Frequency domain criteria

Outline

- Frequency response
 - Asymptotic step response
 - Asymptotic sinusoid response
 - Bode curves
- 2 Frequency domain stability criteria
 - Open-loop stability criterion
 - Closed-loop stability criterion

Modeling of a step signal

Unit pulse

$$\delta(k) = \begin{cases} 1 & k = 0 \\ 0 & k \neq 0 \end{cases}$$

Unit step

$$u(k) = \begin{cases} 1 & k \ge 0 \\ 0 & k < 0 \end{cases}$$

Modeled as pulse response

$$u(k) = \frac{1}{1 - q^{-1}} \delta(k)$$

Check!

$$u(k) = u(k-1) + \delta(k)$$

$$u(0) = u(-1) + \delta(0) = 0 + 1 = 1$$

$$u(1) = u(0) + \delta(1) = 1 + 0 = 1$$

$$u(2) = u(1) + \delta(2) = 1 + 0 = 1$$

$$\vdots$$

Unstable, since pole $\lambda=1$

$$u \not\to 0,$$
 $k \to \infty$
 $u(k) = 1,$ $k \ge 0$

Asymptotic step response

Step response for system $G(q^{-1})$

$$y(k) = G(q^{-1}) \frac{1}{1 - q^{-1}} \delta(k) =$$

$$= G(1) \frac{1}{1 - q^{-1}} \delta(k) + \underbrace{[G(q^{-1}) - G(1)] \frac{1}{1 - q^{-1}} \delta(k)}_{\rightarrow 0}$$

Second term stable!

$$y(k) \to G(1), \quad k \to \infty$$

$$G(q^{-1}) = \frac{2q^{-1} - q^{-2}}{1 - 0.9q^{-1}}$$

Verify that $1 - q^{-1}$ factor in

$$G(q^{-1}) - G(1) = \dots = \frac{(1 - q^{-1})(-10 + q^{-1})}{1 - 0.9q^{-1}}$$

$$y(k) = G(q^{-1}) \frac{1}{1 - q^{-1}} \delta(k) =$$

$$= G(1) \frac{1}{1 - q^{-1}} \delta(k) + [G(q^{-1}) - G(1)] \frac{1}{1 - q^{-1}} \delta(k)$$

$$= \underbrace{G(1) \frac{1}{1 - q^{-1}} \delta(k)}_{\rightarrow G(1) = 10} + \underbrace{\frac{-10 + q^{-1}}{1 - 0.9q^{-1}} \delta(k)}_{\rightarrow 0}$$

Modeling of a sinusoid signal

Sinusoid $u(k) = \cos(\omega k + \theta)$ Introduce complex signal

$$u_c(k) = \left\{ egin{array}{ll} \mathrm{e}^{\mathrm{i}(\omega k + heta)} & k \geq 0 \\ 0 & k < 0 \end{array}
ight.$$

Then $u(k) = \Re u_c(k)$ Modeled as pulse response

$$u_c(k) = \frac{\mathrm{e}^{\mathrm{i}\theta}}{1 - \mathrm{e}^{\mathrm{i}\omega}\mathrm{q}^{-1}}\delta(k)$$

Check!

$$\begin{split} u_c(k) &= \mathrm{e}^{\mathrm{i}\omega} u_c(k-1) + \mathrm{e}^{\mathrm{i}\theta} \delta(k) \\ u_c(0) &= \mathrm{e}^{\mathrm{i}\omega} u_c(-1) + \mathrm{e}^{\mathrm{i}\theta} \delta(0) = \mathrm{e}^{\mathrm{i}\theta} \\ u_c(1) &= \mathrm{e}^{\mathrm{i}\omega} u_c(0) + \mathrm{e}^{\mathrm{i}\theta} \delta(1) = \mathrm{e}^{\mathrm{i}(\omega+\theta)} \\ u_c(2) &= \mathrm{e}^{\mathrm{i}\omega} u_c(1) + \mathrm{e}^{\mathrm{i}\theta} \delta(2) = \mathrm{e}^{\mathrm{i}(\omega2+\theta)} \\ \vdots \\ u_c(k) &= \mathrm{e}^{\mathrm{i}(\omega k + \theta)} \end{split}$$

Unstable pole
$$|\lambda|=|\mathrm{e}^{\mathrm{i}\omega}|=1$$

$$u_c \not\to 0, \quad k \to \infty$$

 $u(k) = \Re u_c(k) = \cos(\omega k + \theta), \quad k \ge 0$

Asymptotic sinusoid response

System response to input $u(k) = \Re u_c(k) = \cos(\omega k + \theta)$ Complex response

$$\begin{array}{ll} y_c(k) &= G(\mathbf{q}^{-1})u_c(k) = G(\mathbf{q}^{-1})\frac{\mathrm{e}^{\mathrm{i}\theta}}{1 - \mathrm{e}^{\mathrm{i}\omega}\mathbf{q}^{-1}}\delta(k) = \\ &= G(\mathrm{e}^{-\mathrm{i}\omega})\frac{\mathrm{e}^{\mathrm{i}\theta}}{1 - \mathrm{e}^{\mathrm{i}\omega}\mathbf{q}^{-1}}\delta(k) + \underbrace{\left[G(\mathbf{q}^{-1}) - G(\mathrm{e}^{-\mathrm{i}\omega})\right]\right)\frac{\mathrm{e}^{\mathrm{i}\theta}}{1 - \mathrm{e}^{\mathrm{i}\omega}\mathbf{q}^{-1}}\delta(k)}_{\to 0} \end{array}$$

Real response $y(k) = \Re y_c(k)$

$$y(k) \to \Re G(e^{-i\omega}) \frac{e^{i\theta}}{1 - e^{i\omega}q^{-1}} \delta(k) = |G(e^{-i\omega})| \Re \frac{e^{i(\theta + \arg G(e^{-i\omega}))}}{1 - e^{i\omega}q^{-1}} \delta(k)$$
$$= |G(e^{-i\omega})| \cos(\omega k + \theta + \arg G(e^{-i\omega}))$$

Frequency response function

$$G(e^{-i\omega}) = |G(e^{-i\omega})|e^{i \operatorname{arg} G(e^{-i\omega})}$$

Polar representation can be found experimentally

$$\begin{array}{ccc}
u \longrightarrow G \longrightarrow Y \\
\cos(\omega k) & |G(e^{-i\omega})|\cos(\omega k + \arg(G(e^{-i\omega})))
\end{array}$$

Frequency analysis experiment, for ω_k , $k = 1, 2, \dots, N$

- **①** Choose a sinusoidal input of frequency ω_k
- After transient, measure amplitude and phase shift

Bode curves

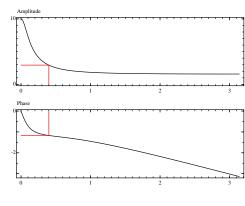
Amplitude: Plot $|G(e^{-i\omega})|$ against ω

Phase: Plot arg $G(e^{-i\omega})$ against ω

Example: Bode curves

$$G(q^{-1}) = \frac{2q^{-1} - q^{-2}}{1 - 0.9q^{-1}}$$

```
B=[0 2 -1];
A=[1 -0.9];
w=0:0.01:pi:
e=exp(-i*w);
Bw=polyval(fliplr(B),e);
Aw=polyval(fliplr(A),e);
Gw=Bw./Aw:
subplot 211
title('Amplitude')
plot(w,abs(Gw));
g04=abs(Gw(41));
plot([0 0.4 0.4],[g04 g04 0],'r');
subplot 212
title('Phase')
plot(w,angle(Gw));
ang04=angle(Gw(41))
plot([0 0.4 0.4],[ang04 ang04 0],'r');
```

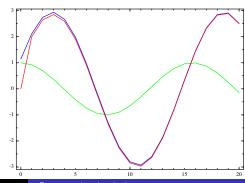


Example: response

```
Response for frequency \omega_1=0.4
Input u(k)=\cos(\omega_1 k)
Output y and asymptotic output y_{\infty}
```

$$y(k)
ightarrow y_{\infty}(k) = |G(\mathrm{e}^{-\mathrm{i}\omega_1})|\cos(\omega_1 k + \mathrm{arg}\ G(\mathrm{e}^{-\mathrm{i}\omega_1}))$$

```
clf;
k=0:20;
u=cos(0.4*k);
yinf=g04*cos(0.4*k+ang04);
y=filter(B,A,u);
plot(k,u,'g');
plot(k,yinf,'b');
plot(k,y,'r');
```



Frequency domain criteria

Low pass

$$G(\mathbf{q}^{-1}) = \frac{0.1\mathbf{q}^{-1}}{1 - 0.9\mathbf{q}^{-1}}$$

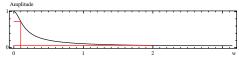
Compare frequencies

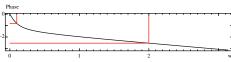
$$\omega_1 \ll \omega_2$$

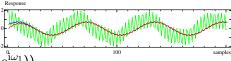
$$u(k) = \cos(\omega_1 k) + \cos(\omega_2 k)$$

Pass of low frequency

$$y(k) \approx |G(e^{i\omega_1})|\cos(\omega_1 k + \arg(G(e^{i\omega_1})))|$$







High pass

$$G({\bf q}^{-1})=0.5(1-{\bf q}^{-1})$$

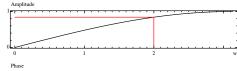
Compare frequencies

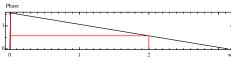
$$\omega_1 << \omega_2$$

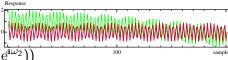
$$u(k) = \cos(\omega_1 k) + \cos(\omega_2 k)$$

Pass of high frequency

$$y(k) \approx |G(e^{i\omega_2})|\cos(\omega_2 k + \arg(G(e^{i\omega_2})))|$$







Root location and change of argument

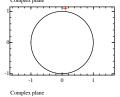
$$A(q^{-1}) = a_0 + a_1 q^{-1} + \ldots + a_n q^{-n} = a_n (q^{-1} - \rho_1) \ldots (q^{-1} - \rho_n)$$

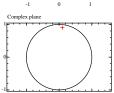
Roots
$$\rho = \frac{1}{\lambda}$$
, $A(\rho) = 0$. Stable pole $|\lambda| < 1 \Rightarrow |\rho| > 1$

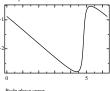
Study total change of argument

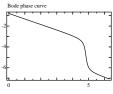
$$arg(e^{-i\omega}-
ho), \quad \omega=0 o 2\pi$$

$$\begin{aligned} |\rho| &> 1 \Rightarrow \Delta_{\mathsf{arg}}(e^{-i\omega} - \rho) = 0 \\ |\rho| &< 1 \Rightarrow \Delta_{\mathsf{arg}}(e^{-i\omega} - \rho) = -2\pi \end{aligned}$$









Stable polynomial

If all poles $|\lambda_k| < 1$ then

$$\Delta_{\mathsf{arg}} \mathcal{A}(\mathrm{e}^{-\mathrm{i}\omega}) = \underbrace{\Delta_{\mathsf{arg}}(\mathrm{e}^{-\mathrm{i}\omega} - \rho_1)}_{=0} + \ldots + \underbrace{\Delta_{\mathsf{arg}}(\mathrm{e}^{-\mathrm{i}\omega} - \rho_n)}_{=0} = 0$$

The modified Mikhaylov criterion

A system with characteristic polynomial $A(q^{-1})$ is stable if and only if the curve $A(e^{-i\omega})$, $\omega=0\to 2\pi$ does not encircle the origin.

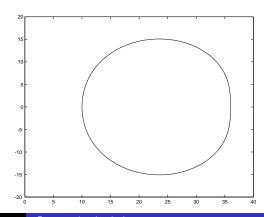
Example

Stable poles?

$$A(q^{-1}) = 24 - 14q^{-1} - q^{-2} + q^{-3}$$

Mikhaylov locus

$$A(\mathrm{e}^{-\mathrm{i}\omega}), \quad \omega = 0 o 2\pi$$



Necessary conditions for stability

Necessary condition $(\omega = 0, \pi)$

$$signA(1) = signA(-1)$$

otherwise origin is enclosed

$$A(q^{-1}) = 1 + \ldots + a_n q^{-n}$$

= $(1 - \lambda_1 q^{-1}) \ldots (1 - \lambda_n q^{-1})$
 $\Rightarrow |a_n| = |\lambda_1 \lambda_2 \ldots \lambda_n|$

Necessary condition

$$|a_n| < 1$$

since $|\lambda_k| < 1, \forall k$

Necessary conditions (easy check!)

$$signA(1) = signA(-1)$$
$$|a_n| < 1$$

Example

$$A(q^{-1}) = 24 - 14q^{-1} - q^{-2} + q^{-3}$$

 $A(1) = 10$
 $A(-1) = 36$
 $A/24 = 1 \dots \frac{1}{24}q^{-3} \Rightarrow a_3 = \frac{1}{24}$

Necessary conditions ok!

Example

$$A(q^{-1}) = 1 - 1.1q^{-1} + 1.16q^{-2} - 0.106q^{-3}$$

Check:

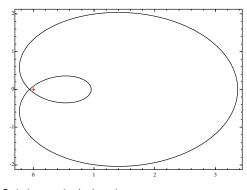
$$A(1) = 0.954$$

 $A(-1) = 3.366$
 $a_3 = -0.106$

Necessary conditions ok!

$$signA(1) = signA(-1), |a_3| < 1$$

But...



Origin encircled twice In fact: $\lambda_{1,2} = 0.5 \pm 0.9i$, $\lambda_3 = 0.1$

Open-loop stability criterion

Second order system

$$\begin{split} \textit{A}(\mathbf{q}^{-1}) &= 1 + \textit{a}_1 \mathbf{q}^{-1} + \textit{a}_2 \mathbf{q}^{-2} &= (1 - \lambda_1 \mathbf{q}^{-1})(1 - \lambda_2 \mathbf{q}^{-1}) \\ &= 1 - (\lambda_1 + \lambda_2)\mathbf{q}^{-1} + \lambda_1 \lambda_2 \mathbf{q}^{-2} \end{split}$$

Start with $\lambda_1 = \lambda_2 = 0$ (stable)

Move poles to make system unstable

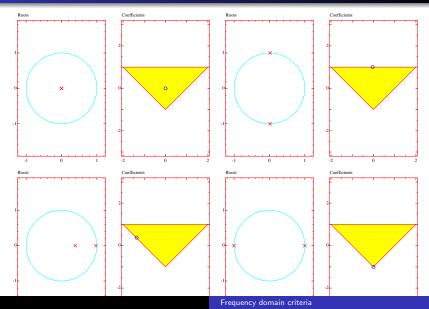
Only three situations possible

- **1** A pole pass out at $\lambda_1=1\Rightarrow A(1)=0=1+a_1+a_2$
- 2 A pole pass out at $\lambda_1 = -1 \Rightarrow A(-1) = 0 = 1 a_1 + a_2$
- **3** Two poles pass out $\lambda_1 \lambda_2 = a_2 = 1$

Three lines enclose stability area

$$\begin{cases} a_2 > -a_1 - 1 \\ a_2 > a_1 - 1 \\ a_2 < 1 \end{cases}$$

Example: second order system



Open and closed-loop relation

Process
$$Ay = Bu$$
, $y = \frac{B}{A}u$
Controller $Ru = Se$, $u = \frac{S}{R}e$
Open loop compensated system (e external)

$$y = G_{open}e$$
, $G_{open} = \frac{BS}{AR} = \frac{B_{open}}{A_{open}}$

Feedback system e = -y

$$ARy = BRu = B(-Sy) \Rightarrow \underbrace{(AR + BS)}_{A_{closed}} y = 0$$

Relation between open and closed loop characteristic polynomials

$$1 + G_{open} = \frac{A_{closed}}{A_{open}}$$

Nyquist theorem

$$A_{closed} = (1 + G_{open})A_{open}$$

Suppose open system has N_u unstable poles Closed loop stable if

$$0 = \Delta_{\text{arg}} A_{closed}(e^{-i\omega})$$

$$= \Delta_{\text{arg}} (1 + G_{open}(e^{-i\omega})) + \underbrace{\Delta_{\text{arg}} A_{open}(e^{-i\omega})}_{-2\pi N_u}$$

$$\Rightarrow \Delta_{\text{arg}} (1 + G_{open}(e^{-i\omega})) = 2\pi N_u$$

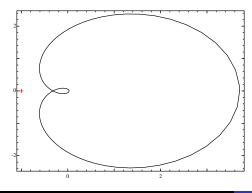
Nyquist theorem

An open-loop system G_{open} with N_u unstable poles is stable in closed loop if and only if $G_{open}(\mathrm{e}^{-\mathrm{i}\omega})$, $\omega=0\to 2\pi$ encircles -1, N_u times in counter-clockwise direction.

Example

Stable open loop

$$G_{open}(\mathbf{q}^{-1}) = \frac{0.1\mathbf{q}^{-2}}{(1 - 0.1\mathbf{q}^{-1})(1 - 0.7\mathbf{q}^{-1})(1 - 0.9\mathbf{q}^{-1})}$$



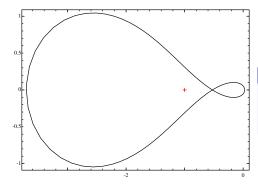
Closed loop stable

Gain margin

Example

Unstable open loop

$$G_{open}(\mathbf{q}^{-1}) = \frac{0.1\mathbf{q}^{-2}}{(1 - 0.1\mathbf{q}^{-1})(1 - 0.7\mathbf{q}^{-1})(1 - 1.1\mathbf{q}^{-1})}$$

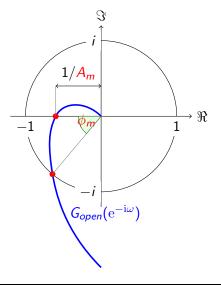


Closed loop stable

Gain margins

$$\frac{1}{3.7} = 0.27 < K < \frac{1}{0.5} = 2$$

Amplitude and phase margins



Nyquist curve in complex plane

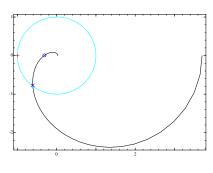
$$G_{open}(\mathrm{e}^{-\mathrm{i}\omega}), \quad \omega = 0 o \pi$$

Closed loop stability margins

Amplitude (gain) margin: A_m

Phase margin: ϕ_m

Example: previous stable system



Closed loop stable for perturbations:

Gain margin

$$G_{open}(e^{-i\omega_o}) = -\frac{1}{A_m} = -0.32$$

 $u(k) = -Ky(k), \ K < A_m = 3.1$

Phase margin

$$|G_{open}(e^{-i\omega_x})| = 1,$$

 $\phi_m = \arg G_{open}(e^{-i\omega_x}) + \pi$
Delay margin $\tau_m = \phi_m/\omega_x = 3.11$
 $u(k) = -y(k-\tau), \ \tau = 0, 1, 2, 3$

Stability margins in closed-loop

Let G_{open} be stable and u(k) = 0

$$y(k) = G_{open}u(k) \rightarrow 0, \quad k \rightarrow \infty$$

Gain variation in feedback

$$u(k) = -Ky(k)$$

Stable for $0 \le K < A_m$

$$y(k) \to 0, k \to \infty$$

 $K = A_m$: Oscillation freq. ω_o

Time delay variation in feedback

$$u(k) = -y(k-\tau)$$

Stable for $au < au_{\it m} = \phi_{\it m}/\omega_{\it x}$

$$y(k) \rightarrow 0, k \rightarrow \infty$$

 $\tau = \tau_m$: Oscillation freq. ω_x