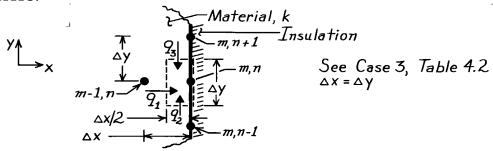
## **PROBLEM 4.34**

KNOWN: Plane surface of two-dimensional system.

**FIND:** The finite-difference equation for nodal point on this boundary when (a) insulated; compare result with Eq. 4.42, and when (b) subjected to a constant heat flux.

## **SCHEMATIC:**



**ASSUMPTIONS:** (1) Two-dimensional, steady-state conduction with no generation, (2) Constant properties, (3) Boundary is adiabatic.

**ANALYSIS:** (a) Performing an energy balance on the control volume,  $(\Delta x/2)\cdot\Delta y$ , and using the conduction rate equation, it follows that

$$\dot{E}_{in} - \dot{E}_{out} = 0$$
  $q_1 + q_2 + q_3 = 0$  (1,2)

$$k\left(\Delta y\cdot 1\right)\frac{T_{m-1,n}-T_{m,n}}{\Delta x}+k\left[\frac{\Delta x}{2}\cdot 1\right]\frac{T_{m,n-1}-T_{m,n}}{\Delta y}+k\left[\frac{\Delta x}{2}\cdot 1\right]\frac{T_{m,n+1}-T_{m,n}}{\Delta y}=0. \quad (3)$$

Note that there is no heat rate across the control volume surface at the insulated boundary. Recognizing that  $\Delta x = \Delta y$ , the above expression reduces to the form

$$2T_{m-1,n} + T_{m,n-1} + T_{m,n+1} - 4T_{m,n} = 0. (4) <$$

The Eq. 4.42 of Table 4.2 considers the same configuration but with the boundary subjected to a convection process. That is,

$$\left(2T_{m-1,n} + T_{m,n-1} + T_{m,n+1}\right) + \frac{2h\Delta x}{k}T_{\infty} - 2\left[\frac{h\Delta x}{k} + 2\right]T_{m,n} = 0.$$
(5)

Note that, if the boundary is insulated, h = 0 and Eq. 4.42 reduces to Eq. (4).

(b) If the surface is exposed to a constant heat flux,  $q_0''$ , the energy balance has the form  $q_1 + q_2 + q_3 + q_0'' \cdot \Delta y = 0$  and the finite difference equation becomes

$$2T_{m-1,n} + T_{m,n-1} + T_{m,n+1} - 4T_{m,n} = -\frac{2q_0'' \Delta x}{k}.$$

**COMMENTS:** Equation (4) can be obtained by using the "interior node" finite-difference equation, Eq. 4.29, where the insulated boundary is treated as a symmetry plane as shown below.

$$m,n+1$$
 Plane of symmetry (insulated surface)

 $m-1,n$   $\bullet$   $m,n$   $\bullet$   $m-1,n$ 
 $m,n-1$