## Notes for libEMMI\_MGFD

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June 23, 2024

#### 1 Input parameters

- mode: mode=0, forward modelling; mode=1, 3D CSEM inversion;
- istretch: istretch=1, nonuniform grid stretching; istretch=0, no grid stretching;
- addair: addair=1, add air layers on top of input model; addair=0, extending the model using topmost value without adding air layers;
- freqs: the frequencies used for CSEM modelling and inversion, a number of frequencies can be given by comma separated values;
- chsrc: source channels (i.e. Ex, Ey, Ez, Hx, Hy, Hz)
- chrec: receiver channels (i.e. Ex, Ey, Ez, Hx, Hy, Hz)
- nx,ny,nz: number of intervals in x, y and z axes for input resistivity model on equispaced FD grid;
- dx,dy,dz: grid spacing of input resistivity model on equispaced FD grid;
- ox, oy, oz: origin of the 3D coordinates in x, y and z directions;
- fbathy: a binary input file of size nx\*ny to specify bathymetry information:
- frho11, frho22, frho33: binary file of size nx\*ny\*z to specify resistivities;
- fsrc: an ASCII file to specify source locations and orientations;
- frec: an ASCII file to specify receiver locations and orientations;
- fsrcrec: an ASCII file to specify the connection between source and receivers;
- niter: number of iterations for nonlinear optimization;
- npar: number of parameters used for inversion, default value=2;
- bound: bound=1 uses bounded LBFGS; bound=0 does not apply bound constraint;

- idxpar: index of the inversion parameter, default value=1,2 indicating horizontal and vertical resistivities;
- minpar: the minimum values for the physical parameters;
- maxpar: the maximum values for the physical parameters;
- gamma1: strength of 1st order Tikhonov regularization;
- gamma2: strength of Total Variational (TV) regularization;

An example job script run.sh using the above parameters is listed in the following.

#### #!/bin/bash

```
export OMP_NUM_THREADS=2
mpirun -n 25 ../bin/main mode=1 \
       istretch=0 \
       addair=1 \
       freqs=0.25,1,2.75 \setminus
       chsrc=Ex \
       chrec=Ex ,Ey,Hx,Hy \setminus
       nx=100 \
       ny=100 \
       nz=100 \
       dx=200 \
       dy=200 \
       dz=40 \
       ox=-10000 \
       oy=-10000 \
       oz=0 \
       fbathy=fbathy \
       frho11=frho_init \
       frho22=frho_init \
       frho33=frho_init \
       fsrc=sources.txt \
       frec=receivers.txt \
       fsrcrec=src_rec_table.txt \
       niter=30 \
       npar=2 \
       bound=1 \
       idxpar=1,2 \
       minpar=1.0,1.0 \
       maxpar=100.0,100.0 \
       gamma1=100 \
       gamma2=0
```

# 2 Source-receiver configuration

The locations and orientations for every source/transmitter and receiver are written in a 6-column table. The following is an example of source table

 $\verb|sources.txt|$  where  $\verb|x,y,z|$  are coordinates,  $\verb|azimuth,dip|$  are orientations,  $\verb|iTx|$  is the index of the transmitter.

x	у	z	azimuth	dip	iTx
-2196.15234	-8196.15234	903.652222	30.0000000	0	1
401.923828	-6696.15234	870.258484	30.0000000	0	2
3000.00000	-5196.15234	834.029785	30.0000000	0	3
5598.07617	-3696.15234	810.434204	30.0000000	0	4
8196.15234	-2196.15234	809.226013	30.0000000	0	5
-3696.15234	-5598.07617	865.961426	30.0000000	0	6
-1098.07617	-4098.07617	832.172302	30.0000000	0	7
1500.00000	-2598.07617	807.180298	30.0000000	0	8
4098.07617	-1098.07617	802.881104	30.0000000	0	9
6696.15234	401.923828	821.753967	30.0000000	0	10

The following is an example of receiver table receivers.txt where x,y,z are coordinates, azimuth,dip are orientations, iRx is the index of the receiver.

х	У	z	azimuth	dip	iRx
-10000.0000	0.00000000	1000.00000	0	0	1
-9800.00000	0.00000000	1000.00000	0	0	2
-9600.00000	0.00000000	1000.00000	0	0	3
-9400.00000	0.00000000	1000.00000	0	0	4
-9200.00000	0.00000000	1000.00000	0	0	5
-9000.00000	0.00000000	1000.00000	0	0	6
-8800.00000	0.00000000	1000.00000	0	0	7
-8600.00000	0.00000000	1000.00000	0	0	8
-8400.00000	0.00000000	1000.00000	0	0	9
-8200.00000	0.00000000	1000.00000	0	0	10
-8000.00000	0.00000000	1000.00000	0	0	11
-7800.00000	0.00000000	1000.00000	0	0	12
-7600.00000	0.00000000	1000.00000	0	0	13
-7400.00000	0.00000000	1000.00000	0	0	14
-7200.00000	0.00000000	1000.00000	0	0	15
-7000.00000	0.00000000	1000.00000	0	0	16

The connections between sources and receivers (which receivers record data from which source) must be specified by a source-receiver connection table <code>src\_rec\_table.txt</code> according to the index of the source and receivers.

isrc	irec
1	1
1	2
1	3
1	4
1	5
1	6
1	7
1	8
1	9

1	10
2	1
2	2
2	3
2	4
2	5
2	6
2	7
2	8
2	9
2	10

## 3 Output EMF files

The simulated CSEM data are stored in ASCII files. An example EM data file emf\_0001.txt from source index 0001 includes index of source and receivers (iTx, iRx), the recording channels of the receiver chrec, frequencies in Hz, real and imaginary part of the frequency domain data. They form a 6-column table in the following.

iTx	iRx	chrec f	requency/	Hz Real{E/H	<pre>} Imag{E/H}</pre>
1	1	Ex	0.25		-15 2.336085e-14
1	2	Ex	0.25	-8.236141e	-15 2.632050e-14
1	3	Ex	0.25	-7.451898e	-15 2.954083e-14
1	4	Ex	0.25	-6.390576e	-15 3.306965e-14
1	5	Ex	0.25	-4.998464e	-15 3.694922e-14
1	6	Ex	0.25	-3.228805e	-15 4.118009e-14
1	7	Ex	0.25	-1.026235e	-15 4.577336e-14
1	8	Ex	0.25	1.681961e-	15 5.075206e-14
1	9	Ex	0.25	4.974577e-	15 5.613805e-14
1	10	Ex	0.25	8.933074e-	15 6.194364e-14
1	1	Ex	1	-1.045790e-12	9.924710e-13
1	2	Ex	1	-1.119678e-12	1.968149e-12
1	3	Ex	1	-8.904390e-13	3.433207e-12
1	4	Ex	1	-1.103422e-13	6.096019e-12
1	5	Ex	1	1.431065e-12	1.066018e-11
1	6	Ex	1	6.458673e-12	2.313294e-11
1	7	Ex	1	2.208377e-11	5.329251e-11
1	8	Ex	1	1.162063e-10	1.498437e-10
1	9	Ex	1	3.530520e-10	3.849713e-10
1	10	Ex	1	-1.178124e-09	6.435691e-10

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## 4 Convergence information on CSEM inversion

After the 3D inversion, the convergence history of the nonlinear optimization will be stored in an ASCII file named iterate.txt.

1-BFGS memory length: 5

Maximum number of iterations: 30 Convergence tolerance: 1.00e-06 maximum number of line search: 5 initial step length: alpha=1

=====	========	========		=======	=====	
iter	fk	fk/f0	gk	alpha	nls	ngrad
0	1.08e+03	1.00e+00	5.30e+00	1.00e+00	0	0
1	9.16e+02	8.49e-01	4.50e+00	4.00e+00	2	3
2	6.48e+02	6.01e-01	5.15e+00	2.50e-01	2	6
3	5.96e+02	5.52e-01	8.72e+00	1.00e+00	0	7
4	4.35e+02	4.03e-01	4.40e+00	1.00e+00	0	8
5	3.35e+02	3.11e-01	3.20e+00	1.00e+00	0	9
6	2.58e+02	2.39e-01	5.29e+00	5.00e-01	1	11
7	2.09e+02	1.94e-01	3.69e+00	1.00e+00	0	12
8	1.71e+02	1.58e-01	2.00e+00	1.00e+00	0	13
9	1.44e+02	1.34e-01	1.53e+00	1.00e+00	0	14
10	1.23e+02	1.14e-01	2.09e+00	1.00e+00	0	15
11	1.16e+02	1.07e-01	2.28e+00	1.00e+00	0	16
12	8.96e+01	8.31e-02	2.02e+00	1.00e+00	0	17
13	7.71e+01	7.15e-02	1.77e+00	1.00e+00	0	18
14	6.27e+01	5.82e-02	8.97e-01	1.00e+00	0	19
15	5.48e+01	5.08e-02	1.11e+00	1.00e+00	0	20
16	4.93e+01	4.57e-02	7.89e-01	1.00e+00	0	21
17	4.45e+01	4.13e-02	6.47e-01	1.00e+00	0	22
18	4.06e+01	3.76e-02	7.92e-01	1.00e+00	0	23
19	3.69e+01	3.42e-02	6.41e-01	1.00e+00	0	24
20	3.42e+01	3.17e-02	7.62e-01	1.00e+00	0	25
21	3.30e+01	3.06e-02	9.15e-01	1.00e+00	0	26
22	3.01e+01	2.79e-02	6.26e-01	1.00e+00	0	27
23	2.80e+01	2.60e-02	6.31e-01	1.00e+00	0	28
24	2.66e+01	2.47e-02	6.19e-01	1.00e+00	0	29
25	2.60e+01	2.41e-02	7.20e-01	1.00e+00	0	30
26	2.58e+01	2.40e-02	1.13e+00	1.00e+00	0	31
27	2.50e+01	2.31e-02	8.96e-01	2.00e+00	1	38
28	2.44e+01	2.26e-02	8.16e-01	1.00e+00	0	39
29		2.18e-02	4.30e-01	1.00e+00	0	40

==>Maximum iteration number reached!

In the above example, each columns has clear meaning:

- iter: the iteration index k;
- fk: the misfit at the k-th iteration;
- fk/f0: the normalized misfit at the k-th iteration;

- | | gk | |: the norm of the gradient;
- alpha: step length used in line search;
- nls: number of line search at the k-th iteration;
- ngrad: number of gradient evaluations

### 5 The Green's function and the reciprocity

Assume only electrical current  $J_j(x_s, \omega) = \delta(x - x_s)e_j$  where  $e_j$  is the j-directed unit vector. We have

$$\begin{cases} \nabla \times G_{ij}^{E|E} - i\omega \mu G_{ij}^{H|E} &= 0\\ \nabla \times G_{ij}^{H|E} - \sigma G_{ij}^{E|E} &= \delta(x - x_s)e_j \end{cases}, \tag{1}$$

which defines two Green's function  $G_{ij}^{E|E}$  and  $G_{ij}^{H|E}$ :  $G_{ij}^{E|E}$  is the *i*th electrical (E) component of Green's function induced by *j*th component of electrical (E) source;  $G_{ij}^{H|E}$  is the *i*th magnetic (H) component of Green's function induced by *j*th component of electrical (E) source. The representation theorem gives

$$E_i = G_{ij}^{E|E} J_j, H_i = G_{ij}^{H|E} J_j.$$
 (2)

We can do the same assuming only a magnetic source  $M_j = \delta(x-x_s)e_j$ :  $G_{ij}^{E|H}$  is the ith electrical (E) component of Green's function induced by jth component of magnetic (H) source;  $G_{ij}^{H|H}$  is the ith magnetic (H) component of Green's function induced by jth component of magnetic (H) source.

$$\begin{cases} \nabla \times G_{ij}^{E|H} - i\omega\mu G_{ij}^{H|H} &= \delta(x - x_s)e_j \\ \nabla \times G_{ij}^{H|H} - \sigma G_{ij}^{E|H} &= 0 \end{cases},$$
(3)

which defines another two Green's function  $G_{ij}^{E|H}$  and  $G_{ij}^{H|H}$ . Similar to equation (2), the representation theorem gives

$$E_i = G_{ij}^{E|H} M_j, H_i = G_{ij}^{H|H} M_j.$$
 (4)

The total electrical and magnetic fields in the coupled system is then the superposition of two contributions:

$$E_{i} = \sum_{j} G_{ij}^{E|E} J_{j} + G_{ij}^{E|H} M_{j}, \quad H_{i} = \sum_{j} G_{ij}^{H|E} J_{j} + G_{ij}^{H|H} M_{j}.$$
 (5)

It is shown that the reciprocity for EM system holds in the following form

$$\begin{cases} G_{ij}^{E|E}(x_s|x_r) = G_{ji}^{E|E}(x_r|x_s), \\ G_{ij}^{H|H}(x_s|x_r) = G_{ji}^{H|H}(x_r|x_s), \\ G_{ij}^{H|E}(x_s|x_r) = -G_{ji}^{E|H}(x_r|x_s). \end{cases}$$
(6)

Without magnetic source, we have

$$\underbrace{\begin{bmatrix} E_{x} \\ E_{y} \\ E_{z} \end{bmatrix}}_{E} = \underbrace{\begin{bmatrix} G_{xx}^{E|E} & G_{xy}^{E|E} & G_{xz}^{E|E} \\ G_{yx}^{E|E} & G_{yy}^{E|E} & G_{yz}^{E|E} \\ G_{zx}^{E|E} & G_{zy}^{E|E} & G_{zz}^{E|E} \end{bmatrix}}_{G^{E|E}} \underbrace{\begin{bmatrix} J_{x} \\ J_{y} \\ J_{z} \end{bmatrix}}_{J_{s}}, \underbrace{\begin{bmatrix} H_{x} \\ H_{y} \\ H_{z} \end{bmatrix}}_{H} = \underbrace{\begin{bmatrix} G_{xx}^{H|E} & G_{xy}^{H|E} & G_{xz}^{H|E} \\ G_{yx}^{H|E} & G_{yy}^{H|E} & G_{yz}^{H|E} \\ G_{zx}^{H|E} & G_{zy}^{H|E} & G_{zz}^{H|E} \end{bmatrix}}_{G^{H|E}} \underbrace{\begin{bmatrix} J_{x} \\ J_{y} \\ J_{z} \end{bmatrix}}_{J_{s}}. \tag{7}$$

If  $J_s|_{x=x_s}=(1,0,0)^{\mathrm{T}}$ , we have the 1st column of the matrix  $G^{E|E}$  and  $G^{H|E}$  extracted from vector fields E and Hextracted from vector fields E and H

$$\begin{bmatrix}
E_{x}(x_{r}) \\
E_{y}(x_{r}) \\
E_{z}(x_{r})
\end{bmatrix} = \begin{bmatrix}
G_{xx}^{E|E}(x_{r}|x_{s}) \\
G_{yx}^{E|E}(x_{r}|x_{s}) \\
G_{zx}^{E|E}(x_{r}|x_{s})
\end{bmatrix} = \begin{bmatrix}
G_{xx}^{E|E}(x_{s}|x_{r}) \\
G_{xy}^{E|E}(x_{s}|x_{r}) \\
G_{xz}^{E|E}(x_{s}|x_{r})
\end{bmatrix}, (8a)$$

$$\begin{bmatrix}
H_{x}(x_{r}) \\
H_{y}(x_{r}) \\
H_{z}(x_{r})
\end{bmatrix} = \begin{bmatrix}
G_{xx}^{H|E}(x_{r}|x_{s}) \\
G_{yx}^{H|E}(x_{r}|x_{s}) \\
G_{xx}^{H|E}(x_{r}|x_{s})
\end{bmatrix} = - \begin{bmatrix}
G_{xy}^{E|H}(x_{s}|x_{r}) \\
G_{xy}^{E|H}(x_{s}|x_{r}) \\
G_{xz}^{E|H}(x_{s}|x_{r})
\end{bmatrix}, (8b)$$

$$\begin{bmatrix}
H_x(x_r) \\
H_y(x_r) \\
H_z(x_r)
\end{bmatrix} = \begin{bmatrix}
G_{xx}^{H|E}(x_r|x_s) \\
G_{yx}^{H|E}(x_r|x_s) \\
G_{zx}^{H|E}(x_r|x_s)
\end{bmatrix} = - \begin{bmatrix}
G_{xx}^{E|H}(x_s|x_r) \\
G_{xy}^{E|H}(x_s|x_r) \\
G_{xz}^{E|H}(x_s|x_r)
\end{bmatrix},$$
(8b)

where the last equality comes from the reciprocity in (6). It implies that by switching the source and receiver position, we can reproduce the  $E_x$ ,  $E_y$  and  $E_z$  response from the  $E_x$ -channel of the receiver at source position by repeating the modeling using the electrical sources at receiver location, i.e.,  $J_s|_{x=x_r} =$  $(1,0,0)^{\mathrm{T}}$ ,  $J_s|_{x=x_r} = (0,1,0)^{\mathrm{T}}$  and  $J_s|_{x=x_r} = (0,0,1)^{\mathrm{T}}$ . Similarly, we should reproduce  $-H_x$ ,  $-H_y$  and  $-H_z$  response from the  $E_x$ -channel of the receiver at source position by repeating the modeling using the magnetic sources at receiver location, i.e.,  $M_s|_{x=x_r} = (1,0,0)^T$ ,  $M_s|_{x=x_r} = (0,1,0)^T$  and  $M_s|_{x=x_r} = (0,1,0)^T$  $(0,0,1)^{\mathrm{T}}$ .

If  $J_s|_{x=x_s}=(0,1,0)^{\mathrm{T}}$ , we have the 2nd column of the matrix  $G^{E|E}$  and  $G^{H|E}$  extracted from vector fields E and H

$$\begin{bmatrix}
E_{x}(x_{r}) \\
E_{y}(x_{r}) \\
E_{z}(x_{r})
\end{bmatrix} = \begin{bmatrix}
G_{xy}^{E|E}(x_{r}|x_{s}) \\
G_{yy}^{E|E}(x_{r}|x_{s}) \\
G_{zy}^{E|E}(x_{r}|x_{s})
\end{bmatrix} = \begin{bmatrix}
G_{yx}^{E|E}(x_{s}|x_{r}) \\
G_{yy}^{E|E}(x_{s}|x_{r}) \\
G_{yz}^{E|E}(x_{s}|x_{r})
\end{bmatrix},$$
(9a)
$$\begin{bmatrix}
H_{x}(x_{r}) \\
H_{y}(x_{r}) \\
H_{z}(x_{r})
\end{bmatrix} = \begin{bmatrix}
G_{xy}^{H|E}(x_{r}|x_{s}) \\
G_{yy}^{H|E}(x_{r}|x_{s})
\end{bmatrix} = - \begin{bmatrix}
G_{yx}^{E|H}(x_{s}|x_{r}) \\
G_{yy}^{E|H}(x_{s}|x_{r}) \\
G_{yy}^{E|H}(x_{s}|x_{r})
\end{bmatrix}.$$
(9b)

$$\begin{bmatrix} H_{x}(x_{r}) \\ H_{y}(x_{r}) \\ H_{z}(x_{r}) \end{bmatrix} = \begin{bmatrix} G_{xy}^{H|E}(x_{r}|x_{s}) \\ G_{yy}^{H|E}(x_{r}|x_{s}) \\ G_{zy}^{H|E}(x_{r}|x_{s}) \end{bmatrix} = - \begin{bmatrix} G_{yx}^{E|H}(x_{s}|x_{r}) \\ G_{yy}^{E|H}(x_{s}|x_{r}) \\ G_{yz}^{E|H}(x_{s}|x_{r}) \end{bmatrix}.$$
(9b)

By switching the source and receiver position, we obtain the  $E_x$ ,  $E_y$  and  $E_z$ response from the  $E_y$ -channel of the receiver at source position by repeating the modeling placing the sources at receiver location, i.e.,  $J_s|_{x=x_r} = (1,0,0)^T$ ,  $J_s|_{x=x_r} = (0,1,0)^{\mathrm{T}}$  and  $J_s|_{x=x_r} = (0,0,1)^{\mathrm{T}}$ . Also, we obtain  $-H_x$ ,  $-H_y$  and  $-H_z$  response from the  $E_y$ -channel of the receiver at source position by repeating the modeling placing the magnetic sources at receiver location, i.e.,  $M_s|_{x=x_r}$  $(1,0,0)^{\mathrm{T}}, M_s|_{x=x_r} = (0,1,0)^{\mathrm{T}} \text{ and } M_s|_{x=x_r} = (0,0,1)^{\mathrm{T}}.$