IInstitute of Information Engineering, Automation, and Mathematics SLOVAK UNIVERSITY OF TECHNOLOGY IN BRATISLAVA FACULTY OF CHEMICAL AND FOOD TECHNOLOGY

Nonlinear Model Predictive Control of Rotary Inverted Pendulum MASTER THESIS

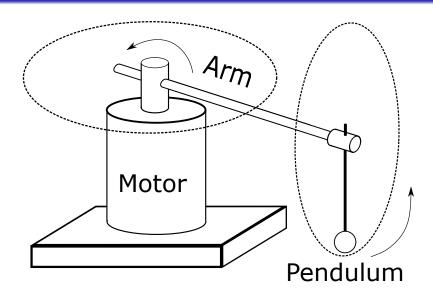
Bc. Alexey Morozov

June, 2020

Supervisor: Ing. Martin Klaučo, PhD.

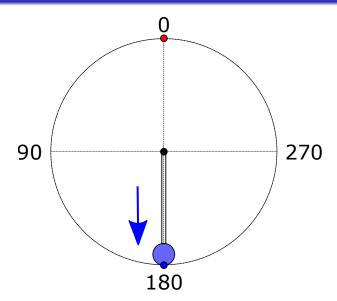
Consultant: Ing. Matúš Furka

Furuta Pendulum Device



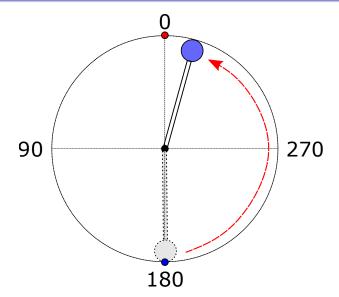
Intro ○●○○○

Swing-Up Control of the Pendulum

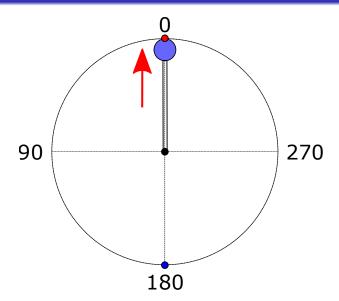


Intro ○○●○○

Swing-Up Control of the Pendulum



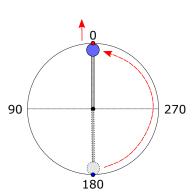
Swing-Up Control of the Pendulum



Swing-Up Control of the Pendulum

Main control strategies

- Heuristic Swing-Up Control strategy
- Optimal Swing-Up Control strategy



Furuta Pendulum Device



Lagrangian Formulation

Lagrangian

$$L = E_{\rm k} - E_{\rm p}$$

Euler-Lagrange Equations

$$\frac{\mathrm{d}}{\mathrm{d}\,t} \left(\frac{\partial L}{\partial \dot{\theta}_0} \right) - \frac{\partial L}{\partial \dot{\theta}_0} = \tau$$

$$\frac{\mathrm{d}}{\mathrm{d}\,t} \left(\frac{\partial L}{\partial \dot{\theta}_1} \right) - \frac{\partial L}{\partial \dot{\theta}_1} = 0$$

Lagrangian Formulation

Equations of motion

$$\ddot{\theta}_{0} = \frac{\gamma(\epsilon\dot{\theta}_{0}^{2} + \rho) - \delta(\tau + \beta\dot{\theta}_{1}^{2} - \sigma\dot{\theta}_{0}\dot{\theta}_{1})}{\gamma^{2} - \alpha\delta}$$
$$\ddot{\theta}_{1} = \frac{\gamma(\tau + \beta\dot{\theta}_{1}^{2} - \sigma\dot{\theta}_{0}\dot{\theta}_{1}) - \alpha(\epsilon\dot{\theta}_{0}^{2} + \rho)}{\gamma^{2} - \alpha\delta}$$

Parametres

$$\alpha = I_0 + L_0^2 m_1 + I_1^2 m_1 \sin^2 \theta_1$$

$$\beta = L_0 m_1 I_1 \sin \theta_1$$

$$\gamma = L_0 m_1 I_1 \cos \theta_1$$

$$\delta = I_1 + I_1^2 m_1$$

$$\epsilon = I_1^2 m_1 \sin \theta_1 \cos \theta_1$$

$$\rho = m_1 g I_1 \sin \theta_1$$

$$\sigma = 2I_1^2 m_1 \sin \theta_1 \cos \theta_1$$

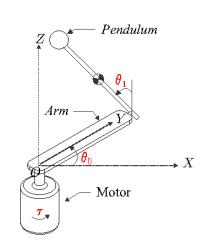
State-Space Formulation

State variables

$$\begin{bmatrix} x_1(t) \\ x_2(t) \\ x_3(t) \\ x_4(t) \end{bmatrix} = \begin{bmatrix} \theta_0(t) \\ \dot{\theta}_0(t) \\ \theta_1(t) \\ \dot{\theta}_1(t) \end{bmatrix}$$

Control input

$$u(t) = \tau(t)$$



Non-linear model

$$\begin{bmatrix} \dot{x}_1(t) \\ \dot{x}_2(t) \\ \dot{x}_3(t) \\ \dot{x}_4(t) \end{bmatrix} = \begin{bmatrix} \dot{\theta}_0 \\ \frac{\gamma(\epsilon\dot{\theta}_0^2 + \rho) - \delta(\tau + \beta\dot{\theta}_1^2 - \sigma\dot{\theta}_0\dot{\theta}_1)}{\gamma^2 - \alpha\delta} \\ \dot{\theta}_1 \\ \frac{\gamma(\tau + \beta\dot{\theta}_1^2 - \sigma\dot{\theta}_0\dot{\theta}_1) - \alpha(\epsilon\dot{\theta}_0^2 + \rho)}{\gamma^2 - \alpha\delta} \end{bmatrix}$$

Linear model

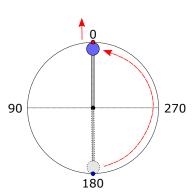
$$A = \begin{bmatrix} 0 & 1 & 0 & 0 \\ 0 & 0 & \frac{-gL_0l_1^2m_1^2}{(m_1L_0^2 + l_0)(m_1l_1^2 + l_1) - L_0^2l_1^2m_1^2} & 0 \\ 0 & 0 & 0 & 1 \\ 0 & 0 & \frac{gl_1m_1(m_1L_0^2 + l_0)}{(m_1L_0^2 + l_0)(m_1l_1^2 + l_1) - L_0^2l_1^2m_1^2} & 0 \end{bmatrix}$$

$$B = \begin{bmatrix} 0 \\ \frac{m_1L_1^2 + l_1}{(m_1L_0^2 + l_0)(m_1l_1^2 + l_1) - L_0^2l_1^2m_1^2} \\ 0 \\ \frac{-L_0l_1m_1}{(m_1L_0^2 + l_0)(m_1l_1^2 + l_1) - L_0^2l_1^2m_1^2} \end{bmatrix}$$

Swing-Up Control of the Pendulum

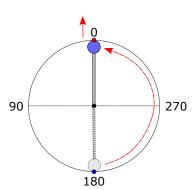
Main control strategies

- Heuristic Swing-Up Control strategy
- Optimal Swing-Up Control strategy



Main control strategies

- Heuristic Swing-Up Control strategy
- Optimal Swing-Up Control strategy



Heuristic Swing-Up Control

Two phases of control:

- Initial excitation of the system (by Energy-Shaping controller)
- Stabilisation of the pendulum (by Predictive controller)

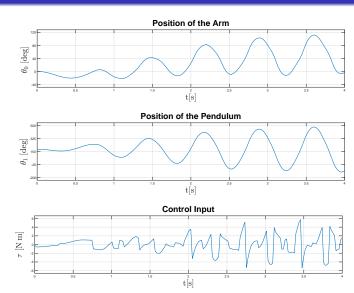
Heuristic Swing-Up Control

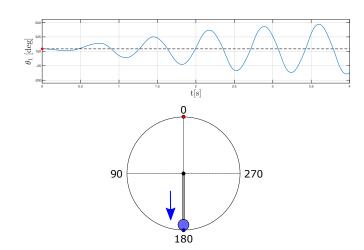
Development of control strategy:

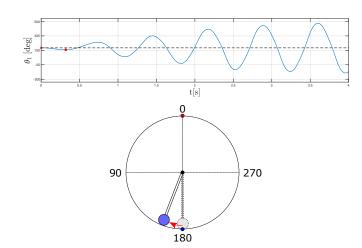
- Design of Energy-Shaping controller
- 2 Design of Model Predictive controller
- 3 Full-range control of the pendulum

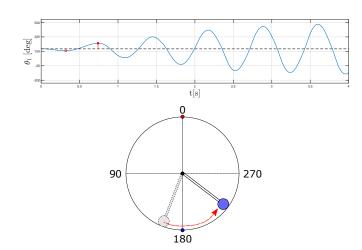
Energy-Shaping controller

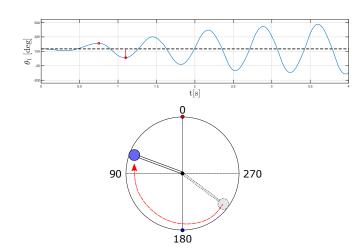
$$E = \frac{m_1 g l_1}{2} \left(\left(\frac{\dot{\theta}_1}{\omega_0} \right)^2 + \cos(\theta_1) - 1 \right)$$
$$u = -4E \operatorname{sign} \left(\dot{\theta}_1 \cos(\theta_1) \right)$$











Stabilisation at the Upright Position

Model Predictive Control strategy

$$\min_{u_0,\dots,u_{N-1}} \sum_{k=0}^{N-1} \left(x_k^\mathsf{T} Q_x x_k + u_k^\mathsf{T} Q_u u_k \right)$$
s.t.
$$x_{k+1} = A x_k + B u_k \qquad k \in \mathbb{N}_0^{N-1}$$

$$u_{\min} \le u_k \le u_{\max} \qquad k \in \mathbb{N}_0^{N-1}$$

$$x_0 = x(0)$$

Parameter	Symbol	Value
Prediction horizon	Ν	20
Initial condition	<i>x</i> ₀	$\begin{bmatrix} 0 & 0 & 28.5 & -40 \end{bmatrix}^{T}$
Constraint on control input-upper bound	u_{max}	10
Constraint on control input-lower bound	u_{\min}	-10

Stabilisation at the Upright Position

Model Predictive Control strategy

$$\min_{u_0,\dots,u_{N-1}} \sum_{k=0}^{N-1} \left(x_k^{\mathsf{T}} Q_{\mathsf{x}} x_k + u_k^{\mathsf{T}} Q_{\mathsf{u}} u_k \right)$$
s.t.
$$x_{k+1} = A x_k + B u_k \qquad \qquad k \in \mathbb{N}_0^{N-1}$$

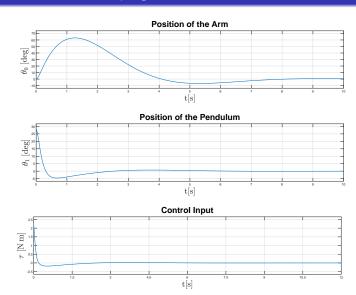
$$u_{\mathsf{min}} \le u_k \le u_{\mathsf{max}} \qquad \qquad k \in \mathbb{N}_0^{N-1}$$

$$x_0 = x(0)$$

Weight matrices

$$Q_{\mathsf{x}} = \begin{bmatrix} 5 & 0 & 0 & 0 \\ 0 & 0.08 & 0 & 0 \\ 0 & 0 & 10 & 0 \\ 0 & 0 & 0 & 0.2 \end{bmatrix} \quad Q_{\mathsf{u}} = 1 \times 10^{-3} \tag{8}$$

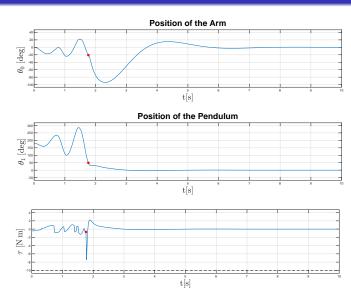
Stabilisation at the Upright Position



Algorithm 1 Heuristic Swing-Up Control strategy

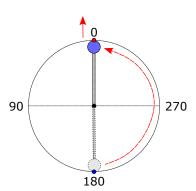
- 1: procedure Heuristic Swing-Up Control
- 2: $\theta_1 \leftarrow 180 \deg$
- 3: Pendulum is controlled by Energy-Shaping controller
- 4: **if** $\theta_1 \in [-50, 50] \text{ deg then}$
- 5: Pendulum is controlled by Predictive controller
- 6: end if
- 7: end procedure

Full-Range Control



Main control strategies

- Heuristic Swing-Up Control strategy
- Optimal Swing-Up Control strategy



Optimal Control Strategy

Two phases of control:

- Initial excitation of the system (by Non-linear Predictive controller)
- Stabilisation of the pendulum (by Non-linear Predictive controller)

Parameter	Symbol	Value
Prediction horizon	Ν	20
Initial condition	<i>x</i> ₀	$[0 \ 0 \ 180 \ 0]^{T}$
Constraint on control input-upper bound	u_{max}	10
Constraint on control input-lower bound	u_{min}	-10

Non-Linerar Model Predictive Control

$$\min_{u_0,\dots,u_{N-1}} \sum_{k=0}^{N-1} (x_k^\mathsf{T} Q_\mathsf{x} x_k + u_k^\mathsf{T} Q_\mathsf{u} u_k)$$

$$\text{s.t. } x_{k+1} = f(x_k, u_k) \qquad \qquad k \in \mathbb{N}_0^{N-1}$$

$$u_{\mathsf{min}} \le u_k \le u_{\mathsf{max}} \qquad \qquad k \in \mathbb{N}_0^{N-1}$$

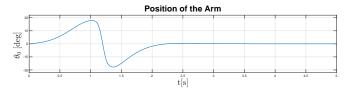
$$x_0 = x(0)$$

Weight matrices

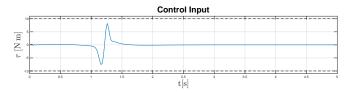
$$Q_{\mathsf{x}} = egin{bmatrix} 1 & 0 & 0 & 0 \ 0 & 0.1 & 0 & 0 \ 0 & 0 & 3 & 0 \ 0 & 0 & 0 & 0.1 \end{bmatrix} \quad Q_{\mathsf{u}} = 0.1$$

Full-Range Control

Control of the arm

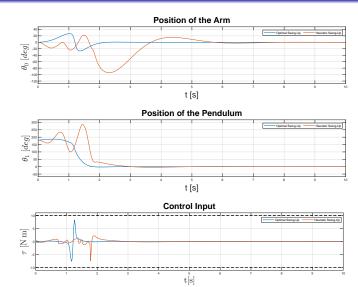


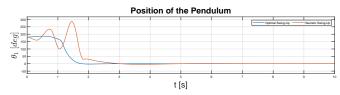


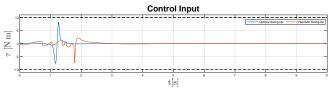


Quality criteria:

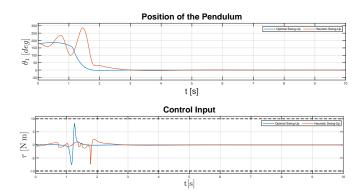
- Settling time
- Sum of absolute error (SAE)
- Sum of squared control differences (SSCD)
- Solver solving time







Strategy Settling Tir	Sottling Time	SAE	SSCD	Solving Time		
	Setting Time			t_{min}	t_{avg}	$t_{\sf max}$
Heuristic Swing-Up	7.51	305.15	86.77	0.0156	0.0234	0.0313
Optimal Swing-Up	3.20	205.56	88.94	0.0313	0.0469	0.0625



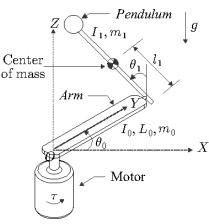
Strategy	Settling Time	SAE	SSCD	Solving Time		
				t_{min}	$t_{\sf avg}$	$t_{\sf max}$
Heuristic Swing-Up	100%	100%	100%	100%	100%	100%
Optimal Swing-Up	42.6%	67.4%	103%	201%	200%	200%

Summary

Main achievements of the thesis

- Design of Optimal Swing-Up control strategy
- Its comparisson against the heuristic method
- Evaluation of control quality and execution time of individual approaches

Parametres of the Pendulum



g-gravitational acceleration [ms $^{-2}$] m_0 -mass of arm [kg] m_1 -mass of pendulum [kg] L_0 -length of arm [m] L_1 -length of pendulum [m] I_0 -arms center of mass [m] I_1 -pendulums center of mass [m] I_0 -arms moment of inertia [kg m⁻²] I_1 -pendulums moment of inertia [kg m⁻²] θ_0 -arm angle[rad] θ_1 -pendulum angle [rad] τ -motor torque [N m]