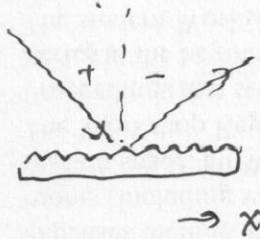


Review.

• grating:

Extra phase by grating: + angular dispersion



$$\phi_{\text{grating}} = -k \cdot x$$

For grating pair, we had



$$\phi''(\omega) = - \frac{4\pi^2 b c}{\cos^3 \chi \cdot d^2 \cdot \omega^3} \quad , \quad \leftarrow \rightarrow$$

always

+ ~~focus~~ imaging elements: such as 4-f system

\Rightarrow normal or abnormal dispersions

* general picture to mode lock.

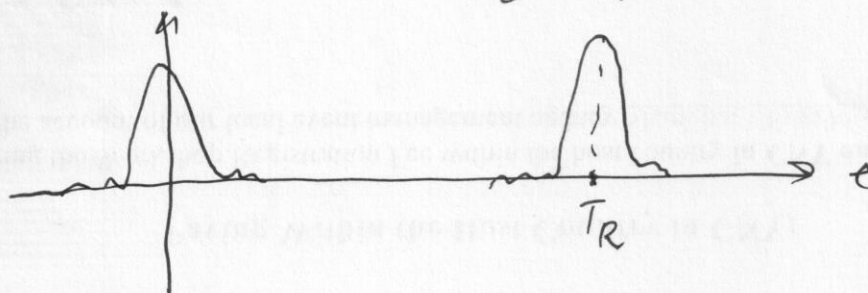
mode locking mechanism: Superposition of multiple

modes

$$\sum_N A_n e^{-j[(\omega_0 + n \cdot \Delta\omega)t - \phi_n]}$$

when ~~same~~ in phase: $\phi_n = 0$

$$A(t) = \frac{\sin(\frac{N}{2} \Delta\omega t)}{\sin(\frac{\Delta\omega}{2} t)}$$



Comments:

①. $A(t) \propto N$

②. $A(t + T_R) = A(t)$

where $T_R = \frac{2\pi}{\Delta\omega}$

③. $\tau \propto \frac{T_R}{N} \Rightarrow \tau \propto \frac{T_R \cdot \Delta\omega}{\delta\omega} = \frac{1}{\Delta f}$

(F.T. transform)

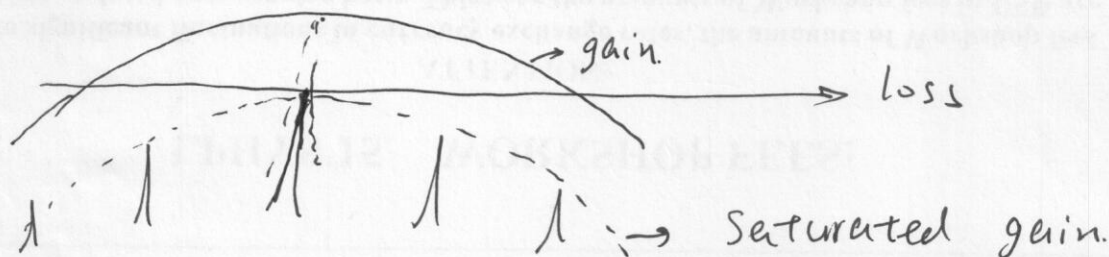
Today:

(how to achieve mode locking.

{ general model for mode locking lasing

mode locking methods: $\left\{ \begin{array}{l} \bullet \text{ Active ML} \\ \bullet \text{ passive ML} \end{array} \right.$

first let's think of why single mode for a conventional CW laser?



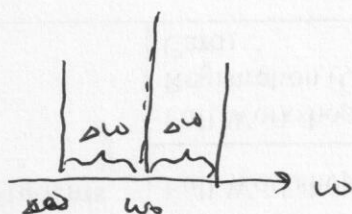
Active mode locking:

modulate ω_0 at $\Delta\omega$ (mode spacing $\sim \text{kHz}$)

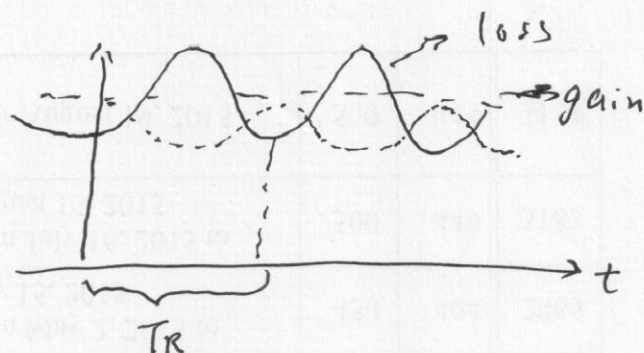
$$\frac{1}{2} A e^{-\gamma_{\text{out}} t} \cos(\omega_m t)$$

$$\alpha_m = \alpha_0 (1 - \cos \omega_m t)$$

Frequency domain:



time domain:



the gain ~~with~~ window is large, why get ML/pulse narrowed?
 assume gain has a Gaussian shape in time

$$e^{-\frac{t^2}{\tau^2}}, \text{ after } n \text{ round trips}$$

$$e^{-\frac{t^2}{(\frac{\tau}{\sqrt{n}})^2}} \rightarrow \text{pulse gets narrowed}$$

i.e. laser shapes the pulse itself, the peak gets amplified more and more.

where n is ~~photon~~ life how many times a photon can travel in the cavity.

$$n \sim \frac{\text{cavity photon life} \rightarrow \text{related to linewidth / a factor} \sim \text{ms}}{\text{round trip time} \sim \text{ns}}$$

$\Rightarrow n$ is a large number

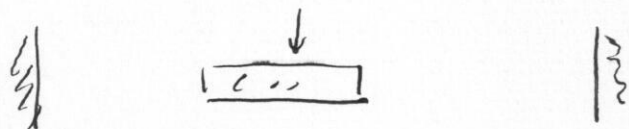
β (ank.

→ passive mode locking
straightforward way:

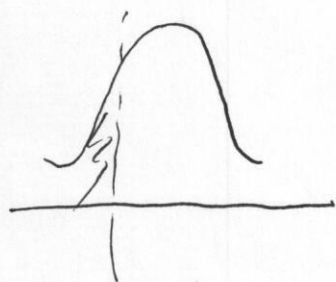
LA8

④
⑤

saturable absorber



but in need of : a fast absorber



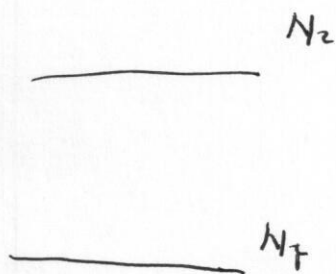
① leading edge saturate the absorber

② trailing edge is benefited by ①

by cutting the edges, a short pulse forms

realization of SA

①



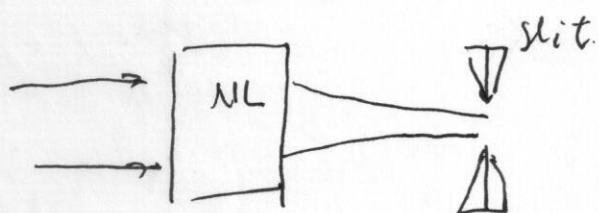
population inversion

$N_2 = N_1 \Rightarrow$ transparent

examples: dye, quantum well

② Nonlinear mechanism.

self focusing



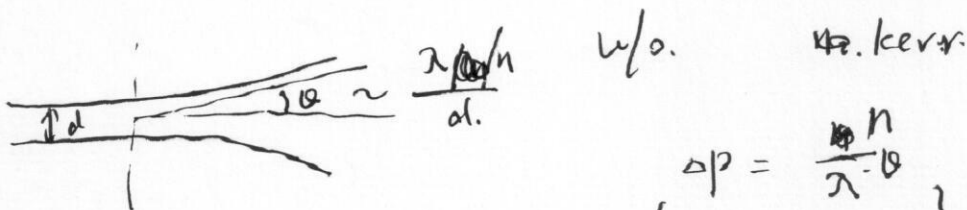
High power \rightarrow go through

low power \rightarrow blocked.

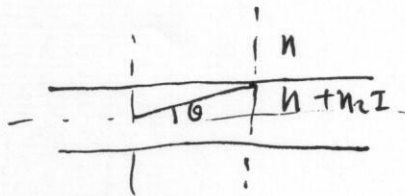
For a specific example: Kerr-lens

a simplified model:

~~4.22 13.4.2016~~ ⑥
L#8 ⑥



$$\left. \begin{aligned} \Delta p &= \frac{n}{\lambda \cdot \theta} \\ \Delta x &= d \end{aligned} \right\} \Rightarrow \Delta p \cdot \Delta x \sim 1$$



Treat as. Total reflection.

$$\cos \theta \cdot (n + n_2 I) = n$$

$$\Rightarrow \frac{1}{\cos \theta} = 1 + \frac{n_2}{n} I$$

a small θ

$$\Rightarrow \frac{1}{1 - \frac{1}{2} \theta^2} \approx 1 + \frac{1}{2} \theta^2 = 1 + \frac{n_2}{n} I$$

$$\Rightarrow I \cdot \frac{n_2}{n} = \frac{1}{2} \frac{\lambda^2}{n^2 d^2}$$

$$\Rightarrow P \approx I \cdot d^2 = \frac{\lambda^2}{2 \pi n_2} \Rightarrow \text{critical power}$$

Comments: 1. only power matters

2. if $P > P_{cr}$. beam will be focused.

Extending thinking:

smaller than diffraction limited spot?

No. other nonlinear effects will also consume the pump power.

An example:

LA8 (7)

$$n_2 : \sim 3 \times 10^{-20} \text{ m}^2/\text{W}$$

$$n=1.5, \quad \lambda \sim 800 \text{ nm}$$

$$\Rightarrow P_{cr} = \frac{\lambda^2}{2\pi n} = \frac{(800 \times 10^{-9})^2}{2\pi \times 3 \times 10^{-20} \cdot 1.5} \\ \sim 10^6 \text{ (W)}$$

$$\text{fs laser: } \frac{1 \text{ nJ}}{100 \text{ fs}} \sim 10^4 \text{ W}$$

actually inside the cavity the power is much stronger.

To solve the above problem precisely,

Let's recall the approach:

For including nonlinearity:

$$k_z = \sqrt{k^2 - k_x^2 - k_y^2} + \underbrace{\frac{2\pi}{\lambda} \cdot n_2 I}_{\text{NL term}}$$

$$k_z = k - \frac{k_x^2 + k_y^2}{2k} + \frac{2\pi}{\lambda} \cdot n_2 I$$

$$k_z - k = - \frac{k_x^2 + k_y^2}{2k} + \frac{2\pi}{\lambda} \cdot n_2 I$$

$$i(k - k_z) \sim \frac{\partial}{\partial z}$$

$$i k_x \sim \frac{\partial}{\partial x}$$

$$i k_y \sim \frac{\partial}{\partial y}$$

$$\Rightarrow -j \frac{\partial}{\partial z} = \frac{1}{2k} \left(\frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} \right) + \frac{2\pi}{\lambda} \cdot n_2 I$$

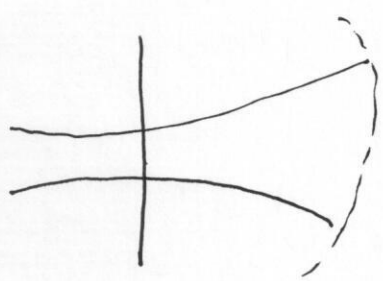
$$-j 2k \frac{\partial}{\partial z} = \nabla_T^2 + \frac{2k^2}{n} n_2 I$$

$$\Rightarrow \nabla_T^2 A + j 2k \frac{\partial A}{\partial z} + \frac{2k^2}{n} n_2 |A|^2 A = 0$$

$$A = A(x, y, z) e^{j k z}$$

$$e^{-j \frac{\pi}{\lambda R} (x^2 + y^2)}$$

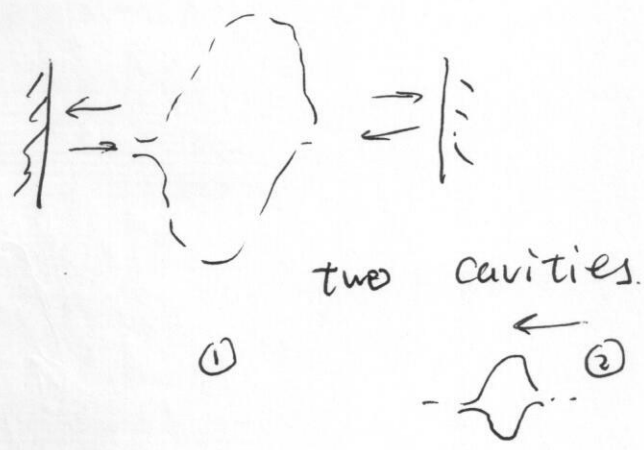
$$e^{-\frac{\pi (x^2 + y^2)}{w_0^2}}$$



kerr. effect: $e^{j \frac{2\pi}{\lambda} \cdot n_2 I} \rightarrow I = I_0 e^{-\frac{\pi (x^2 + y^2)}{w_0^2}}$
 \Downarrow
 $I_0 (1 - \frac{\pi (x^2 + y^2)}{w_0^2})$

3) Another mechanism for passive mode-locking

APM: Additive phase mode lock.



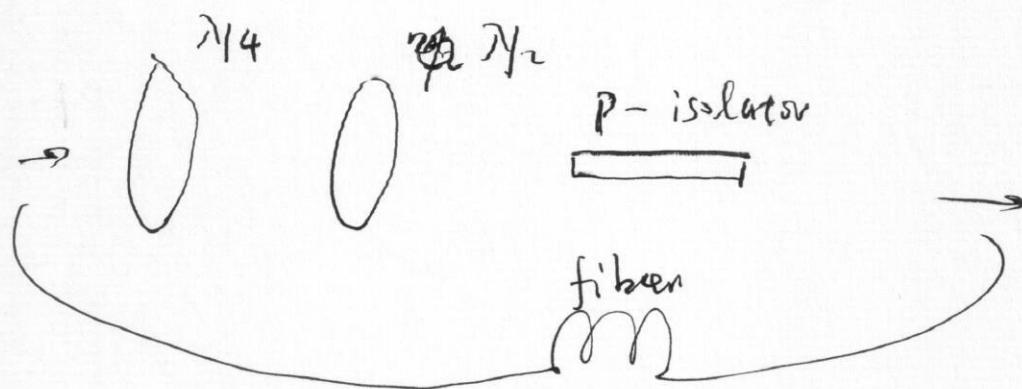
* ② return pulse: center part is in phase w/ pulse in ①, Amplify the center

* wing of returned pulse is out of phase as that of ①.

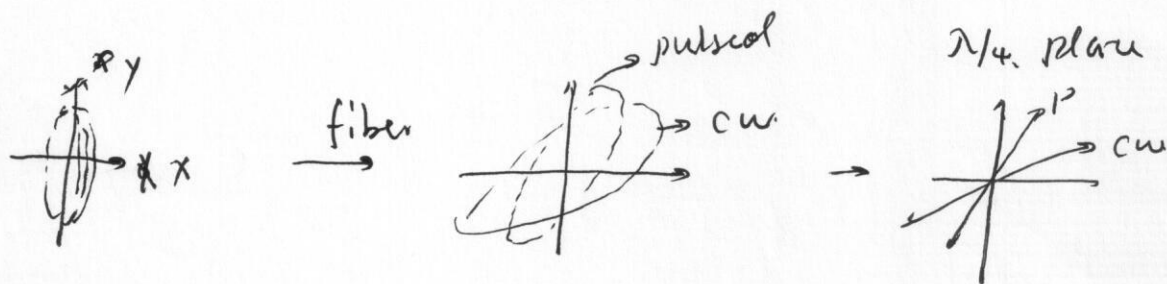
4). Nonlinear polarization Rotation
or (kerr-gating)

L#8

8
9



$$n = n_0 + n_1 I \quad \begin{matrix} x \\ y \end{matrix}$$

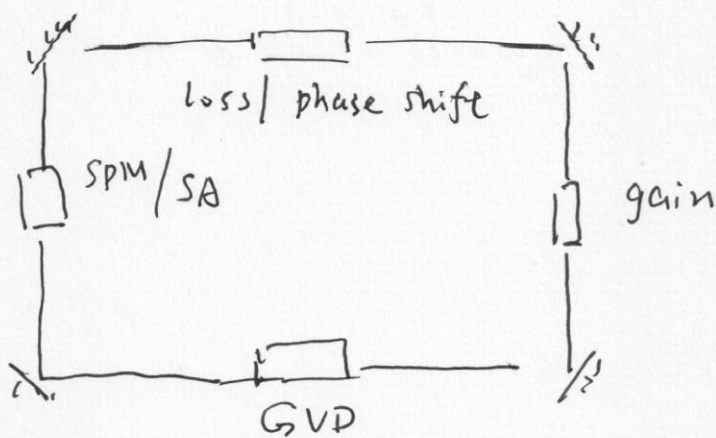


why can obtain fs scale & by using

NIR ?

passive mode locking

General round-trip model



① Loss / phase shift:

$$a(t + T_R) = e^{-(\alpha - j\beta)L} \cdot a(t)$$

↓
envelope

$$= e^{-(1 - jx)} \cdot a(t)$$

$$\approx [1 - (1 - jx)] \cdot a(t)$$

$$\Rightarrow \Delta a(t) = -(1 - jx) a(t)$$

② Gain: $\Delta a = g a$, but we have to consider the bandwidth / profile of the gain

$$g(\omega) = \frac{g_0}{1 + \frac{(\omega - \omega_0)^2}{\Omega_g^2}} \approx g_0 \left[1 - \frac{(\omega - \omega_0)^2}{\Omega_g^2} \right]$$

$\Rightarrow \frac{1}{\Omega_g^2} \frac{d^2}{dt^2}$

in frequency domain: $g(\omega) \cdot \tilde{a}(\omega)$ in time domain: $\Delta a = g \left(1 + \frac{1}{\Omega_g^2} \frac{d^2}{dt^2} \right) \cdot a(t)$

③ GVD: $\Delta a = j D \frac{\partial^2}{\partial t^2}$

where $e^{jk(\omega) \cdot L} = e^{j[k_0 + k' \cdot \Delta\omega + \frac{1}{2} k'' \cdot \Delta\omega^2] \cdot L}$

$$\sim e^{j \frac{1}{2} k'' \cdot \Delta\omega^2 \cdot L} \sim 1 - \frac{1}{2} k'' \cdot \Delta\omega^2 \cdot L$$

$$D \Rightarrow -\frac{1}{2} k'' L$$

④ SPM:

LA8 (11)

$$a'(t) = e^{j\Delta\phi(t)} \cdot a(t)$$

$$\dot{a}(t) = [1 + j\Delta\phi(t)] \cdot a(t)$$

$$\Rightarrow \Delta a(t) = j\delta \cdot |A|^2 \cdot a(t)$$

⑤ SA:

$$\Delta a = r |A|^2 a(t)$$

$$\alpha_{loss} = (\alpha_0 - r |A|^2) \Rightarrow e^{-\alpha_{loss} \cdot t}$$

$$\approx 1 - (\alpha_0 - r |A|^2) \cdot t$$

$$\approx 1 + r |A|^2 \cdot t$$

For steady state: $\sum \Delta a(t) = 0$

$$\left[-\delta(1 - j\kappa) + g \left(1 + \frac{1}{\Omega_y^2} \frac{\partial^2}{\partial t^2} \right) + jD \frac{\partial}{\partial t} \right.$$

$$\left. + j\delta |A|^2 + r |A|^2 \right] a(t) = 0$$