

VE320 Intro to Semiconductor Devices

Summer 2024 — Problem Set 6

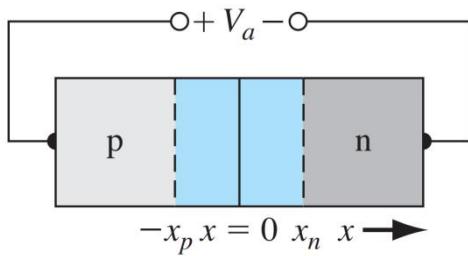
Due: 11:59pm 10th July

Note: In the following problems, assume $T = 300\text{K}$ and the following parameters unless otherwise stated.

For silicon pn junctions: $D_n = 25\text{cm}^2/\text{s}$, $D_p = 10\text{cm}^2/\text{s}$, $\tau_{n0} = 5 \times 10^{-7}\text{s}$, $\tau_{p0} = 10^{-7}\text{s}$

For GaAs pn junctions: $D_n = 205\text{cm}^2/\text{s}$, $D_p = 9.8\text{cm}^2/\text{s}$, $\tau_{n0} = 5 \times 10^{-8}\text{s}$, $\tau_{p0} = 10^{-8}\text{s}$

- 1) Explain the physical mechanism of the a) generation current and b) recombination current in depletion region of pn junction
- 2) Consider an ideal pn junction diode at $T = 300\text{K}$ operating in the forward-bias region.
 - a) Calculate the change in diode voltage that will cause a factor of 10 increase in current.
 - b) Repeat part a) for a factor of 100 increase in current.
- 3) Consider an ideal silicon pn junction diode with the geometry shown in the figure.



The doping concentrations are $N_a = 5 \times 10^{16}\text{cm}^{-3}$ and $N_d = 1.5 \times 10^{16}\text{cm}^{-3}$, and the minority carrier lifetimes are $\tau_{n0} = 2 \times 10^{-7}\text{s}$, $\tau_{p0} = 8 \times 10^{-8}\text{s}$. The cross-sectional area is $A = 5 \times 10^{-4}\text{cm}^2$. Calculate:

- a) the ideal reverse-saturation current due to holes
 - b) the ideal reverse-saturation current due to electrons
 - c) the hole concentration at $x = x_n$ for $V_a = 0.8V_{bi}$
 - d) the electron current at $x = x_n$ for $V_a = 0.8V_{bi}$
 - e) the electron current at $x = x_n + (1/2)L_p$ for $V_a = 0.8V_{bi}$
- 4) Consider an ideal GaAs pn junction diode.
 - a) What must be the ratio of N_d/N_a so that 90 percent of the current in the depletion region is due to the flow of electrons?
 - b) Repeat part a) if 80 percent of the current in the depletion region is due to the flow of holes.
 - 5) The reverse-biased saturation current is a function of temperature.
 - a) Assuming that I_s varies with temperature only from the intrinsic carrier concentration, show that we can write $I_s = CT^3 \exp(-E_g/kT)$ where C is a constant and a function only of the diode parameters.
 - b) Determine the increase in I_s as the temperature increases from $T = 300\text{K}$ to $T = 400\text{K}$ for a
 - (i) germanium diode

- 2) Consider an ideal pn junction diode at $T = 300K$ operating in the forward-bias region.
 a) Calculate the change in diode voltage that will cause a factor of 10 increase in current.
 b) Repeat part a) for a factor of 100 increase in current.

$$I = I_s \cdot (e^{\frac{V_a}{V_t}} - 1) \quad \Rightarrow \quad \frac{I'}{I} = \frac{e^{\frac{V'_a}{V_t}} - 1}{e^{\frac{V_a}{V_t}} - 1} = e^{\frac{V'_a - V_a}{V_t}}$$

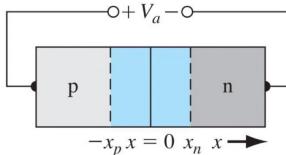
and at $T = 300K$, $V_t = 0.0259V$

$$I' = I_s \cdot (e^{\frac{V'_a - V_a}{V_t}} - 1)$$

a) $\frac{I'}{I} = e^{\frac{V'_a - V_a}{0.0259}} = 10 \Rightarrow V'_a - V_a = 0.0259 \ln 10 = 0.06V$

b) $\frac{I'}{I} = 100 \Rightarrow V'_a - V_a = 0.0259 \ln 100 = 0.12V$

- 3) Consider an ideal silicon pn junction diode with the geometry shown in the figure.



The doping concentrations are $N_p = 5 \times 10^{16} \text{ cm}^{-3}$ and $N_n = 1.5 \times 10^{16} \text{ cm}^{-3}$, and the minority carrier lifetimes are $\tau_{n0} = 2 \times 10^{-7} \text{ s}$, $\tau_{p0} = 8 \times 10^{-8} \text{ s}$. The cross-sectional area is $A = 5 \times 10^{-4} \text{ cm}^2$. Calculate:

- the ideal reverse-saturation current due to holes
- the ideal reverse-saturation current due to electrons
- the hole concentration at $x = x_n$ for $V_a = 0.8V_{bi}$
- the electron current at $x = x_n$ for $V_a = 0.8V_{bi}$
- the electron current at $x = x_n + (1/2)L_p$ for $V_a = 0.8V_{bi}$

a) $I_{sp} = J_{sp} \cdot A = e n_i^2 \left(\frac{1}{N_d} \sqrt{\frac{D_p}{\tau_{p0}}} \right) \cdot A = 1.6 \times 10^{-19} \cdot (1.5 \times 10^{16})^2 \cdot \left(\frac{1}{1.5 \times 10^{16}} \cdot \sqrt{\frac{10}{8 \times 10^{-8}}} \right) 5 \times 10^{-4}$
 $= 1.342 \times 10^{-14} \text{ A}$

b) $I_{sn} = J_{sn} \cdot A = e n_i^2 \left(\frac{1}{N_n} \sqrt{\frac{D_n}{\tau_{n0}}} \right) \cdot A = 4.025 \times 10^{-15} \text{ A}$

c) $p_n(x=x_n) = p_{n0} e^{\frac{eV_a}{kT}} = \frac{n_i^2}{N_n} e^{\frac{e \cdot 0.8V_{bi}}{kT}}$ where $V_{bi} = V_t \ln \frac{N_p N_n}{n_i^2} = 0.747V$

$\Rightarrow p_n(x=x_n) = 1.57 \times 10^{14} \text{ cm}^{-3}$

d) $I_n(x=x_n) = I_{sn} \cdot (e^{\frac{V_a}{V_t}} - 1) = 4.22 \times 10^{-5} \text{ A}$

e) $I_n(x=x_n + \frac{1}{2}L_p) = I_n(x=x_n) \cdot e^{-\frac{x}{L_p}} = 2.56 \times 10^{-5} \text{ A}$

- 1) Explain the physical mechanism of the a) generation current and b) recombination current in depletion region of pn junction

- The generation current in the depletion region of a pn junction arises when electron-hole pairs are generated by thermal energy, leading to a drift of electrons towards the n-region and holes towards the p-region due to the electric field.
- The recombination current occurs when electrons from the n-region and holes from the p-region recombine in the depletion region, resulting in a reduction of the number of charge carriers and contributing to the overall current flow across the junction. These processes are influenced by the electric field in the depletion region, which separates the charge carriers, thereby sustaining the generation and recombination currents.

4) Consider an ideal GaAs pn junction diode.

- a) What must be the ratio of N_d/N_a so that 90 percent of the current in the depletion region is due to the flow of electrons?

- b) Repeat part a) if 80 percent of the current in the depletion region is due to the flow of holes.

a)

$$\frac{I_n}{J_p} = \frac{I_n}{I_p} = \frac{e D_n n_{p0}}{L_n} \cdot \frac{L_p}{e D_p p_{n0}} = \frac{D_n}{\sqrt{D_n T_{n0}}} \cdot \frac{n_i^2}{N_a} \cdot \sqrt{D_p T_{p0}} \cdot \frac{1}{D_p} \frac{N_d}{n_i^2} = \frac{N_d}{N_a} \sqrt{\frac{T_{p0} D_n}{T_{n0} D_p}} = 9$$

$$\Rightarrow \frac{N_d}{N_a} = 9 \cdot \sqrt{\frac{T_{n0} D_n}{T_{p0} D_p}} = 9 \times \sqrt{\frac{5 \times 10^{-8} \times 9.8}{10^{-8} \times 205}} = 4.4$$

$$b) \frac{N_d}{N_a} = 4 \times \sqrt{\frac{5 \times 10^{-8} \times 9.8}{10^{-8} \times 205}} = 0.122$$

5) The reverse-biased saturation current is a function of temperature.

- a) Assuming that I_s varies with temperature only from the intrinsic carrier concentration, show that we can write $I_s = CT^3 \exp(-E_g/kT)$ where C is a constant and a function only of the diode parameters.

- b) Determine the increase in I_s as the temperature increases from $T = 300K$ to $T = 400K$ for a
(i) germanium diode (ii) silicon diode

a) effective density of states : $N_c = N_{c300} T^{\frac{3}{2}}$, $N_v = N_{v300} T^{\frac{3}{2}}$

intrinsic carrier concentration : $n_i^2 = N_c N_v e^{-\frac{E_g}{kT}} = N_{c300} N_{v300} T^3 e^{-\frac{E_g}{kT}}$

\Rightarrow reverse saturation current is given by : $I_s = J_A = e A \left(\frac{D_p}{L_p} \frac{n_i^2}{N_d} + \frac{D_n}{L_n} \frac{n_i^2}{N_a} \right)$

$= e A \left(\frac{D_p}{L_p N_d} + \frac{D_n}{L_n N_a} \right) N_{c300} N_{v300} T^3 e^{-\frac{E_g}{kT}}$ where the front terms consist of the constant C

b) (i) $I_{s, Ge} = C T^3 \exp\left(\frac{-0.66 \text{ eV}}{8.62 \times 10^{-5} \text{ eV}/\text{k} \cdot T}\right)$

$$\Rightarrow \frac{I_{s, Ge}(T=400K)}{I_{s, Ge}(T=300K)} = \left(\frac{400}{300}\right)^3 \cdot \exp\left(\frac{-0.66 \text{ eV}}{8.62 \times 10^{-5} \text{ eV}/\text{k} \cdot 400K} - \frac{-0.66 \text{ eV}}{8.62 \times 10^{-5} \text{ eV}/\text{k} \cdot 300K}\right)$$

$$= \left(\frac{4}{3}\right)^3 \cdot \exp(-10.82753) = 4.0 \times 10^{-3}$$

or $I_{s, Ge}(T=400K) - I_{s, Ge}(T=300K) = C \cdot (400)^3 \cdot \exp\left(\frac{-0.66 \text{ eV}}{8.62 \times 10^{-5} \text{ eV}/\text{k} \cdot 400K}\right) - (300)^3 \cdot \exp\left(\frac{-0.66 \text{ eV}}{8.62 \times 10^{-5} \text{ eV}/\text{k} \cdot 300K}\right)$

(ii) $I_{s, Si} = C T^3 \exp\left(\frac{-1.12 \text{ eV}}{8.62 \times 10^{-5} \text{ eV}/\text{k} \cdot T}\right) = -3.26 \times 10^{18} \cdot C$

$$\Rightarrow \frac{I_{s, Si}(T=400K)}{I_{s, Si}(T=300K)} = \left(\frac{400}{300}\right)^3 \cdot \exp\left(\frac{-1.12 \text{ eV}}{8.62 \times 10^{-5} \text{ eV}/\text{k} \cdot 400K} - \frac{-1.12 \text{ eV}}{8.62 \times 10^{-5} \text{ eV}/\text{k} \cdot 300K}\right)$$

$$= \left(\frac{4}{3}\right)^3 \cdot \exp(-10.82753) = 4.7 \times 10^{-5}$$

or $I_{s, Si}(T=400K) - I_{s, Si}(T=300K) = C \cdot (400)^3 \cdot \exp\left(\frac{-1.12 \text{ eV}}{8.62 \times 10^{-5} \text{ eV}/\text{k} \cdot 400K}\right) - (300)^3 \cdot \exp\left(\frac{-1.12 \text{ eV}}{8.62 \times 10^{-5} \text{ eV}/\text{k} \cdot 300K}\right)$

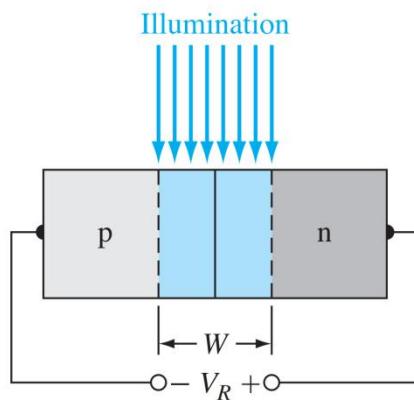
$$= -1.74 \times 10^{26} \cdot C$$

(ii) silicon diode

6) Consider a silicon pn junction diode with an applied reverse-biased voltage of $V_R = 5V$. The doping concentrations are $N_a = N_d = 4 \times 10^{16} \text{ cm}^{-3}$ and the cross-sectional area is $A = 10^{-4} \text{ cm}^2$. Assume minority carrier lifetimes of $\tau_0 = \tau_{n0} = \tau_{p0} = 10^{-7} \text{ s}$. Calculate:

- a) ideal reverse-saturation current
- b) reverse-biased generation current
- c) the ratio of the generation current to ideal saturation current

7) Consider a uniformly doped silicon pn junction at $T = 300\text{K}$ with impurity doping concentrations of $N_a = N_d = 5 \times 10^{15} \text{ cm}^{-3}$ and minority carrier lifetimes of $\tau_0 = \tau_{n0} = \tau_{p0} = 10^{-7} \text{ s}$. A reverse-biased voltage of $V_R = 10V$ is applied as shown in the figure. A light source is incident only on the space charge region, producing an excess carrier generation rate of $g' = 4 \times 10^{19} \text{ cm}^{-3}\text{s}^{-1}$. Calculate the generation current density.



- 6) Consider a silicon pn junction diode with an applied reverse-biased voltage of $V_R = 5V$. The doping concentrations are $N_a = N_d = 4 \times 10^{16} \text{ cm}^{-3}$ and the cross-sectional area is $A = 10^{-4} \text{ cm}^2$. Assume minority carrier lifetimes of $\tau_0 = \tau_{n0} = \tau_{p0} = 10^{-7} \text{ s}$. Calculate:
- ideal reverse-saturation current
 - reverse-biased generation current
 - the ratio of the generation current to ideal saturation current

a) diffusion coefficient : $D_p = 10 \text{ cm}^2 \cdot \text{s}^{-1}$, $D_n = 25 \text{ cm}^2 \cdot \text{s}^{-1}$

reverse saturation current : $I_s = eA n_i^2 \left(\frac{1}{N_d} \sqrt{\frac{D_p}{\tau_{p0}}} + \frac{1}{N_a} \sqrt{\frac{D_n}{\tau_{n0}}} \right) = 2.323 \times 10^{-15} \text{ A}$

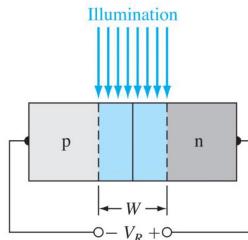
b) built-in potential : $V_{bi} = \frac{kT}{e} \ln \frac{N_a N_d}{n_i^2} = 0.766 \text{ V}$

depletion width : $W = \sqrt{\frac{2\varepsilon_s(V_{bi} + V_R)}{e}} \frac{N_a + N_d}{N_a N_d} = 6.108 \times 10^{-5} \text{ cm}$

generation current : $I_{gen} = A J_{gen} = A e n_i \frac{W}{2\tau_0} = 7.33 \times 10^{-11} \text{ A}$

c) ratio : $\frac{I_{gen}}{I_s} = 3.155 \times 10^4$

- 7) Consider a uniformly doped silicon pn junction at $T = 300K$ with impurity doping concentrations of $N_a = N_d = 5 \times 10^{15} \text{ cm}^{-3}$ and minority carrier lifetimes of $\tau_0 = \tau_{n0} = \tau_{p0} = 10^{-7} \text{ s}$. A reverse-biased voltage of $V_R = 10V$ is applied as shown in the figure. A light source is incident only on the space charge region, producing an excess carrier generation rate of $g' = 4 \times 10^{19} \text{ cm}^{-3} \text{s}^{-1}$. Calculate the generation current density.



$$V_{bi} = V_T \ln \left(\frac{N_a N_d}{n_i^2} \right) = 0.0259 \ln \left(\frac{(5 \times 10^{15})^2}{(6.5 \times 10^{10})^2} \right) = 0.6587 \text{ V}$$

$$W = \sqrt{\frac{2\varepsilon_s(V_{bi} + V_R)}{e}} \left(\frac{N_a + N_d}{N_a N_d} \right) = 2.35 \times 10^{-4} \text{ cm}$$

$$J_{gen} = \int_0^W g' dx = g' W = 1.5 \times 10^{-3} \text{ A/cm}^2$$