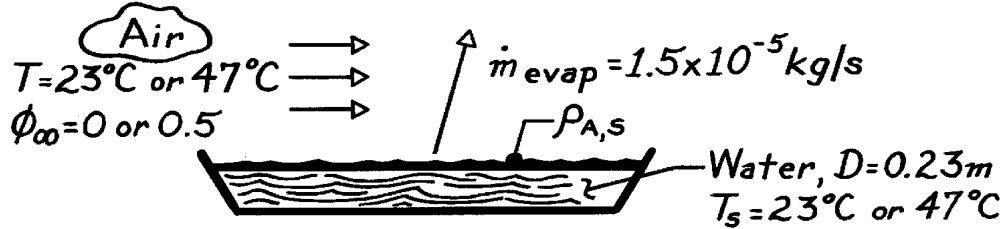


PROBLEM 6.43

KNOWN: Evaporation rate from pan of water of prescribed diameter. Water temperature. Air temperature and relative humidity.

FIND: (a) Convection mass transfer coefficient, (b) Evaporation rate for increased relative humidity, (c) Evaporation rate for increased temperature.

SCHEMATIC:



ASSUMPTIONS: (1) Water vapor is saturated at liquid interface and may be approximated as a perfect gas.

PROPERTIES: Table A-6, Saturated water vapor ($T_s = 296\text{K}$): $\rho_{A,\text{sat}} = v_g^{-1} = (49.4 \text{ m}^3/\text{kg})^{-1} = 0.0202 \text{ kg/m}^3$; ($T_s = 320 \text{ K}$): $\rho_{A,\text{sat}} = v_g^{-1} = (13.98 \text{ m}^3/\text{kg})^{-1} = 0.0715 \text{ kg/m}^3$.

ANALYSIS: (a) Since evaporation is a convection mass transfer process, the rate equation has the form $\dot{m}_{\text{evap}} = \bar{h}_m A (\rho_{A,s} - \rho_{A,\infty})$ and the mass transfer coefficient is

$$\bar{h}_m = \frac{\dot{m}_{\text{evap}}}{(\pi D^2/4)(\rho_{A,s} - \rho_{A,\infty})} = \frac{1.5 \times 10^{-5} \text{ kg/s}}{(\pi/4)(0.23 \text{ m})^2 0.0202 \text{ kg/m}^3} = 0.0179 \text{ m/s} <$$

with $T_s = T_\infty = 23^\circ\text{C}$ and $\phi_\infty = 0$.

(b) If the relative humidity of the ambient air is increased to 50%, the ratio of the evaporation rates is

$$\frac{\dot{m}_{\text{evap}}(\phi_\infty = 0.5)}{\dot{m}_{\text{evap}}(\phi_\infty = 0)} = \frac{\bar{h}_m A [\rho_{A,\text{sat}}(T_s) - \phi_\infty \rho_{A,\text{sat}}(T_\infty)]}{\bar{h}_m A \rho_{A,\text{sat}}(T_s)} = 1 - \phi_\infty \frac{\rho_{A,\text{sat}}(T_\infty)}{\rho_{A,\text{sat}}(T_s)}.$$

$$\text{Hence, } \dot{m}_{\text{evap}}(\phi_\infty = 0.5) = 1.5 \times 10^{-5} \text{ kg/s} \left[1 - 0.5 \frac{0.0202 \text{ kg/m}^3}{0.0202 \text{ kg/m}^3} \right] = 0.75 \times 10^{-5} \text{ kg/s.} <$$

(c) If the temperature of the ambient air is increased from 23°C to 47°C , with $\phi_\infty = 0$ for both cases, the ratio of the evaporation rates is

$$\frac{\dot{m}_{\text{evap}}(T_s = T_\infty = 47^\circ\text{C})}{\dot{m}_{\text{evap}}(T_s = T_\infty = 23^\circ\text{C})} = \frac{\bar{h}_m A \rho_{A,\text{sat}}(47^\circ\text{C})}{\bar{h}_m A \rho_{A,\text{sat}}(23^\circ\text{C})} = \frac{\rho_{A,\text{sat}}(47^\circ\text{C})}{\rho_{A,\text{sat}}(23^\circ\text{C})}.$$

$$\text{Hence, } \dot{m}_{\text{evap}}(T_s = T_\infty = 47^\circ\text{C}) = 1.5 \times 10^{-5} \text{ kg/s} \frac{0.0715 \text{ kg/m}^3}{0.0202 \text{ kg/m}^3} = 5.31 \times 10^{-5} \text{ kg/s.} <$$

COMMENTS: Note the highly nonlinear dependence of the evaporation rate on the water temperature. For a 24°C rise in T_s , \dot{m}_{evap} increases by 350%.