

RATE OF REACTION,  $O + H_2 \rightarrow OH + H$ , IN FLAMES

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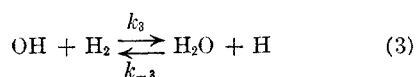
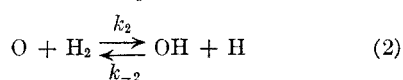
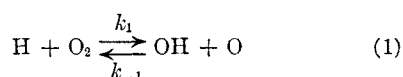
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By probing low pressure flames of  $H_2$ - $O_2$ - $N_2$ - $N_2O$ , and using the ratios of rate constants previously determined in flames, we find that the rate constant for the reaction of oxygen atoms with hydrogen molecules is  $2.5 \pm 0.4 \times 10^8$  l. mole<sup>-1</sup> sec.<sup>-1</sup> at 1660°K. and  $3.0 \pm 0.3 \times 10^8$  at 1815°. These values agree with a long extrapolation of Baldwin's results at about 800°K., and combine with them to give  $k = 2.5 \times 10^9 e^{-7.7 \text{ kcal./RT}}$  l. mole<sup>-1</sup> sec.<sup>-1</sup>.

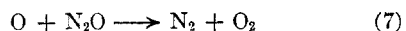
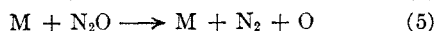
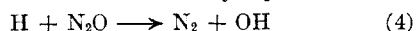
## Introduction

Of the three important bimolecular reactions in  $H_2$ - $O_2$  mixtures



$k_1^{1-4}$  and  $k_3^{5,6}$  are moderately well known over a considerable range of temperature, but  $k_2^2$  has not been measured above 820°K. and estimates of its value at high temperatures would be worthwhile. Measurement of  $k_2$  in some  $H_2$ - $O_2$ - $N_2$ - $N_2O$  flames are reported in this paper.

Nitrous oxide is included in the reactants because its irreversible decomposition in low pressure  $H_2$ - $O_2$  flames allows the measurement of radical concentrations. It reacts chiefly by



of which (4) is the fastest by far.

It is assumed that no important reaction of oxygen atoms has been omitted, so that we can write out the expression for  $d[O]/dt$  due to the chemical reactions above and solve the resulting expression for  $k_2$ . Any consumption of oxygen atoms in the recombinations  $2O + M \rightarrow O_2 + M$  or  $O + H + M \rightarrow OH + M$  has been ignored, but these termolecular recombinations must be small compared to the reverse of reaction 1 which is included. Another simplification may as well be made from the start; it will always be possible to neglect the reverse of reaction 2 in the region where  $k_2$  is evaluated, as will be shown, and to choose this region so that  $d[O]/dt$  is approximately zero. Then

$$k_2 = \frac{-d[O_2]/dt + k_5[N_2O][M] - d[NO]/2dt}{[H_2][O]}$$

and everything on the right side of this expression can be measured.

The rates of change of  $[O_2]$  and  $[NO]$  can be obtained by probing flat, one dimensional flames and

correcting the traverses for diffusion. The composition traverses also allow estimates of  $k_5[N_2O][M]$  and  $[H_2]$  at any point.

$[O]$  can be estimated in two independent ways. First, since the nitric oxide formed in reaction 6 does not undergo appreciable decomposition,  $[O]$  can be obtained from

$$d[NO]/dt = 2k_6[O][N_2]$$

Second, it can also be estimated from the three reactions 4, 3 and 1 because

$$-d[N_2O]/dt = k_4[H][N_2O]$$

accounts for most of the decomposition of nitrous oxide and gives an estimate of  $[H]$  which can be substituted into

$$d[H_2O]/dt = k_3[OH][H_2] - k_{-3}[H_2O][H]$$

to get  $[OH]$ . Both  $[H]$  and  $[OH]$  can then be substituted in

$$-d[O_2]/dt + k_7[O][N_2O] = k_1[H][O_2] - k_{-1}[OH][O]$$

to get  $[O]$ . In the last expression, the term in  $k_7$  can be omitted whenever  $d[NO]/dt$  is small compared to  $-d[O_2]/dt$  because  $k_7 < k_6/2$ .

Although the determination of  $[O]$  from reactions 4, 3 and 1 may seem involved, this method has two advantages over the simpler determination by reaction 6. It does not really depend on the separate values of  $k_4$ ,  $k_3$ ,  $k_1$  but only on their ratios; and since these constants were measured relative to one another in the temperature range in which we use them, the ratios are probably more accurate than the separate values.  $[O]$  from reaction 6 does of course depend on the separate value of  $k_6$ .

Also the reaction rates one uses in (4), (3) and (1) are fairly large and can be tested for internal consistency. In a region where  $d[O]/dt$  and  $d[OH]/dt$  are small, one should have  $-d[N_2O]/dt - 2d[O_2]/dt = d[H_2O]/dt + d[NO]/dt$  since oxygen must be conserved. This relation holds experimentally within 10%, and  $d[NO]/dt$  is always small compared to the three other terms in the equality. Therefore the three larger terms are at least consistent among themselves. The small  $d[NO]/dt$  used in the determination of  $[O]$  via reaction 6 cannot be tested in the same way because it does not make a very significant contribution to the conservation of oxygen or nitrogen.

The values adopted for the rate constants are quoted in Table I.  $k_1$ ,  $k_3$ ,  $k_4$  and  $k_5$  are correct relative to one another to perhaps 30%, and  $k_1$  and  $k_3$  also agree within a factor of two with independent estimates in the literature.  $k_5$  is obtained from a correlation of much of the data on the pseudo-unimolecular, thermal decomposition of nitrous oxide.<sup>7</sup> The limiting low pressure con-

(1) N. N. Semenov, *Acta Physicochim.*, **20**, 290 (1945).

(2) R. R. Baldwin, *Trans. Faraday Soc.*, **52**, 1344 (1956).

(3) G. L. Schott and J. L. Kinsey, *J. Chem. Phys.*, **29**, 1177 (1958).

(4) C. P. Fenimore and G. W. Jones, *J. Phys. Chem.*, **63**, 1154 (1959).

(5) L. Avramenko and R. Lorentso, *Zhur. Fiz. Khim.*, **24**, 207 (1950).

(6) C. P. Fenimore and G. W. Jones, *J. Phys. Chem.*, **62**, 693 (1958).

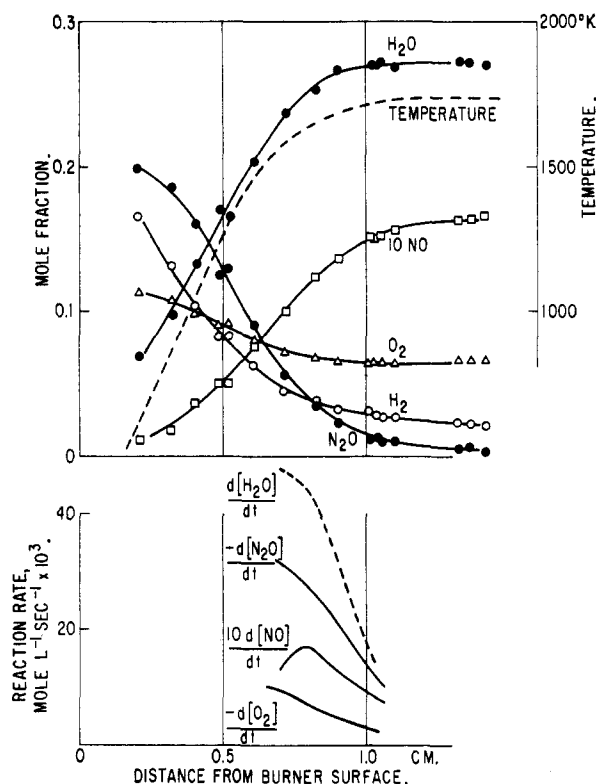


Fig. 1.—Traverses through a flame of reactant composition  $\text{H}_2 + 0.66\text{N}_2\text{O} + 1.81$  air burnt at 2 cm. pressure of mercury with a mass flow of  $2.32 \times 10^{-3}$  g. cm.<sup>-2</sup> sec.<sup>-1</sup>. Calculated reaction rates are plotted in the lower part of the graph.

stant listed is appropriate to initially pure nitrous oxide where  $[\text{M}]$  represents initial  $[\text{N}_2\text{O}]$ . If  $[\text{M}]$  represents the total concentration of a mixture of other gases, as it does in our flames, the

TABLE I  
BIMOLECULAR RATE CONSTANTS<sup>a</sup>

Reaction	Rate constant, mole l. <sup>-1</sup> sec. <sup>-1</sup>	Ref.
1	$6 \times 10^{11} e^{-18/RT}$	4
3	$2.5 \times 10^{11} e^{-10/RT}$	6
4	$4 \times 10^{11} e^{-16.3/RT}$	4
5	$4 \times 10^{12} e^{-59/RT}$	7
6	$1 \times 10^{11} e^{-28/RT}$	8
7	$k_7 < k_6/2$	9

<sup>a</sup> For reactions 1, 2 and 3, the rate constants for the reverse reactions can be obtained from the constants for the forward reactions and the equilibrium constants;  $k_1/k_{-1} = 35e^{-16.6/RT}$ ,  $k_2/k_{-2} = 2e^{-3.0/RT}$ ,  $k_3/k_{-3} = 0.25e^{15.5/RT}$ .

pre-exponential factor of  $k_5$  could be wrong by a factor of about two, and we will discuss this possibility later. For any use we make of  $k_7$ , it will be enough to know that at the temperatures of interest  $k_7$  is smaller than  $k_6$ .

The diffusion corrections to get  $d[\text{NO}]/dt$ ,  $-d[\text{O}_2]/dt$ ,  $-d[\text{N}_2\text{O}]/dt$ ,  $d[\text{H}_2\text{O}]/dt$  from experimental composition traverses caused us some trouble. With the diffusion coefficients  $D_{\text{NO}}$ ,  $D_{\text{O}_2}$ , etc., assumed the chemical reaction rates were

(7) H. S. Johnston, *J. Chem. Phys.*, **19**, 663 (1951).

(8) C. P. Fenimore and G. W. Jones, 8th Combustion Symposium at Pasadena, Calif., Sept. 1960.

(9) F. Kaufman, N. J. Gerri and R. E. Bowman, *J. Chem. Phys.*, **25**, 106 (1956).

calculated just as before.<sup>4</sup> The flames were 60 to 70% nitrogen, and we first tried approximate  $D_{\text{NO}}$  values appropriate to binary NO-N<sub>2</sub> mixtures.<sup>10</sup> These gave too great a correction however, and resulted in negative calculated values of  $d[\text{NO}]/dt$  in the early parts of some flames. After several trials in different runs, we eventually used

$$D_{\text{NO}} = 2.3 \times 10^{-4} T^{1.67} \text{ cm.}^2 \text{ sec.}^{-1}$$

in all flames at 4 cm. pressure of mercury. For other species, the diffusion coefficient was taken from  $D_{\text{NO}}$  under the assumption that  $D$  was inversely proportional to the square root of the molecular weight. For other pressures, it was assumed that  $D$  varied inversely with pressure. The value chosen for  $D_{\text{NO}}$  is near the greatest value which did not overcorrect the nitric oxide traverse.

The calculation of  $[\text{O}]$  by means of reaction 6 is considerably more sensitive to changes in the diffusion coefficient than is the calculation *via* (4), (3) and (1). A smaller  $D_{\text{NO}}$  decreases the maximum  $[\text{O}]$  as calculated from (6).

### Experimental

The arrangement was the same as used before. It included a water-cooled, porous, flat flame burner<sup>11</sup> of 31.1 cm.<sup>2</sup> surface area mounted in a bell jar which was also equipped with a movable quartz probe ( $\sim 0.1$  mm. diam.), movable quartz coated thermocouple (made of butt-welded Pt-Pt, Rh wires 0.012 mm. diam.), pumps, and externally mounted cathetometer. The reactants were metered through critical flow orifices. Thermocouple readings were corrected for radiation<sup>11</sup> to get temperature traverses. Composition traverses of the stable components were obtained from mass spectrometric analyses of samples drawn through the quartz probe at critical flow rates.

**Determination of  $k_2$ .**—The upper half of Fig. 1 presents typical traverses through a flame burnt at 2 cm. pressure. The lower part of the figure shows reaction rates calculated from the traverses.  $[\text{O}]$  as calculated from

$$[\text{O}] = d[\text{NO}]/2k_6[\text{N}_2\text{O}]dt$$

attains a maximum value of  $6.0 \times 10^{-6}$  mole l.<sup>-1</sup> at 0.8 to 0.95 cm. from the burner surface.

Calculating  $[\text{O}]$  in the alternate way described above, we find that

$$[\text{H}] = -d[\text{N}_2\text{O}]/k_4[\text{N}_2\text{O}]dt$$

is relatively constant through most of the flame. At a position 0.8 to 0.95 cm. from the burner surface,  $[\text{H}] = 1.4 \times 10^{-6}$  mole l.<sup>-1</sup>; and then in turn,  $[\text{OH}] = 0.83 \times 10^{-6}$  from reaction 3 and  $[\text{O}] = 3.7 \times 10^{-6}$  from reaction 1.

The  $[\text{O}]$  obtained from reactions 4, 3 and 1 is smaller by a factor of 1.6 than  $[\text{O}]$  calculated from reaction 6. A similar discrepancy occurs in all the flames, by a factor of 3.6 in the worst case and 1.6 in the best, and always in the sense that  $[\text{O}]$  from reaction 6 is the larger.

Since  $[\text{O}]$  from reaction 6 is more sensitive to a change in the diffusion coefficient, we trust it less. Other reasons for preferring the smaller  $[\text{O}]$  from reactions 4, 3 and 1 have been given in the introduction; and we use the smaller  $[\text{O}]$  for estimating  $k_2$ .

For the flame described in Fig. 1, at 0.8 to 0.95

(10) A. A. Westenberg, *Combustion and Flame*, **1**, 346 (1957).

(11) W. E. Kaskan, "6th Symposium on Combustion," Reinhold Publ. Corp., New York, N. Y., 1957, p. 134.

cm. from the burner surface, the reverse of (2) is small compared to the forward reaction. This is apparent because the product of reaction partners for the forward process,  $[O][H_2]$ , is twenty times the product for the reverse,  $[OH][H]$ ; but the equilibrium constant,  $k_2/k_{-2}$ , is of order unity.

$d[O]/dt$  is very small in the region 0.8 to 0.95 cm. from the burner surface, so we substitute into

$$k_2 = \frac{-d[O]_2/dt + k_5[N_2O][M] - d[NO]/2dt}{[O][H_2]}$$

to get  $k_2 = 2.8 \times 10^8$  l. mole<sup>-1</sup> sec.<sup>-1</sup> at 1675°K. The term,  $k_5[N_2O][M]$ , is small compared to  $-d[O]_2/dt$  and could have been omitted in this example.

Estimates of  $k_2$ , obtained in a similar way in each flame, are listed in Table II. The first four runs are fuel rich flames, the last two are fuel lean. The last column of Table II gives the percentage contribution of the term  $k_5[N_2O][M]$  to the value of  $k_2$ . If  $k_5$  were wrong, only runs no. 2 and 3 would be affected.

TABLE II  
ESTIMATES OF  $k_2$

Run	P, cm.	T, °K.	$[O] \times 10^6$ , mole l. <sup>-1</sup>	$k_2 \times 10^{-8}$ , l. mole <sup>-1</sup> sec. <sup>-1</sup>	$k_5$ term, <sup>a</sup> %
1	4	1825	1.2	3.0	~0
2	6	1830	0.4	1.7	75
3	4	1790	.8	1.8	33
4	4	1640	.8	2.0	~0
5	2	1675	3.7	2.8	~0
6	4	1670	3.0	2.8	~0

<sup>a</sup> Contribution of the term,  $k_5[N_2O][M]$ , to the value deduced for  $k_2$  if  $k_5$  is assumed to have the value in Table I. Actually  $k_5$  is eventually assumed to be 2.25 times larger than this value, see text, and the eventual values of  $k_2$  in runs 2 and 3 are  $3.3$  and  $2.6 \times 10^8$ , respectively.

As they stand, the first three runs in Table II average to  $k_2 = 2.2 \times 10^8$  at about 1815°K. with a mean deviation of 26%. But  $k_5$  is not known better than to a factor of about two, as was explained in the Introduction, and it is legitimate to vary the pre-exponential factor of  $k_5$  in order to get the best agreement in  $k_2$ . If  $k_5$  is multiplied by 2.25, the average deviation in  $k_2$  decreases to only 8% and the average becomes identical with the only value of  $k_2$  which is independent of  $k_5$ . Therefore we increase the  $k_5$  given in Table I and accept  $k_2 = 3.0 \pm 0.3 \times 10^8$  at 1815°.

The last three runs give an average at 1660°K. of  $k_2 = 2.5 \pm 0.4 \times 10^8$ , independent of  $k_5$ .

**Comparison with Other Work.**—Baldwin<sup>2</sup> deduced from the low pressure limit of explosions in  $H_2$ - $O_2$ - $N_2$  mixtures that  $k_2$  (or  $k_3$ ) =  $2.0 \times 10^7$  l. mole<sup>-1</sup> sec.<sup>-1</sup> at 793°K. The ambiguity arose because reactions 2 and 3 have an identical dependence on  $[H_2]$ ; but since  $2 \times 10^7$  is only  $1/10^5$  or  $1/20^8$  of the value expected for  $k_3$  from other work, it is probably  $k_2$ . He also reported an activation energy of 9.2 kcal., but disclaimed much accuracy; for  $k_2$  was reproducible only within  $\pm 12\%$  at constant temperature, and the variation over the whole temperature range was 44%. Perhaps it is not unfair to suggest that his error might have been  $\pm 3$  kcal.

If his estimate at 793° is extrapolated to 1815°, using 9.2 kcal. activation energy, it gives  $k_2 = 5.4 \times 10^8$  as compared to our observed  $3 \times 10^8$ . This is good agreement. His and our estimates combine to

$$k_2 = 2.5 \times 10^8 e^{-7.7/RT} \text{ l. mole}^{-1} \text{ sec.}^{-1}$$

and 7.7 is the same as 9.2 kcal. within the probable error of the latter. If the pre-exponential factor is taken proportional to  $T^{1/2}$ , part of the temperature dependence is absorbed by this factor, and  $E_2$  becomes 6.4 rather than 7.7 kcal.

In much the same way as Baldwin, but with less complete data and interpretations, Azatian and co-workers<sup>12</sup> found  $k_2 = 9 \times 10^{10} e^{-12.1/RT}$  at 840 to 930°K. from the lower explosion limits of  $CO$ - $O_2$  mixtures containing 0.76 to 8.0% added hydrogen. Their result extrapolates to twice Baldwin's estimate at 793° and to ten times our estimate at 1815°. It is not possible to reconcile our measurements with those of Azatian, *et al.*, and still maintain an activation energy of  $9 \pm 3$  kcal.

**NOTE ADDED IN PROOF.**—Clyne and Thrush<sup>13</sup> reported just recently an estimate of  $k_2 = 1.2 \times 10^{10} e^{-9.2/RT}$  l. mole<sup>-1</sup> sec.<sup>-1</sup> at 409 to 733°K. by a very different method; O atoms were generated in known concentration by titrating N atoms with nitric oxide, and the decay of the O atoms when mixed with hydrogen was followed by the radiation from the O + NO emission. Their estimate of  $k_2$  is systematically larger than the expression deduced in this paper by a factor of 2 to 3; but a disagreement of this order is perhaps within the error of any of the data.

(12) V. V. Azatian, V. V. Voevodskii and A. B. Nalbandian, *Dokl. Akad. Nauk. SSSR*, **132**, 864 (1960).

(13) M. A. A. Clyne and B. A. Thrush, *Nature*, **189**, 135 (1961).