

ADJOINT INVERSION OF ATMOSPHERIC DUST SOURCES  
FROM SATELLITE OBSERVATIONS

by

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Abstract to be filled ...

## **DEDICATION**

To the memory of my grandparents

**Zhaoxiang Xu**

and

**Shi Zhao Xu**

## ACKNOWLEDGMENTS

Arma virumque cano, Troiae qui primus ab oris Italiam, fato profugus, Laviniaque venit  
litora, multum ille et terris iactatus et alto vi superum saevae memorem Iunonis ob iram;  
multa quoque et bello passus, dum conderet urbem, inferretque deos Latio, genus unde  
Latinum, Albanique patres, atque altae moenia Romae.

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## CHAPTER 1

### INTRODUCTION

#### 1.1 Background and Motivation

Mineral dust represents the second productive component of atmospheric aerosol following after the sea-salt aerosol [Textor *et al.*, 2006]. Naturally, these mineral particles are produced mainly by the aerolian wind erosion in arid and semiarid areas. Anthropogenic sources of mineral aerosols include road dust and mineral dust due to land changes by human activities [References check with my proposal]. Mineral aerosols can place important impacts on the Earth system through interactions with atmospheric chemistry, solar and terrestrial radiation, clouds, and biosphere [Shao *et al.*, 2011]. An accurate representation of dust cycle in the Earth climate model is thus critical to assess these impacts. However, significant uncertainties prevail in quantifying mineral dust sources due to poor understanding of dust uplifting mechanisms and the lack of in situ measurements over the desert region.

Parameterization of processes such as saltation bombardment and sandblasting in a chemistry transport model (CTM) requires knowledge of many parameters that are poorly characterized, including surface wind speed, soil moisture, soil texture, and surface state [Tegen and Fung, 1994; Ginoux *et al.*, 2001; Zender *et al.*, 2003]. Not surprisingly, recent estimates in CTMs span from a few hundreds to over 4000 Tg for annual global dust emissions [Huneus *et al.*, 2011] and can vary by a factor as large as 10 at regional scales for the same dust event(s) [Uno *et al.*, 2006]. An observation-based approach, therefore, is

needed to reduce these large uncertainties in estimate of dust emissions and further improve the global modeling of atmospheric dust distribution and their impacts.

### **1.1.1 Impacts of dust aerosols**

Atmospheric aerosols play a crucial role in the global climate change. They affect earth energy budget directly by scattering and absorbing solar and terrestrial radiation, and indirectly through altering the cloud formation, lifetime, and radiative properties [Haywood and Boucher, 2000; Ramanathan et al., 2001]. However, quantification of these effects in the current climate models is fraught with uncertainties. The global average of aerosol effective radiative forcing (ERF) were estimated to range from -0.1 to -1.9 Wm<sup>2</sup> with the best estimate of -0.9 Wm<sup>2</sup> [Boucher et al., 2013], indicating that the cooling effects of aerosol might counteract the warming effects of 1.820.19 Wm<sup>2</sup> caused by the increase of carbon dioxide since the industrial revolution [Myhre et al., 2013]. The climate effects of aerosol particles depend on their geographical distribution, optical properties, and efficiency as cloud condensation nuclei (CCN). Key quantities pertain to the aerosol optical and cloud-forming properties include particle size distribution (PSD), chemical composition, mixing state, and morphology [Boucher et al., 2013]. While the daily aerosol optical depth (AOD) can be well measured from current satellite and ground-based remote sensing instrumentations [e.g., Holben et al., 1998; Kaufman et al., 2002], the accurate quantification of aerosol ERF is in no small part hindered by our limited knowledge about the aerosol PSD and refractive index (describing chemical composition and mixing state). To fully understand the role of aerosol particles in the global climate change, further development in observations along with retrieval algorithms for these aerosol microphysical properties from different platforms are thus highly needed [Mishchenko et al., 2004], and the focus of this two-part series study is the characterization of aerosol properties from ground-based passive remote sensing

[*Henze et al.*, 2007].

### 1.1.2 Parameterizations of dust emissions

### 1.1.3 Observations of dust aerosols

In the last decade, the in situ and satellite remote sensing observations have greatly enhanced our understanding of the spatiotemporal variations of dust aerosols.

### 1.1.4 Recent inverse modeling studies for improving dust emission

In parallel with the advancement of in situ and remote sensing observations of dust aerosols, techniques have been developed to use these observations as constraints on dust sources.

*Koven and Fung* [2008] have investigated ...

Source function can be estimated based topography [*Ginoux et al.*, 2001],

## 1.2 Main Goals of This Work

Based on the preceding discussions, this work aims at improved estimates of global dust emissions through adjoint integration of AOD retrievals from multiple satellite platforms (MODIS and MISR) with a CTM (GEOS-Chem). The overall goal is to conduct the satellite-based global model estimates of atmospheric dust distribution, and thereby advance the understanding of the impacts of atmospheric mineral dust on climate change and air quality. To accomplish this goal, this work pursues the following specific objectives:

- Develop a top-down numerical inversion scheme for constraining global dust emissions with a combined use of multi-platform AOD products and CTM adjoint, which also includes the sensitivity and error budget analysis for the optimization.

- Apply the inversion scheme developed in step 1 for a one year (i.e. 2008) of dust emissions with level 3 quality-controlled MODIS DB and MISR AOD products.
- A long-term (from 2001 to 2010) analysis of dust emissions will follow, along with studies on the seasonal and inter-annual variability of dust emissions, loadings, and direct radiative effects.
- Wherever possible, ground-based and field data will be used to validate and analyze the uncertainties of the inversion results.

Although the adjoint optimization technique we use is similar to that in Dubovik et al. [2008] and Yumimoto et al. [2007], this study differs from the those previous studies in that: (a) Multi-platform AOD products utilized to optimize dust emissions can provide tremendous dust information in fine spatial and temporal scales; (b) This study uses the satellite AOD retrievals only over and near dust source regions where dust has been transported a short distance with minimal influence of precipitation and anthropogenic aerosols; (c) Optimization of the long-term dust emissions is conducted for every grid box as a function of time (e.g., on the weekly or month scale). Although the criteria for separation of a natural and anthropogenic dust source is not clear and sometime controversial in the literature [Denman et al., 2007], especially when considering the climatic feedback on dust emissions [Zhang et al., 2002], we believe that satellite-based optimization of global dust emissions in the last decade could improve our modeling of dust radiative forcing and potentially illuminate anthropogenic components of dust sources and loadings, currently estimated at 0-20% though values as large as 50% has been postulated [Ginoux et al., 2011; Tegen et al., 1996; 2004; Mahowald et al., 2004,].

## 1.3 Organization of This Dissertation

We describe the GEOS-Chem simulation of mineral dust in Chapter 2 with emphasizing the physical parameterization of dust sources, after which we present the implements for the AOD observation operator and the adjoint capacity of dust emission within the GEOS-Chem adjoint model in Chapter 3. In chapter 4, we present a case study on optimizing the dust emission estimates from the satellite (MODIS) radiances over the eastern Asia, in which we also attempt to simultaneously constrain the anthropogenic emissions of the  $\text{SO}_2$ ,  $\text{NO}_2$ ,  $\text{NH}_3$ , and carbaceous aerosols together with the dust aerosols. In chapter 5, we optimize the dust source parameterization from multi-satellite AOD products, particularly in improving the the estimates of soil erodibility and wind friction threshold for sand saltation over the northern Africa. Finally, we summarize the dissertation and outlook future work in Chapter 6.

## CHAPTER 2

### MODELING OF ATMOSPHERIC DUST

*Overview* This chapter presents how the physical process that mineral dust involved are quantitatively represented in a chemistry transport model, i.e., the GEOS-Chem model. These processes include the uplifting of dust from soil surface, the transport within the atmosphere, and deposition of dust to the surface.

## 2.1 Modeling of Dust Emission

### 2.1.1 Physical parameterization of the dust emission

The dust emission, aerolian wind erosion that results in production of mineral aerosols from soil grains, involves complex and nonlinear processes that are governed by the meteorology as well as by the state and properties of the land surfaces. Laboratory [Iversen and White, 1982] and field [Shao et al., 1996; Zender et al., 2003] wind tunnel studies suggested that dust is primarily injected into the atmosphere during the sandblasting caused by the saltation bombardment [Alfaro and Gomes, 2001; Grini et al., 2002]. The clay- and silt-sized soil particles have strong inter-cohesive force... The saltation of sand-sized particles ... requires least threshold of wind speed...

The most important factors include wind friction velocity and its threshold for saltation, vegetation cover, soil mineralogy, and surface soil moisture.



In this study, the physical parameterization of dust emission is taken from a Dust Entrainment and Deposition (DEAD) model developed by Zender et al [2003a]. The DEAD scheme calculates the wind friction threshold ( $u_{*t}$ ) as a function of the Reynolds number following Iversen and White [1982] and Marticorena and Bergametti [1995]. Three processes are also considered to modify the  $u_{*t}$ : the drag partitioning owing to the momentum captured by nonerodible roughness elements, the Owen effect, and moisture inhibition. The horizontal saltation flux ( $Q_s$ ) that is defined as the vertical integral of the stream-wise soil flux density is calculated following the theory of White [1979]:

$$Q_s(u_*, u_{*t}) = \frac{c_s \rho}{g} u_*^3 \left(1 - \frac{u_{*t}}{u_*}\right) \left(1 + \frac{u_{*t}}{u_*}\right)^2, \quad (2.1)$$

where,  $c_s = 2.61$ ,  $\rho$  is the air density at surface level, and  $u_*$  is the wind friction velocity. Thus, it assumes the saltation flux is quasi-linearly the  $u_*^3$  when  $u_*$  exceeds the  $u_{*t}$ . It also neglect the dependence of total  $Q_s$  on the soil size.

the total vertical mass flux of dust into transport bin  $j$  is

$$E_{d,j} = \begin{cases} T_0 A_m S \alpha Q_s \sum_{i=1}^3 M_{i,j} & \text{if } u_* \geq u_{*t}, \\ 0 & \text{if } u_* < u_{*t}, \end{cases} \quad (2.2)$$

where,  $T_0$  is a tuning factor chosen to adjust the global amount,  $A_m$  is the fraction of bare soil exposed in a model grid cell,  $S$  is called "erodibility" or "preferential source function",  $\alpha$  is the sandblasting mass efficiency factor which depends on the mass fraction of clay particles in the parent soil, and  $M_{i,j}$  indicates the mass fraction of  $i$ th source mode carried into the  $j$ th transport mode.

### 2.1.2 Development of the wind speed distribution

In order to incorporate the variability of wind speed due to the subgrid scale circulations, we introduce a probability density function (PDF) of the wind speed within each grid box. The dust emission is computed according to the fraction of the PDF that exceeds the threshold value:

$$E_d = \int_{u_{*t}}^{\infty} E(u_*) p(u_*) du_*. \quad (2.3)$$

Where  $E(u_*)$  is the emission as a function of the surface wind friction velocity, and  $p(u_*)$  is the PDF of  $u_*$  within the grid box.

The PDF for surface wind speeds can be represented by a Weibull distribution [Justus et al., 1978] and has been used in recent studies [e.g., Grini and Zender, 2004; Grini et al., 2005; Ridley et al., 2013] to characterize the subgrid dust emissions. The PDF of a Weibull random variable  $x$  is described by a shape factor  $k$  and a scale factor  $c$ :

$$p(x; c, k) = \frac{k}{c} (x/c)^{k-1} \exp \left[ -(x/c)^k \right], \text{ for } x > 0. \quad (2.4)$$

One of the advantages in using the Weibull PDF is that it is analytically integrable with the cumulative distribution function:

$$P(x \leq x_1; c, k) = 1 - \exp \left[ -(x/c)^k \right]. \quad (2.5)$$

Based on above cumulative function, we cut off wind speeds with a minimum and a maximum wind speed to retain the central 98% of the wind PDF. As a result, the lower and

upper limits of wind speed are respectively:

$$x_l = c [-\ln 0.99]^{\frac{1}{k}} \quad (2.6)$$

$$x_u = c [-\ln 0.01]^{\frac{1}{k}} \quad (2.7)$$

Parameters  $k$  and  $c$  can be estimated from the statistical mean  $\bar{x}$  and variance  $\sigma^2$  (of  $x$ ), since they are related to  $\bar{x}$  and  $\sigma^2$ :

$$\bar{x} = c\Gamma(1 + 1/k) \quad (2.8)$$

$$\sigma^2 = c^2 [\Gamma(1 + 2/k) - \Gamma^2(1 + 1/k)] \quad (2.9)$$

Where  $\Gamma()$  is a gamma function. According to Justus et al. [1978],  $k$  and  $c$  can be best estimated by:

$$k = (\sigma/\bar{x})^{-1.086} \quad (2.10)$$

$$c = \bar{x} [\Gamma(1 + 1/k)]^{-1} \quad (2.11)$$

Thus, the only parameter that must be supplied beyond the mean wind speed is the variance ( $\sigma^2$ ) of subgrid wind speeds within the grid box. Cakmur et al [2004] calculated the  $\sigma^2$  by incorporating information from the parameterizations of the planetary boundary layer along with dry and moist convection. Here, we follow Grini and Zender [2004] and Grini et al [2005] that assumed an approximation of  $k$  based on Justus et al. [1978]:

$$k = 0.94u_*^{\frac{1}{2}} \quad (2.12)$$

Finally, the dust emission flux is calculated by

$$E_{d,j} = A_m S \alpha \left( \sum_{i=1}^3 M_{i,j} \right) \frac{c_s \rho}{g} \int_{u_{*l}}^{u_{*u}} u_*^b \left( 1 - \frac{u_{*l}}{u_*} \right) \left( 1 + \frac{u_{*l}}{u_*} \right)^2 p(u_*) du_*. \quad (2.13)$$

Where  $u_{*u}$  is the upper limit of wind speed determined by equation (2.7).

## 2.2 Modeling of Dust Transport and Deposition

## CHAPTER 3

### ADJOINT INVERSION OF DUST EMISSIONS

#### 3.1 The Inversion Framework

Let  $\mathbf{x}$  denote a state vector of  $n$  parameters to be constrained and  $\mathbf{y}$  an observation vector assembled by  $m$  measurements, and let  $\mathbf{F}$  indicate a forward model that describes the physics of the measurement process. Then, we can express the relationship between the observation vector and the state vector as

$$\mathbf{y} = \mathbf{F}(\mathbf{x}) + \boldsymbol{\epsilon}, \quad (3.1)$$

where  $\boldsymbol{\epsilon}$  is an experimental error term that includes observation noise and forward modeling uncertainty.

For this work, the observation vector  $\mathbf{y}$  comprises aerosol mass concentrations or aerosol optical depth (AOD).

## 3.2 GEOS-Chem Adjoint

## 3.3 Implement Adjoint of DEAD

In simple, The dust emission flux considering subgrid wind speeds in equation (2.13) can be written

$$E_{d,j} = C_j S' \int_{u_{*f}}^{u_{*u}} Q_s(u_*, u_{*f}, b) p(u_*) du_*, \quad (3.2)$$

where  $S' = S\alpha$ , and  $C_j = A_m \sum_{i=1}^3 M_{i,j}$ . We combine the erodibility  $S$  and sandblasting factor  $\alpha$ , because both of them not only are related to the soil texture but also describe the strength efficiency of dust emission. Given the the state of land surface and the properties of surface soil, the dust emission is a function of  $S'$ ,  $b$ , and  $u_{*f}$ .

Here we implement the adjoint calculation for three parameters, i.e.,  $S'$ ,  $b$ , and  $u_{*f}$ . This implementation requires the partial derivatives of  $E_{d,j}$  with respect to these parameters (when  $u_* \geq u_{*f}$ ):

$$\frac{\partial E_{d,j}}{\partial S'} = \frac{E_{d,j}}{S'}, \quad (3.3)$$

$$\frac{\partial E_{d,j}}{\partial b} = C_j S' \int_{u_{*f}}^{u_{*u}} \frac{\partial Q_s}{\partial b} p(u_*) du_*, \quad (3.4)$$

$$\frac{\partial E_{d,j}}{\partial u_{*f}} = C_j S' \int_{u_{*f}}^{u_{*u}} \frac{\partial Q_s}{\partial u_{*f}} p(u_*) du_*. \quad (3.5)$$

These gradients of  $Q_s$  in equations (3.4 and 3.5) can be calculated by

$$\frac{\partial Q_s}{\partial b} = Q_s(u_*, u_{*f}, b) \ln u_* \quad (3.6)$$

$$\frac{\partial Q_s}{\partial u_{*f}} = \frac{c_s \rho}{g} u_*^b \left[ \frac{1}{u_*} - \frac{2u_{*f}}{u_*^2} - \frac{3u_{*f}^2}{u_*^3} \right] \quad (3.7)$$

## CHAPTER 4

### OPTIMIZING DUST EMISSION ESTIMATES

#### **4.1 Introduction**

#### **4.2 Constraints from Satellite Radiances**

#### **4.3 Case Study of Eastern Asian Dust**

#### **4.4 Simultaneous Inversion for Species-Specified Aerosol Sources**

#### **4.5 Summary**

## CHAPTER 5

### OPTIMIZING DUST SOURCE PARAMETERIZATION

#### **5.1 Introduction**

#### **5.2 Constraints from Multi-Satellite Observations**

#### **5.3 Experiment Design**

#### **5.4 Constrained Dust Emission Scheme**

#### **5.5 Validations**

#### **5.6 Summary**



## CHAPTER 6

### SUMMARY AND OUTLOOK

#### **6.1 Summary of the Dissertation**

#### **6.2 Main Conclusions of This Work**

#### **6.3 Outlook and Future Work**

APPENDIX A

**ABBREVIATIONS AND ACRONYMS**

## APPENDIX B

### **SYMBOLS**

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