10, USP-10B, SOP-8

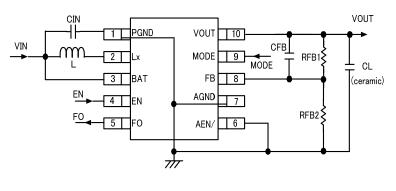
Flag Output (FO) : Open-drain output

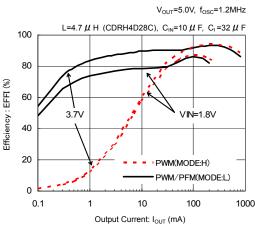
TYPICAL APPLICATION CIRCUIT

TYPICAL PERFORMANCE CHARACTERISTICS

Efficiency vs. Output Current

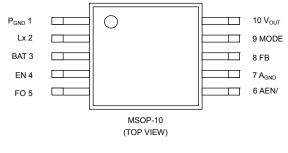
XC9128B45CDx

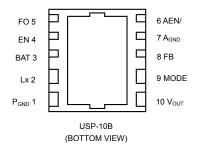


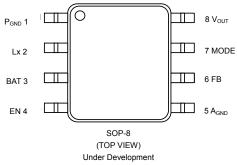


XC9128/XC9129 Series

PIN CONFIGURATION







PIN ASSIGNMENT

PIN NUMBER			DININIAME	FUNCTION			
MSOP-10*	USP-10B *	SOP-8 **	PIN NAME	FUNCTION			
1	1	1	PGND	Power Ground			
2	2	2	Lx	Output of Internal Power Switch			
3	3	3	BAT	Battery Input			
4	4	4	EN	Chip Enable			
5	5	Ī	FO	Flag Output			
6	6	Ī	AEN/	Adaptor Enable			
7	7	5	Agnd	Analog Ground			
8	8	6	FB	Output Voltage Monitor			
9	9	7	MODE	Mode Switch			
10	10	8	Vout	Output Voltage			

^{*} For MSOP-10 and USP-10B packages, please short the GND pins (pins 1 and 7).

^{*}The dissipation pad for the USP-10B package should be solder-plated following the recommended mount pattern and metal masking so as to enhance mounting strength and heat release. If the pad needs to be connected to other pins, it should be connected to the Ground pins (pins 1 and 7).

^{**} For SOP-8 package, please short the GND pins (pins 1 and 5).

FUNCTION CHART

1. EN, AEN/ Pin Function

EN PIN	AEN/ PIN	IC OPERATIONAL STATE	SOFT-START FUNCTION
L→H	L	Operation	Available
Н	H→L	Operation	Not Available
Н	Н	Step-Up Operation Shut-Down	-
L	L	Shut-Down	-
L	Н	Shut-Down	-

^{*} Do not leave the EN and AEN/ Pins open.

2. MODE Pin Function

MODE PIN	FUNCTION
Н	PWM Control
L	PWM/PFM Automatic Switching Control

^{*} Do not leave the MODE Pin open.

PRODUCT CLASSIFICATION

Ordering Information

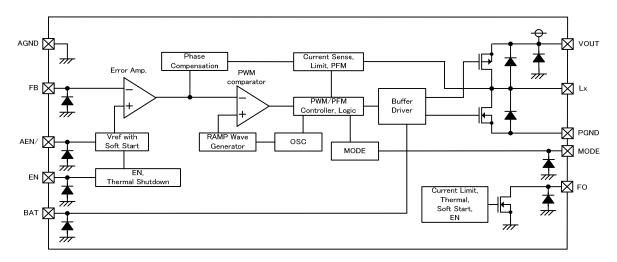
XC9128①②③④⑤⊕···· MSOP-10, USP-10B

XC9129(1)(2)(3)(4)(5)(6)···· SOP-8 (Under Development)

DESIGNATOR	DESCRIPTION	SYMBOL	DESCRIPTION
1	Transistor Built-In, Output Voltage Freely Set (FB voltage),	В	: With integral protection
•	Integral Protection Type	D	: Without integral protection
23	Reference Voltage	45	: Fixed reference voltage 0.45V
	receivance voltage	70	2=4, 3=5
4	Oscillation Frequency	С	: 1.2MHz
		Α	: MSOP-10
(5)	Packages	D	: USP-10B
		S	: SOP-8
6	Device Orientation	R	: Embossed tape, standard feed
	Device Orientation	L	: Embossed tape, reverse feed

BLOCK DIAGRAM

XC9128 Series



XC9129 Series

The AEN/Pin and FO Pin are not connected to the circuit in the block diagram of the XC9129 series.

ABSOLUTE MAXIMUM RATINGS

Ta=25°C

PARAMETER		SYMBOL	RATINGS	UNITS
V _{OUT} Pi	n Voltage	Vout	- 0.3~6.5	V
AEN/ Pi	n Voltage	VAEN/	- 0.3~6.5	V
FO Pin	Voltage	VFO	- 0.3~6.5	V
FO Pin	Current	lfo	10	mA
FB Pin	Voltage	VFB	- 0.3~6.5	V
BAT Pir	n Voltage	VBAT	- 0.3~6.5	V
MODE P	Pin Voltage	VMODE	- 0.3~6.5	V
EN Pin Voltage		VEN	- 0.3~6.5	V
L _X Pin	Voltage	VLx	- 0.3~V _{OUT} +0.3	V
L _X Pin	Current	lLx	2000	mA
	MSOP-10		350 ^(*1)	
Power Dissipation	USP-10B	Pd	150	mW
Tower Bioorpation	SOP-8 (Under Development)	1 0	300	111111
Operating Temperature Range		Topr	- 40 ~ +85	°C
Storage Temperature Range		Tstg	- 55 ∼ +125	°C

^{*1:} When implemented on a PCB.

ELECTRICAL CHARACTERISTICS

XC9128/XC9129 Series Topr=25 °C

PARAMETER	SYMBOL	CONDITIONS	MIN.	TYP.	MAX.	UNITS	CIRCUIT
		CONDITIONS		IIF.			CINCOTT
Input Voltage	Vin	- V _{OUT} =V _{IN} =3.3V, Vpull=3.3V, V _{FO} =0V	-	<u>-</u>	6.0	V	-
FB Voltage	VfB	Voltage to start oscillation during FB=0.46V \rightarrow 0.44V	0.44	0.45	0.46	V	
Output Voltage Setting Range	Voutset	-	1.8	-	5.3	V	
Operation Start Voltage	VST1	Connect to external components, $R_L = 1k\Omega$	-	-	0.8	V	
		Connect to external components, R _L =33Ω	-	-	0.9 (*1)	V	
Oscillation Start Voltage	VsT2	Voltage to start oscillation during V_{IN} =0V \rightarrow 1V	-	0.8	-	V	
Operation Hold Voltage	VHLD	Connect to external components, R _L =1kΩ	-	0.7	-	V	
Supply Current 1	IDD1	$V_{IN} = V_{OUT} = 3.3V$, $FB = V_{FB} \times 0.9$	-	3	6	mA	
Supply Current 2	IDD2	$V_{IN} = V_{OUT} = 3.3V$ FB=V _{FB} ×1.1 (Oscillation stops), MODE=0V	ı	30	80	μΑ	
Input Pin Current	I _{BAT}	V _{IN} =3.3V, V _{OUT} =1.8V, EN=0V	-	2	10	μA	
Stand-by Current	I _{STB}	$V_{IN} = V_{OUT} = 3.3V$, EN=0V	-	2	10	μΑ	
Oscillation Frequency	f _{OSC}	$V_{IN} = V_{OUT} = 3.3V, V_{FO} = 0V, FB = V_{FB} \times 0.9$	1.02	1.20	1.38	MHz	
Maximum Duty Cycle	MAXDTY	$V_{IN} = V_{OUT} = 3.3V, V_{FO} = 0V, FB = V_{FB} \times 0.9$	85	92	96	%	
Minimum Duty Cycle	MINDTY	$V_{IN} = V_{OUT} = 3.3V, V_{FO} = 0V, FB = V_{FB} \times 1.1$	-	-	0	%	
PFM Switching Current	IРFМ	Connect to external components, MODE=0V, I _{OUT} =10mA	1	250	400	mA	
Efficiency (*2)	EFFI	Connect to external components, I _{OUT} =100mA	-	93	-	%	
Lx SW "Pch" ON Resistance	RLxP	$V_{IN}=V_{OUT}+50$ mV, FB=V _{FB} ×1.1, MODE=0V (*3)	-	0.20	0.35 (*1)	Ω	
Lx SW "Nch" ON Resistance	RLxN	V_{IN} =3.3V, V_{OUT} =3.3V,Lx=50mV, FB= V_{FB} ×0.9 (*4)	1	0.20 (*1)	0.35 (*1)	Ω	
Lx Leak Current	ILXL	V _{OUT} =VLx=V _{IN} =3.3V, EN=0V, FB=0V, MODE=0V	-	1	-	μА	
Current Limit (*5)	ILIM	V _{OUT} >2.5V	1.2	1.5	2.0	Α	
Integral Latch Time ^(*6)	TLAT	Time to stop oscillation during RL=33 $\Omega \to 3.3\Omega, V_{FO}$ =L \to H	-	3.5	-	ms	
Soft-Start Time 1	Tss1	Time to start oscillation during V_{EN} =0V \rightarrow V_{IN} at V_{IN} = V_{OUT} =3.3V, V_{FO} =0V, FB = V_{FB} ×0.95	1.7	5.3	10.5	ms	
Soft-Start Time 2	Tss2	$V_{\text{IN}} = V_{\text{OUT}} = 3.3V, V_{\text{F0}} = 0V, \text{FB} \times V_{\text{FB}} \times 0.95$ Time to start oscillation during $V_{\text{AEN}} = V_{\text{IN}} \rightarrow 0V$.	-	0.02	0.04	ms	
Soft-Start Time 3	Tss3	$V_{IN} = V_{OUT} = 3.3V$, $V_{FO} = 0V$, FB< $V_{FB} \times 0.8$ Time to start oscillation during $V_{AEN/} = V_{IN} \rightarrow 0V$	1.7	5.3	10.5	ms	
Thermal Shutdown Temperature	TTSD	-	-	150	-	°C	-
Hysteresis Width	Thys	-	-	20	-	°C	-
Output Voltage Drop Protection (*6)	LVP	V_{IN} =3.3V Voltage to stop oscillation during V_{OUT} =1.56V \rightarrow 1.3V	1.3	1.48	1.56	V	
FO Output Current (*7)	IFO_OUT	V _{IN} =V _{OUT} =3.3V, V _{FO} =0.25V	1.3	1.7	2.2	mA	
FO Leak Current (*7)	IFO_Leak	V _{IN} = V _{OUT} =3.3V, EN=0V ,V _{FO} =1V	-	0	1	μΑ	

ELECTRICAL CHARACTERISTICS (Continued)

●XC9128/XC9129 Series (Continued)

Topr=25 °C

PARAMETER	SYMBOL	CONDITIONS		TYP.	MAX.	UNITS	CIRCUIT
EN "H" Voltage	VENH	V_{IN} =V _{OUT} =3.3V, V _{FO} =0V Voltage to start oscillation during FB=V _{FB} ×0.9, EN= 0.2V \rightarrow 0.65V	0.65	-	-	٧	
EN "L" Voltage VENL		$V_{IN} = V_{OUT} = 3.3V, V_{FO} = 0V$ Voltage to stop oscillation during FB=V _{FB} ×0.9, EN= 0.65V \rightarrow 0.2V		ı	0.2	>	
MODE "H" Voltage	VMODEH	I _{OUT} =10mA, Voltage operates at PWM control	0.65	-	1	V	
MODE "L" Voltage	VMODEL	I _{OUT} =10mA, Voltage operates at PFM control	-	-	0.2	V	
AEN/ Voltage (*7)	VAEN/	V_{IN} = V_{OUT} =3.3V, V_{FO} =0V Voltage to start oscillation during AEN= 0.9V \rightarrow 0.7V	0.7	0.8	0.9	٧	
EN "H" Current	lenh	V _{OUT} =FB=EN=6.0V	-	ı	0.1	μΑ	
EN "L" Current	IENL	V _{OUT} =FB=6.0V, EN=0V	-0.1	1	-	μΑ	
MODE "H" Current	I MODEH	V _{OUT} =FB=MODE=6.0V	-	1	0.1	μΑ	
MODE "L" Current	IMODEL	V _{OUT} =FB=6.0V, MODE=0V	-0.1	ı	ı	μΑ	
AEN/ "H" Current (*7)	IAEN/H	V _{OUT} =FB=AEN/=6.0V	-	1	0.1	μΑ	
AEN/ "L" Current (*7)	IAEN/L	V _{OUT} =6.0V, EN=0V, AEN/=0V	-0.1	-	-	μΑ	
FB "H" Current	ent IFBH V _{OUT} =FB=6.0V		-	ı	0.1	μΑ	
FB "L" Current	IFBL	V _{OUT} =6.0V, FB=0V	-0.1	-	-	μΑ	

Conditions: Unless otherwise stated,

operate at V_{OUT} =3.3V, V_{IN} = 1.8V, EN=3.3V, FB=0V, MODE=3.3V, V_{FO} =3.3V, VpuII=3.3V, AEN/=0V

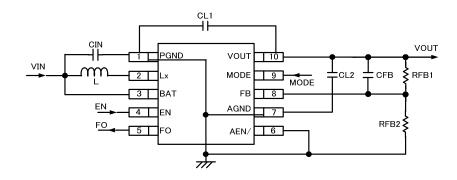
External Components: RFB1=270k Ω , RFB2=43k Ω , CFB=12pF, L=4.7 μ H (LTF5022 TDK)

 C_{L1} =22 μ F(ceramic), C_{L2} =10 μ F(ceramic), C_{IN} =10 μ F(ceramic)

NOTE:

- 1: Designed value
- *2 : Efficiency ={(output voltage) X (output current)} ÷ {(input voltage) X (input current)} X 100
- *3 : L_X SW "P-ch" ON resistance=(V_{Lx}-V_{OUT} pin test voltage) ÷100mA
- $^{*}4$: Testing method of L_X SW "N-ch" ON resistance is stated at test circuits.
- *5 : Current flowing through the Nch driver transistor is limited.
- 6: The XC9128D series does not have integral protection. This is only available with the XC9128B series.
- *7 : The XC9129 series does not have FO or AEN/ pins. These are only available with the XC9128 series.

TYPICAL APPLICATION CIRCUIT



<Output Voltage Setting>

Output voltage can be set by adding external split resistors. Output voltage is determined by the following equation, based on the values of RFB1 and RFB2. The sum of RFB1 and RFB2 should normally be $500k\Omega$ or less. $Vout=0.45 \times (RFB1 + RFB2) / RFB2$

The value of C_{FB} , speed-up capacitor for phase compensation, should be $f_{ZFB} = 1 / (2 \times \pi \times C_{FB1} \times R_{FB1})$ which is in the range of 10 kHz to 50 kHz. Adjustments are depending on application, inductance (L), load capacitance (CL) and dropout voltage.

[Example of calculation]

When RfB1=270k , RfB2=43k ,

 $Vout1 = 0.45 \times (270k+43k) / 43k = 3.276V$

[Typical example]

Vout (V)	(V) RFB1 (k) RFB2 (k)		CfB (pF)
1.8	300	100	10
2.5	270	59	12
3.3	270	43	12
5.0	180	17.8	15

[External Components]

1.2MHz:

L : 4.7 µ H (CDRH4D28C SUMIDA)

CL1: 22 μ F (ceramic) CL2: 10 μ F (ceramic) CIN: 10 μ F (ceramic)

* For CL, use output capacitors of 30 µ F or more. (Ceramic capacitor compatible)

* If using Tantalum or Electrolytic capacitors please be aware that ripple voltage will be higher due to the larger ESR (Equivalent Series Resistance) values of those types of capacitors. Please also note that the IC's operation may become unstable with such capacitors so we recommend that you fully check actual performance.

OPERATIONAL EXPLANATION

The XC9128/XC9129 series consists of a reference voltage source, ramp wave circuit, error amplifier, PWM comparator, phase compensation circuit, N-channel driver transistor, P-channel synchronous rectification switching transistor and current limiter circuit. The series compares, using the error amplifier, the internal reference voltage to the FB pin with the voltage fedback via resistors RFB1 and RFB2. Phase compensation is performed on the resulting error amplifier output, to input a signal to the PWM comparator to determine the turn-on time of the N-ch driver transistor during PWM operation. The PWM comparator compares, in terms of voltage level, the signal from the error amplifier with the ramp wave from the ramp wave circuit, and delivers the resulting output to the buffer driver circuit to cause the Lx pin to output a switching duty cycle. This process is continuously performed to ensure stable output voltage. The current feedback circuit monitors the N-channel driver transistor's turn-on current for each switching operation, and modulates the error amplifier output signal to provide multiple feedback signals. This enables a stable feedback loop even when a low ESR capacitor, such as a ceramic capacitor, is used, ensuring stable output voltage.

<Reference Voltage Source>

The source provides the reference voltage to ensure stable output of the DC/DC converter.

<Ramp Wave Circuit>

The ramp wave circuit determines switching frequency. The frequency is fixed internally at 1.2MHz. The Clock generated is used to produce ramp waveforms needed for PWM operation, and to synchronize all the internal circuits.

<Error Amplifier>

The error amplifier is designed to monitor output voltage. The amplifier compares the reference voltage with the feedback voltage divided by the internal resistors (RFB1 and RFB2). When the FB pin is lower than the reference voltage, output voltage of the error amplifier increases. The gain and frequency characteristics of the error amplifier are optimized internally.

< Maximum Current Limit>

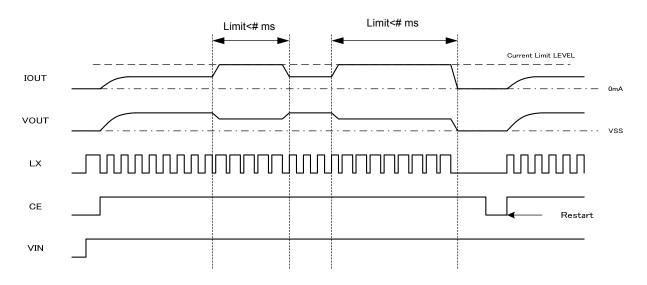
The current limiter circuit monitors the maximum current flowing through the N-ch driver transistor connected to the Lx pin, and features a combination of the current limit and latch function.

- ① When the driver current is greater than a specific level (equivalent to peak coil current), the maximum current limit function starts to operate and the pulses from the Lx pin turn off the N-ch driver transistor at any given time.
- When the driver transistor is turned off, the limiter circuit is then released from the maximum current limit detection state.
- 3At the next pulse, the driver transistor is turned on. However, the transistor is immediately turned off in the case of an over current state.
- ④ When the over current state is eliminated, the IC resumes its normal operation.

The XC9128B/XC9129B series waits for the over current state to end by repeating the steps 1 through 3. If an over current state continues for several ms and the above three steps are repeatedly performed, the IC performs the function of latching the OFF state of the Nch driver transistor, and goes into operation suspension mode. After being put into suspension mode, the IC can resume operation by turning itself off once and then re-starting via the EN pin, or by restoring power to the V IN pin.

The XC9128D/XC9129D series does not have this latch function, so operation steps ① through ③ repeat until the over current state ends.

Integral latch time may be released from a over current detection state because of the noise. Depending on the state of a substrate, it may result in the case where the latch time may become longer or the operation may not be latched. Please locate an input capacitor as close as possible.



OPERATIONAL EXPLANATION (Continued)

<Thermal Shutdown>

For protection against heat damage, the thermal shutdown function monitors chip temperature. When the chip's temperature reaches 150° C (TYP.), the thermal shutdown circuit starts operating and the driver transistor will be turned off. At the same time, the output voltage decreases. When the temperature drops to 130° C (TYP.) after shutting off the current flow, the IC performs the soft start function to initiate output startup operation.

<MODE>

The MODE pin operates in PWM mode by applying a high level voltage and in PFM/PWM automatic switching mode by applying a low level voltage.

<Shut-Down>

The IC enters chip disable state by applying low level voltage to the EN pin. At this time, the P-ch synchronous switching transistor turns on when VIN>VOUT and vise versa the transistor turns off when VIN>VOUT.

<Adaptor Enable>

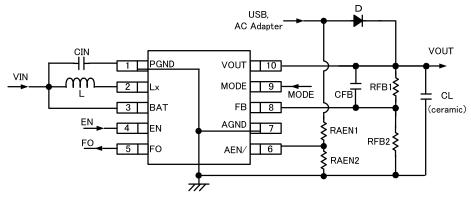
While using step-up DC/DC converters in parallel with an added power source such as AC adaptors, the circuit needs the step-up DC/DC converter to be transient-efficient for sustaining output voltage in case the added power source runs down. The AEN/ pin voltage determines whether the added power source is supplied or not so that high-speed following operation is possible. The IC starts operating although the driver transistor is off when a high level voltage is applied to the AEN/ pin after a high level voltage is also applied to the EN pin. If the AEN/ pin voltage changes from high level to low level while the EN pin sustains a high level voltage, the step-up operation starts with high-speed following mode (without soft-start).

<Error Flag >

The FO pin becomes high impedance during over current state, over temperature state, soft-start period, and shut-down period.

NOTE ON USE

- 1. Please do not exceed the stated absolute maximum ratings values.
- 2. The DC/DC converter / controller IC's performance is greatly influenced by not only the ICs' characteristics, but also by those of the external components. Care must be taken when selecting the external components.
- 3. Make sure that the PCB GND traces are as thick as possible, as variations in ground potential caused by high ground currents at the time of switching may result in instability of the IC.
- 4. Please mount each external component as close to the IC as possible and use thick, short traces to reduce the circuit impedance.
- 5. When the device is used in high step-up ratio, the current limit function may not work during excessive load current. In this case, the maximum duty cycle limits maximum current.
- 6. When the adaptor enable function is used in the below circuit, please use a diode with low reverse bias current. The sum of R_{AEN1}'s and R_{AEN2}'s resistance should be set to manage the reverse bias current.



NOTE ON USE (Continued)

7. P-ch synchronous switching transistor operation

The parasitic diode of the P-ch synchronous transistor is placed between Lx (anode) and V_{OUT} (cathode), so that the power line can not be turned off from Lx to V_{OUT} . On the other hand, the power line switch from V_{OUT} to Lx is shown in the table below.

EN Pin	AEN/Pin	P-ch Synchronous Switch Transistor Operation
Н	Н	OFF
Н	L	Switching
L	Н	OFF
L	L	Undefined

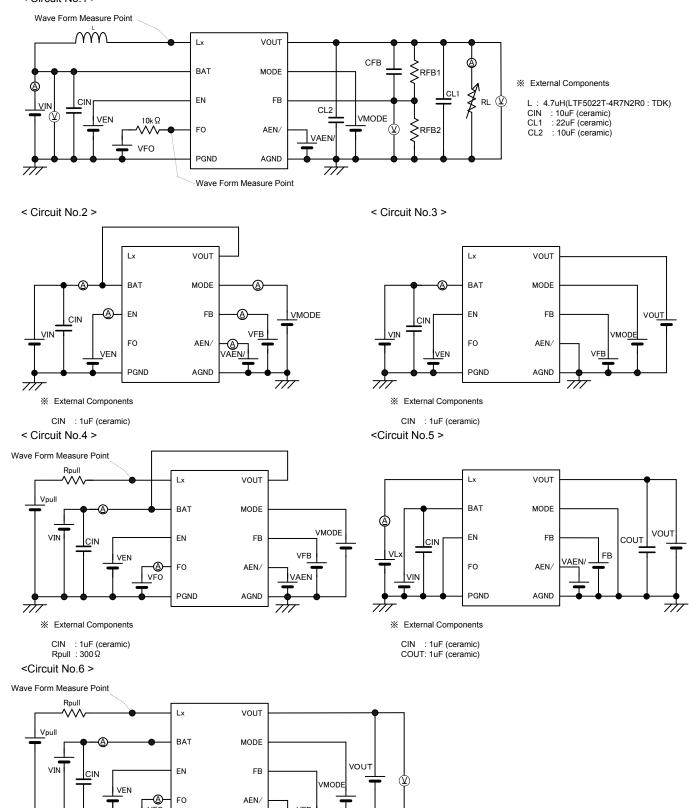
With the XC9128B/XC9129B series, when step-up operation stops as a result of the latch condition working when the maximum current limit level is reached, the synchronous P-ch transistor will remain ON.

With the XC9128B/XC9129B series, when step-up operation stops as a result of the latch condition working when the low output voltage protection level is reached, the synchronous P-ch transistor will remain ON.

- 8. The maximum current limiter controls the limit of the N-ch driver transistor by monitoring current flow. This function does not limit the current flow of the P-ch synchronous transistor.
- 9. The integral latch time of the XC9128B/XC9129B series could be released from the maximum current detection state as a result of board mounting conditions. This may extend integral latch time or the level required for latch operation to function may not be reached. Please connect the output capacitor as close to the IC as possible.
- 10. When used in small step-up ratios, the device may skip pulses during PWM control mode.

TEST CIRCUITS

< Circuit No.1 >



External Components

PGND

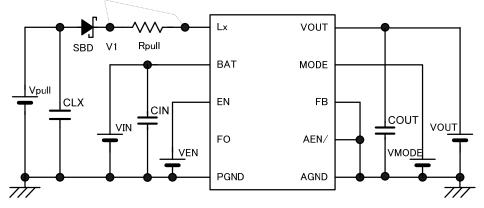
AGND

CIN : 1uF (ceramic) Rpull : $300\,\Omega$

TEST CIRCUITS (Continued)

<Circuit No.7 >

Wave Form Measure Point



※ External Components

CIN : 1uF (ceramic) COUT : 1uF (ceramic) SBD : XBS304S17(TOREX)

Rpull : 0.5Ω

Measurement method for ON resistance of the Lx switch

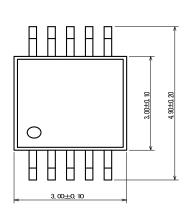
Using the layout of circuit No.7 above, set the LX pin voltage to 50mV by adjusting the Vpull voltage whilst the N-ch driver transistor is turned on. Then, measure the voltage difference between both ends of Rpull. ON Resistance is calculated by using the following formula:

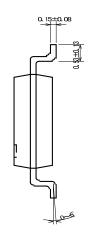
 R_{LXN} =0.05 ÷ ((V1 – 0.05) ÷ 0.5)

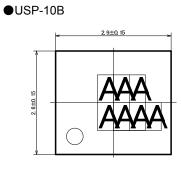
where V1 is a voltage between SBD and Rpull, measured by an oscilloscope.

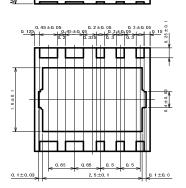
PACKAGING INFORMATION

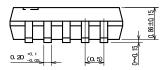
MSOP-10





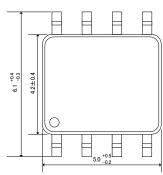


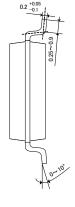


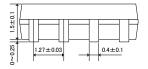


●SOP-8









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