



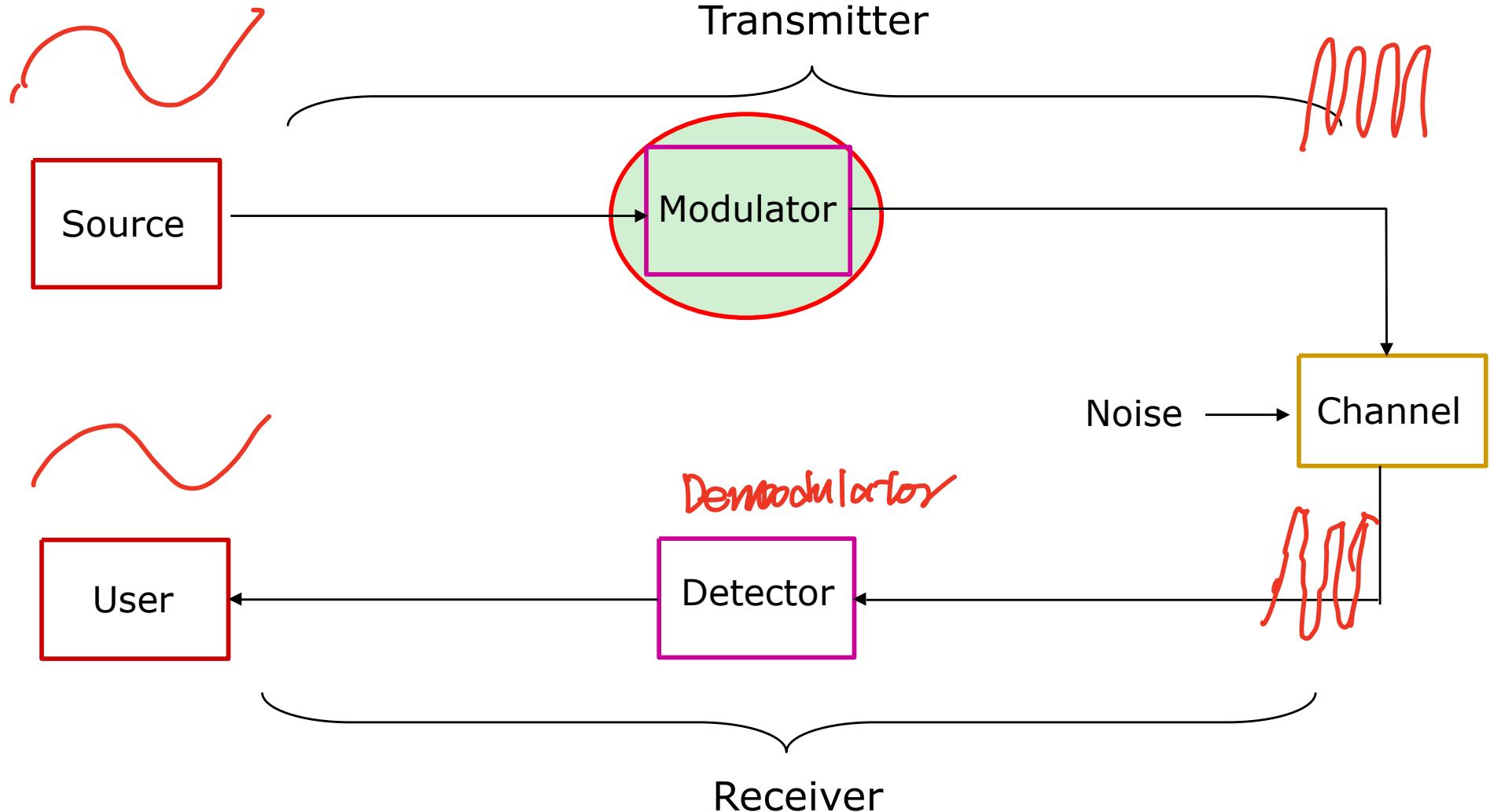
上海科技大学
ShanghaiTech University

EE140 Introduction to Communication Systems

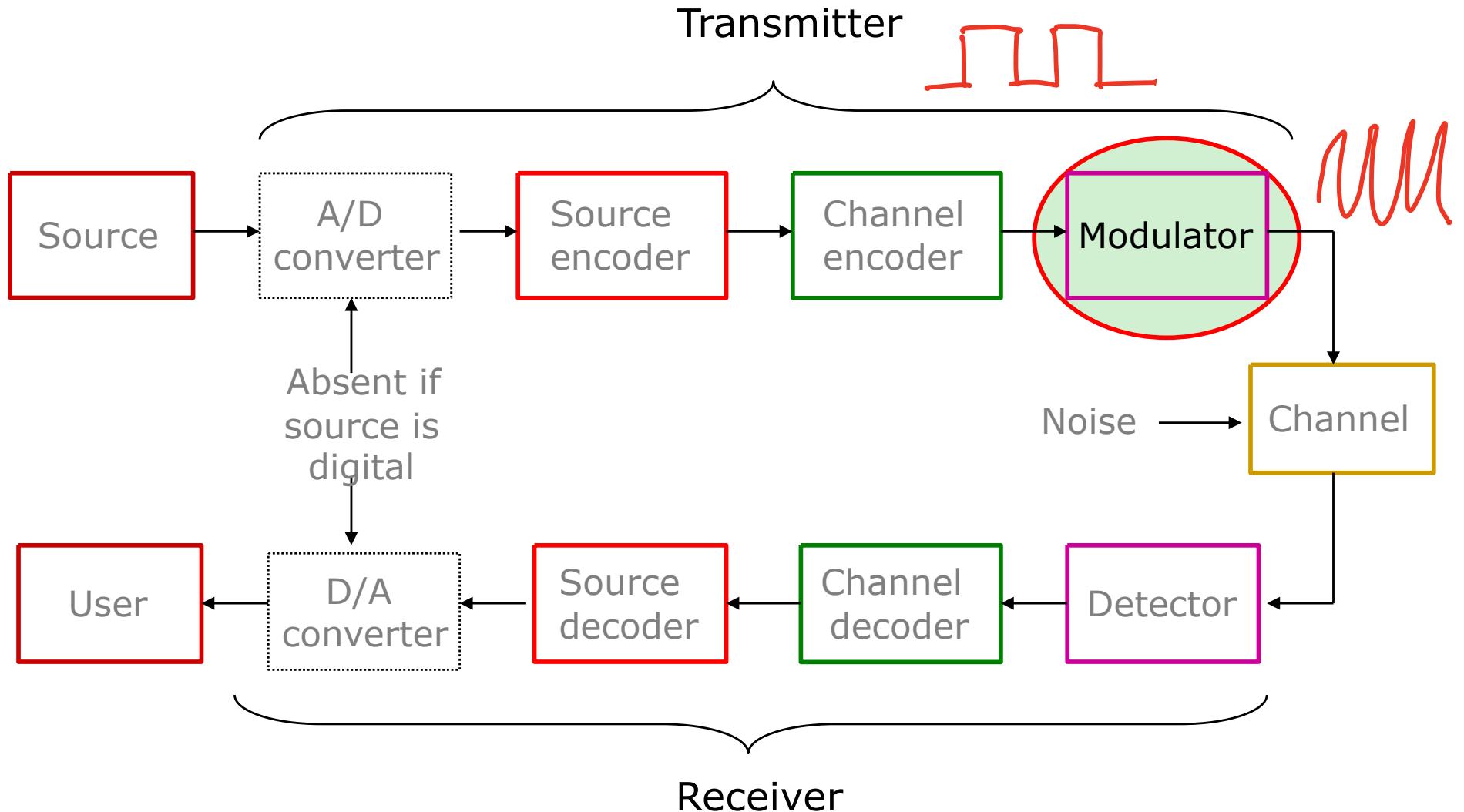
Lecture 6

Instructor: Prof. Lixiang Lian
ShanghaiTech University, Fall 2025

Architecture of an Analog Communication System



Architecture of a (Digital) Communication System



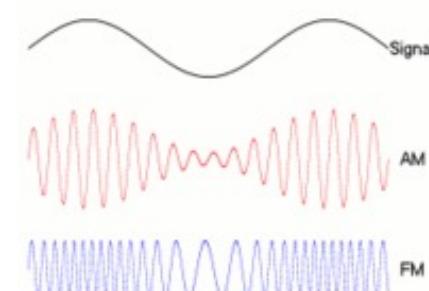
Examples of Analog Modulation



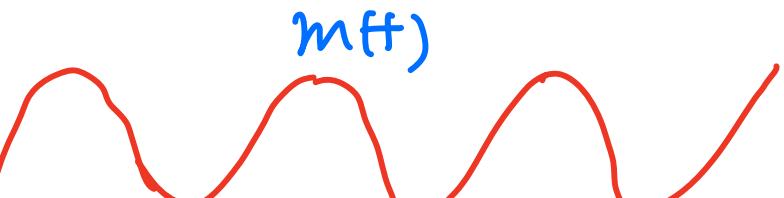
Telephony,
Analog TV, radio
broadcasting

Modulation

- What is modulation?
 - Transform a message into another signal to facilitate transmission over a communication channel
 - Generate a carrier signal at the transmitter
 - Modify some characteristics of the carrier with the information to be transmitted
 - Detect the modifications at the receiver
- Why modulation?
 - Frequency translation
 - Frequency-division multiplexing
 - Noise performance improvement



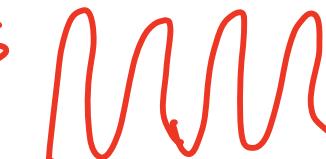
source



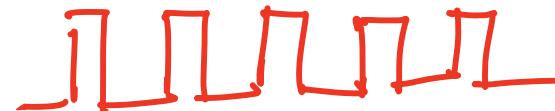
Baseband signal
Modulating signal

Carrier

Analog continuous wave $\tilde{s}_m \cos(Ct)$



Analog pulse wave



modulated signal

$\underline{x}_c(t)$

Carrier

$\tilde{s}_m \cos$

Analog continuous wave mod.

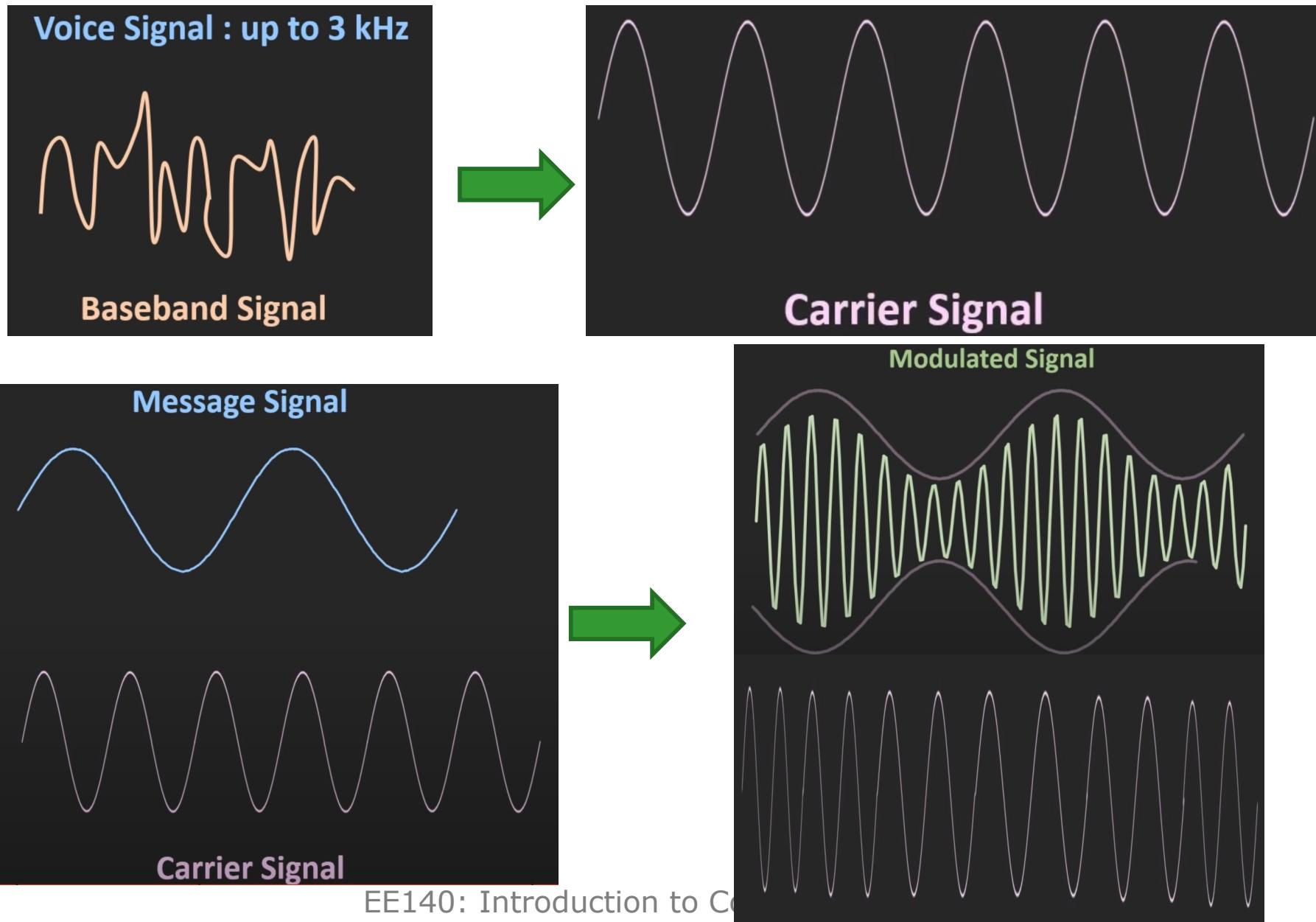
AM FM PM

$\underline{\Pi \Pi \Pi \Pi}$

Analog pulswave Mod

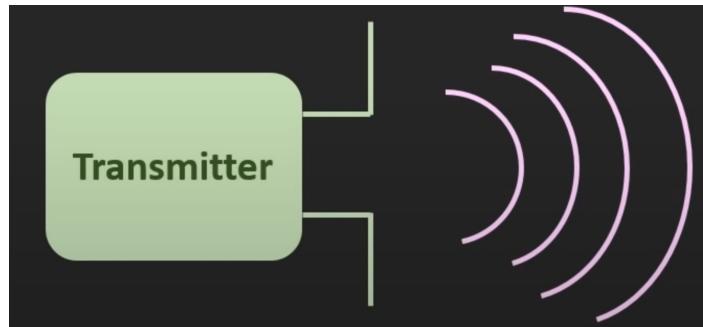
PAM PWM PPM

Modulation



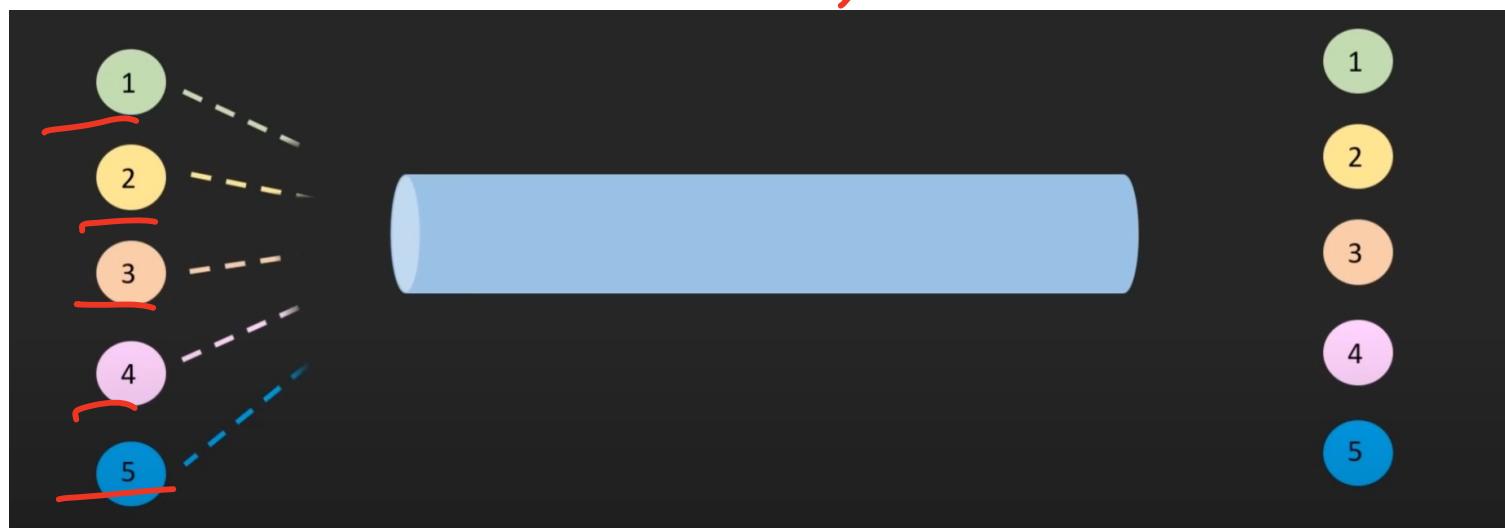
Modulation

1. Reduce antenna size



- ① $d \propto \lambda$
- ② FDM
- ③ reliability

2. Reduce the interference, allow multiplexing of signal



Analog Continuous-Wave Modulation

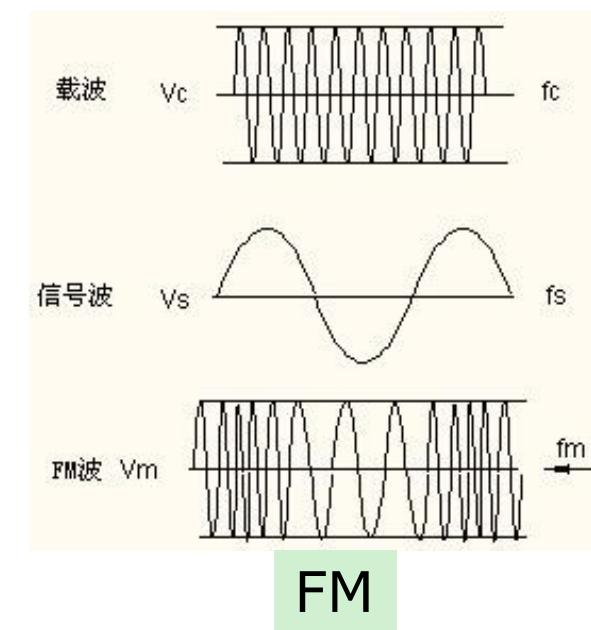
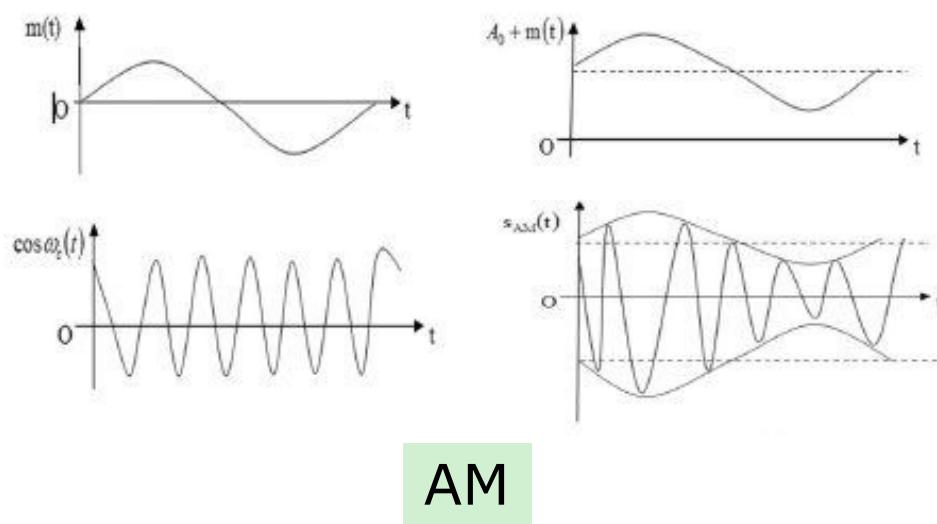
- Characteristics that can be modified in the carrier

$$C(t) = A(t) \cos(2\pi f(t)t + \theta(t))$$

A(t) - Amplitude AM → Amplitude modulation

f(t) - Frequency FM → Angle modulation

$\theta(t)$ - Phase PM

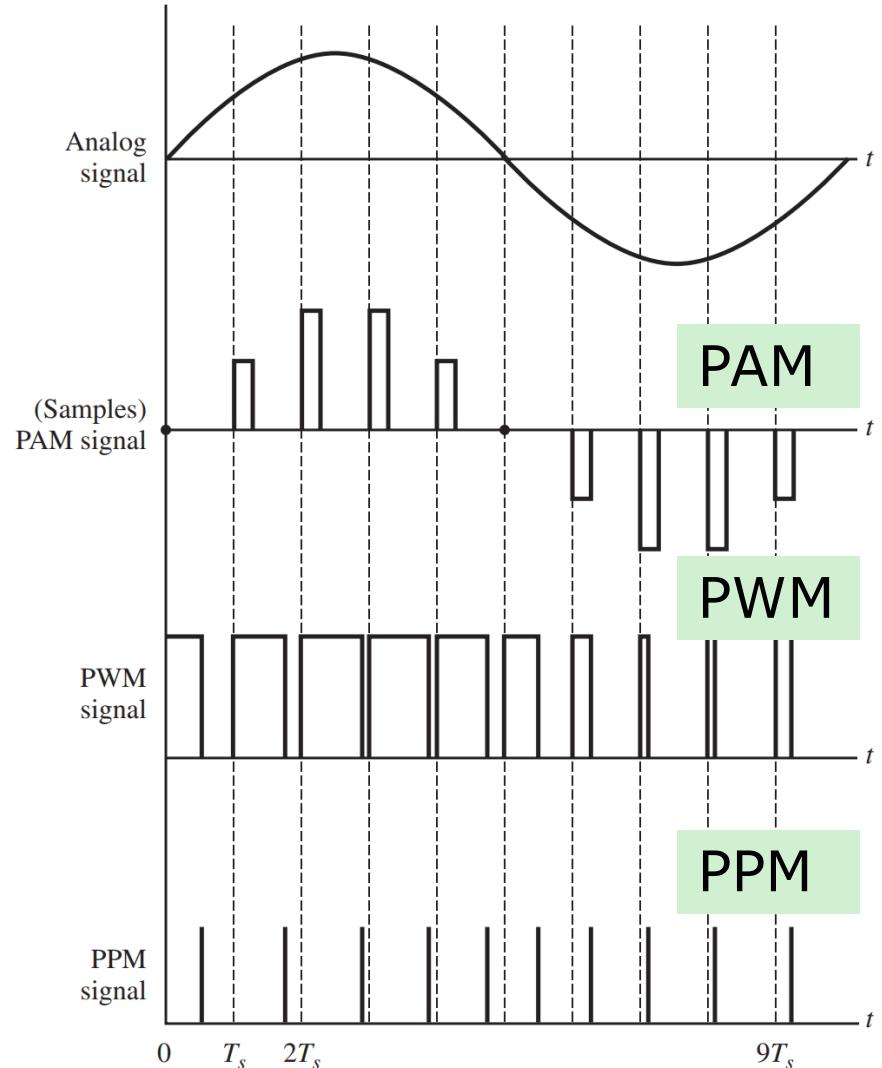


Analog Pulse Modulation

- Characteristics that can be modified in the carrier

$$C(t) = \sum_n \Pi\left(\frac{t - nT_s + \frac{1}{2}\tau}{\tau}\right)$$

- Amplitude \Rightarrow Amplitude modulation
- Width } \Rightarrow Angle Modulation
- Position }



Outline



Continuous-wave modulation:
amplitude modulation



Pulse modulation:
amplitude modulation



Linear
Modulation



Continuous-wave modulation:
angle modulation



Pulse modulation:
angle modulation



Non-linear
Modulation

Contents

- Analog Modulation
 - Continuous-Wave Amplitude Modulation
 - DSB { DSB-SC
DSB - LC(AM)
 - SSB
 - VSB
 - Pulse Amplitude Modulation
 - Angle Modulation (phase/frequency)

Amplitude Modulation

- Double-sideband suppressed-carrier AM (DSB-SC)

- Baseband signal (modulating wave):

$$m(t)$$

- Carrier wave

$$C(t) = A_c \cos(2\pi f_c t)$$

- Modulated wave

$$x_c(t) = \underline{m(t)} \underline{C(t)}$$

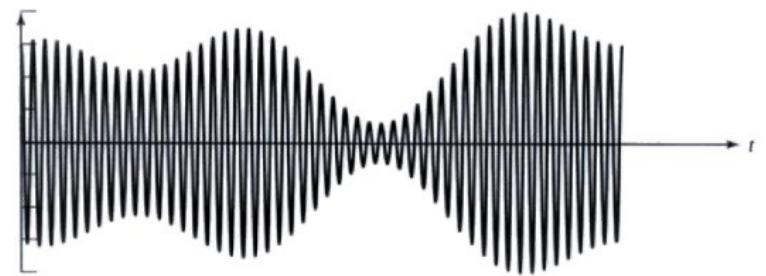
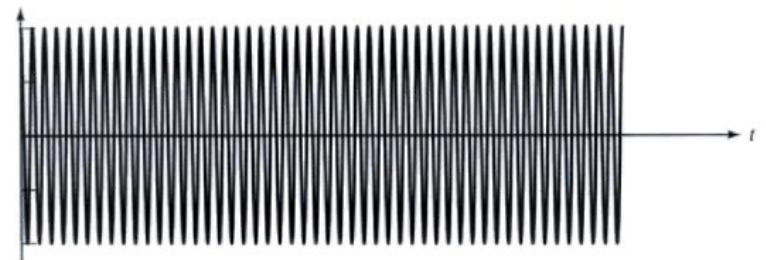
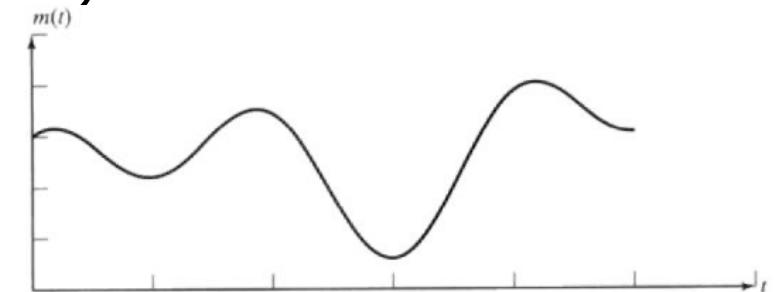
$$= A_c m(t) \cos(2\pi f_c t)$$

$$\underline{X_c(f)}$$

$$= \frac{1}{2} A_c M(f + f_c) + \frac{1}{2} A_c M(f - f_c)$$



(DSB-SC)



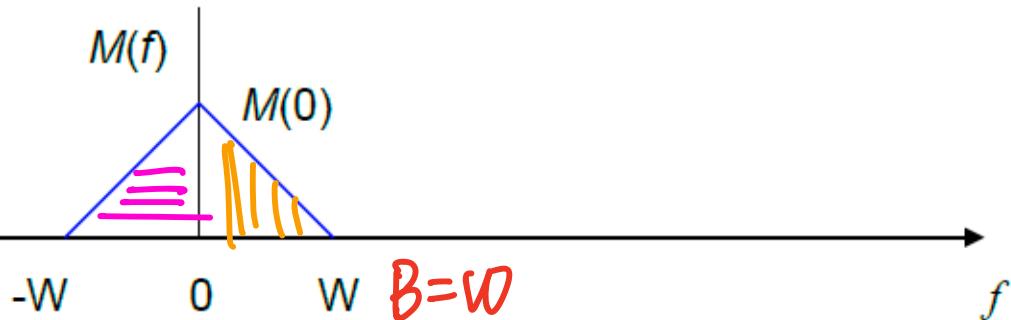
① USB $|f| \geq f_c$ ② SC, No Carrier ③ Linear Mod

LSB $|f| \leq f_c$ DSB-SC Spectrum

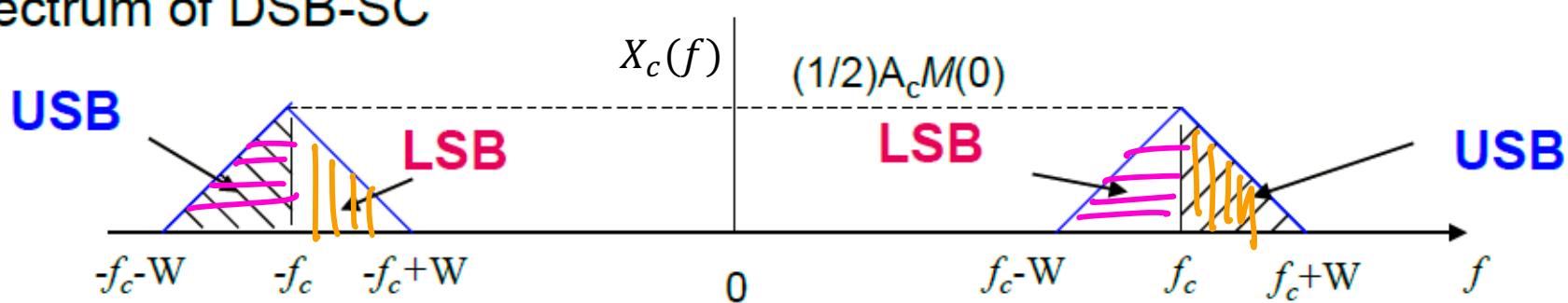
$$B = 2W$$

Time. $\gamma(t) = m(t)$
Freq.: $C(t)$

Spectrum of message



Spectrum of DSB-SC

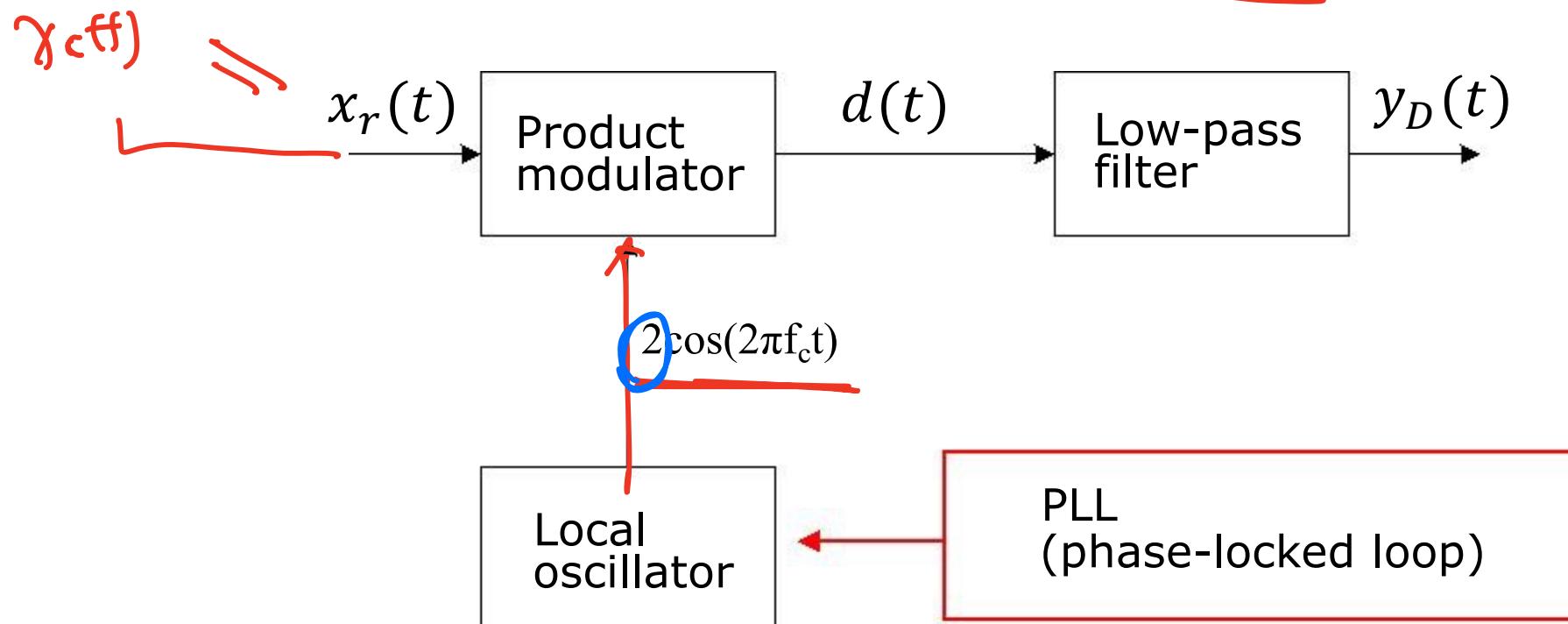


$$X_c(f) = \frac{1}{2} A_c [M(f - f_c) + M(f + f_c)]$$

Demodulation of DSB-SC Signals

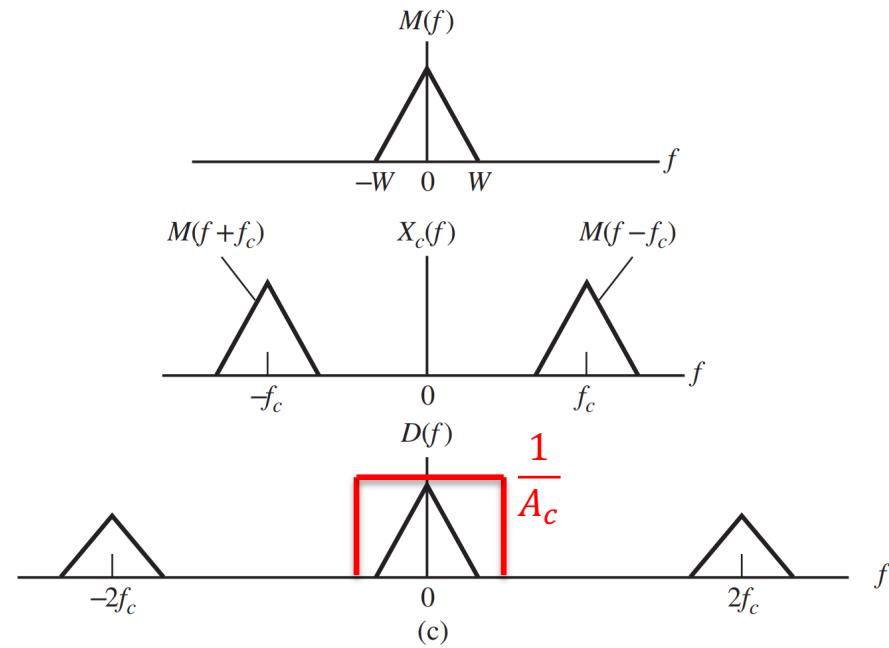
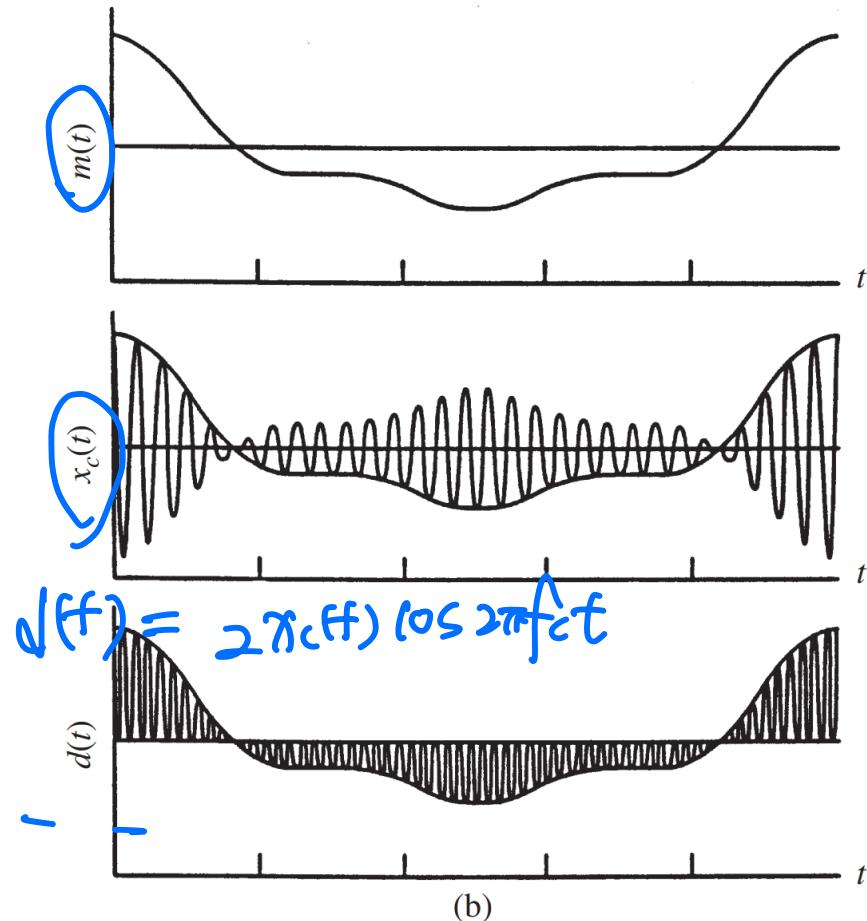
- Phase-coherent demodulation

$$d(t) = \underline{x_c(t)} 2 \cos 2 \pi f_c t = \underline{A_c m(t)} 2 \cos^2 2 \pi f_c t$$
$$= \underline{\underline{A_c m(t)}} + \underline{\underline{A_c m(t)}} \cos 4 \pi f_c t$$



Demodulation of DSB-SC Signals

- DSB-SC demodulation: graphic interpretation



LP filter

Comment on DSB-SC

- Good:
 - 100% power efficient
 - Bad:
 - High transmission bandwidth: $B=2W$
 - Demodulation is difficult: Phase Coherent
 - **Phase error** → serious distortion
- ① Modulation easy
- $\Rightarrow SSB: \underline{B=0}$
- $d(t) = \underline{x_c(t)} \underline{2 \cos(2\pi f_c t + \theta(t))}$
- $= \underline{A_c} \cos \theta(t) m(t) + \underline{A_c m(t)} \cos(4\pi f_c t + \theta(t))$
- $y_D(t) = m(t) \cos \theta(t)$
- Time-varying phase error
- Serious distortion
- How to generate phase coherent demodulation carrier
 - Sol 1: Costas phase-locked loop: Complicate the receiver design
 - Sol 2: Transmit the carrier component with the DSB signal, simplify the demodulation design → **Double-sideband, Large-carrier (DSB-LC)**

Double-sideband, Large-carrier (DSB-LC)

- DSB-LC signal (conventional AM signal) = DSB-SC signal + a carrier term

$$\underline{x_c(t)} = \underline{A_c m(t) \cos 2\pi f_c t} + \underline{A_c \cos 2\pi f_c t} = A_c (1 + m(t)) \cos 2\pi f_c t$$

$$\underline{x_c(t)} = A_c [1 + \underline{am_n(t)}] \cos 2\pi f_c t$$

- a: modulation index, $0 < a \leq 1$
- $m_n(t) = \frac{m(t)}{|\min[m(t)]|} \geq -1$
- Envelope of the AM signal $A_c[1 + am_n(t)]$ is nonnegative for all t

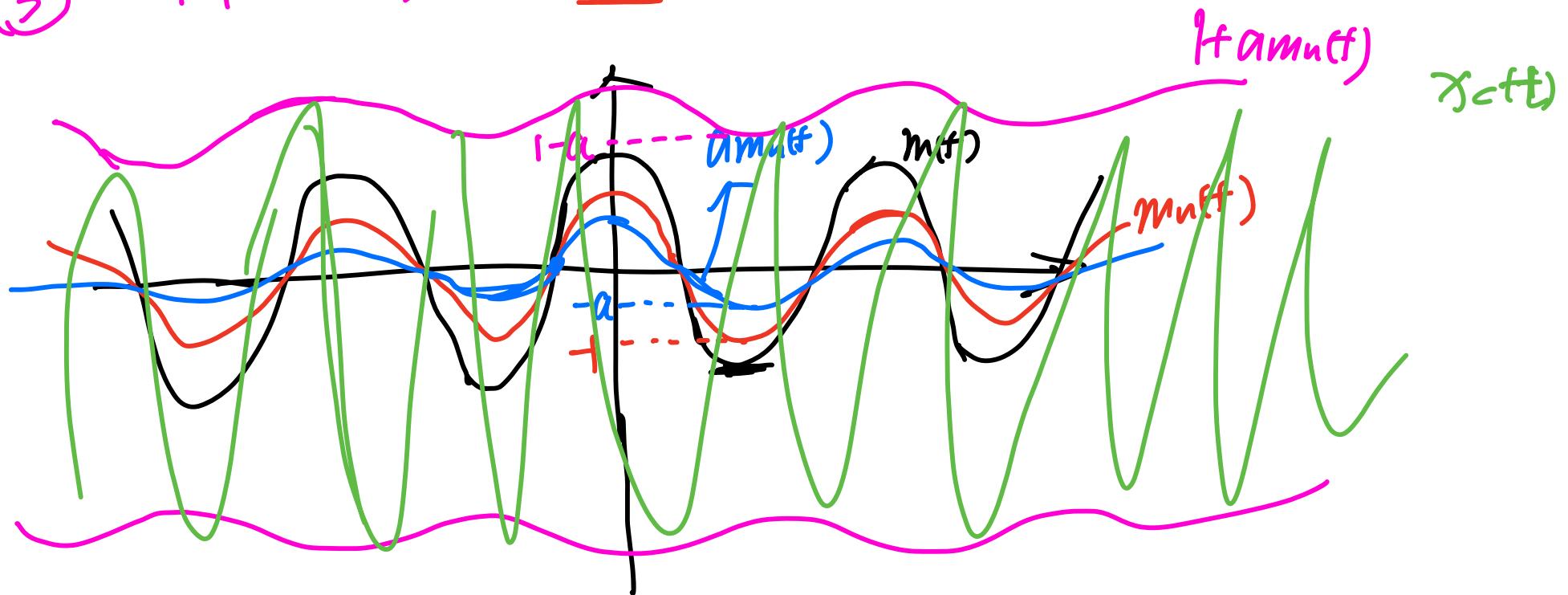
$$\textcircled{1} \quad m_{\text{eff}}(t) = \frac{m(t)}{\left| \min m(t) \right|} \geq -1$$

$$\textcircled{2} \quad a: 0 < a \leq 1$$

$$a m_{\text{eff}}(t) \geq -a \geq -1$$

$$\textcircled{3} \quad 1 + a m_{\text{eff}}(t) \geq 1 - a \geq 0$$

$$\textcircled{4} \quad \begin{aligned} x_{\text{eff}}(t) &= A_c (1 + a m_{\text{eff}}(t)) \cos 2\pi f_c t \\ &= \underline{A_c \cos 2\pi f_c t} \\ &\quad + A_c a m_{\text{eff}}(t) \cos 2\pi f_c t \end{aligned}$$

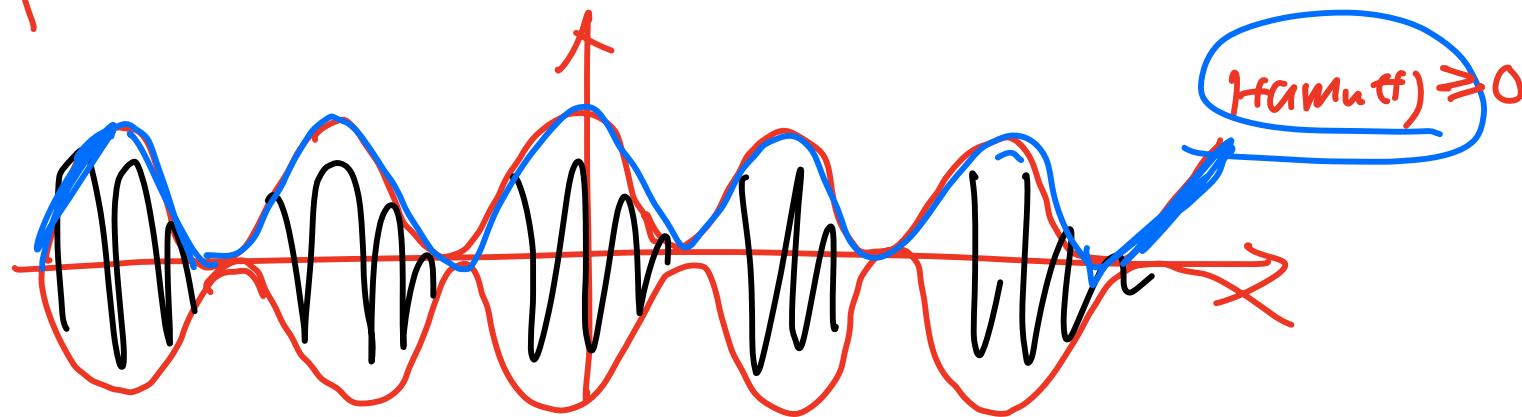


α : Modulation Index

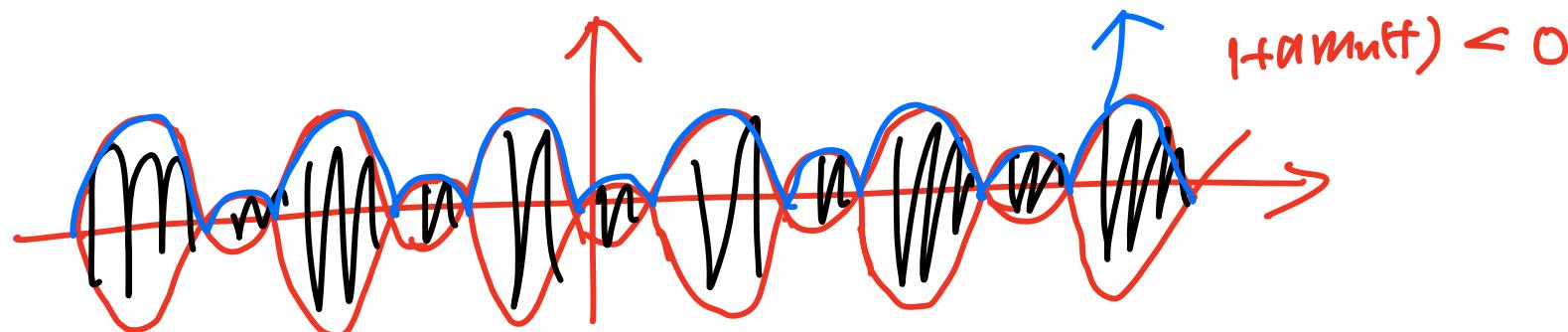
$$0 < \alpha \leq 1$$

$$x_c(t) = A_c(1+a_m(t)) \cos 2\pi f_c t$$

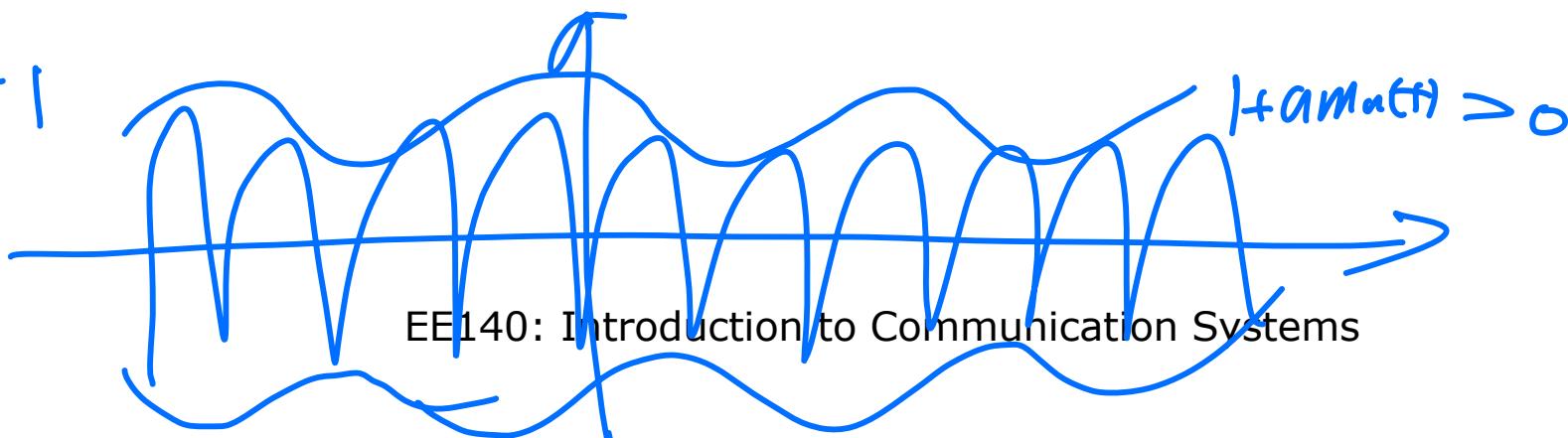
if $\alpha=1$



if $\alpha > 1$

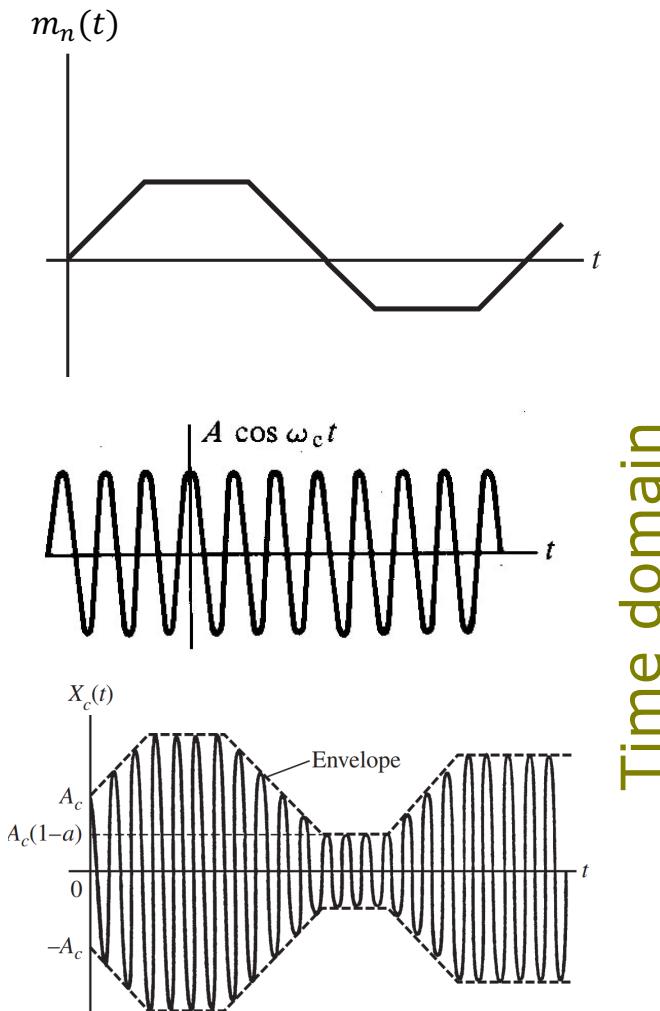


if $\alpha < 1$

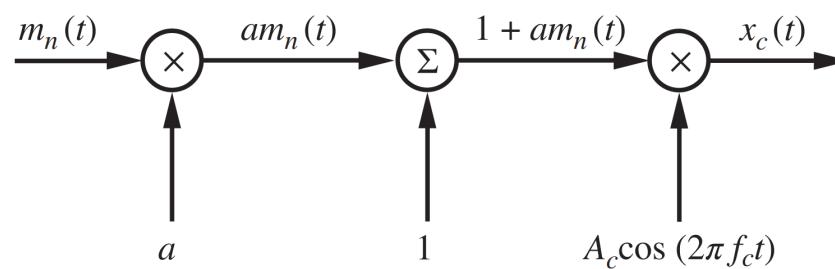


Graphic Interpretation

- DSB-LC signal

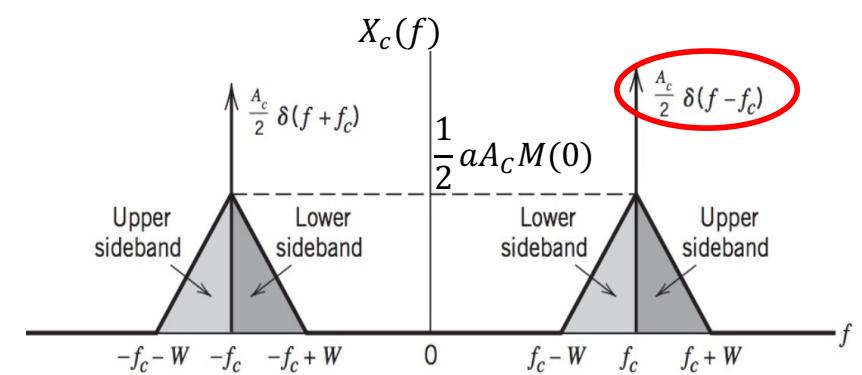
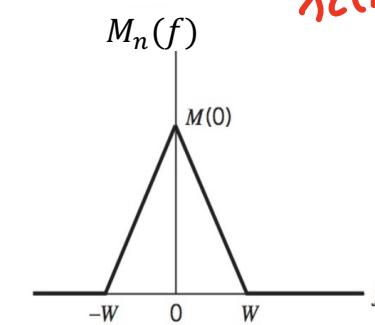


Time domain



$$x_c(t) = A_c \cos 2\pi f_c t + A_c a m_n(t) \cos 2\pi f_c t$$

Frequency domain

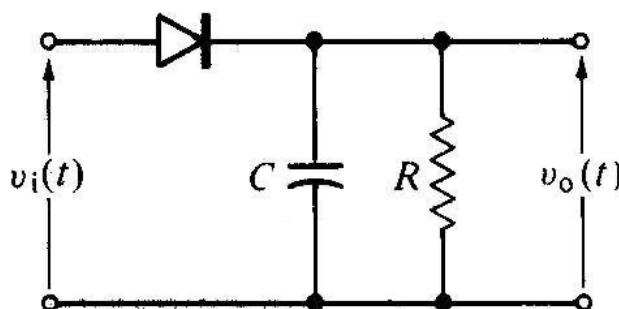


$$B = 2W$$

$$PE < 1$$

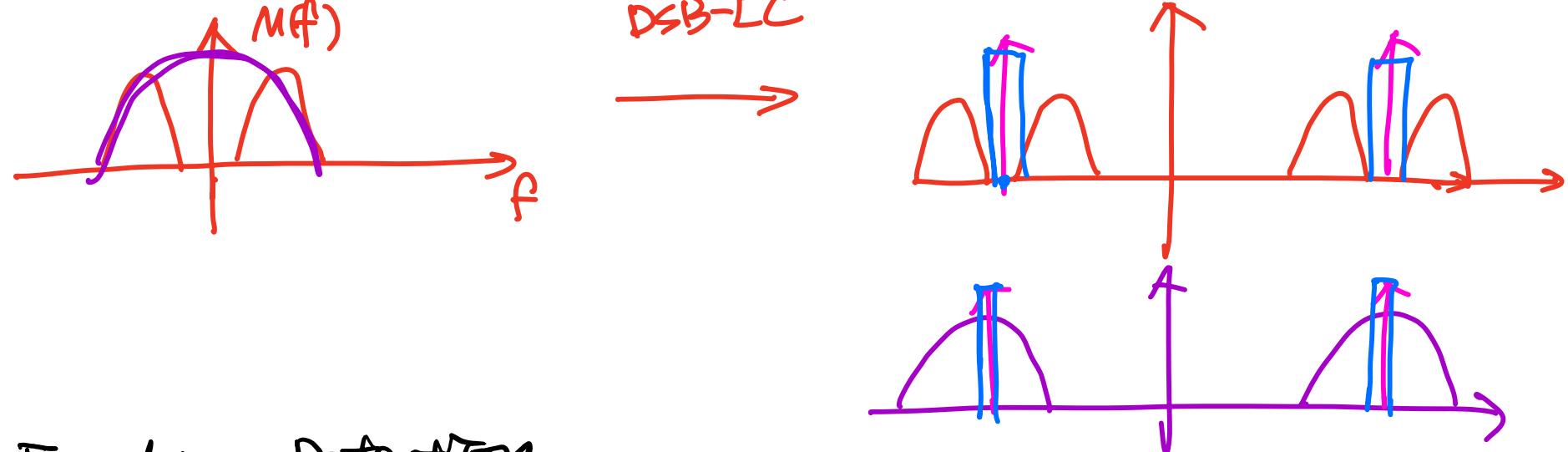
Demodulation of DSB-LC Signals

- Coherent demod: possible, but not easy.
 - Phase and frequency synchronizations are required;
- Noncoherent demod: envelope detection
 - The RC circuit can perform low pass filtering
 - Condition: $1.1 + am_n(t) \geq 0 \iff 0 < a \leq 1, m_n(t) \geq -1$
 2. $f_c \gg W$

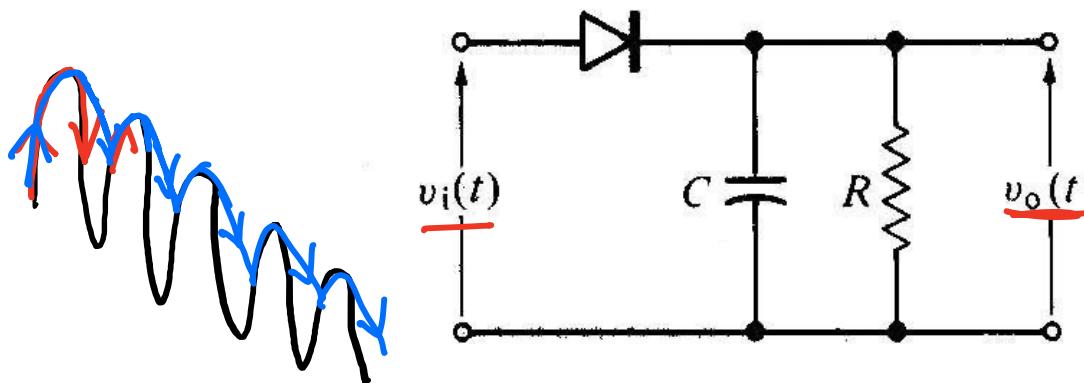


The simplicity of envelop detector has made Conventional AM a practical choice for AM-radio broadcasting

1. Coherent Demodulation

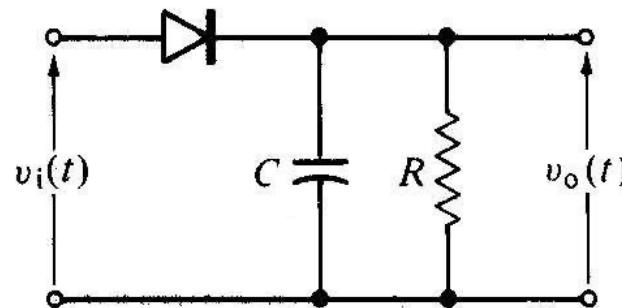


2. Envelope Detection

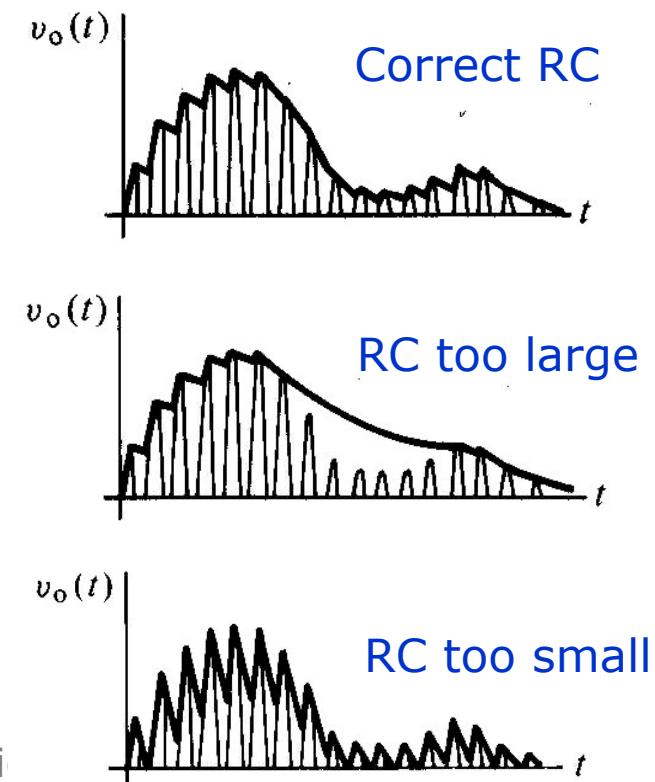


Demodulation of DSB-LC Signals

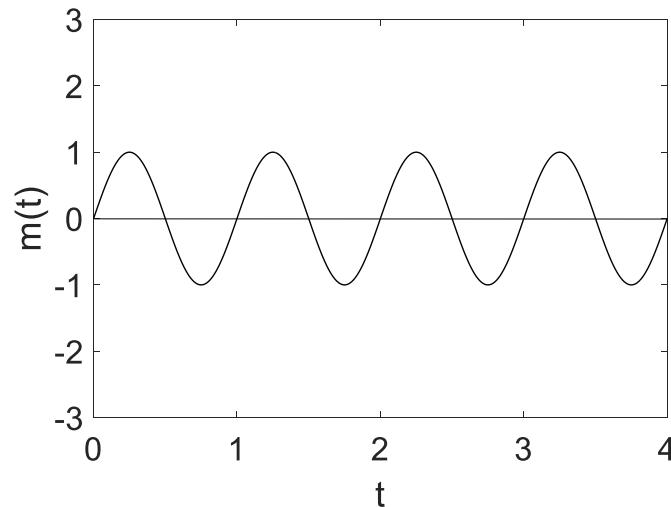
- Coherent demod: possible, but not easy.
 - Phase and frequency synchronizations are required;
- Noncoherent demod: envelope detection
 - The RC circuit can perform low pass filtering
 - Condition: $0 < a \leq 1, m_n(t) \geq -1 \& f_c \gg W$



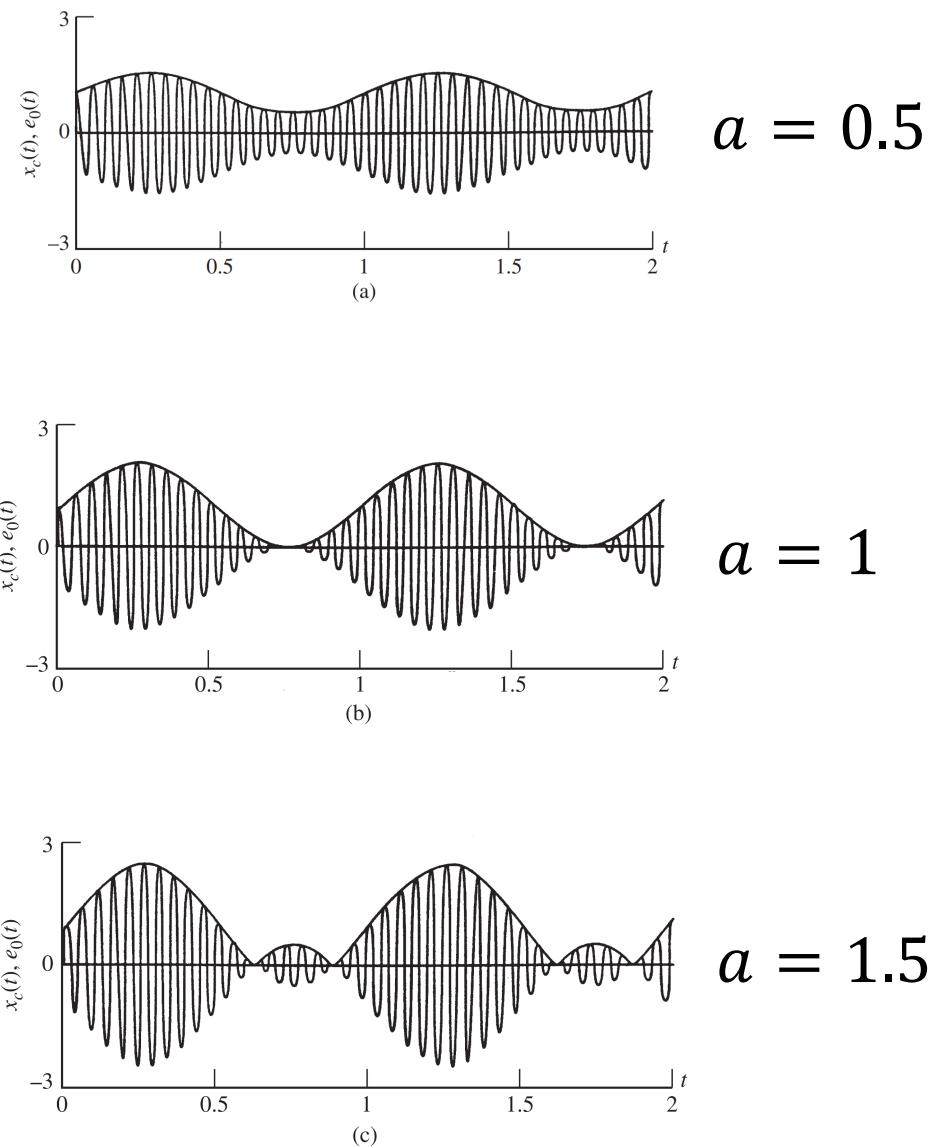
The simplicity of envelop detector has made Conventional AM a practical choice for AM-radio broadcasting



DSB-LC Properties



- The role played by modulation index a
 - $a < 1$: the envelope is always positive.
 - $a = 1$: minimum value of envelope is zero
 - $a > 1$: envelope detection output is badly distorted.



$$X_{eff} = \text{Accusfact} + \text{Acammfact}$$

Transmission Efficiency

- Transmission (modulation,power) efficiency:

$$\begin{aligned}
 \langle x_c^2(t) \rangle &= \langle A_c^2 [1 + am_n(t)]^2 \cos^2(2\pi f_c t) \rangle \\
 &= \left\langle \frac{1}{2} A_c^2 [1 + am_n(t)]^2 (1 + \cos(4\pi f_c t)) \right\rangle \\
 &= \left\langle \frac{1}{2} A_c^2 [1 + am_n(t)]^2 \right\rangle \\
 &= \frac{1}{2} A_c^2 + \frac{1}{2} A_c^2 a^2 \langle m_n^2(t) \rangle
 \end{aligned}$$

$m_n(t)$ is slowly varying w.r.t. carrier
 $m_n(t)$: zero-average
 $\frac{1}{2} A_c^2 (1 + a^2 \langle m_n^2(t) \rangle + 2a \langle am_n(t) \rangle)$

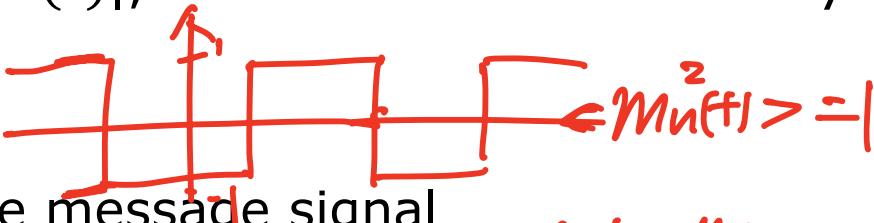
- The transmission efficiency

$$\mu = \frac{P_s}{P_t} = \frac{\frac{1}{2} A_c^2 a^2 \langle m_n^2(t) \rangle}{\frac{1}{2} A_c^2 a^2 \langle m_n^2(t) \rangle + \frac{1}{2} A_c^2} = \frac{a^2 \langle m_n^2(t) \rangle}{a^2 \langle m_n^2(t) \rangle + 1}$$

- If $|\min m(t)| = |\max m(t)|$, the maximum efficiency is 50% for $a=1$.

- $\langle m_n^2(t) \rangle \leq 1$

- Square-wave-type message signal



Comments on μ	$\frac{\langle m_n^2(t) \rangle}{\langle m_n^2(t) \rangle + 1}$
① $\mu < 1$	$\frac{1}{2}$
② $a \uparrow \mu \uparrow a=1 \mu_{max}=$	$\frac{1}{2}$
③ $\langle m_n^2(t) \rangle \uparrow \mu \uparrow$	$\frac{1}{2}$

$$a=1, \mu = \frac{1}{1+1} = 50\%$$

Transmission Efficiency

- The transmission efficiency

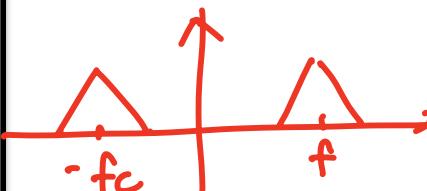
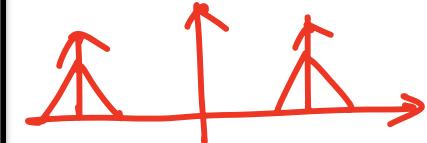
$$\mu = \frac{P_s}{P_t} = \frac{\frac{1}{2}A_c^2 a^2 \langle m_n^2(t) \rangle}{\frac{1}{2}A_c^2 a^2 \langle m_n^2(t) \rangle + \frac{1}{2}A_c^2} = \frac{a^2 \langle m_n^2(t) \rangle}{a^2 \langle m_n^2(t) \rangle + 1}$$

- If $|\min m(t)| = |\max m(t)|$, the maximum efficiency is 50% for $a=1$. $m_{n+T} = m(t)$ $\mu = \frac{\frac{1}{2}}{\frac{1}{2} + 1} = \frac{1}{3}$
- If $m(t) = \cos(2\pi t)$, $\langle m^2(t) \rangle = \frac{1}{2} \rightarrow \mu = 33\%$ for $a=1$.
- For comparison, the transmission efficiency of a DSB-SC system is 100%.

Comment on DSB-LC (AM)

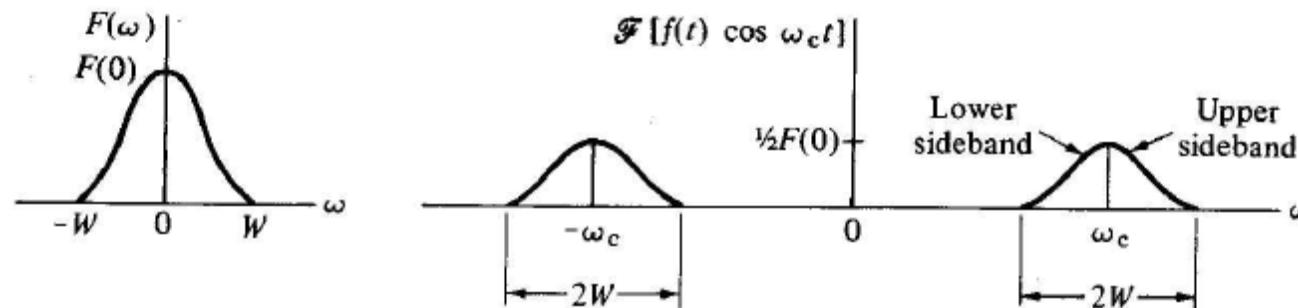
- Good:
 - Demodulation is simple and inexpensive: envelope detection
- Bad:
 - Low power efficiency
 - High transmission bandwidth: $B=2W$

Mod / Demod.

AM	Modulation	Demodulation	Bandwidth	Power	Complexity
DSB-SC	$x_c(t) = m(t)c(t)$	Coherent Dem. $LP(x_c(t) \cdot c(t))$	$B = 2W$	$PE = 1$	Simple / Complicated
					
DSB-LC	$x_c(t) = A_c(1 + a_m(t)) \cos(\pi f_c t)$	Envelope Det. ($0 < a \leq 1$)	$B = 2W$	$PE = \frac{a^2}{\alpha^2 \geq 1}$	Simple / Simple
					
SSB			$B = W$	$PE = 1$	Complicated / Complicated
VSB			$W < B < 2W$	$PE = 1$	Simple / Complicated

Single-sideband (SSB) Modulation

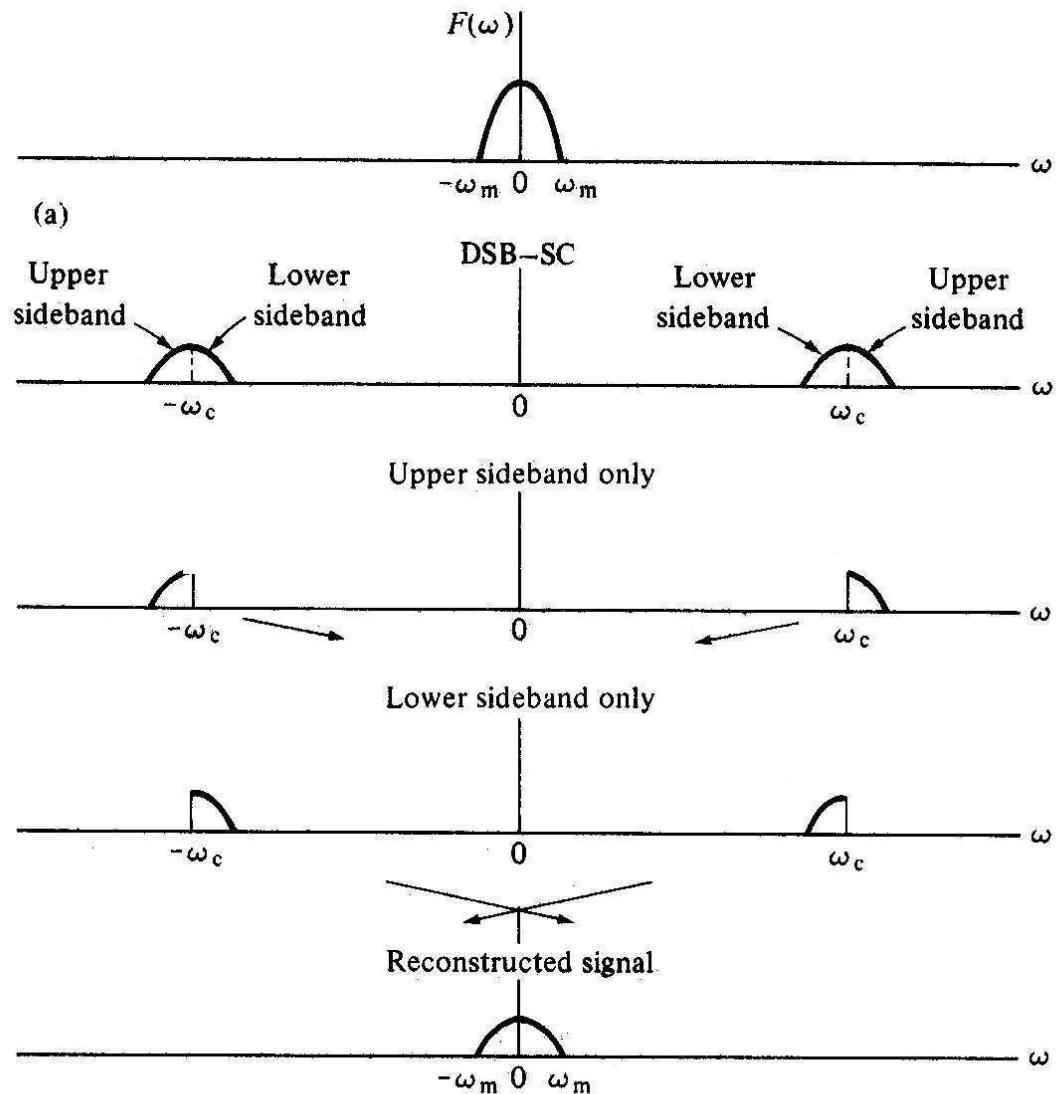
- DSB modulation results in a doubling of the bandwidth of a given signal.



- Each pair of sidebands (i.e. upper or lower) contains the complete information of the original signal.
- The original signal can be recovered again from either the upper or lower pair of sidebands by an appropriate frequency translation. → single-sideband modulation

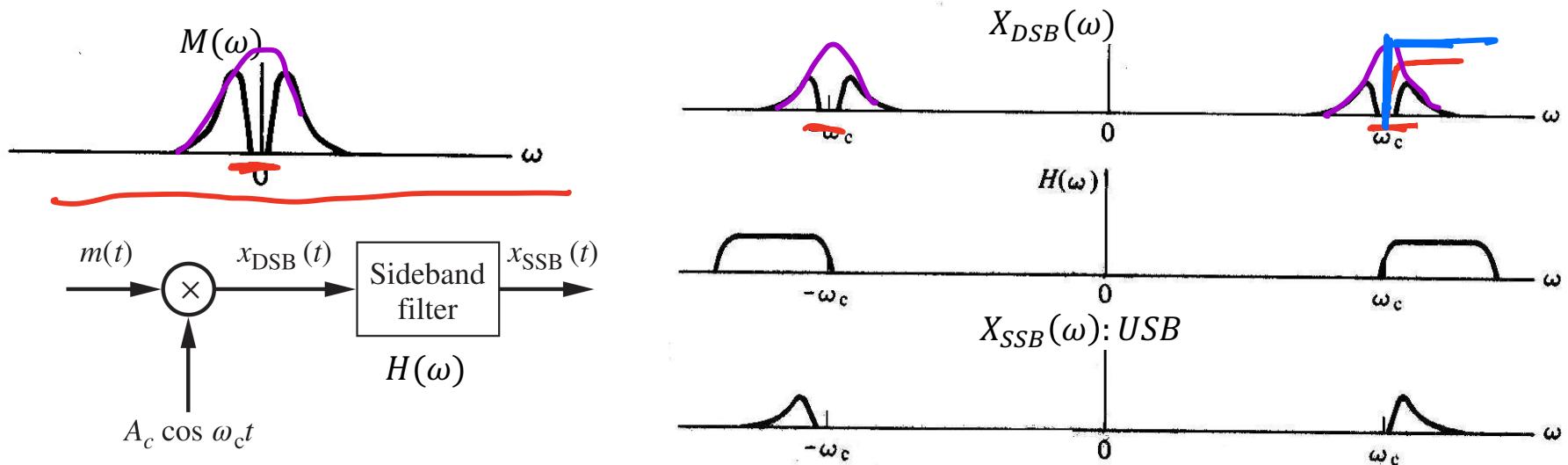
SSB

- Advantage: SSB modulation is efficient because it requires no more bandwidth than that of the original signal and only half that of the corresponding DSB signal.



Generation of SSB Signals

- Generation of SSB signals
- Method 1: sideband filtering
 - generate a DSB-SC signal;
 - filter out one pair of sidebands (upper or lower).
- **Requirement** of method 1:
 - does not contain significant low-frequency components;
 - Ideal filter if low-freq is contained in $m(t)$.



Generation of SSB Signals (Cont'd)

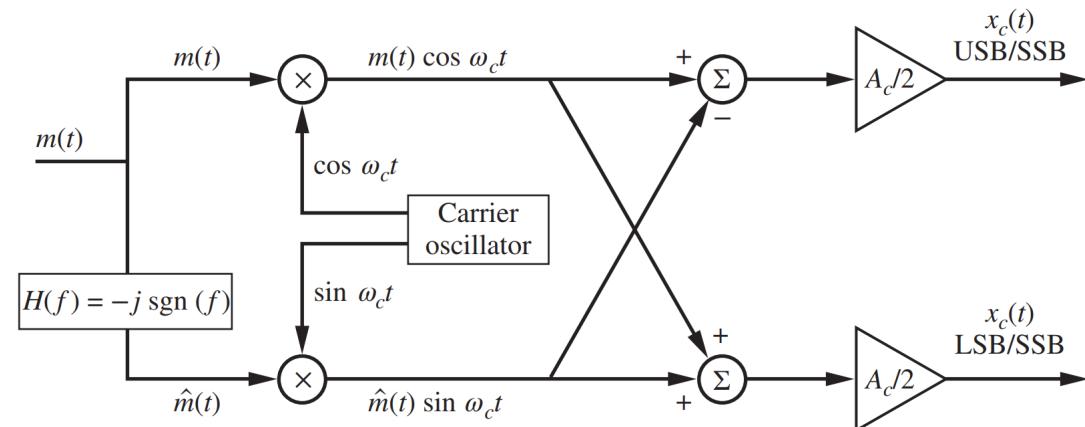
- Method 2: phase-shift

- generate the quadrature function $\hat{m}(t)$ by shifting the phase of $m(t)$ by 90 degrees at each frequency component.
- Upper (SSB+) sideband and lower (SSB-) sideband are given by

$$x_c(t) = x_{SSB\mp}(t) = \frac{1}{2}A_c m(t) \cos 2\pi f_c t \pm \frac{1}{2}A_c \hat{m}(t) \sin 2\pi f_c t$$

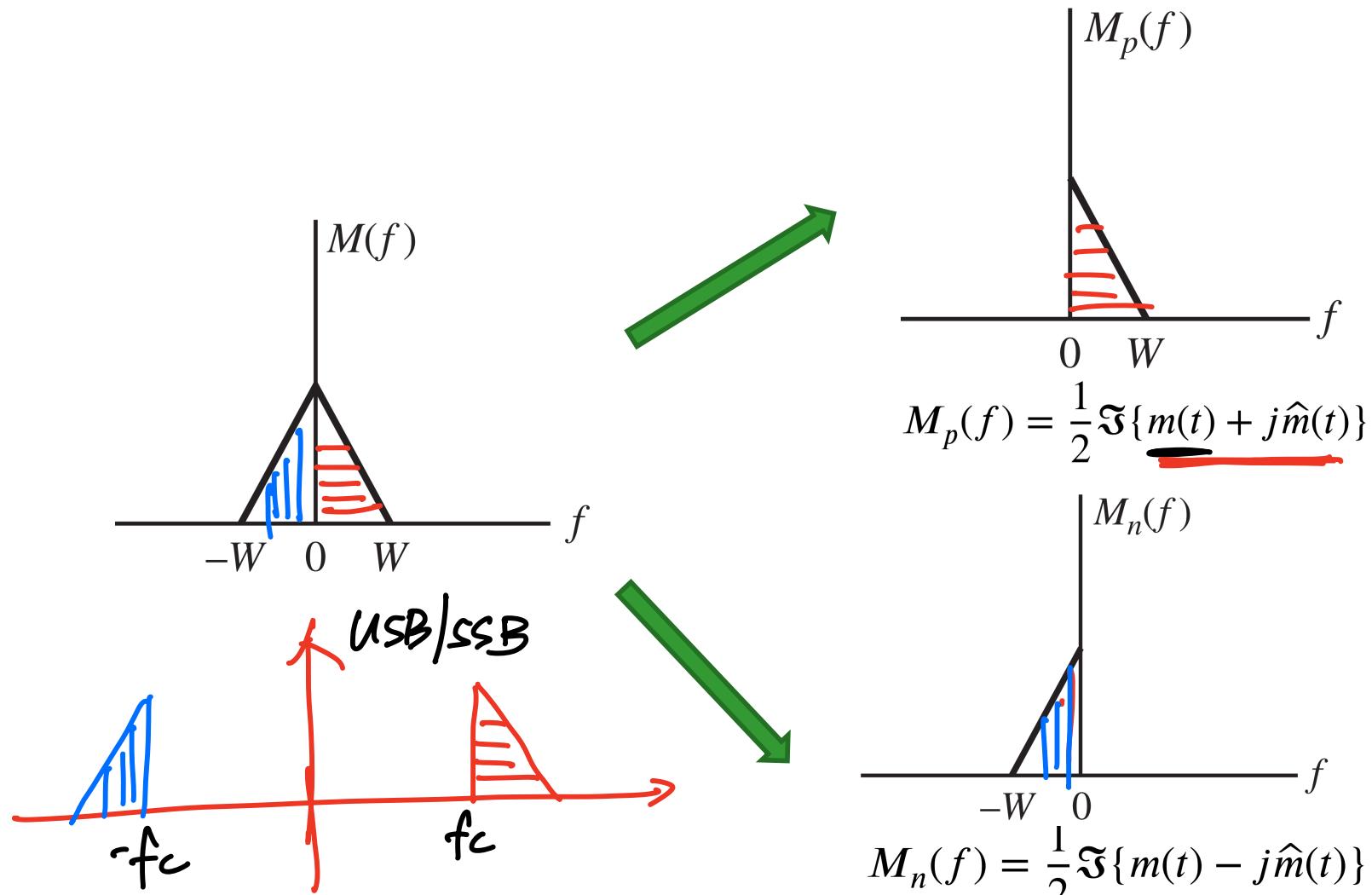
- Requirement:

- phase shifted by exactly 90 degrees.
- Ideal wideband phase shifter



Generation of SSB Signals (Cont'd)

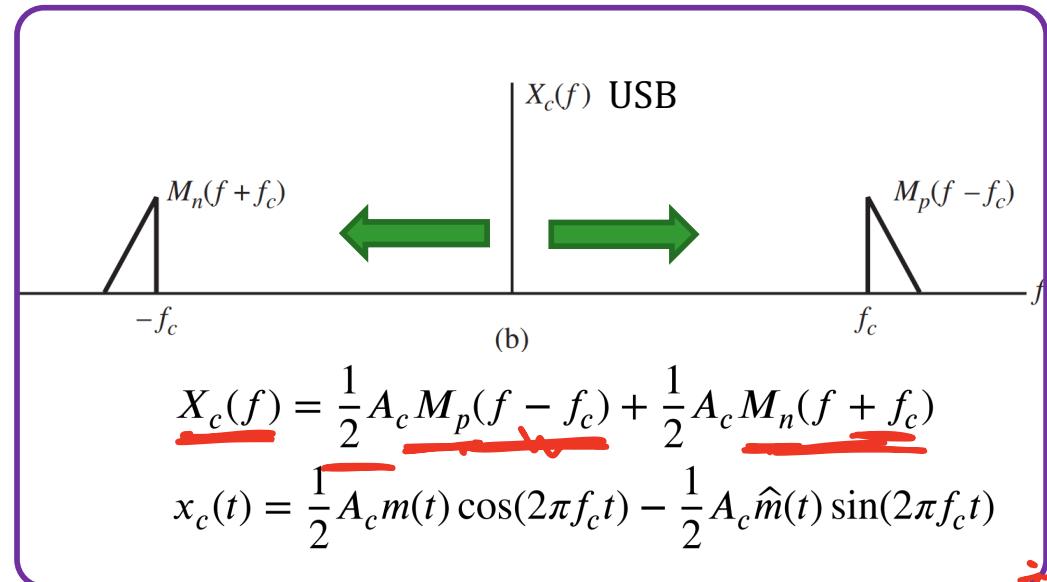
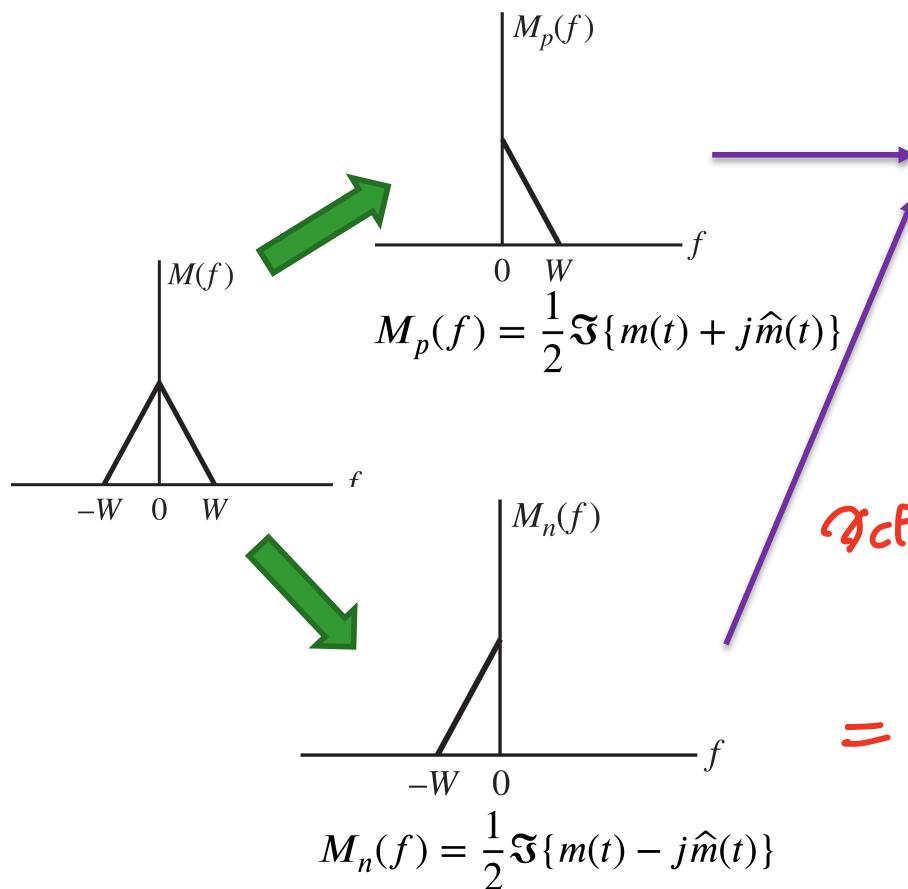
- Method 2: phase-shift



Generation of SSB Signals (Cont'd)

$$DSB \quad X_c(f) = \frac{1}{2}A_c M(f-f_c) + \frac{1}{2}A_c M(f+f_c)$$

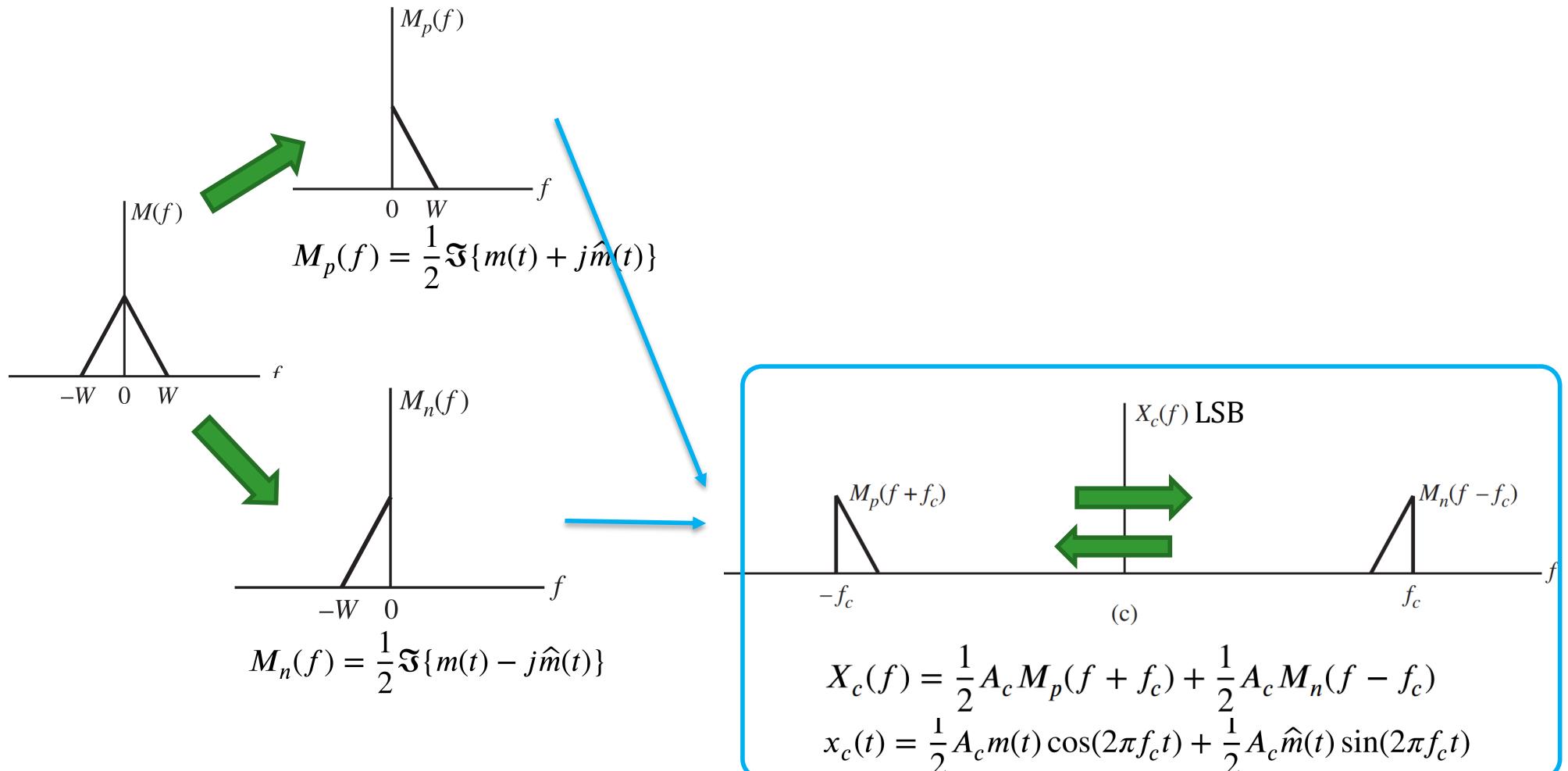
- Method 2: phase-shift



$$\begin{aligned} X_c(f) &= \text{IFT}[X_c(f)] = \frac{1}{2}A_c \left[\frac{1}{2}(m(t) + j\hat{m}(t)) e^{j\pi f_c t} + \frac{1}{2}A_c \left(\frac{1}{2}(m(t) - j\hat{m}(t)) e^{-j\pi f_c t} \right) \right] \\ &= \frac{1}{4}A_c m(t) \left(e^{j\pi f_c t} + e^{-j\pi f_c t} \right) + \frac{1}{4}A_c j \hat{m}(t) \left(e^{j\pi f_c t} - e^{-j\pi f_c t} \right) \\ &= \frac{1}{2}A_c m(t) \cos 2\pi f_c t + \frac{1}{2}A_c j \hat{m}(t) \sin 2\pi f_c t \end{aligned}$$

Generation of SSB Signals (Cont'd)

- Method 2: phase-shift



SSB Demodulation

- Synchronous detection

- Received SSB signal:

$$x_c(t) = \frac{1}{2} A_c m(t) \cos 2\pi f_c t \pm \frac{1}{2} A_c \hat{m}(t) \sin 2\pi f_c t$$

- Local generated carrier signal:

$$C(t) = 4 \cos[2\pi f_c t + \theta(t)]$$

Time-varying
phase error

$$\begin{aligned} x_c(t)C(t) &= [\frac{1}{2} A_c m(t) \cos 2\pi f_c t \pm \frac{1}{2} A_c \hat{m}(t) \sin 2\pi f_c t] 4 \cos[2\pi f_c t + \theta(t)] \\ &= A_c m(t) \{\cos[\theta(t)] + \cos[4\pi f_c t + \theta(t)]\} \mp A_c \hat{m}(t) \{\sin[\theta(t)] - \sin[4\pi f_c t + \theta]\} \end{aligned}$$

- Through a low-pass filter (LPF), the output is given by:

$$y_D(t) = m(t) \cos \theta(t) \mp \hat{m}(t) \sin \theta(t)$$

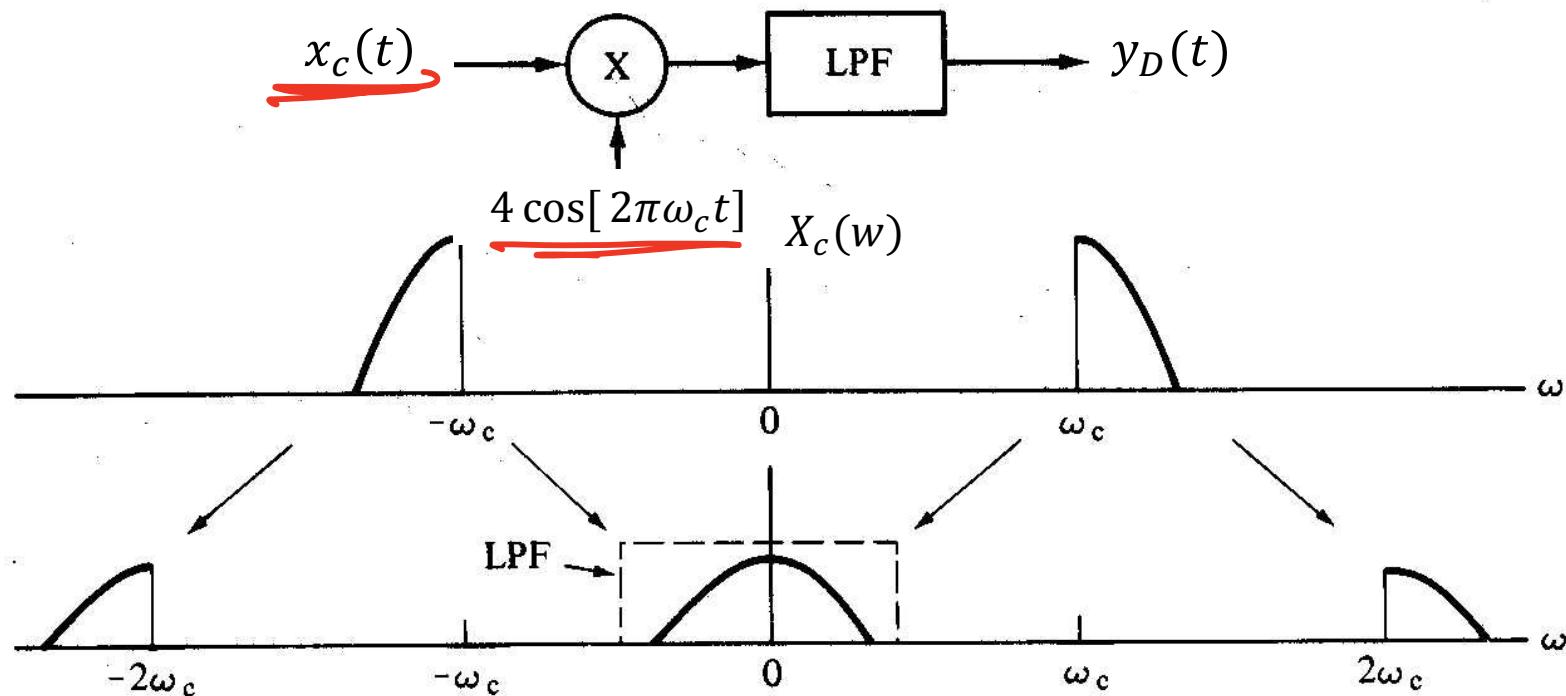
Serious distortion

- If no error

$$y_D(t) = m(t)$$

SSB Demodulation (Cont'd)

- Frequency domain graphic interpretation

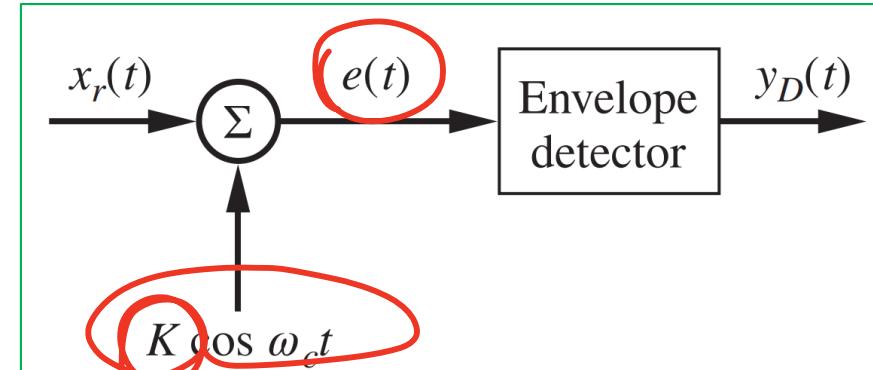


SSB Demodulation

Carrier Reinsertion

- After carrier reinsertion

$$e(t) = \left[\frac{1}{2} A_c m(t) + K \right] \cos 2\pi f_c t \pm \frac{1}{2} A_c \hat{m}(t) \sin 2\pi f_c t$$



- Envelope detection, not straightforward

$$y_D(t) = \sqrt{\left[\frac{1}{2} A_c m(t) + K \right]^2 + \left[\frac{1}{2} A_c \hat{m}(t) \right]^2}$$

$\approx \frac{1}{2} A_c m(t) + K$

[$\frac{1}{2} A_c m(t) + K$]² ≫ [$\frac{1}{2} A_c \hat{m}(t)$]²

- Requirement of envelope detection

- The carrier is much larger than the SSB envelope
- Phase coherent with original modulation carrier

Comments on SSB

- Good:
 - Save spectrum
 - Save energy
- Bad:
 - Complex implementation (modulation and demodulation)

Vestigial-sideband (VSB) Modulation

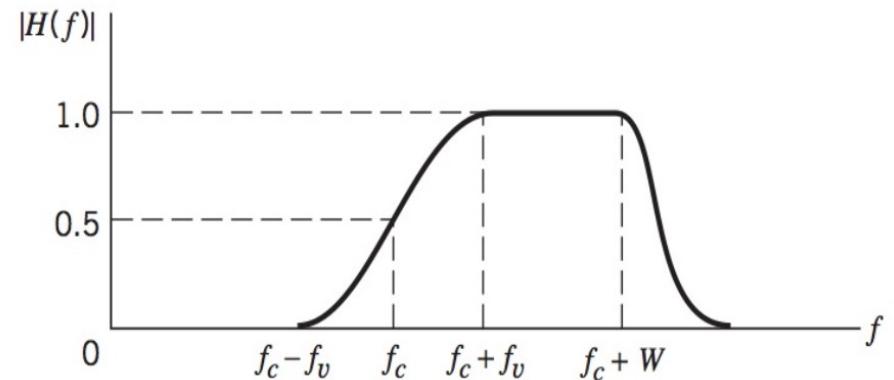
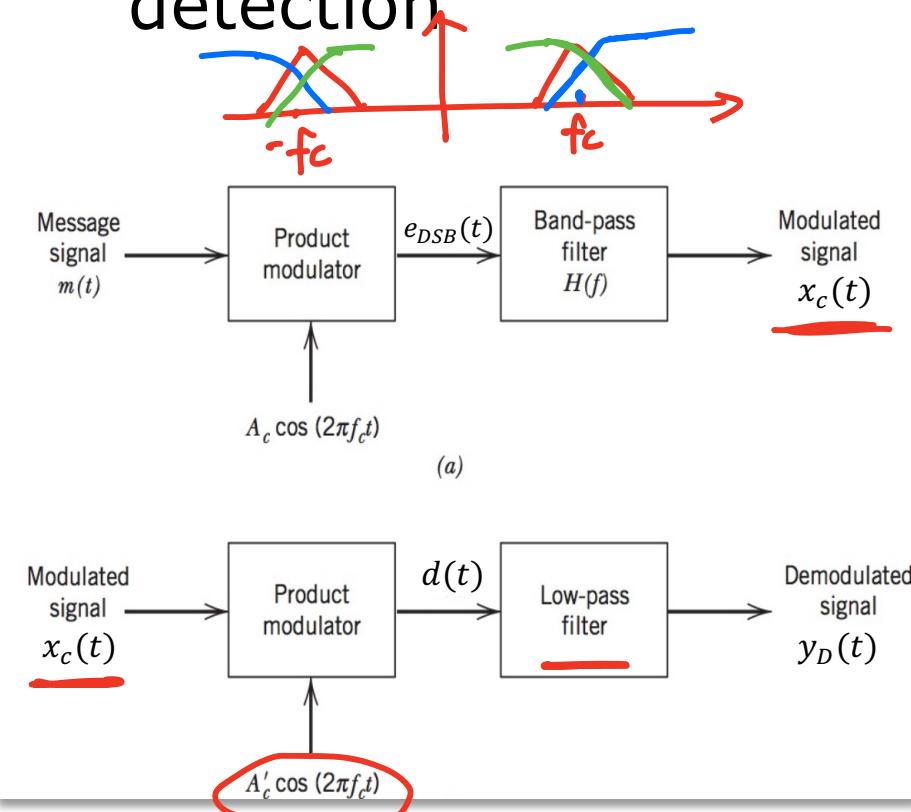
- The generation of SSB signals may be quite difficult when the modulating signal bandwidth is wide or where one cannot disregard the low-frequency components.
- In Vestigial-sideband (VSB) modulation, a portion of one sideband is transmitted.
- VSB is a compromise between SSB and DSB.
- Generation of VSB-SC signals: in frequency domain

$$X_{VSB-SC}(f) = \frac{A_c}{2} [M(f + f_c) + M(f - f_c)] H(f)$$

- Where filter $H(f)$ passes some of the lower (or upper) sideband and most of the upper (or lower) sideband.

Vestigial-sideband (VSB) Modulation

- The requirement on the filter
- Consider coherent detection



$$X_c(f) = \frac{A_C}{2} [M(f + f_c) + M(f - f_c)] H(f)$$

$$d(t) = A'_C x_c(t) \cos 2\pi f_c t$$

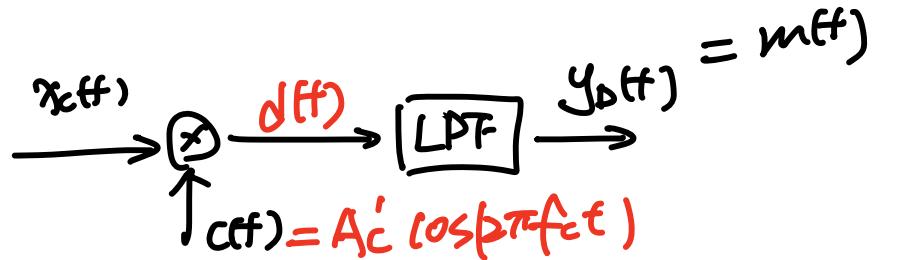
$$D(f) = \frac{A'_C}{2} [X_c(f + f_c) + X_c(f - f_c)] =$$

$$\begin{aligned} &= \frac{A_C A'_C}{4} \{ [H(f - f_c) + H(f + f_c)] M(f) \\ &+ M(f + 2f_c) H(f + f_c) \\ &+ M(f - 2f_c) H(f - f_c) \} \end{aligned}$$

$$Y_D(f) = \frac{A_C A'_C}{4} M(f) [H(f - f_c) + H(f + f_c)]$$

How to design $H(f)$?

$$X_{VSB}(f) = \frac{A_c}{2} [M(f+f_c) + M(f-f_c)] H(f)$$



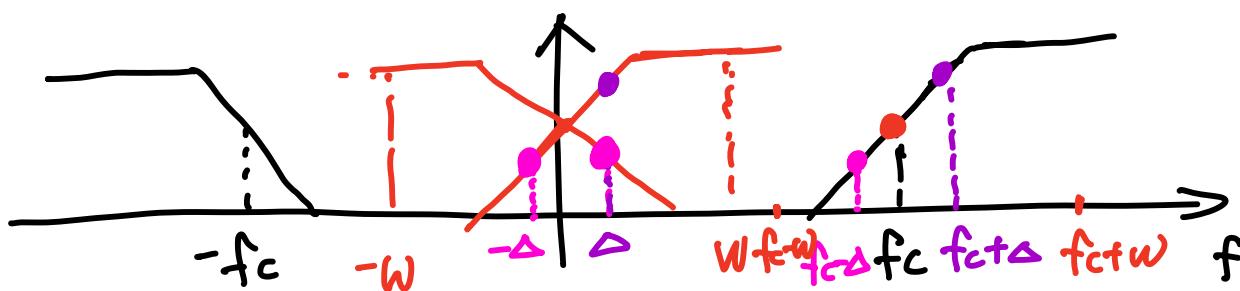
$$d(f) = A_c' x_c(f) \cos 2\pi f_c t$$

$$D(f) = \frac{A_c'}{2} [x_c(f-f_c) + x_c(f+f_c)]$$

$$= \frac{A_c'}{2} \left[\frac{A_c}{2} [M(f) + M(f-f_c)] H(f-f_c) + \frac{A_c}{2} [M(f+2f_c) + M(f)] H(f+f_c) \right]$$

$$\text{LPF}[D(f)] = \frac{A_c A_c'}{4f} [M(f) H(f-f_c) + M(f) H(f+f_c)]$$

$$= \frac{A_c A_c'}{4f} \frac{[H(f-f_c) + H(f+f_c)] M(f)}{|f| \leq w}$$



$$\begin{cases} H(f_c+\Delta) + H(f_c-\Delta) = C = 2H(f_c) & |f| \leq w \\ H(f) \text{ is odd symmetric at } f_c & f_c - w \leq |f| \leq f_c + w \end{cases}$$

EE140: Introduction to Communication Systems

Vestigial-sideband (VSB) Modulation

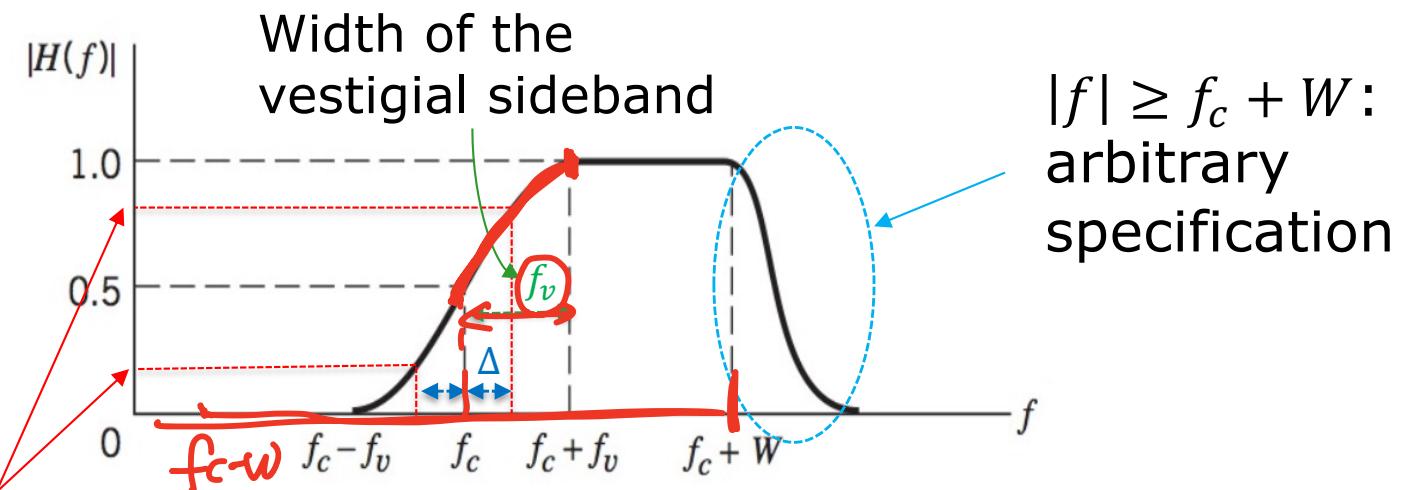
- The requirement on the filter

$$Y_D(f) = \frac{A_c A'_c}{4} M(f)[H(f - f_c) + H(f + f_c)]$$

- Recover the $m(t)$ without distortion

$$H(f - f_c) + H(f + f_c) = 2H(f_c), -W \leq f \leq W$$

- Cutoff portion of $H(f)$ is odd symmetric around f_c .

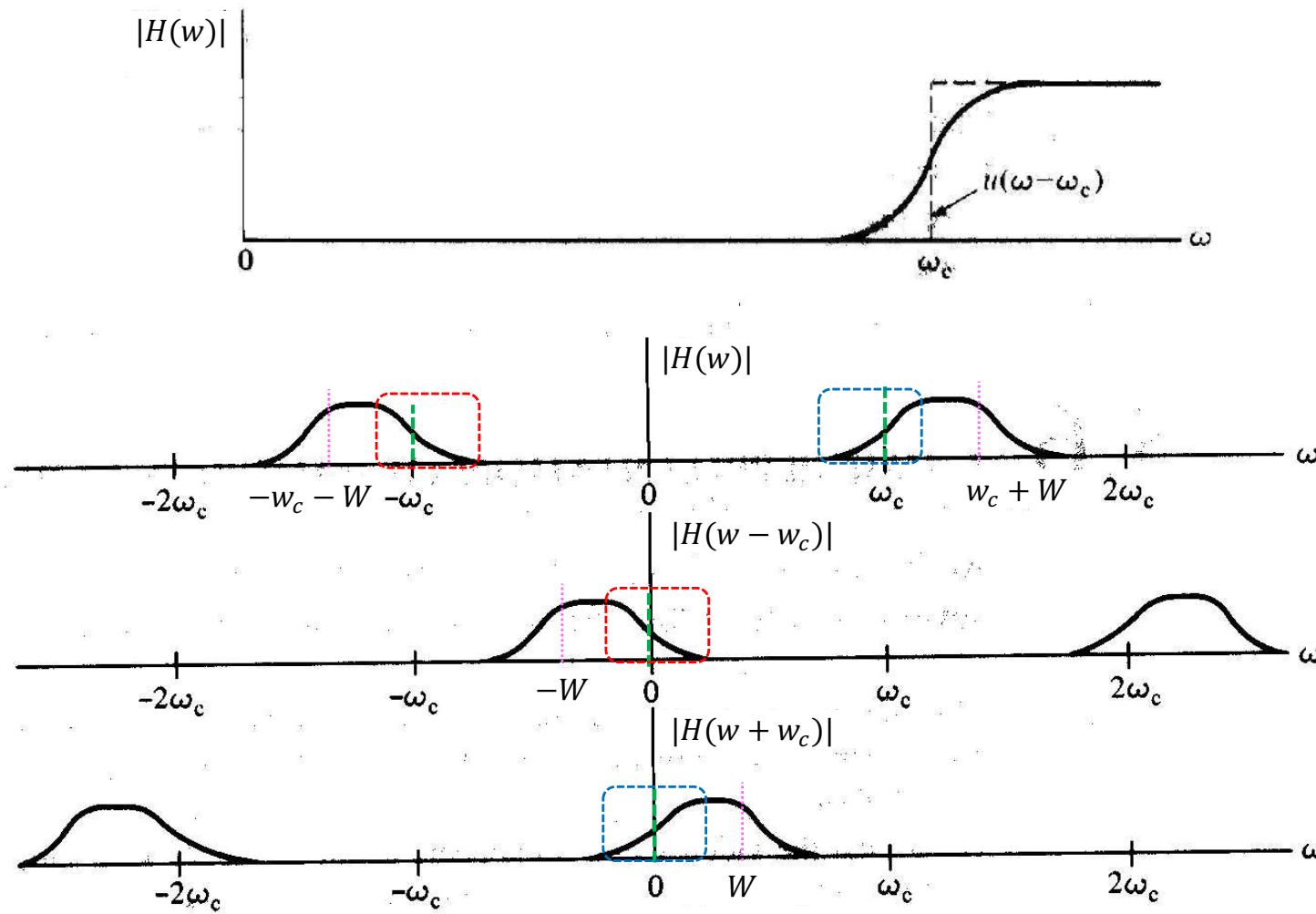


Odd symmetry: $H(f_c + \Delta) + H(f_c - \Delta) = 2H(f_c), |\Delta| \leq f_v$

44

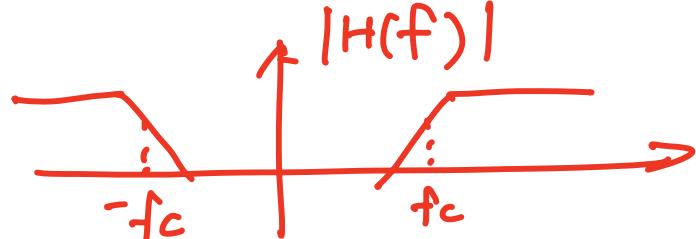
VSB Modulation (Cont'd)

- Frequency domain graphic interpretation



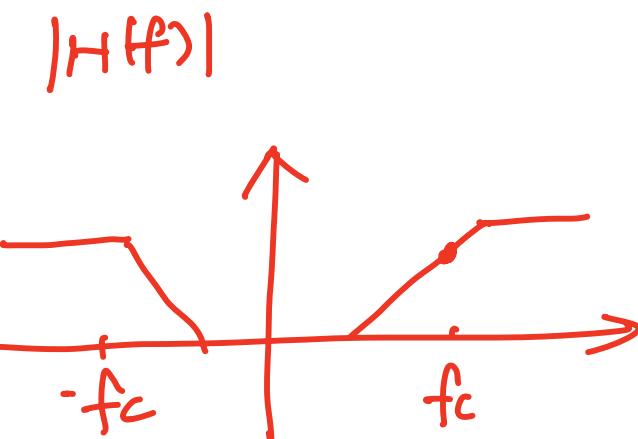
$$\underline{M(f)} \underline{[H(f - f_c) + H(f + f_c)]}$$

Case1: $[H(f - f_c) + H(f + f_c)] = C$

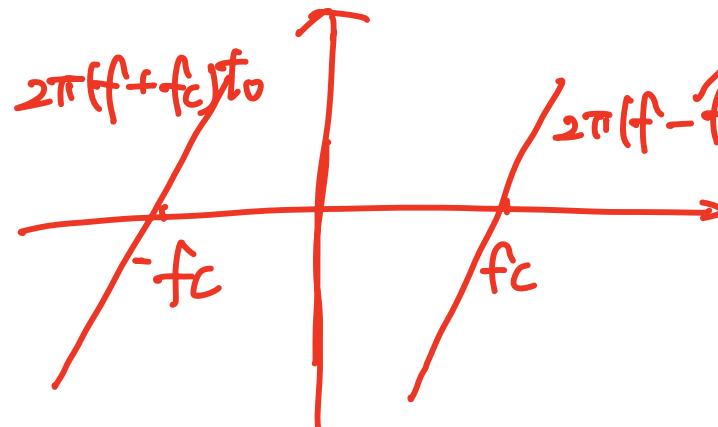


$$H(f_c + \Delta) + H(f_c - \Delta) \Rightarrow H(f_c), |\Delta| \leq \omega$$

Case2: $[H(f - f_c) + H(f + f_c)] = \underline{C e^{j2\pi f t_0}}$

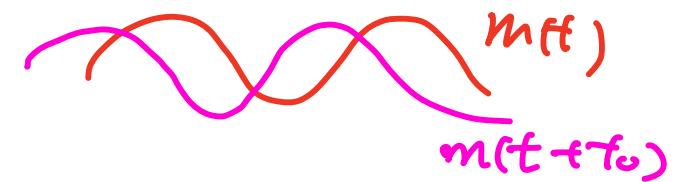


$$\angle H(f)$$

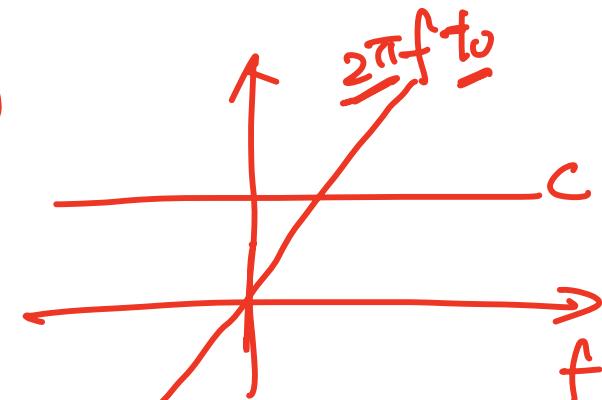


$$|H(f_c + \Delta)| + |H(f_c - \Delta)|$$

$$= C, |\Delta| \leq \omega$$



$$\angle H(f) = 0$$



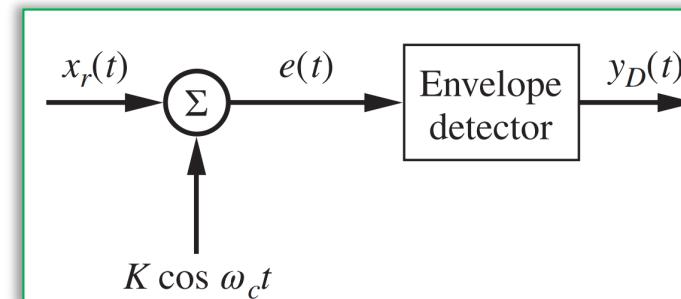
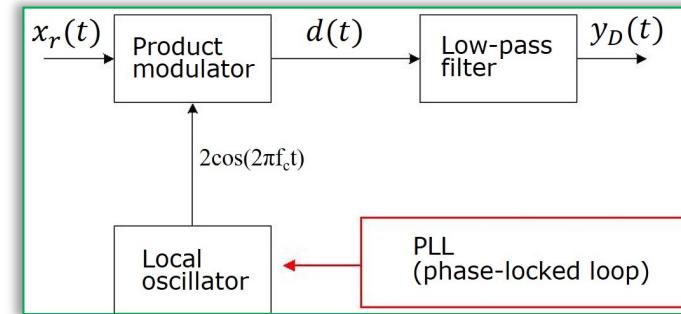
Comparison of AM Techniques

- DSB-SC:
 - more power efficient. Seldom used
- DSB-LC (AM):
 - simple envelop detector
 - Example: AM radio broadcast
- SSB:
 - requires minimum transmitter power and bandwidth. Suitable for point-to-point and over long distances
- VSB:
 - bandwidth requirement between SSB and DSBSC.
 - Example: TV transmission



Comparison of AM Techniques

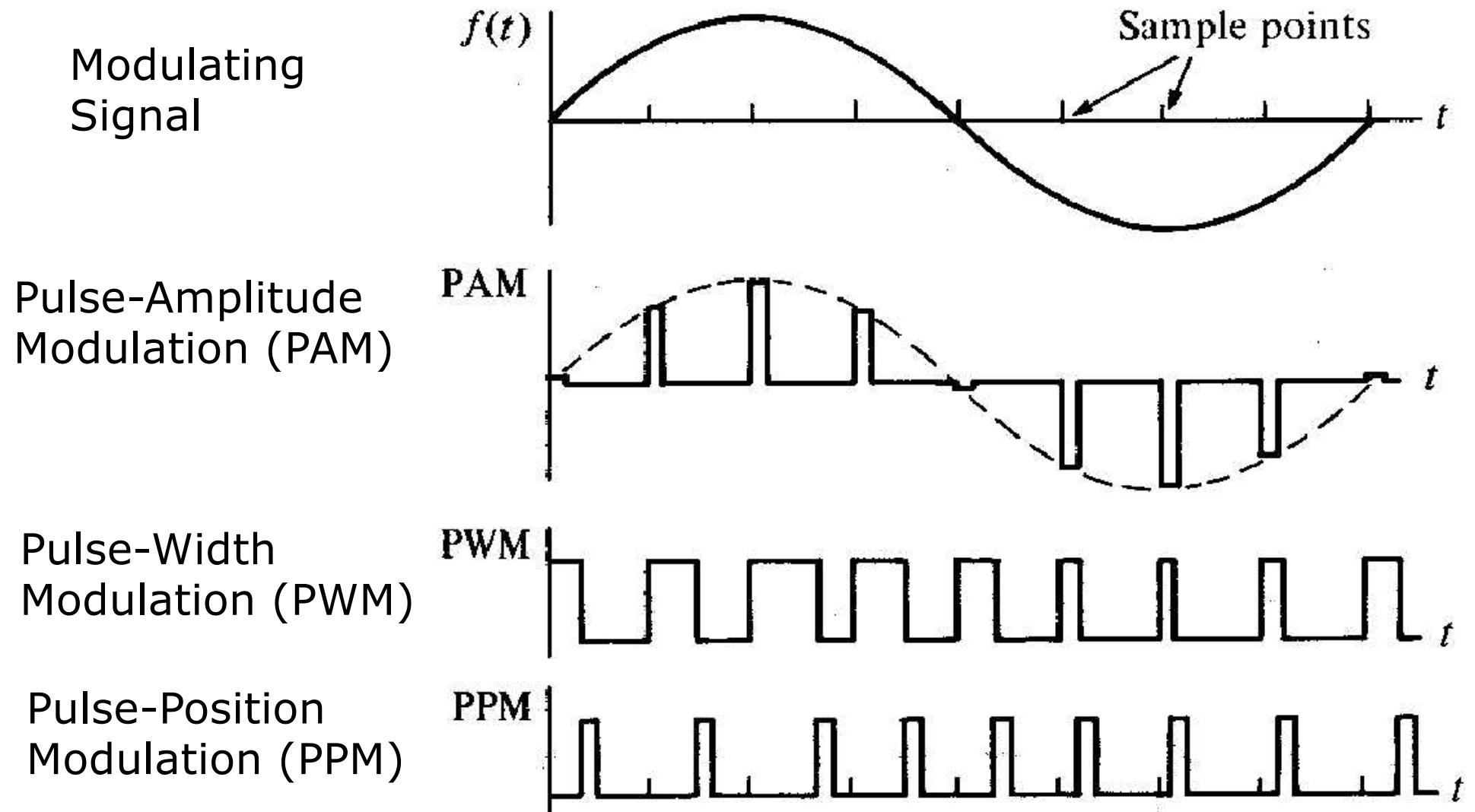
- Demodulation
 - Coherent Demodulation
 - All linear modulation
 - Envelope Detection
 - DSB-LC(AM)
 - SSB + Carrier reinsertion
 - VSB + Carrier reinsertion



Contents

- Analog Modulation
 - Amplitude modulation
 - Pulse amplitude modulation
 - Angle modulation (phase/frequency)

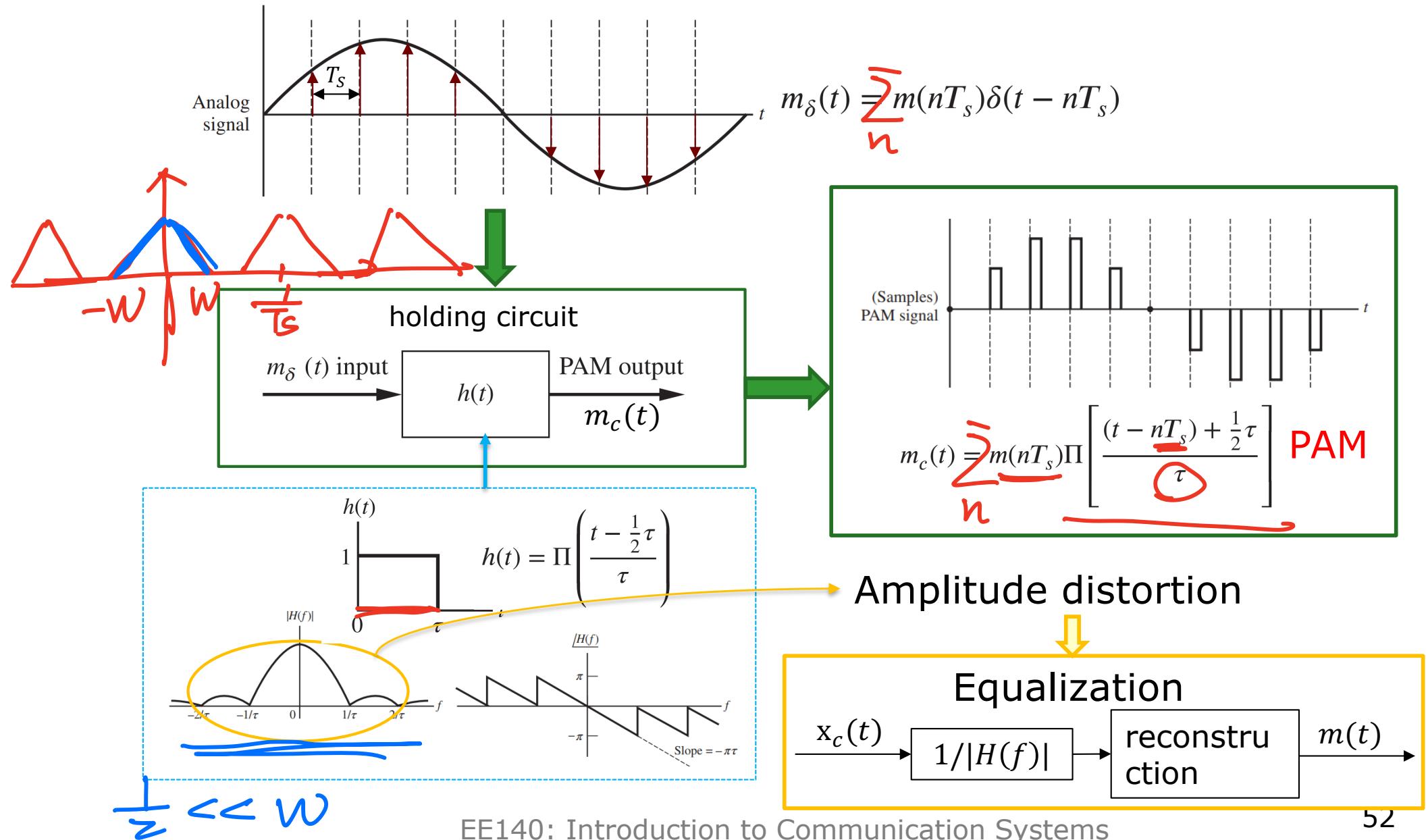
Analog Pulse Modulation



Analog Pulse Modulation (cont'd)

- PAM: constant-width, uniformly spaced pulses whose amplitude is proportional to the values of the input at the sampling instants.
- PWM: constant-amplitude pulses whose width is proportional to the values of the input at the sampling instants.
- PPM: constant-width, constant-amplitude pulses whose position is proportional to the values of the input at the sampling instants.

Pulse Amplitude Modulation (PAM)





上海科技大学
ShanghaiTech University

Thanks for your kind attention!

Questions?