

# EARTHQUAKE'S EFFECT ON MULTISTORY BUILDINGS: A SIMPLE MODEL

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# Model Description

- Motion of earth caused by earthquake puts buildings into motion
- Multistory buildings modelled as point-masses connected via springs and dashpots



Figure: Reality

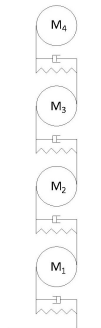


Figure: Simplification

- Consider mass  $m_i$ , spring constant  $k_i$ , damping constant  $c_i$ , displacement  $x_i$ , and velocity  $v_i$  of the  $i^{th}$  floor

- Forces on each floor depend on the floors above and below

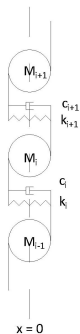


Figure:  $i^{th}$  floor statics

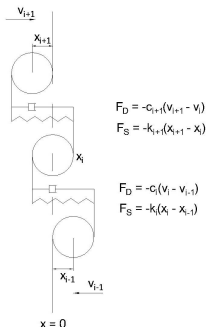


Figure:  $i^{th}$  floor dynamics

- Hooke's law describes the spring force  $F_S = -kx$
- A linear damping force is considered in a similar manner  $F_D = -c\dot{x}$

# Equation of Motion

- Define system of equations for  $n$  floors

$$\mathbf{M}\ddot{\mathbf{X}} + \mathbf{C}\dot{\mathbf{X}} + \mathbf{K}\mathbf{X} = \mathbf{F} \quad (1)$$
$$\mathbf{X}(0) = \mathbf{D}_0, \dot{\mathbf{X}}(0) = \mathbf{V}_0$$

$$\mathbf{K} = \begin{bmatrix} k_1 + k_2 & -k_2 & 0 & 0 & \cdots & 0 & 0 & 0 \\ -k_2 & k_2 + k_3 & -k_3 & 0 & \cdots & 0 & 0 & 0 \\ \vdots & \vdots & \vdots & \vdots & \ddots & \vdots & \vdots & \vdots \\ 0 & 0 & 0 & 0 & \cdots & 0 & -k_n & k_n \end{bmatrix},$$

$$\mathbf{C} = \begin{bmatrix} c_1 + c_2 & -c_2 & 0 & 0 & \cdots & 0 & 0 & 0 \\ -c_2 & c_2 + c_3 & -c_3 & 0 & \cdots & 0 & 0 & 0 \\ \vdots & \vdots & \vdots & \vdots & \ddots & \vdots & \vdots & \vdots \\ 0 & 0 & 0 & 0 & \cdots & 0 & -c_n & c_n \end{bmatrix},$$

$$\mathbf{M} = \begin{bmatrix} m_1 & 0 & 0 & \cdots & 0 \\ 0 & m_2 & 0 & \cdots & 0 \\ \vdots & \vdots & \vdots & \ddots & \vdots \\ 0 & 0 & 0 & \cdots & m_n \end{bmatrix}, \quad \mathbf{F} = \begin{bmatrix} f_1(t) \\ 0 \\ \vdots \\ 0 \end{bmatrix}, \quad \mathbf{X} = \begin{bmatrix} x_1(t) \\ \vdots \\ x_n(t) \end{bmatrix}$$

- Discretization of position and velocity using truncated Taylor series expansions that have defined constants  $\beta$  and  $\gamma$

$$D_{n+1} = D_n + V_n \Delta t + \frac{A_n \Delta t^2}{2} + 2\beta \dot{A}_n \Delta t^3$$
$$V_{n+1} = V_n + A_n \Delta t + \gamma \dot{A}_n \Delta t^2$$

- Definition of derivative approximation

$$\dot{A}_n = \frac{A_{n+1} - A_n}{\Delta t}$$

- The Newmark method is defined by the following 3 equations

$$\mathbf{M}A_{n+1} + \mathbf{C}V_{n+1} + \mathbf{K}X_{n+1} = F_{n+1} \quad (2)$$

$$D_{n+1} = D_n + V_n \Delta t + \frac{\Delta t^2}{2} [(1 - 2\beta)A_n + 2\beta A_{n+1}] \quad (3)$$

$$V_{n+1} = V_n + \Delta t [(1 - \gamma)A_n + \gamma A_{n+1}] \quad (4)$$

# Implementation of Newmark Method

- ➊ Using initial conditions  $D_0$  and  $V_0$  calculate  $A_0$

$$A_0 = \mathbf{M}^{-1}(F_0 - \mathbf{C}V_0 - \mathbf{K}D_0)$$

- ➋ Define constants

$$c_1 = \frac{1}{\beta \Delta t^2} \quad c_2 = \frac{1}{\beta \Delta t} \quad c_3 = \frac{1}{2\beta} - 1$$
$$c_4 = \frac{\gamma}{\beta \Delta t} \quad c_5 = 1 - \frac{\gamma}{\beta} \quad c_6 = \Delta t \left(1 - \frac{\gamma}{2\beta}\right)$$

- ➌ Define inverted matrix allowing for explicit calculation of  $D_{n+1}$

$$\left( \frac{\mathbf{M}}{\Delta t^2 \beta} + \frac{\mathbf{C}\gamma}{\Delta t \beta} + \mathbf{K} \right) D_{n+1} = F_{n+1} + \mathbf{M} \left( \frac{\tilde{D}_{n+1}}{\Delta t^2 \beta} \right) - \mathbf{C} \left( \tilde{V}_{n+1} - \frac{\gamma \tilde{D}_{n+1}}{\Delta t \beta} \right)$$

- ➍ For each time step calculate  $D_{n+1}$ ,  $V_{n+1}$  and  $A_{n+1}$

$$\tilde{A}_{n+1} = -c_1 D_n + c_2 V_n + c_3 A_n$$

$$\tilde{V}_{n+1} = c_4 D_n + c_5 V_n + c_6 A_n$$

$$D_{n+1} = \mathbf{W}[F_{n+1} + \mathbf{M}\tilde{A}_{n+1} - \mathbf{C}\tilde{V}_{n+1}]$$

$$V_{n+1} = c_4 D_{n+1} + \tilde{V}_{n+1}$$

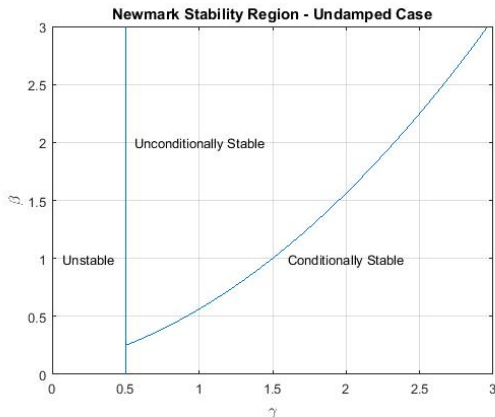
$$A_{n+1} = c_1 D_{n+1} - \tilde{A}_{n+1}$$

# Stability of Undamped Motion

- Stability condition  $\rho \leq 1 \Rightarrow \gamma \geq \frac{1}{2}$  and  $(\gamma + \frac{1}{2})^2 - 4\beta \leq \frac{4}{\Omega_i^2}$
- Unconditionally stable condition

$$\beta \geq \frac{1}{4} \left( \gamma + \frac{1}{2} \right)^2 \quad (5)$$

- Average constant acceleration method:  $\gamma = \frac{1}{2}$  and  $\beta = \frac{1}{4}$



- Consider  $\ddot{x} + x = 0$  with initial conditions  $x(0) = 1$ ,  $\dot{x}(0) = 0$  and solution  $x = \cos(t)$

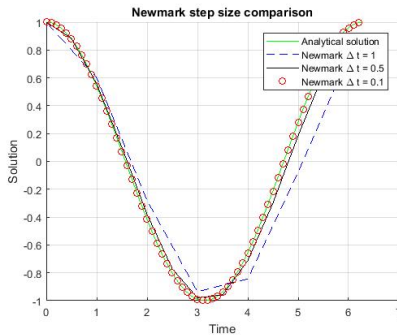


Figure: Newmark method solution with different step sizes

- Amplitude error

$$\rho - 1 = -\frac{1}{2} \left( \gamma - \frac{1}{2} \right) \omega^2 \Delta t^2 + O(\Delta t^4)$$

- Periodicity error

$$\frac{\Delta T}{T} = \frac{\omega \Delta t}{\phi} - 1 = \frac{1}{2} \left( \beta - \frac{1}{12} \right) \omega^2 \Delta t^2 + O(\Delta t^3)$$



# Parameters of the Newmark method

Algorithm	$\gamma$	$\beta$	$\Omega$	$\rho - 1$	$\frac{\Delta T}{T}$
Unconditionally stable	1	$\frac{3}{2}$	$\infty$	$-\frac{\Omega^2}{4}$	$\frac{17\Omega^2}{24}$
Conditionally stable	2	$\frac{1}{2}$	0.97	$-\frac{3\Omega^2}{4}$	$\frac{5\Omega^2}{24}$
Unstable	1	$\frac{1}{4}$	0	$-\frac{\Omega^2}{4}$	$\frac{\Omega^2}{12}$
Constant Acceleration	$\frac{1}{2}$	$\frac{1}{4}$	$\infty$	$O(\Delta t^4)$	$\frac{\Omega^2}{12}$
Purely Explicit	0	0	0	$\frac{\Omega^2}{4}$	$-\frac{\Omega^2}{24}$
Linear Acceleration	$\frac{1}{2}$	$\frac{1}{6}$	3.46	$O(\Delta t^4)$	$\frac{\Omega^2}{24}$

# Order of Newmark error

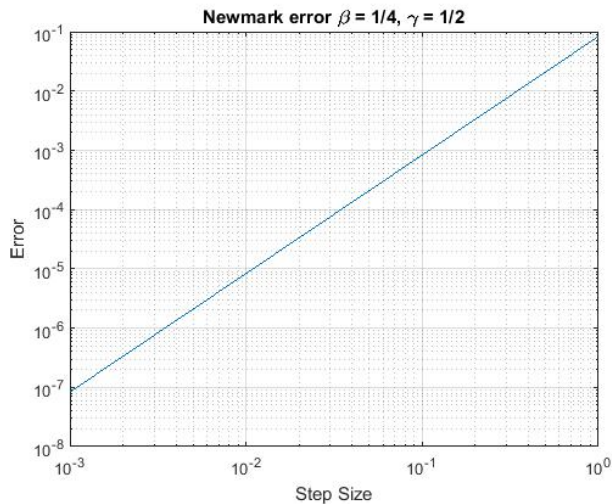


Figure: Newmark method error with different step sizes

# El Centro earthquake

- Earthquake: 1940, Imperial Valley in California, 6.9 on the Richter Scale
- 2-story house:  $m_i = 100,000 \text{ kg}$ ,  $k_i = 12 \times 10^5 \frac{\text{kg}}{\text{s}^2}$ ,  $c_i = 10^5 \frac{\text{kg}}{\text{s}}$

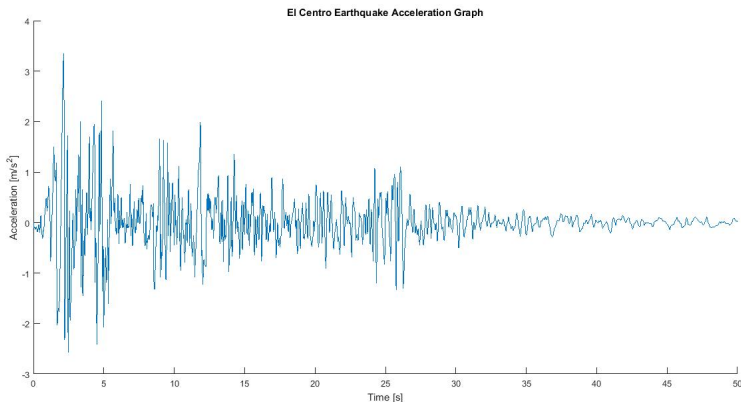


Figure: Acceleration data and 1st floor behavior

# El Centro earthquake effect on 2-story house

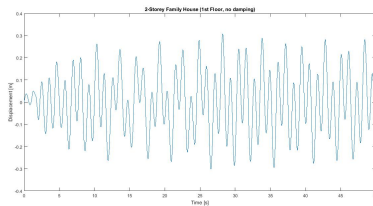


Figure: 1<sup>st</sup> floor without damping

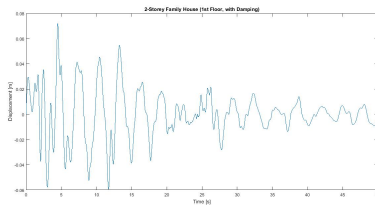


Figure: 1<sup>st</sup> floor with damping



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*El Centro Earthquake Page*. Vibration Data.

Thank You For Your Attention!