

SLOVAK UNIVERSITY OF TECHNOLOGY IN BRATISLAVA  
FACULTY OF CHEMICAL AND FOOD TECHNOLOGY  
Institute of Information Engineering, Automation, and Mathematics

# Nonlinear Model Predictive Control of Rotary Inverted Pendulum

## MASTER THESIS

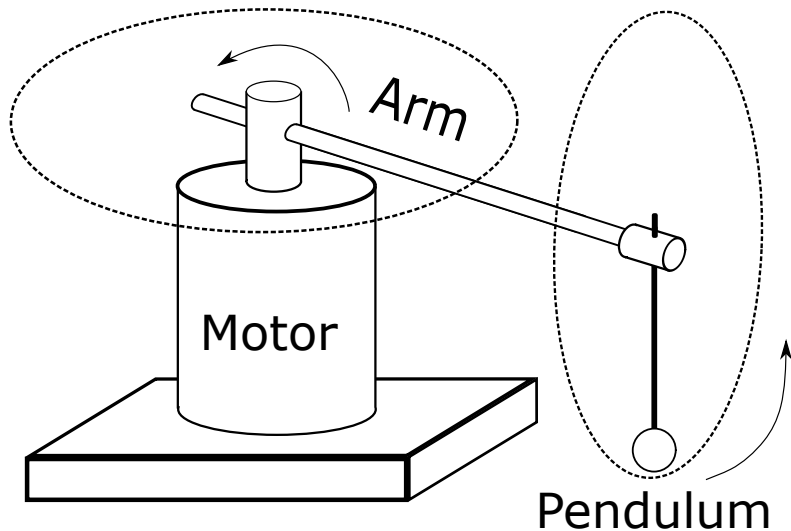
Bc. Alexey Morozov

Supervisor: Ing. Martin Klaučo, PhD.

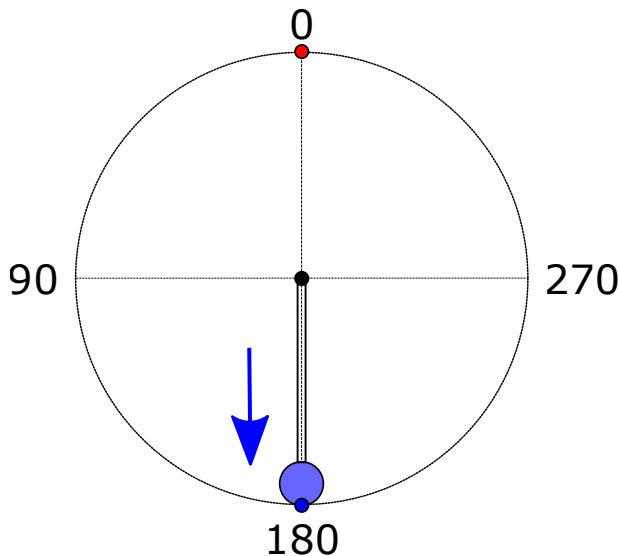
Consultant: Ing. Matúš Furka

June, 2020

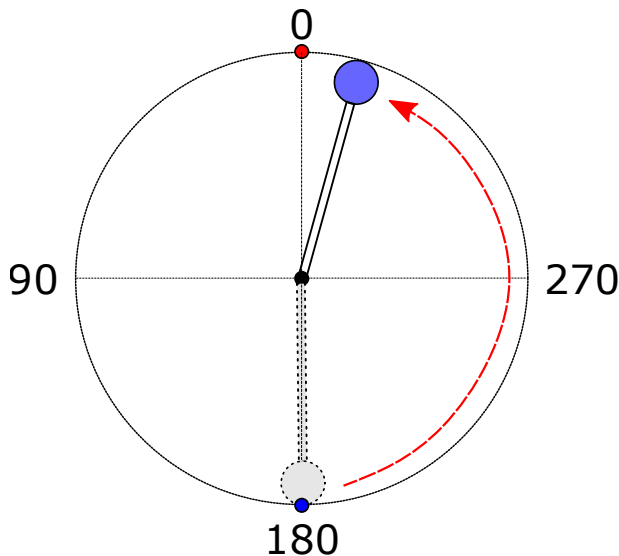
# Furuta Pendulum Device



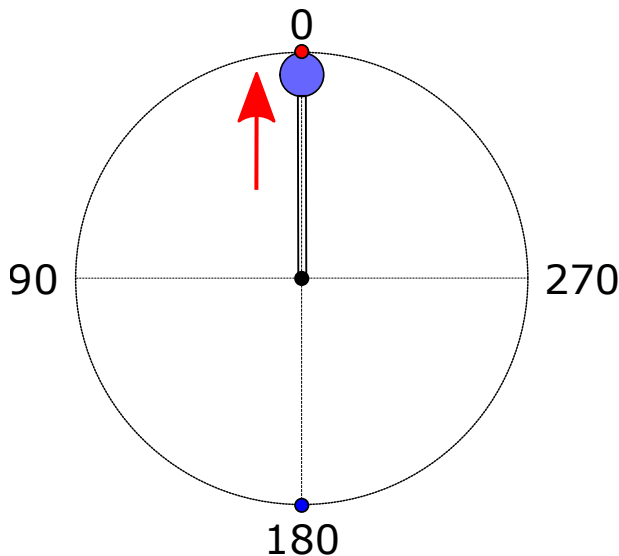
# Swing-Up Control of the Pendulum



# Swing-Up Control of the Pendulum



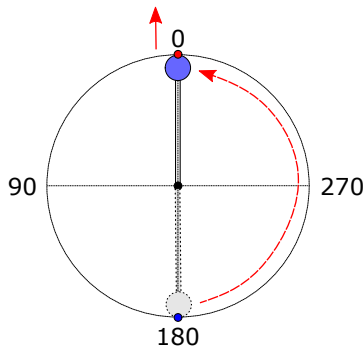
# Swing-Up Control of the Pendulum



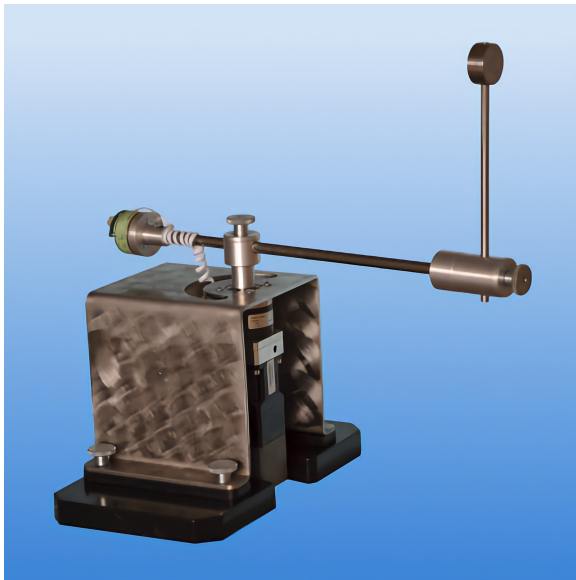
# Swing-Up Control of the Pendulum

Main control strategies

- 1 Heuristic Swing-Up Control strategy
- 2 Optimal Swing-Up Control strategy



# Furuta Pendulum Device



# Derivation of the Mathematical Model

## Lagrangian Formulation

Lagrangian

$$L = E_k - E_p$$

Euler-Lagrange Equations

$$\frac{d}{dt} \left( \frac{\partial L}{\partial \dot{\theta}_0} \right) - \frac{\partial L}{\partial \theta_0} = \tau$$

$$\frac{d}{dt} \left( \frac{\partial L}{\partial \dot{\theta}_1} \right) - \frac{\partial L}{\partial \theta_1} = 0$$



# Derivation of the Mathematical Model

## Lagrangian Formulation

### Equations of motion

$$\ddot{\theta}_0 = \frac{\gamma(\epsilon\dot{\theta}_0^2 + \rho) - \delta(\tau + \beta\dot{\theta}_1^2 - \sigma\dot{\theta}_0\dot{\theta}_1)}{\gamma^2 - \alpha\delta}$$

$$\ddot{\theta}_1 = \frac{\gamma(\tau + \beta\dot{\theta}_1^2 - \sigma\dot{\theta}_0\dot{\theta}_1) - \alpha(\epsilon\dot{\theta}_0^2 + \rho)}{\gamma^2 - \alpha\delta}$$

### Parametres

$$\alpha = l_0 + L_0^2 m_1 + l_1^2 m_1 \sin^2 \theta_1$$

$$\beta = L_0 m_1 l_1 \sin \theta_1$$

$$\gamma = L_0 m_1 l_1 \cos \theta_1$$

$$\delta = l_1 + l_1^2 m_1$$

$$\epsilon = l_1^2 m_1 \sin \theta_1 \cos \theta_1$$

$$\rho = m_1 g l_1 \sin \theta_1$$

$$\sigma = 2l_1^2 m_1 \sin \theta_1 \cos \theta_1$$

# Derivation of the Mathematical Model

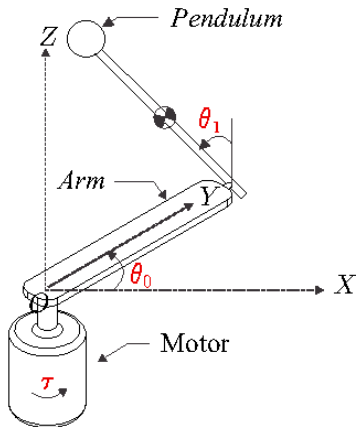
## State-Space Formulation

State variables

$$\begin{bmatrix} x_1(t) \\ x_2(t) \\ x_3(t) \\ x_4(t) \end{bmatrix} = \begin{bmatrix} \theta_0(t) \\ \dot{\theta}_0(t) \\ \theta_1(t) \\ \dot{\theta}_1(t) \end{bmatrix}$$

Control input

$$u(t) = \tau(t)$$



# Derivation of the Mathematical Model

## State-Space Formulation

Non-linear model

$$\begin{bmatrix} \dot{x}_1(t) \\ \dot{x}_2(t) \\ \dot{x}_3(t) \\ \dot{x}_4(t) \end{bmatrix} = \begin{bmatrix} \dot{\theta}_0 \\ \frac{\gamma(\epsilon\dot{\theta}_0^2 + \rho) - \delta(\tau + \beta\dot{\theta}_1^2 - \sigma\dot{\theta}_0\dot{\theta}_1)}{\gamma^2 - \alpha\delta} \\ \dot{\theta}_1 \\ \frac{\gamma(\tau + \beta\dot{\theta}_1^2 - \sigma\dot{\theta}_0\dot{\theta}_1) - \alpha(\epsilon\dot{\theta}_0^2 + \rho)}{\gamma^2 - \alpha\delta} \end{bmatrix}$$

# Derivation of the Mathematical Model

## State-Space Formulation

Linear model

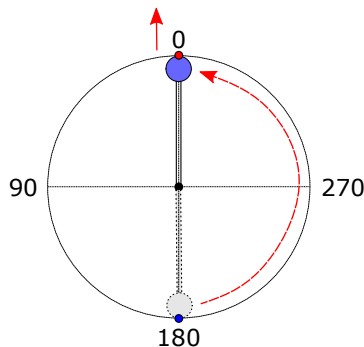
$$A = \begin{bmatrix} 0 & 1 & 0 & 0 \\ 0 & 0 & \frac{-gL_0 l_1^2 m_1^2}{(m_1 L_0^2 + l_0)(m_1 l_1^2 + l_1) - L_0^2 l_1^2 m_1^2} & 0 \\ 0 & 0 & 0 & 1 \\ 0 & 0 & \frac{gl_1 m_1 (m_1 L_0^2 + l_0)}{(m_1 L_0^2 + l_0)(m_1 l_1^2 + l_1) - L_0^2 l_1^2 m_1^2} & 0 \end{bmatrix}$$

$$B = \begin{bmatrix} 0 \\ \frac{m_1 L_1^2 + l_1}{(m_1 L_0^2 + l_0)(m_1 l_1^2 + l_1) - L_0^2 l_1^2 m_1^2} \\ 0 \\ \frac{-L_0 l_1 m_1}{(m_1 L_0^2 + l_0)(m_1 l_1^2 + l_1) - L_0^2 l_1^2 m_1^2} \end{bmatrix}$$

# Swing-Up Control of the Pendulum

## Main control strategies

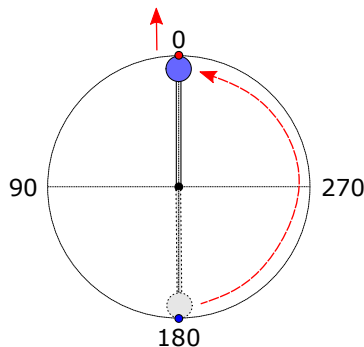
- 1 Heuristic Swing-Up Control strategy
- 2 Optimal Swing-Up Control strategy



# Swing-Up Control of the Pendulum

## Main control strategies

- 1 Heuristic Swing-Up Control strategy
- 2 Optimal Swing-Up Control strategy



# Heuristic Swing-Up Control

Two phases of control:

- 1 Initial excitation of the system  
(by Energy-Shaping controller)
- 2 Stabilisation of the pendulum  
(by Predictive controller)

# Heuristic Swing-Up Control

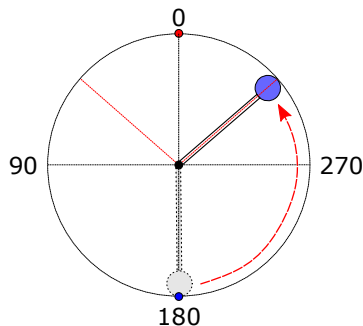
Development of control strategy:

- ① Design of Energy-Shaping controller
- ② Design of Model Predictive controller
- ③ Full-range control of the pendulum



# First Phase of Control

Pendulum is controlled by  
Energy-Shaping controller.



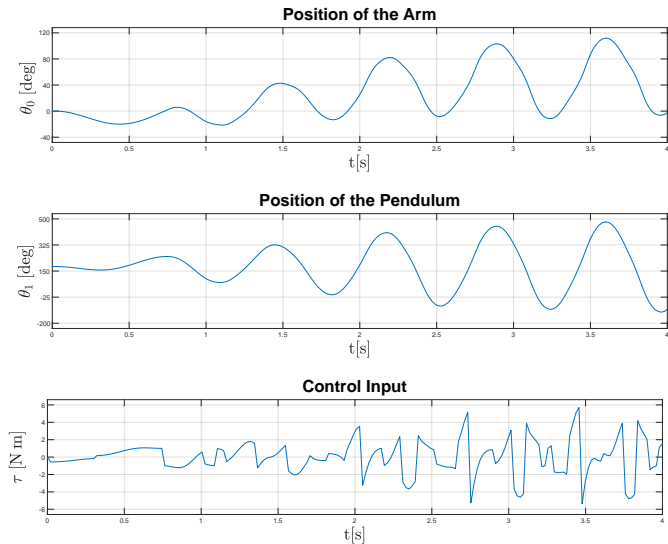
# First Phase of Control

Energy-Shaping controller

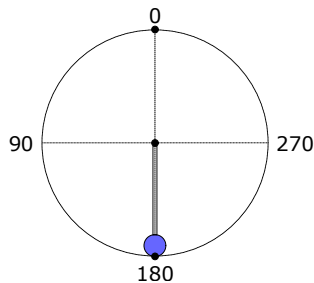
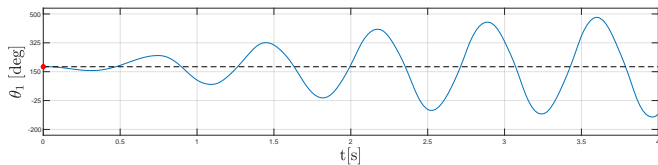
$$E = \frac{m_1 g l_1}{2} \left( \left( \frac{\dot{\theta}_1}{\omega_0} \right)^2 + \cos(\theta_1) - 1 \right)$$

$$u = -4E \operatorname{sign}(\dot{\theta}_1 \cos(\theta_1))$$

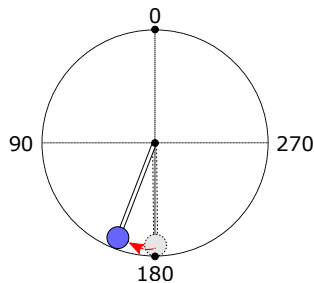
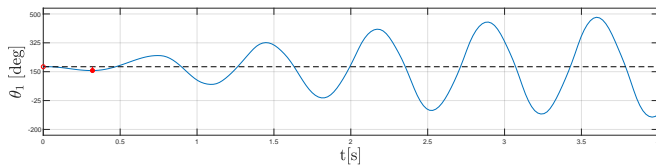
# First Phase of Control



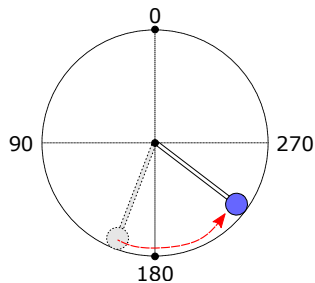
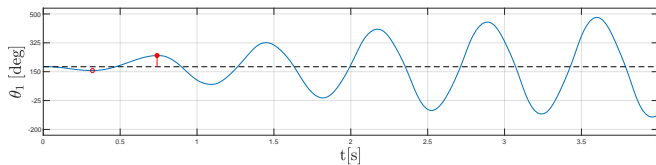
# First Phase of Control



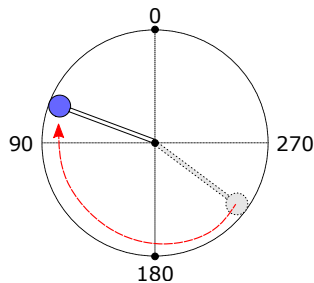
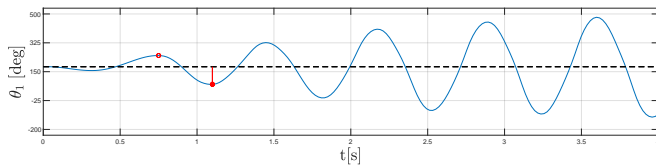
# First Phase of Control



# First Phase of Control

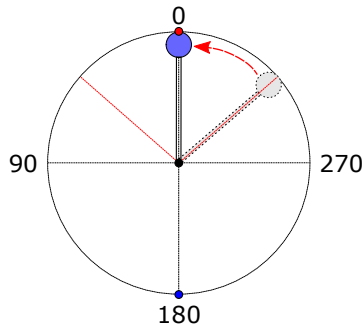


# First Phase of Control



## Second Phase of Control

Pendulum is controlled by  
Predictive controller.





## Second Phase of Control

### Model Predictive Control strategy

$$\begin{aligned}
 \min_{u_0, \dots, u_{N-1}} \quad & \sum_{k=0}^{N-1} (x_k^\top Q_x x_k + u_k^\top Q_u u_k) \\
 \text{s.t.} \quad & x_{k+1} = Ax_k + Bu_k & k \in \mathbb{N}_0^{N-1} \\
 & u_{\min} \leq u_k \leq u_{\max} & k \in \mathbb{N}_0^{N-1} \\
 & x_0 = x(0)
 \end{aligned}$$

Parameter	Symbol	Value
Prediction horizon	$N$	20
Initial condition	$x_0$	$[0 \ 0 \ 28.5 \ -40]^\top$
Constraint on control input-upper bound	$u_{\max}$	10
Constraint on control input-lower bound	$u_{\min}$	-10

## Second Phase of Control

### Model Predictive Control strategy

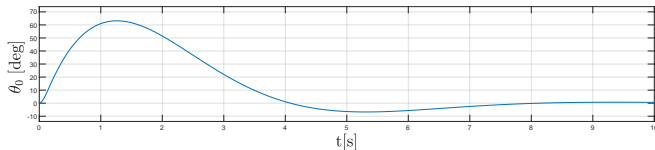
$$\begin{aligned}
 \min_{u_0, \dots, u_{N-1}} \quad & \sum_{k=0}^{N-1} (x_k^T Q_x x_k + u_k^T Q_u u_k) \\
 \text{s.t.} \quad & x_{k+1} = Ax_k + Bu_k & k \in \mathbb{N}_0^{N-1} \\
 & u_{\min} \leq u_k \leq u_{\max} & k \in \mathbb{N}_0^{N-1} \\
 & x_0 = x(0)
 \end{aligned}$$

### Weight matrices

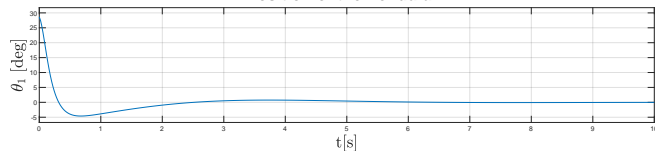
$$Q_x = \begin{bmatrix} 5 & 0 & 0 & 0 \\ 0 & 0.08 & 0 & 0 \\ 0 & 0 & 10 & 0 \\ 0 & 0 & 0 & 0.2 \end{bmatrix} \quad Q_u = 1 \times 10^{-3}$$

# Second Phase of Control

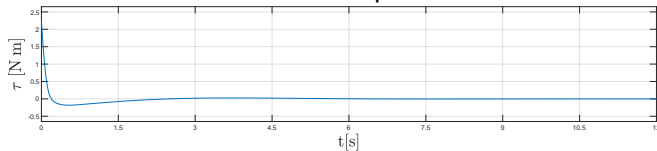
### Position of the Arm



### Position of the Pendulum



### Control Input



# Full-Range Control

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**Algorithm 1** Heuristic Swing-Up Control strategy

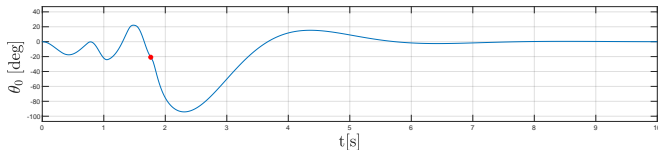
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```
1: procedure HEURISTIC SWING-UP CONTROL
2:    $\theta_1 \leftarrow 180$  deg
3:   Pendulum is controlled by Energy-Shaping controller
4:   if  $\theta_1 \in [-50, 50]$  deg then
5:     Pendulum is controlled by Predictive controller
6:   end if
7: end procedure
```

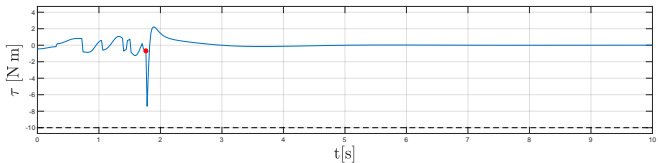
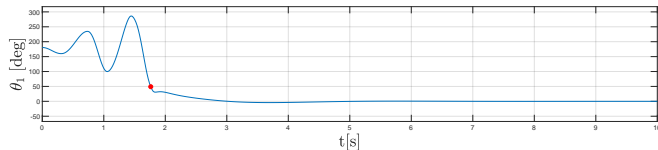
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# Full-Range Control

Position of the Arm



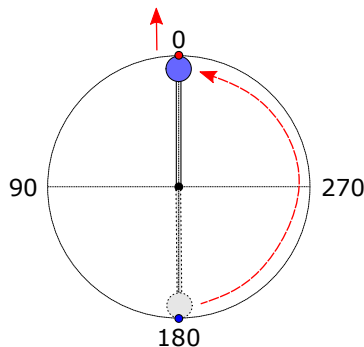
Position of the Pendulum



# Swing-Up Control of the Pendulum

## Main control strategies

- 1 Heuristic Swing-Up Control strategy
- 2 Optimal Swing-Up Control strategy



# Optimal Control Strategy

Two phases of control:

- 1 Initial excitation of the system  
(by Non-linear Predictive controller)
- 2 Stabilisation of the pendulum  
(by Non-linear Predictive controller)

# Non-Linear Model Predictive Control

$$\min_{u_0, \dots, u_{N-1}} \sum_{k=0}^{N-1} (x_k^T Q_x x_k + u_k^T Q_u u_k)$$

$$\text{s.t. } x_{k+1} = f(x_k, u_k)$$

$$k \in \mathbb{N}_0^{N-1}$$

$$u_{\min} \leq u_k \leq u_{\max}$$

$$k \in \mathbb{N}_0^{N-1}$$

$$x_0 = x(0)$$

Parameter	Symbol	Value
Prediction horizon	$N$	20
Initial condition	$x_0$	$[0 \ 0 \ 180 \ 0]^T$
Constraint on control input-upper bound	$u_{\max}$	10
Constraint on control input-lower bound	$u_{\min}$	-10



# Non-Linear Model Predictive Control

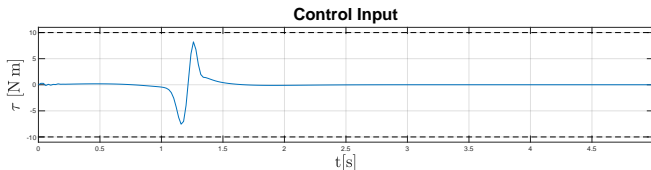
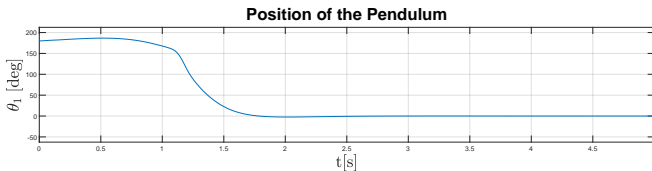
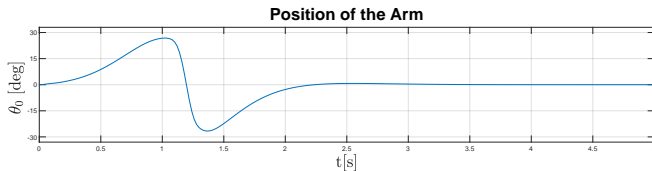
$$\begin{aligned}
 \min_{u_0, \dots, u_{N-1}} \quad & \sum_{k=0}^{N-1} (x_k^\top Q_x x_k + u_k^\top Q_u u_k) \\
 \text{s.t.} \quad & x_{k+1} = f(x_k, u_k) & k \in \mathbb{N}_0^{N-1} \\
 & u_{\min} \leq u_k \leq u_{\max} & k \in \mathbb{N}_0^{N-1} \\
 & x_0 = x(0)
 \end{aligned}$$

Weight matrices

$$Q_x = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 0.1 & 0 & 0 \\ 0 & 0 & 3 & 0 \\ 0 & 0 & 0 & 0.1 \end{bmatrix} \quad Q_u = 0.1$$

# Full-Range Control

## Control of the arm

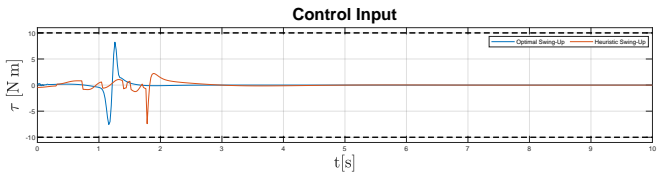
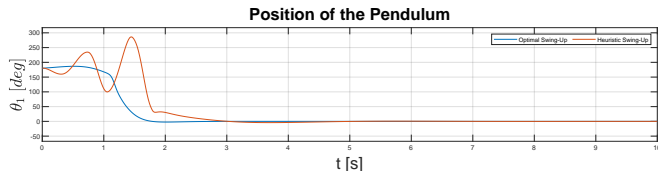
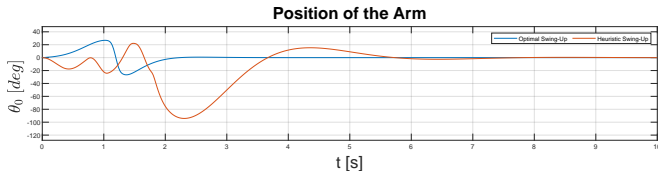


# Discussion About Results

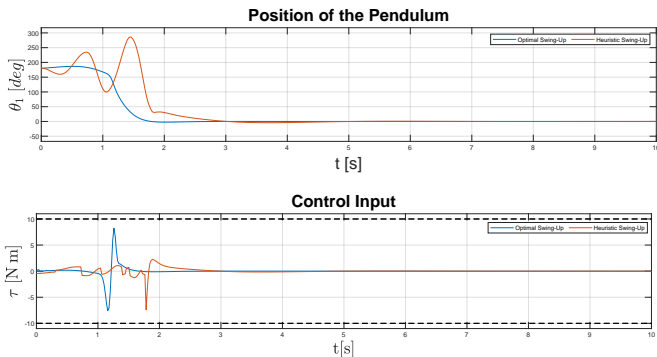
Quality criteria:

- Settling time
- Sum of absolute error (SAE)
- Sum of squared control differences (SSCD)
- Solver solving time

# Discussion About Results

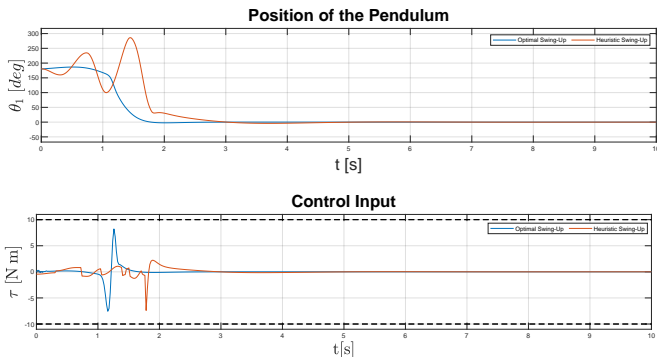


# Discussion About Results



Strategy	Settling Time	SAE	SSCD	Solving Time		
				$t_{\min}$	$t_{\text{avg}}$	$t_{\max}$
Heuristic Swing-Up	7.51	305.15	86.77	0.0156	0.0234	0.0313
Optimal Swing-Up	3.20	205.56	88.94	0.0313	0.0469	0.0625

# Discussion About Results



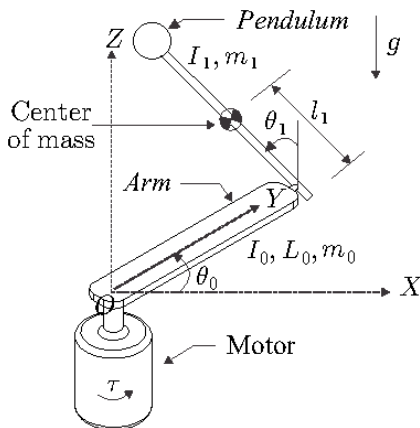
Strategy	Settling Time	SAE	SSCD	Solving Time		
				$t_{\min}$	$t_{\text{avg}}$	$t_{\max}$
Heuristic Swing-Up	100%	100%	100%	100%	100%	100%
Optimal Swing-Up	42.6%	67.4%	103%	201%	200%	200%

# Summary

## Main achievements of the thesis

- Design of Optimal Swing-Up control strategy
- Its comparisson against the heuristic method
- Evaluation of control quality and calculation time of individual approaches

# Parametres of the Pendulum



$g$ -gravitational acceleration [ $\text{ms}^{-2}$ ]

$m_0$ -mass of arm [kg]

$m_1$ -mass of pendulum [kg]

$L_0$ -length of arm [m]

$L_1$ -length of pendulum [m]

$l_0$ -arms center of mass [m]

$l_1$ -pendulums center of mass [m]

$I_0$ -arms moment of inertia [ $\text{kg m}^{-2}$ ]

$I_1$ -pendulums moment of inertia [ $\text{kg m}^{-2}$ ]

$\theta_0$ -arm angle[rad]

$\theta_1$ -pendulum angle [rad]

$\tau$ -motor torque [N m]