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ÚSTAV MECHANIKY TĚLES, MECHATRONIKY A BIOMECHANIKY

PREDICTIVE MAINTENANCE OF PNEUMATIC PISTONS

MOŽNOSTI PREDIKTIVNÍ ÚDRŽBY PNEUMATICKÝCH PÍSTŮ

MASTER'S THESIS

DIPLOMOVÁ PRÁCE

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Assignment Master's Thesis

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As provided for by the Act No. 111/98 Coll. on higher education institutions and the BUT Study and Examination Regulations, the director of the Institute hereby assigns the following topic of Master's Thesis:

Predictive maintenance of pneumatic pistons

Brief Description:

With the ever-increasing degree of automation in the industry, a widespread effort to measure, record, and exploit information and signals related to the state of a given machine and its production quality, is becoming more relevant. Predictive Maintenance (PM) is a relatively new method, which builds on and further expands the ideas of the already established Fault Detection and Analysis (FDA). The purpose of this work is to demonstrate various approaches to Predictive Maintenance (e.g., signal-based and model-based) using the Matlab/Simulink software tools on a double-acting pneumatic piston as a case-study.

Master's Thesis goals:

1. Conduct research in the area of Predictive Maintenance, Fault Detection and Analysis, and related approaches and try to define their similarities and differences. Provide a practical demonstration for each of the approaches.
2. Create a simulation model of the demonstration device, including models of the sensors. Test different methods to create the model (e.g., software simulation, physical properties, black-box identification, etc.) and identify the models with real data.
3. Apply Predictive Maintenance techniques to a test dataset without using a simulation model.
4. Apply Predictive Maintenance techniques to a test dataset using a simulation model.
5. Evaluate the suitability of each approach for the application of PM and FDA.

Recommended bibliography:

PRITCHARD, Philip J. Introduction to Fluid Mechanics, 9th edition, Wiley, ISBN 978-1118921876.

NELLES, Oliver. Nonlinear system identification: from classical approaches to neural networks and fuzzy models. Berlin: Springer, 2011. ISBN 978-364-2086-748.

LJUNG, Lennart. System identification: theory for the user. 2nd ed. Upper Saddle River, NJ: Prentice Hall PTR, 1999. ISBN 978-0136566953.

VALÁŠEK, Michael. Mechatronika. Dot. 1. vyd. Praha: České vysoké učení technické, 1996. ISBN 80-010-1276-X.

NOSKIEVIČ, Petr. Modelování a identifikace systémů. Ostrava: Montanex, 1999. ISBN 80-722-50-0-2.

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1 Introduction

Since the beginning of the industrial revolution, the complexity of production machines and serial lines has gradually increased and requires constant monitoring of the conditions of the systems for economic reasons. On the other hand, critical systems such as aircraft, spacecraft, automotive systems, nuclear reactors, and others require immediate alarm on fault, localize occurred fault, and even more predict possible future faults. These requirements have become prerequisites for Fault Detection and Analysis and Predictive Maintenance fields.

The production process always included elements of fault control and online monitoring. From the first methods of fault detection, such as visual inspection, today's factories move to automated systems consisting of sensors and computing units to evaluate the faults. Sometimes it is critical to monitor processing equipment in real-time to prevent damage caused by fault or anomaly. Every single fault can cause a slowing down of the production process and thus reducing the profit.

Device real-time monitoring algorithms have formed the Fault Detection and Analysis (FDA) field. FDA methods, in most cases, do not require machine learning techniques and can detect failures, using fundamental algorithms from Fourier analysis and trend checking algorithms to more complex techniques such as Gaussian Mixture Models.

Due to the amount of data collected in recent years and the expansion of data storage technology as cloud services and computation efficiency, it has become possible to use more advanced algorithms for fault detection and analysis. Using classification machine learning techniques, it is possible to isolate where does the fault occur. Another option that becomes available with a large amount of data is to estimate the remaining useful life (RUL) of the entire system. These techniques have led to predictive maintenance as an effort for optimal maintenance solutions. The current technical condition of the equipment is always available by information extracted from measured signals. It is possible to use current system conditions to estimate remaining useful life in time or distance measurements such as days, kilometers, or cycles. Estimated residual lifetime gives an option to plan maintenance concerning actual system conditions.

These remaining useful life estimation algorithms, the fault detection methods and system modeling and identification techniques form a new predictive maintenance field.

System modeling allows providing experiments and developing solutions offline before physical hardware implementations. Unavailable or challenging to implement measurements can be replaced by generated data from the simulation model and finally helps to deploy a robust algorithm.

This thesis provides a brief introduction to fault detection and predictive maintenance methodologies and a basic terminology. The 2 chapter describes the main goal and problems in these areas and focuses on similarities and differences between these two approaches.

Developing the simulation model of the double-acting pneumatic actuator and com-

paring it with the real-life equipment using different approaches is described in chapter 3, 4, and 5.

The following chapter 6 illustrates signal-based predictive maintenance methods using different sensors available in a demonstration device. Applying preprocessing, feature extraction, and classification model, sensors were evaluated in terms of functionality, accuracy, and price.

The model-based predictive maintenance techniques and simulation model exploitation are demonstrated in chapter 7. The simulation model is used to determine the residual signals between the measured data and the simulation model's output. Also, using a simulation model, degradation data are generated and used in the remaining useful life estimation.

2 Theoretical Survey

This chapter contains a short introduction to the main goals and problems presented in fault detection and analysis and predictive maintenance techniques. A brief review of methodologies used in these fields and general approaches. Section 2.4 digital twin describes scenarios where a simulation model is used in predictive maintenance and helps develop robust, efficient algorithms.

2.1 Problem Definition

In practice many types of machinery require some calibration and monitoring for adequate working. An anomaly or fault detection in time can prevent machinery from damage that causes loss of money due to non-working or destroyed equipment. Predicting where the fault appears reduces the cost of diagnosis and replacement operations. The possibility of estimating the remaining useful life allows to optimize a maintenance process and reduce maintenance costs.

Smart manufacturing, the combination of sensors, the possibility of preprocessing and extracting useful information from measurements and decision algorithms based on this information, allows increasing production efficiency and significantly reducing maintenance operations.

Types of Maintenance There are three main types of maintenances 2.1. Each following type of maintenance requires increasing complexity of monitoring and decision algorithms:

- Reactive maintenance, where maintenance coming after the life of the system is excess.
- Preventive maintenance is driven item by schedules that may keep the system safe but not optimal from an efficiency/cost perspective.
- Predictive maintenance is an effort to optimize a maintenance strategy.

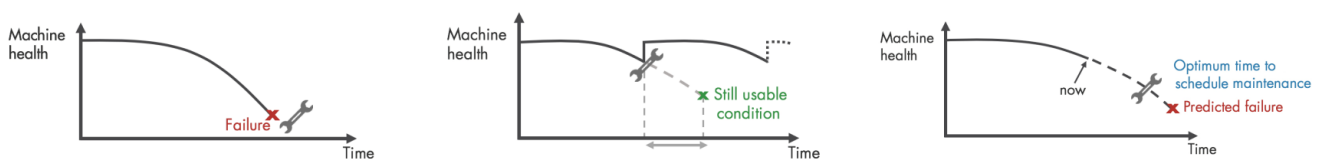


Figure 2.1: Reactive, preventive and predictive types of maintenance

Fault Types A fault is not an acceptable deviation of at least one characteristic or parameter of the system from the standard condition. There are different faults by their sources.

- Plant faults appear in system behavior and cause manufacturing performance.
- Component fault
- Sensor faults occurred in the sensor during measurements.
- Combination of faults

In many cases, faults lead to a system failure and the system is no longer able to perform required functions. There may also be a malfunction after which the system returns to normal operation.

Faults can be classified by the location where they appear, by a fault form, or based on the form in which the fault is added to the system.

2.2 Fault Detection and Analysis (FDA)

Fault Detection and Analysis, FDA (Fault Detection and Isolation, FDI) is a subfield of control engineering focused on detecting the fault and identifying where this fault is located. The main goals of FDI are

- Fault detection, detect anomalies in real-time
- Fault isolation, find the root cause
- Fault identification, estimation of the magnitude, type, or nature of the fault

Several methods are partly overlapped but divided into two main categories.

Signal-Based methods Signal-Based methods (SB), explore measured data and extract useful information in the form of features 2.2. The following methods belong to the SB approach:

- Limit and trend checking
- Spectral analysis
- Data analysis (PCA)
- Pattern recognition

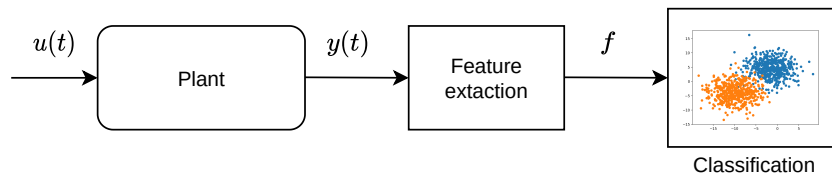


Figure 2.2: Signal-Based Method

Model-Based methods Model-Based methods exploit models identified from real-life systems 2.3. The model-based approach is suitable when it is difficult to gain useful information using only measured signals. If the system structure is known, it is possible to extract features such as state variables or some system parameters. Another option is to compare real system behavior with nominal healthy model and use residuals as inputs to decision algorithms. Typical model-based techniques include

- Residual estimation (compare measurements with "healthy" model)
- Polynomial coefficients
- State variables estimated using state observers
- Parameter estimation

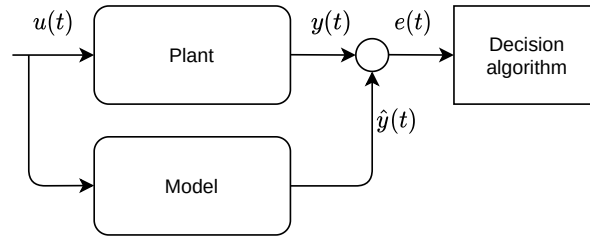


Figure 2.3: Model-Based Method

Automated fault detection depends on input from sensors and postprocessing algorithms. In many manufacturing applications, sensor failures are the most common equipment failure.

The result of FDI is the detection and identification of faults that occur during the operation of the device. Subsequently, predicted faults are processed using fault tolerance and predictive maintenance algorithms.

Fault Tolerance: Provide the system with the hardware architecture and software mechanisms that will allow, if possible, to achieve a given objective in normal operation and given fault situations.

2.3 Predictive maintenance (PdM)

Predictive maintenance (PdM) is cost-effective maintenance strategy that predicts time to failure and warns of an anticipated location where this could occur.

2.3.1 Goals

There are two main goals of predictive maintenance, remaining useful life (RUL) estimation and identification where the future failure can appear or what is the reason for decreasing RUL. As a result of PdM is RUL representing the number of cycles, days or time before the fault occurred. And the probability of when or where this fault can appear.

2.3.2 Overview of the PdM development workflow

Figure 2.4 represents the recommended PdM development workflow. The development of predictive maintenance algorithms starts with raw measured signals from sensors. For

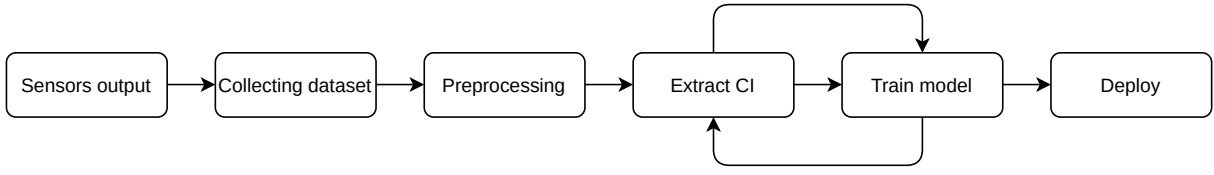


Figure 2.4: Predictive maintenance development sequence

further working with data, it is a good manner to combine measurements to a dataset with a logical structure of elements. In this thesis, a common data ensemble structure was used. Each measurement has its own data file with all measured signals at a particular time.

If collected data require some preprocessing techniques as data cleaning, smoothing or filter the signal, detrend, normalizing, etc., it can be done at this step.

The next step is to extract condition indicators using predictive maintenance methods described in 2.3.3. As long as the optimal solution is not found, try to figure out the best combination of condition indicators described in 2.3.4 and train different classification models iteratively. After the efficient solution is found, deploy the algorithm to work recursively with the study-case system.

2.3.3 Condition Indicators

In the prediction maintenance field, features extracted from measured signals are called **Condition Indicators, CI**.

Condition Indicators represent some system behavior and hide information about system operation conditions. Generally, CI is represented by three main domains. There is a time domain, frequency domain, time-frequency domain. But in fact, CI can be any system parameter or value corresponding with the system's current condition.

The methods of extracting condition indicators from the signal are defined in the same way as in FDI 2.2.

The **signal-based approach** is suitable when we have measurements from the system in different operating conditions. But there is a problem that signal-based approach enables classifying and learning just the patterns observed in the training dataset. On the other hand, the **model-based approach** uses physical failure models and does not require a large dataset of failure data. And they may work in situations never observed in data before. Moreover, the model-based method is helpful in case the measured signal has a more complex relationship with the input signal.

Between common signal-based CI belongs:

- Time-domain: mean, standard deviation, RMS, skewness, etc.
- Frequency-domain: mean frequency, peak values/frequencies, power bandwidth, etc.
- Time-frequency domain: Spectral entropy/kurtosis, moments, etc.

Model-based approach use model properties such as:

- poles and zeros location
- damping coefficient
- state variables values

- modal analysis
- residual values

2.3.4 Condition Indicators Ranking

Multiple condition indicators can be extracted from each sensor signal. A good practice to reduce the number of CI and keep only those which provide essential information.

One of the possibilities is applying Principle Component Analysis (PCA) to transform features from one coordinate system to a new orthogonal basis. Data reduced by using the first n principal components that optimally describe the variance of the dataset. Applying the PCA algorithm still requires the extraction of all condition indicators from the signal.

Another option is to rank the features using the Analysis of Variance (ANOVA) algorithm. This algorithm describes relations among CI in the form of their mean values. The result gives information about how much particular CI represents data. Using the first n CI, we reduce the number of CI and reduce the number of extracted features from measured signals. This fact means that using ANOVA reduced the time and complexity of calculations.

2.3.5 Fault Classification

Classification models are used to recognize faults from a set of CI. The set of CI must contain labels that determine the current condition of the device in the form of fault code, string, etc. The correlation between different CI can be explored using a 2D or 3D scatter plot. The model performance is usually represented by total accuracy and confusion matrix, where on one axis there are true labels and on the other there are predicted from the model. The common types of classification models are:

- Decision Trees
- Supported Vector Machines (SVM)
- Neighbourhood Neighbors (KNN)
- Ensemble Classifiers
- Neural Networks (ANN)

A good practice is to divide an original dataset of CI into train, validation and test sub-datasets to prevent model overfitting. Choosing the best classification model depends on training data and requires experiments with different models.

2.3.6 Remaining useful life

The remaining useful life (RUL) is the expected time remaining before the machine requires repairment or replacement, and it is a central goal of PdM.

The problem of estimating the remaining useful life is connected with evaluating condition indicators associated with the system's degradation process. These condition indicators must satisfy the requirements for monotonicity, trendability, and prognosability.

The models used to estimate the remaining useful life depend on the historical data which are available. There are three types of possible models.

Survival model The survival model is considered when we have only failure data available, but the whole degradation history is not recorded. The probability density function can be obtained from failure data and used to estimate RUL.

Degradation model The degradation model gives an option to estimate RUL based on data without failure moment captured but only recorded degradation process. In this situation, it is necessary to determine a safety threshold that CI must not cross.

Similarity model In case we have the whole history of the degradation process of similar systems, including failure, the similarity model can be used. The upcoming CI is compared with historical degradation paths obtained from the training dataset and the best similarity trend is evaluated as RUL value.

2.4 Digital twin

A digital twin is a digital representation of the real-life system. It can be represented as a component, a system of components, or as a system of systems.

A digital twin can be updated with incoming data from sensors. Fitting the model to new data, the digital twin represents the current condition state of the real-world object. There are many advantages of using models in PdM. A digital twin can hold historical data about system behavior. Apart from this, it can be used for simulation system operation in different conditions, designing control and simulating future behavior (RUL, "What-if"). The dataset extended by data from the simulation model represents synthetic dataset. This dataset type can contain different measured fault and healthy data of the system and hard to realizable in real-world fault situations.

A mathematical model of the real-world system can be created using different approaches.

- First-principles modeling requires an understanding of the fundamental process of the system.
- Physical modeling (Simscape).
- Data-driven modeling where the system is represented as a Blackbox.
- Combination of multiply approaches.

2.5 Comparison PdM and FDA approaches

Figure 2.5 presents a relative arrangement of Predictive Maintenance (PdM) and Fault Detection and Identification (FDI or FDA) algorithms. From the figure, it is clear that Predictive Maintenance is an extension of the FDI approach, with recommended workflow techniques suitable for optimizing system maintenance.

Both methods are closely overlapped and use quite similar techniques. However, predictive maintenance over the FDA is extended by RUL estimation. And it leads not only to fault detection and monitoring at a given moment but also to the possible prediction of a fault in the near future.

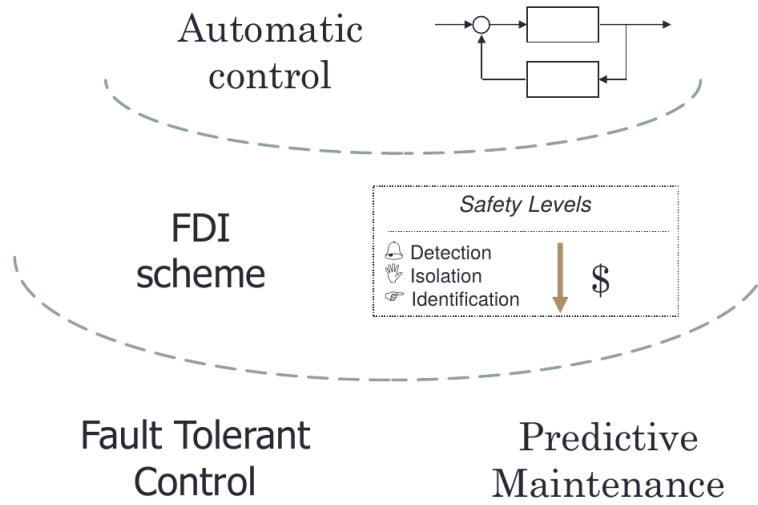


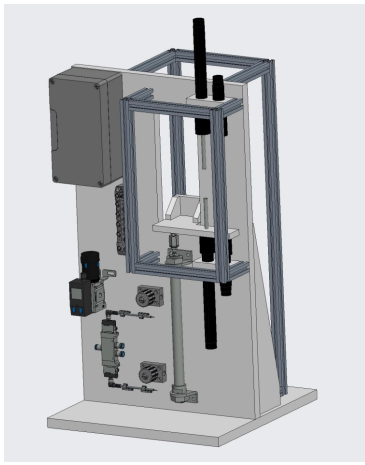
Figure 2.5: Relative arrangement of PdM and FDI algorithm [?]

2.6 Applications

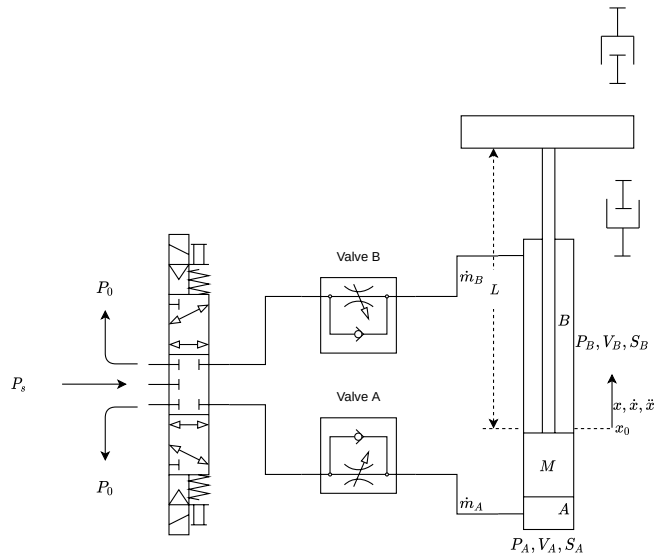
The most significant interest in PdM is the manufacturing sector that requires efficiency maintenance strategies to increase productivity and reduce money-lost. The PdM is used in the field that is highly dependent on safety types of machinery such as aircraft or rail industry. Using the PdM condition monitoring, it is possible to prevent unexpected fails. The oil and gas industry supports the PdM field; due to the amount of data collected in these industries, the PdM techniques are beneficial.

3 Demonstration Device Overview

3.1 Double-Acting Pneumatic Actuator



(a) 3D render of the demonstration device



(b) Schematically representation of the demonstration device

Figure 3.1: Demonstration device

The case study of this thesis is the double-acting pneumatic piston, with a pneumatic circuit and mechanical assembly driven by a piston. Figure 3.1b is a schematical representation of the system. Figure 3.1a is a 3D render of the system.

Pneumatic systems use air to transmit power between components in the circuit. The air is a compressible gas, and we have to consider this when designing a model. Pneumatic actuators are highly efficient and fast drives. Using compressed air pneumatic actuator can move with high velocities and supply nominal force in the kN range. One of the advantages of a pneumatic system with a piston is that only one supply line is necessary, giving many opportunities to design and maintain the system. The basic pneumatic system includes an air reservoir with supplied air, pressure lines connection, pneumatic actuator and control valve to connect the supply pressure and actuator. Resistance to movement places a mass that acts on the piston.

In this thesis, a double-acting pneumatic actuator, as shown in figure 3.1b was used. Throttling valves A and B regulate the air mass flow to the piston's chambers. Proportion valve connects supply and ambient pressure lines to achieve piston control. There are two pairs of dampers installed to prevent possible destruction impact and simulate different material penetration resistance.

The demonstration device can be used in stamping, drilling, moving applications.

3.2 Sensors

There are seven types of sensors located on the system. Table 3.1 describes a sensor purpose, signal name in the datastore, and the signal unit.

Sensor	Unit	Description	Name
Encoder	m	displacement	LeverPosition
Encoder	m/s	velocity	LeverVelocity
Accelerometer	g	accelerometer on moving part	AccelerometerMovin_axisZ/Y
Accelerometer	g	accelerometer on static part	AccelerometerStatic_axisZ/Y
Flow Sensor	l/min	air flow extrusion to A chamber	FlowExtrusion
Flow Sensor	l/min	air flow contraction from A chamber	FlowContraction
Pressure	bar	pressure measurement in reservoir	AirPressure
Microphone	V	microphone on upper bumper	MIC_uBumper
Microphone	V	microphone on bottom bumper	MIC_bBumper
Microphone	V	ambient microphone	MIC_Ambient
Temperature	°C	cylinder temperature measurement	TempCylinder
Temperature	°C	ambient temperature measurement	TempAmbient

Table 3.1: Sensors overview

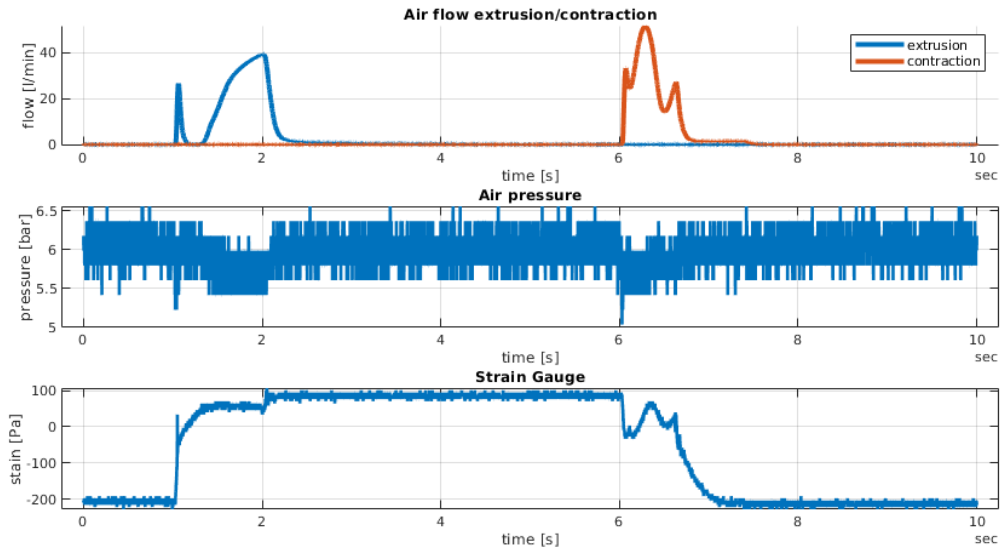


Figure 3.2: Caption

The dataset measured on the system contains almost five thousand measurements in different operating conditions. Each measurement includes a 10-second recording of moving the pistol up and down. This data was given in the format of massive files with the ".mat" extension, which was divided into files contains only one measurement. The divided dataset is easier to maintain, and Matlab recommends this type of datastores called Data Ensemble ??.

The measured examples are shown in figures 3.2,3.2, and 3.2.

4 First Principle Modeling

First-principle modeling is a common engineering modeling approach. Models developed using physical laws such as energy and mass balance, heat transfer, and so on. First-principle modeling requires knowledge of the system and the physical processes that take place in this system.

First principle models (FPMs) are usually designed in the form of a system of differential equations, algebraic differential equations, transfer functions, state-space systems, etc. In designing FPMs, it is necessary to determine the assumptions and simplifications that correspond to the level of technical resolution in a particular problem.

This chapter introduces the design of a double-acting pneumatic piston assembly model, including sensors using a first-principle modeling approach.

4.1 General physical principles

Assumptions

1. The effect of accelerated air mass is neglected.
2. The gas is ideal.
3. All the thermal processes are adiabatic.

Equation of state Equation of state for an ideal gas 4.1, describe the relationships between temperature, mass, pressure and volume of the gas, where $R = 287.1[\text{Jkg}^{-1}\text{K}^{-1}]$ is an ideal gas constant.

$$pV = mRT \quad (4.1)$$

Adiabatic process All processes take place without heat exchange with the environment by given equation 4.2, where $\kappa = c_p/c_v$ is a heat capacity ratio.

$$p_1 V_1^\kappa = p_2 V_2^\kappa = \text{const} \quad (4.2)$$

Relation between heat capacities and an ideal gas constant is given by Mayer's equation as $c_p = c_v + R$.

Bernoulli's principle Bernoulli's equation 4.3 describes flow dynamics as a sum of kinetic, potential and internal energies.

$$H_1 + \frac{mw_1^2}{2} + mgz_1 + Q = H_2 + \frac{mw_2^2}{2} + mgz_w + W_T \quad (4.3)$$

Transition to specific values:

$$h_1 - h_2 = - \int_1^2 v dp = c_p(T_1 - T_2) = c_p T_1 \left(1 - \frac{T_2}{T_1} \right) \quad (4.4)$$

Continuity equation Continuity equation 4.5 describes a mass flow through a control volume.

$$\dot{m} = S_1 w_1 \rho_1 = S_2 w_2 \rho_2 = \text{const} \quad (4.5)$$

4.2 Air Expansion

Air expansion from the reservoir, one of the fundamental sets of equations used in pneumatic elements.

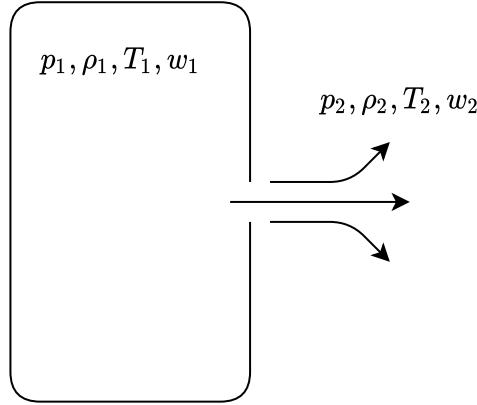


Figure 4.1: Air expansion from tank

Assuming that $W_T = 0$, $Q = 0$ there is no work and heat shared with the the environment, there is no difference in height $z_1 = z_2$ and the velocity difference is vast $w_2 \ll w_1$, applying equation 4.3, get 4.7.

$$w_2 = \sqrt{2(h_1 - h_2)} \quad (4.6)$$

$$w_2 = \sqrt{2c_p T_1 \left(1 - \frac{T_2}{T_1} \right)} \quad (4.7)$$

where

$$T_1 = \frac{p_1}{R\rho_1} \quad c_p = R \left(\frac{\kappa}{\kappa - 1} \right) \quad \frac{T_2}{T_1} = \left(\frac{p_2}{p_1} \right)^{\frac{\kappa-1}{\kappa}} \quad (4.8)$$

Combine equations 4.7, ?? to get air expansion velocity 4.9.

$$w_2 = \sqrt{2 \frac{\kappa}{\kappa - 1} \frac{p_1}{\rho_1} \left[\left(1 - \left(\frac{p_2}{p_1} \right)^{\frac{\kappa-1}{\kappa}} \right) \right]} \quad (4.9)$$

From equations ?? express air density 4.10.

$$\rho_2 = \frac{p_1}{RT_1} \left(\frac{p_2}{p_1} \right)^{\frac{1}{\kappa}} \quad (4.10)$$

Using continuity equation 4.5 and 4.9 describe mass flow as ??:

$$\dot{m} = Ap_1 \sqrt{\frac{2}{RT_1}} \sqrt{\frac{\kappa}{\kappa - 1} \frac{p_1}{\rho_1} \left[\left(1 - \left(\frac{p_2}{p_1} \right)^{\frac{\kappa-1}{\kappa}} \right) \right]} \quad (4.11)$$

where 4.12 is the outflow function.

$$\psi \left(\frac{p_2}{p_1} \right) = \sqrt{\frac{\kappa}{\kappa - 1} \frac{p_1}{\rho_1} \left[\left(1 - \left(\frac{p_2}{p_1} \right)^{\frac{\kappa-1}{\kappa}} \right) \right]} \quad (4.12)$$

Finally mass flow from the reservoir is given by equation 4.13:

$$\dot{m} = Ap_1 \sqrt{\frac{2}{RT_1}} \cdot \psi \left(\frac{p_2}{p_1} \right) \quad (4.13)$$

Critical flow velocity The outflow function depends on the pressure ratio p_2/p_1 . This function has a maximum value when the critical pressure is reached; the mass flow becomes choked. Critical pressure is presented by 4.21. For the overcritical pressure ratio, the mass flow depends only on p_1 and T_1 [?].

$$\left(\frac{p_2}{p_1} \right)_{crit} = \left(\frac{2}{\kappa + 1} \right)^{\frac{\kappa}{\kappa-1}} = \beta_k \quad (4.14)$$

Critical pressure for air is $\beta_k = 0.528$ and critical velocity is give by outflow function ??. Combine equations for overcritical and undercritical pressure ratio using equations 4.21, ?? we get the final equation for overflow function ??.

$$\psi_{max}(\beta_k) = \left(\frac{2}{\kappa + 1} \right)^{\frac{\kappa}{\kappa-1}} \sqrt{\frac{\kappa}{\kappa + 1}} = 0.484 \quad (4.15)$$

$$\psi \left(\frac{p_2}{p_1} \right) = \begin{cases} \sqrt{\frac{\kappa}{\kappa-1} \frac{p_1}{\rho_1} \left[\left(1 - \left(\frac{p_2}{p_1} \right)^{\frac{\kappa-1}{\kappa}} \right) \right]} & 0.528 < \frac{p_2}{p_1} \leq 1 \\ \left(\frac{2}{\kappa+1} \right)^{\frac{1}{\kappa+1}} \sqrt{\frac{\kappa}{\kappa+1}} & 0 \leq \frac{p_2}{p_1} \leq 0.528 \end{cases} \quad (4.16)$$

A detailed derivation of the equation ?? can be found in [?],[].

4.3 Pneumatic Piston Pressure Model

A construction principle of the double-acting pneumatic piston is shown in the figure ??. There are two chambers connected to the control valve. If the control valve is connected to chamber A, the supply pressure drives mass flow into chamber A. At the same time, the port at chamber B is connected to the ambient. Due to the pressure difference between chambers, pneumatic piston stroke start moving in a positive direction. After the bound is reached and the pressure in the chamber equalizes to supply pressure, there is no longer any mass flow coming inside.

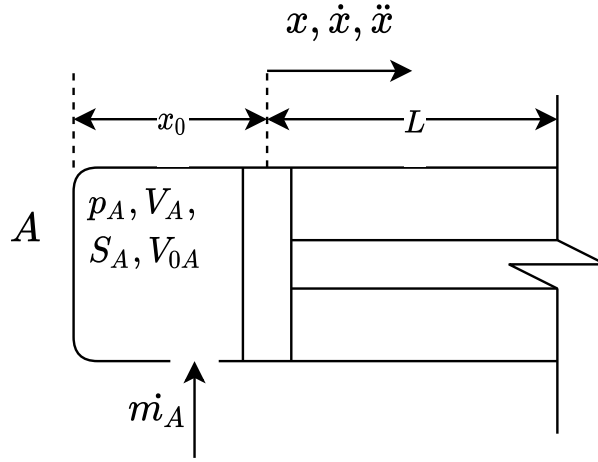


Figure 4.2: Piston chamber

Assuming an isothermal process, derivation of the equation of state $m = \rho V$ get the equation ??.

$$\dot{m} = \dot{\rho}V + \rho\dot{V} \quad (4.17)$$

where

$$\rho = \frac{p}{RT} \quad \dot{\rho} = \frac{\dot{p}}{RT} \quad (4.18)$$

Equation 4.28 describe pressure difference in chamber due mass flow.

$$\dot{p} = -\frac{p}{V}\dot{V} + \frac{RT}{V}\dot{m} \quad (4.19)$$

For the adiabatic model of the pressure difference in the chamber, moreover, heat capacity ratio added 4.29.

$$\dot{p} = -\frac{\kappa p}{V}\dot{V} + \frac{\kappa RT}{V}\dot{m} \quad (4.20)$$

Volumes of the chambers can be represented concerning figure ?? as volumes equations ??.

$$V_A = S_A x + V_{0A} \quad (4.21)$$

$$V_B = S_B(L - x) + V_{0B} \quad (4.22)$$

$$\dot{V}_A = S_A \dot{x} \quad (4.23)$$

$$\dot{V}_B = -S_B \dot{x} \quad (4.24)$$

The pneumatic piston with chambers A, B is described by the system of differential equations ??, ??. These equations describe a pneumatic cylinder entirely. Furthermore, all the parameters can be directly measured or found in the datasheet [].

$$\dot{p}_A = \frac{\kappa}{S_A x + V_{0A}} (-p_A S_A \dot{x} + RT_A \dot{m}_A) \quad (4.25)$$

$$\dot{p}_B = \frac{\kappa}{S_B(L - x) + V_{0B}} (p_B S_B \dot{x} + RT_B \dot{m}_B) \quad (4.26)$$

4.4 Control Valve Model

4.4.1 Input/Output mass flows

$$\dot{m}T = \dot{m}_{in}T_s - \dot{m}_{out}T_{A/B} \quad (4.27)$$

4.4.2 Valve model

S_{eq}	m^2	Equivalent cross section
S_{max}	m^2	Maximum cross section
C_d	—	Coefficient of contraction
u	—	Regulation variable

Valve flow model with simply input control signal For regulation flow this model used input control signal directly without spool mechanics.

Coefficient of contraction 4.37:

$$C_d = \frac{S_{eq}}{S_{max}} \quad (4.28)$$

For flow control regulation $u \in \langle -1, 1 \rangle$ can be used.

$$u = \begin{cases} u \in \langle -1, 0 \rangle & \text{discharge the chamber} \\ u = 0 & \text{valve closed} \\ u \in (0, 1) & \text{filling the chamber} \end{cases} \quad (4.29)$$

$$\dot{m} = u S_{max} C_d p_1 \sqrt{\frac{2}{RT_1}} \cdot \psi \left(\frac{p_2}{p_1} \right) \quad (4.30)$$

For filling the chamber:

- $p_1 = p_s$
- $p_2 = p_A$ or p_B
- $T_1 = T_s$

For discharge the chamber:

- $p_1 = p_A$ or p_B
- $p_2 = p_0$
- $T_1 = T_A, T_B$

where p_s is supply pressure. p_0 atmospheric pressure. As T_i - atmospheric temperature using according to isothermal process.

$$\dot{m}_A = \begin{cases} u S_v C_d p_s \sqrt{\frac{2}{RT_s}} \cdot \psi\left(\frac{p_A}{p_s}\right) & , u \in (0, 1) \\ 0 & , u = 0 \\ u S_v C_d p_A \sqrt{\frac{2}{RT_A}} \cdot \psi\left(\frac{p_0}{p_A}\right) & , u \in \langle -1, 0 \rangle \end{cases} \quad (4.31)$$

$$\dot{m}_B = \begin{cases} u S_v C_d p_s \sqrt{\frac{2}{RT_s}} \cdot \psi\left(\frac{p_B}{p_s}\right) & , u \in (0, 1) \\ 0 & , u = 0 \\ u S_v C_d p_A \sqrt{\frac{2}{RT_B}} \cdot \psi\left(\frac{p_0}{p_B}\right) & , u \in \langle -1, 0 \rangle \end{cases} \quad (4.32)$$

Valve flow with spool mechanic included With respect to valve spool modeled as 1DOF system 4.48 and mechanical and geometrical properties following equation were used.

Valve flow with spool In this model we accept a spool displacement x_s , controlled by input voltage u .

$$\dot{m}(P_u, P_d) = \begin{cases} C_f A_v \left(\frac{\kappa}{R} \left(\frac{2}{\kappa-1}\right)\right)^{\frac{1}{2}} \cdot \frac{P_u}{\sqrt{T}} \left(\frac{P_d}{P_u}\right)^{\frac{1}{\kappa}} \cdot \sqrt{1 - \left(\frac{P_d}{P_u}\right)^{\frac{\kappa-1}{\kappa}}} & , \text{ if } \frac{P_d}{P_u} > P_{cr} \text{ (subsonic)} \\ C_f A_v \frac{P_u}{\sqrt{T}} \cdot \sqrt{\frac{\kappa}{R} \left(\frac{2}{\kappa+1}\right)^{\frac{\kappa+1}{\kappa-1}}} & , \text{ if } \frac{P_d}{P_u} \leq P_{cr} \text{ (sonic)} \end{cases} \quad (4.33)$$

where C_f is discharge coefficient, A_v is the effective are of valve orifice.

$$A_v = \frac{\pi x_s^2}{4} \quad (4.34)$$

$$x_s = C_v u \quad (4.35)$$

where C_v is the valve constant.

Valve model by Endler Require fitting constants and generally system identification. Mass flow rates are given by following equations:

$$\begin{aligned}\dot{m}_A(u, p_A) &= g_1(p_A, \text{sign}(u)) \arctg(2u) \\ \dot{m}_B(u, p_B) &= g_2(p_B, \text{sign}(u)) \arctg(2u)\end{aligned}\tag{4.36}$$

where g_1, g_2 are signal functions given:

$$\begin{aligned}g_1(p_A, \text{sign}(u)) &= \beta \Delta p_A = \begin{cases} (p_s - p_A) \beta^{ench} & , \text{ if } u \geq 0 \\ (p_A - p_0) \beta^{esv} & , \text{ if } u < 0 \end{cases} \\ g_2(p_B, \text{sign}(u)) &= \beta \Delta p_B = \begin{cases} (p_s - p_B) \beta^{ench} & , \text{ if } u < 0 \\ (p_B - p_0) \beta^{esv} & , \text{ if } u \geq 0 \end{cases}\end{aligned}\tag{4.37}$$

where $\beta^{ench}, \beta^{esv}$ are constant coefficients. For fitting model stop piston (speed of piston is null). This mean that volume is constant. We can measure flow rate \dot{m} versus input voltage u with given pressure difference.

Valve dead-zone For more precision control and modeling of the valve system, valve dead-zone can be used 4.47.

$$u_z = \begin{cases} g_z(u) < 0 & , \text{ if } u \leq u_n \\ 0 & , \text{ if } u_n < u < u_p \\ h_z(u) > 0 & , \text{ if } u \geq u_p \end{cases}\tag{4.38}$$

4.5 Mechanical assembly

4.5.1 Equation of motion

The motion of the pneumatic piston mechanism describes in terms of the general 1dof dynamical equation 4.48.

$$m\ddot{x} + b\dot{x} + kx = u\tag{4.39}$$

In the case of the pneumatic piston, the equation 4.48 transforms into an equation 4.49.

$$(M + M_L)\ddot{x} + F_{damp} + F_g + F_{hs} = F_p\tag{4.40}$$

Where M represents a mass of the all moveable part of the piston, M_L is load mass, F_g gravity force acting to mechanical moving assembly, F_{hs} - models endpoints (hard stop), F_{damp} represents shock absorbers acted at endpoints, F_p is a force produced by the pneumatic piston 4.50.

$$F_p = P_A S_A - P_B S_B - P_0 S_0\tag{4.41}$$

4.5.2 Hard stop

Hard stop can be represented as spring and dumps:

$$F_{HS} = \begin{cases} K_p(x - g_p) + D_p v & \text{for } x \geq g_p \\ 0 & \text{for } g_n < x < g_p \\ K_n(x - g_n) + D_n v & \text{for } x \leq g_n \end{cases} \quad (4.42)$$

4.5.3 Shock Absorbers

4.5.4 Friction

Friction force can be modeled in the different ways.

TO MUCH 4.52.

$$F_f = \begin{cases} C\dot{x} + \left(f_c + (f_s - f_c)e^{-\left(\frac{\dot{x}}{v_s}\right)^\delta} \right) \text{sign}(\dot{x}) & , \text{ if } \dot{x} \leq v_e \\ \mu\dot{x} & , \text{ if } \dot{x} > v_e \end{cases} \quad (4.43)$$

where C - viscous friction coefficient, f_c - Coulomb friction, f_s - maximum static friction, μ - dynamic friction factor, v_s - Stribeck velocity, δ - arbitrary index, v_e critical velocity.

4.6 Sensors Modeling

- Sensors models

4.7 Parameter identification

4.7.1 Mechanical assembly

In mechanical system there is F_f force represented by frictions accruing in the system. This force can be modeled by different friction models with respect to $??$. Friction force parameters can be estimated using "gray-box" method. Using \dot{m} mass flow data versus x position measured on real assembly and use these data as an input and output, we can fit F_f . Simplify model can contain TODO:

- F_C static friction
- C_v viscous
- C_p Pressure difference

4.7.2 Cylinder

Dead volume: $p_1 V_1^n = p_2 V_2^n$ or datasheet.

4.7.3 Valve

For valve system there are two parameters that need to be estimated. According to equation 4.53 with constant p_1 (pressure supply) and p_2 (atmospheric pressure), we can estimate C if we neglect Valve Spool dynamic. If in experiment we determine that spool dynamic necessary to include. We provide same experiment with spool model including

to "Gray-box" fitting model.

$$\dot{m} = \boldsymbol{u}(x_s) \boldsymbol{C} p_1 \sqrt{\frac{2}{RT_1}} \cdot \psi\left(\frac{p_2}{p_1}\right) \quad (4.44)$$

5 Alternative modeling techniques

This chapter deals with other possibilities of modeling the technical system, particularly the double-acting pneumatic piston. Physical modeling and data-driven modeling methods were examined in terms of suitability for applying FDI and PdM strategies.

5.1 Physical Modeling

Physical modeling operates with models with a compiled layout that matches the structure of the different physical domains. In this type of software, it is possible to combine different domains to create a complex system model.

Matlab/Simulink provides a physical modeling library, Simscape, that meets the above specifications. Using Simscape software, the user combines a model from different blocks representing different physical functions (spring, resistance, hydraulic valve), and connection links represent some types of energy flow.

5.1.1 The double-acting pneumatic piston in Simscape

In this part, the same assumption applies as in section ???. All the processes take place adiabatically, i.e., without heat exchange with the environment.

The resulting model was compiled using gas and mechanical domains ??.

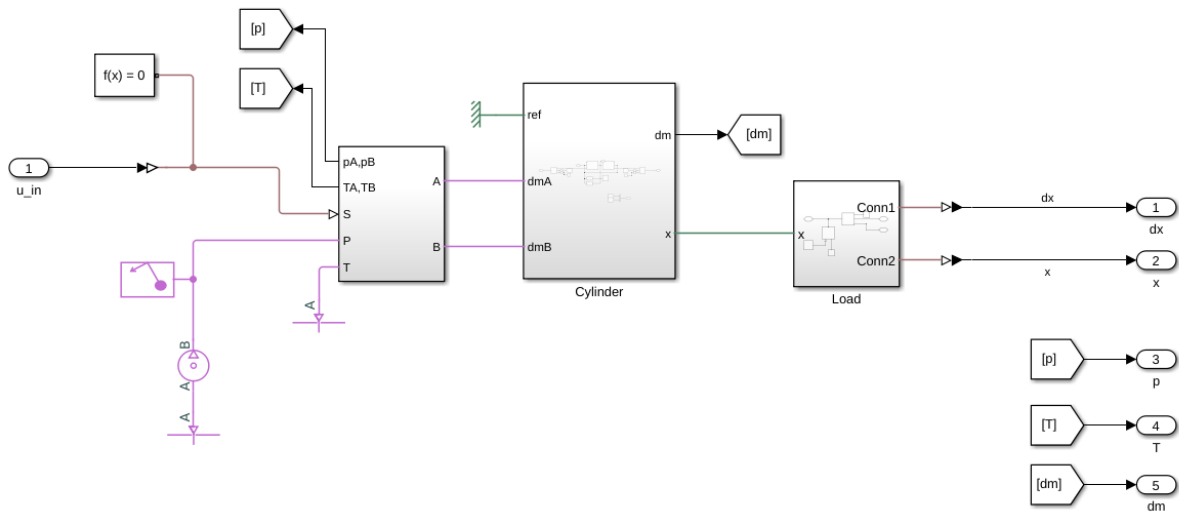


Figure 5.1: The double-acting pneumatic piston developed using Simscape software

5.1.2 Limitations

It is necessary to know well the parameters of the system.

For example, we need to have a precision-measured characteristic of flow control valve

adjustment in the form of a lookup table to use a throttle valve block.

Providing simplification and reduce the model to the only control valve, there are still a few parameters that are not available such as valve and dampers coefficients mentioned before ??.

The main problem is the computational complexity of the model compared with the first principle model. During the parameter estimation, the first principle model is much faster than the Simscape model and gives an option to experiment with different fault states analysis.

However, both models showed quite close behavior during testing with the same parameters; results shown in figure ??.

5.2 Data-Driven Models

Between data-driven modeling techniques include:

- Parametric
- Non-parametric

Non Parametric models include artificial neural networks and others.

6 Models comparison (2-3 pages)

6.1 First Principle Model

This model 6.1 was developed with respect to equations represented before.

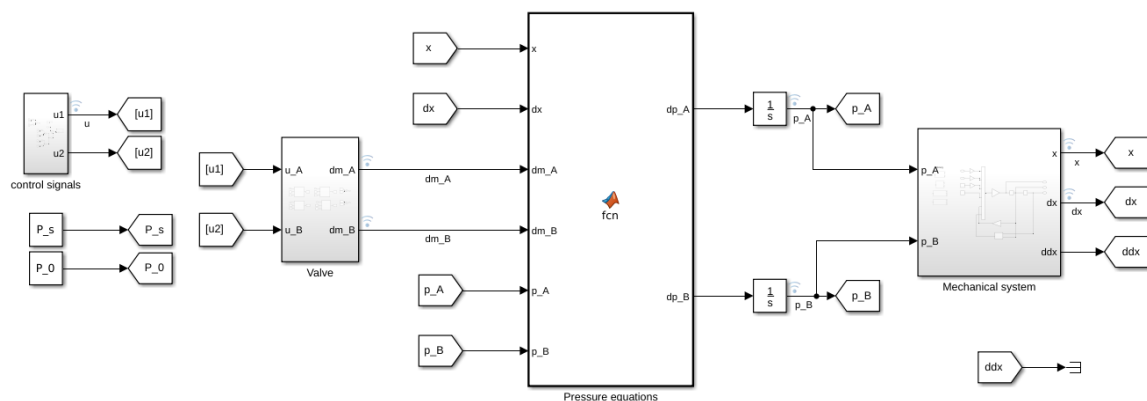


Figure 6.1: Simulink model based on equations

6.2 Alternative Modeling Techniques (3 pages)

Generally with dataset of input-output signals approximation model can be fit. Using System Identification Toolbox and modeled as Black-Box or Gray-Box models. This section attempted to fit some models using data from SimScape and Equation model presented before.

Fit approximation model make sense only if we know what to fit. Using signal process techniques and identify dominant signals that providing best classification features we will train models with respect to this signals.

6.2.1 Physical Model (SimScape)

Working, very slow. Equations are faster for estimation parameters. Model 6.2 was developed using SimScape toolbox.

6.2.2 State-space/ARX Models

Not working, Nonlinearities.

6.2.3 Hammerstein-Wiener Model

Working only for Position.

7 Signal-Based PdM (15 pages)

Signal-Based Predictive Maintenance.

General

Workflow

7.1 Sensors

Sensors comparison, cost.

7.2 Data exploring

Data has been collect from 8 types of sensors corresponding table 7.1:

Signal name	Description
FlowExtrusin	Flow sensor
FlowContraction	Flow sensor
AirPressure	Pressure sensor
AccelerometerMoving_axisY	Accelerometer
AccelerometerMoving_axisZ	Accelerometer
AccelerometerStat_axisY	Accelerometer
AccelerometerStat_axisZ	Accelerometer
	Temperature sensor
	Proximity sensor
	Strain gauge
	Microphones

Table 7.1: Measured signals

There are 660 measurements with different parameters system parameters 7.2.

Adjusting valve 1	
Adjusting valve 2	

Table 7.2: Device parameters

Dataset was divided to 5 main categories.

Data has been accumulated to ".mat" files. Each file contains signals from sensors during 10 seconds measurements with different pneumatic actuator configuration. Example results from one experiment are represented in figures ??, ??.

7.3 Data management

Data Ensembles Data files have been reshaped to Data Ensembles format used for Condition monitoring purposes. This format allows processing data without copying the whole dataset to memory at once but processes them one by one. In large datasets it gives an option to manipulate with data without problems with allocated memory.

Divided to 3 datasets:

- Train data
- Validation data
- Test data

7.4 Preprocessing

Measured signals require preprocessing concerning the preservation of the information base. For smoothing data Moving Average function were used. As an example, the figure ?? is shown the "raw" and filtered signals. The whole dataset of preprocessed data is relatively big. For time-saving, parallel computing was used for all computationally demanding parts of the code.

7.5 FDI methods

7.5.1 Line checking

We can use Proximity sensor time delay between input signal and upper proximity sensor signal to evaluate if there is some fault.

Same with Position, if not reach some end position, there is a fault.

Flow sensor, check if the float mean value is under some threshold, there is fault.

7.6 Condition Indicators extraction

For classification task purpose from the signals have been extracted statistical features such as mean, median, peak to peak value, etc. As a condition "FaultCode" variable were used. This variable represent configuration of pneumatic actuator during the measurement.

All calculated features were added to the dataset and were ranked by Kruskal-Wallis ANOVA algorithm. Following table ?? contain 5 first best features ranked for classification purpose.

Kruskal-Wallis is very suitable to ranking features before using PCA or SVD.

Selecting Condition Indicators There is a problem if we will deploy classification task with large features dataset. There are different possibilities to reduce data before train classification model or do a prediction. One of them is to rank a features by Analysis of Variation algorithm to evaluate a good representation features.

7.6.1 Microphones

Cheap, good results, but maybe problems with real life integration (noise from another machines). Another problem cannot be modeled in simulation system. For predictive

purposes require data from real model.

7.6.2 Encoder

Good results, useful in simulations and compare results with Digital Twin. Can be used in Model-Based CI. Digital twin can generate fault data, that will be applicable with encoder sensor.

7.6.3 Acceleration sensors

Not good, not bad. Can be used for classification task. But encoder has more accuracy information.

7.6.4 Proximity Sensors

Cheap. Very correlated features. Can not be used for classification. But suitable to detect binary classification (Health, Failed). Only statistical features, no Frequency domain.

7.6.5 Flow Sensors

Very expensive sensors. Not so good results.

7.6.6 Air Pressure

This sensor always used, to control pressure valve. But not good results. Maybe in combination with another sensor.

7.6.7 Strain Gauge

Expensive, Normal results of classification. But not suitable for Simulation Model.

7.6.8 Temperature

Good results on data. But only because Ambient temperature was changed between measurements. In one day it was warm, another colder :)

7.7 Classification Task

The main goal of the classification task is to train a model that can predict the "Fault-Code", or "Label" signalized about pneumatic actuator behavior by calculated features.

Using Kuskal-Wallis one way analysis of variance, features were ranked by importance with respect to correlation. This gives opportunity to reduce number of features before PCA analysis.

Principal component analysis (PCA) has been used to reduce the number of features and chose the best representants.

The trained model has been exported to **models/** directory.

8 PdM using a Simulation Model (10-15 pages)

8.1 Differences between Model-Based PdM and PdM using Digital Twin

There is a difference between using Model-Based PdM and using Simulation Model as a Digital Twin.

8.2 Using Digital Twin to Generate Fault Data

We can use Digital Twin to model situations that were not captured in the original dataset or if it is hard to model some cases with real-world hardware. As an example, we can model sensors fault such as sensor drift or complete signal loss.

8.3 Model-Based Condition Indicators

Model-Based approach is suitable when it's difficult to identify condition indicators using only signals. In some cases it's useful to fit some model from data and extract condition indicators as some system parameter.

8.3.1 Static and Dynamic Models

If the system behavior can be fit from the data as a static model, than we can extract condition variables from this model. For example, if model was fitting to a polynomial model, than polynomial coefficients can be use as condition indicators.

Signals showing dynamic behavior can be fitted to dynamic models such as State-Space or AR, ARX, NLARX (Nonlinear auto recursive model) and so on. Then condition indicators can be extracted as poles, zeros damping coefficients from estimated model.

8.3.2 Using Hammerstain-Weiner Model

Demo using Hammerstain-Wiener Model. Fit model to position signal and extract coefficients from model as Condition indicators. Classification.

8.4 Using Simulation Model for Residuals Estimation

Another option is using the Simulink model with **prediction error minimization function** to compute difference between Simulink model and measured data. From this difference we can separate fault condition and healthy operation.

8.4.1 Comparison with Nominal System Model

Same thing as section 8.4

Compare actual system behavior with system model. This will generate some error $e(t) = y(t) - \hat{y}(t)$. From this error residual can be generated in form $r(t) = \Phi(u_t, y_t, \varepsilon_t, v_t, d)$ and after some decision.

8.5 Using Digital Twin to Generate Prognostic Data

Another option is to use Digital Twin to generate a system degradation process. We can evaluate CI from sensor signal by changing a system's mechanical properties as friction or mass flow leakage. Another advantage is that we can design experiments on the model to evaluate what type of data we require from a real-world system to develop a robust algorithm.

8.6 RUL

Demo RUL using generated from model degradation dataset.

9 Conclusion

The goal of this thesis was to demonstrate and verify fault detection and predictive maintenance techniques on the double-acting pneumatic piston assembly as a case-study object.

9.1 Simulation Model

One of the outcomes from the thesis is a simulation model of the double-acting pneumatic piston system built based on differential equations from the pneumatic-mechanical domain, modeled and developed using Matlab/Simulink software. The simulation model was estimated with parameters of healthy system behavior. However, there is an option to reestimate parameters to fault state and simulate the system in a fault condition.

Due to the available measured data and significantly nonlinear dynamics of the system, the simulation model shows good agreement with the measured data. In contrast to the model built using Simulink/Simscape library, it is distinctly less computationally expensive while maintaining numerical stability. These facts are fundamental when parameter estimation is in progress.

The simulation model was used to experiment with the system's behavior in different conditions, model fault situations and generate data to design and develop robust predictive maintenance algorithms.

9.2 Signal-Based PdM

Another outcome is verifying the possibility of classification and detection of a fault condition applying predictive maintenance techniques, using signal-based and model-based methods.

The experiments were performed on a dataset measured on a demonstration device using seven types of sensors.

A signal-based method is based on the extraction of useful information directly from the signal in time-frequency domains. Each sensor required an individual approach for preprocessing, extracting features, ranking features and building the classification models. But generally, there is minimal preprocessing needed to keep the possible helpful information.

The table 9.1 contains the comparison of sensors in 2 categories, accuracy performed in the test dataset and sensor cost. The graph 9.1 visualizes these data.

Surprisingly, all sensors showed an accuracy of more than 75 %. Microphones offer excellent performance from a cost/accuracy perspective, and they are suitable for installation and maintenance.

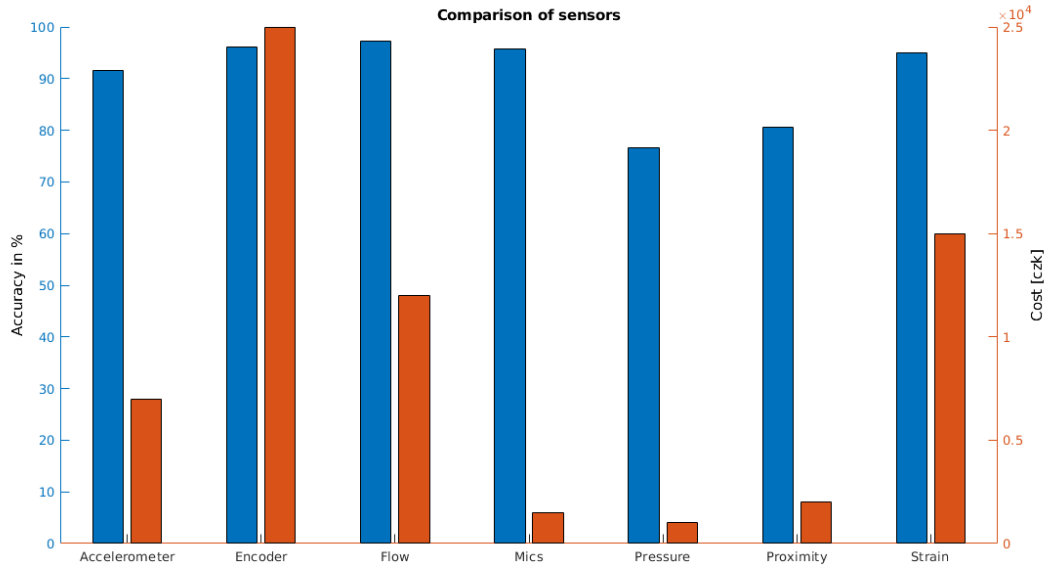


Figure 9.1: Comparison of sensors from accuracy/cost perspective

Sensor	Acc	Encoder	Flow	Mics	Pressure	Proximity	Strain
Accuracy [%]	91.6	96.1	97.2	95.8	76.6	80.5	95.0
Cost [czk]	2x 3500	25000	6000	3x 500	1000	2x 1000	15000

Table 9.1: Comparison of sensors from accuracy/cost perspective

9.3 Model-Based PdM

The next part of this thesis was to apply model-based methods and using a simulation model for predictive maintenance algorithms. These algorithms are practical when it is hard to extract useful information using a signal-based method. Or it is suitable in some cases where we understand the system dynamics and know how to exploit some system variables as condition indicators.

The use of the method of extraction features in the form of a Nonlinear system identification model coefficient, specifically with the Hammerstein-Wiener model, did not give reliable results. Extracted features have no statistical dependence, and it is impossible to predict fault type using this method on the measured data from the pneumatic piston as a case study.

On the other hand, the residual estimation using the simulation model showed excellent results. The measured position signal was compared with the signal from the simulation model in normal behavior. This residual signal was used to classify the fault condition and achieve 99 % on a smaller dataset. But given the results obtained using the signal-based method, the residual estimation method may seem unnecessary. In this particular case, from a practical point of view, the improvement of the result by a few percent does not bring fundamental changes, but the calculation time increases significantly.

The possibility of modeling and simulation sensor faults was also verified using the simulation model. Although it is challenging to collect fault data from the sensor in real-life conditions, fault data can be generated from the simulation model and even combined with the primary dataset to create a synthetical dataset.

9.3.1 RUL

One of the main goals of predictive maintenance is to estimate the remaining useful life. The original dataset does not contain a record of historical data that shows degradation behavior.

A common problem in the maintenance of pneumatic actuators is the leakage of air from the chamber where the piston is located. This situation was modeled on the simulation model and generated data were used for RUL estimation.

The generated dataset contains 25 simulations with different failure dynamics. Each simulation includes a different number of cycles depending on the failure dynamic before the system failure occurs. Each cycle contains a 10-second measurement of the system's response. In the experiment, a flow signal was chosen as an object of interest. From the flow signal, the shape factor parameter was calculated and used as a condition indicator.

The outcome is that it is possible to estimate the remaining useful life on generated degradation dataset by using the residual similarity model, pairwise similarity model and linear degradation model. The prediction results are satisfying.

9.4 Further Development

As a further development, it would be appropriate to estimate the modeled system parameters piecewise to improve the results, emphasizing the characteristics of throttle valves and dampers with adjustments.

Perform air leak fault condition measurements and collect historical degradation data from a real pneumatic piston. Subsequently, evaluate the dynamics of the failure caused by the air leak. Verify the possibility of estimating the remaining useful life using a flow sensor. It could be an interesting case study to verify a possibility of RUL estimation using microphones. If the performance of the available sensors is deficient, the pressure measurements in the chamber can be performed. The pressure in the chamber is directly dependent on the air leakage from the chamber, as presented in equation ???. An example of pressure changes from the simulation model is shown in figure ??.

List of Abbreviations

LWL Locally Weighted Learning

LS Least Squares Method

RLS Recursive Least Squares Method

RFWR Receptive Field Weighted Regression

LOLIMOT Local Linear Model Tree

EGR Exhaust Gas Recirculation

PID Proportional-Integrational-Derivative controller