



## Instrumentation Tutorial 3 Answers

Instrumentation (Flinders University)

#### QUESTION 1

Given a Gaussian distribution i.e.  $\mathcal{N}(\mu, \sigma) = \frac{1}{\sqrt{2\pi\sigma^2}} e^{-\frac{\mu^2}{2\sigma^2}}$

- a) Find the support from the likelihood of an **odometry based** motion model, given;
- The robots state space is  $[x, y, \theta]$  with its initial state,  $x$ , of  $[5\text{m}, 5\text{m}, 30^\circ]$
  - The command sequence of;
    1. Rotation 1 =  $-20^\circ$
    2. Translation =  $20\text{ m}$
    3. Rotation 2 =  $30^\circ$
  - With the error model;
    - $\sigma_{rot1} = \alpha_1 |\hat{\delta}_{rot1}| + \alpha_2 \hat{\delta}_{trans}$
    - $\sigma_{rot1} = \alpha_3 \hat{\delta}_{trans} + \alpha_4 (|\hat{\delta}_{rot1}| + |\hat{\delta}_{rot2}|)$
    - $\sigma_{rot2} = \alpha_1 |\hat{\delta}_{rot2}| + \alpha_2 \hat{\delta}_{trans}$
    - With
      - $\alpha_1 = 0.05$
      - $\alpha_2 = 0.001$
      - $\alpha_3 = 0.05$
      - $\alpha_4 = 0.01$
  - With a proposed final state,  $x'$ , of  $[9\text{m}, 25\text{m}, 45^\circ]$
- b) In this case we used a standard Gaussian distribution,
- How can these calculation be simplified? (Hint: scaling factors)
  - Secondly, what are the consequences of this simplification. (Hint: what value would be the support be if both the odometry and predicted state matched perfectly.)

## QUESTION 2

In a 6DOF system, given the current vehicle state;

Surge :  $u$  = 1 m/s  
Sway :  $v$  = 0 m/s  
Heave :  $w$  = 0.1 m/s  
North :  $x$  = 5 m  
East :  $y$  = 10 m  
Down :  $z$  = 20 m  
Roll :  $\phi$  =  $6^\circ$   
Pitch :  $\theta$  =  $12^\circ$   
Yaw :  $\psi$  =  $24^\circ$

Acc<sub>x</sub> :  $a_x$  = -2 m/s<sup>2</sup>  
Acc<sub>y</sub> :  $a_y$  = 1 m/s<sup>2</sup>  
Acc<sub>z</sub> :  $a_z$  = 9.5 m/s<sup>2</sup>  
Gyro<sub>x</sub> :  $\omega_x$  = 0.1 rad/s  
Gyro<sub>y</sub> :  $\omega_y$  = 0.2 rad/s  
Gyro<sub>z</sub> :  $\omega_z$  = 0.3 rad/s

- Calculate the vehicle's **linear velocity transformation matrix**,  $R_b^n(\theta)$
- Calculate the vehicle's **angular velocity transformation matrix**,  $T_\theta(\theta)$
- Calculate the vehicles;
  - rate of change in velocity,  $\dot{v}_b$ .
  - rate of change in position,  $\dot{p}_n$ .
  - rate of change in orientation,  $\dot{\theta}$ .
- Using Euler integration, with a time step  $T = 0.1$  sec, calculate the vehicle pose at the next time step. (Hint:  $x_t = x_{t-1} + T\dot{x}_t$ )

### QUESTION 3

All robot models in this section were kinematic. In this exercise, you will consider a robot with dynamics. Consider a robot that lives in a 1-D coordinate system. Its location will be denoted by  $x$ , its velocity by  $\dot{x}$ , and its acceleration by  $\ddot{x}$ . Suppose we can only control the acceleration  $\ddot{x}$ .

Develop a mathematical motion model that computes the posterior over the pose  $x'$  and the velocity  $\dot{x}'$  from an initial pose  $x$  and velocity  $\dot{x}$ , assuming that the acceleration  $\ddot{x}$  is the sum of a commanded acceleration and a zero-mean Gaussian noise term with variance  $\sigma^2$  (and assume that the actual acceleration remains constant in the simulation interval  $\Delta t$ ).

Are  $x'$  and  $\dot{x}'$  correlated in the posterior? Explain why/why not.

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## ANSWER

a) -----

$p = \text{motion\_model\_odometry}(x, x', u)$

$$\delta_{trans} = u(2)$$

$$\delta_{rot1} = u(1)$$

$$\delta_{rot2} = u(3)$$

$$\hat{\delta}_{trans} = \sqrt{(x' - x)^2 + (y' - y)^2}$$

$$\hat{\delta}_{rot1} = \text{atan2}(y' - y, x' - x) - \theta$$

$$\hat{\delta}_{rot2} = \theta' - \theta - \hat{\delta}_{rot1}$$

$$p_{trans} = \text{pdf}(\delta_{trans} - \hat{\delta}_{trans}, \alpha_3 \hat{\delta}_{trans} + \alpha_4 (|\hat{\delta}_{rot1}| + |\hat{\delta}_{rot2}|))$$

$$p_{rot1} = \text{pdf}(\delta_{rot1} - \hat{\delta}_{rot1}, \alpha_1 |\hat{\delta}_{rot1}| + \alpha_2 \hat{\delta}_{trans})$$

$$p_{rot2} = \text{pdf}(\delta_{rot2} - \hat{\delta}_{rot2}, \alpha_1 |\hat{\delta}_{rot2}| + \alpha_2 \hat{\delta}_{trans})$$

$$\text{return } p = p_{trans} p_{rot1} p_{rot2}$$

-----  
 $p = \text{motion\_model\_odometry}([5, 5, 30], [9, 25, 45], [-20, 20, 30])$

$$\delta_{trans} = u(2) = 20$$

$$\delta_{rot1} = u(1) = \text{deg2rad}(-20) = -0.3491$$

$$\delta_{rot2} = u(3) = \text{deg2rad}(30) = 0.5880$$

$$\hat{\delta}_{trans} = \sqrt{(9 - 5)^2 + (25 - 5)^2} = 20.3961$$

$$\hat{\delta}_{rot1} = \text{atan2}(25 - 5, 9 - 5) - \text{deg2rad}(30) = -0.3262$$

$$\hat{\delta}_{rot2} = \text{deg2rad}(45) - \text{deg2rad}(30) - -0.3262 = 0.5880$$

$$\begin{aligned} p_{trans} &= \text{pdf}(20 - 20.3961, 0.05 \times 20.3961 + 0.01 \times (0.3262 + 0.5880)) \\ &= 8.9522 \end{aligned}$$

$$\begin{aligned} p_{rot1} &= \text{pdf}(-0.3491 + 0.3262, 0.05 \times 0.3262 + 0.001 \times 20.3961) \\ &= 0.36 \end{aligned}$$

$$\begin{aligned} p_{rot2} &= \text{pdf}(0.5880 - 0.5880, 0.05 \times 0.5880 + 0.001 \times 20.3961) \\ &= 1.8053 \end{aligned}$$

$$\text{return } p = 8.9522 \times 0.36 \times 1.8053 = 5.8176$$

- b) • The scale factor in front of the exponential part can be removed  
• As a consequence the value  $p$  return is between 0 and 1 with 1 meaning that there is zero error between  $x'$  and the state produced using  $u$ .

S. Thrun, W. Burgard, and D. Fox, *Probabilistic robotics* vol. 1: MIT press Cambridge, 2005.

## QUESTION 2

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## ANSWER

a)

$$\mathbf{R}_b^n(\boldsymbol{\theta}) = \begin{bmatrix} \cos \psi \cos \theta & -\sin \psi \cos \phi + \cos \psi \sin \theta \sin \phi & \sin \psi \sin \phi + \cos \psi \sin \theta \cos \phi \\ \sin \psi \cos \theta & \cos \psi \cos \theta + \sin \phi \sin \theta \sin \psi & -\cos \psi \sin \phi + \sin \theta \sin \psi \cos \phi \\ -\sin \theta & \cos \theta \sin \phi & \cos \theta \cos \phi \end{bmatrix}$$

$$\sin \phi = \sin(0.1047) = 0.1045$$

$$\cos \phi = \cos(0.1047) = 0.9945$$

$$\sin \theta = \sin(0.2094) = 0.2079$$

$$\cos \theta = \cos(0.2094) = 0.9781$$

$$\sin \psi = \sin(0.4189) = 0.4067$$

$$\cos \psi = \cos(0.4189) = 0.9135$$

$$\mathbf{R}_b^n(\boldsymbol{\theta}) =$$

$$\begin{bmatrix} 0.9135 \times 0.9781 & -0.4067 \times 0.9945 + 0.9135 \times 0.2079 \times 0.1045 & 0.4067 \times 0.1045 + 0.9135 \times 0.2079 \times 0.9945 \\ 0.4067 \times 0.9781 & 0.9135 \times 0.9781 + 0.1045 \times 0.2079 \times 0.4067 & -0.9135 \times 0.1045 + 0.2079 \times 0.4067 \times 0.9945 \\ -0.2079 & 0.9781 \times 0.1045 & 0.9781 \times 0.9945 \end{bmatrix}$$

$$= \begin{bmatrix} 0.8936 & -0.3847 & 0.2314 \\ 0.3978 & 0.9174 & -0.0114 \\ -0.2079 & 0.1022 & 0.9728 \end{bmatrix}$$

b)

$$\mathbf{T}_\theta(\boldsymbol{\theta}) = \begin{bmatrix} 1 & \sin \phi \tan \theta & \cos \phi \tan \theta \\ 0 & \cos \phi & -\sin \phi \\ 0 & \sin \phi / \cos \theta & \cos \phi / \cos \theta \end{bmatrix}$$

From Part a)

$$\sin \phi = \sin(0.1047) = 0.1045$$

$$\cos \phi = \cos(0.1047) = 0.9945$$

$$\cos \theta = \cos(0.2094) = 0.9781$$

$$\tan \theta = \sin \theta / \cos \theta = \frac{0.2079}{0.9781} = 0.2126$$

$$\mathbf{T}_\theta(\boldsymbol{\theta}) = \begin{bmatrix} 1 & 0.1045 \times 0.2126 & 0.9945 \times 0.2126 \\ 0 & 0.9945 & -0.1045 \\ 0 & 0.1045/0.9781 & 0.9945/0.9781 \end{bmatrix}$$

$$= \begin{bmatrix} 1 & 0.0222 & 0.2114 \\ 0 & 0.9945 & -0.1045 \\ 0 & 0.1069 & 1.0167 \end{bmatrix}$$



$$\text{c) } \dot{\mathbf{v}}_b = \mathbf{a}_b - \mathbf{R}_b^n(\boldsymbol{\theta})^T \begin{bmatrix} 0 \\ 0 \\ g \end{bmatrix} = \begin{bmatrix} 2 \\ 1 \\ 9.5 \end{bmatrix} - \begin{bmatrix} 0.8936 & 0.3978 & -0.2079 \\ -0.3847 & 0.9174 & 0.1022 \\ 0.2314 & -0.0114 & 0.9728 \end{bmatrix} \begin{bmatrix} 0 \\ 0 \\ 9.81 \end{bmatrix} = \begin{bmatrix} 0.0396 \\ -0.0030 \\ -0.0431 \end{bmatrix}$$

$$\dot{\mathbf{p}}_n = \mathbf{R}_b^n(\boldsymbol{\theta}) \mathbf{v}_b = \begin{bmatrix} 0.8936 & -0.3847 & 0.2314 \\ 0.3978 & 0.9174 & -0.0114 \\ -0.2079 & 0.1022 & 0.9728 \end{bmatrix} \begin{bmatrix} 1 \\ 0 \\ 0.1 \end{bmatrix} = \begin{bmatrix} 0.9167 \\ 0.3967 \\ -0.1106 \end{bmatrix}$$

$$\dot{\boldsymbol{\theta}} = \mathbf{T}_{\boldsymbol{\theta}}(\boldsymbol{\theta}) \boldsymbol{\omega}_{nb}^b = \begin{bmatrix} 1 & 0.0222 & 0.2114 \\ 0 & 0.9945 & -0.1045 \\ 0 & 0.1069 & 1.0167 \end{bmatrix} \begin{bmatrix} 0.1 \\ 0.2 \\ 0.3 \end{bmatrix} = \begin{bmatrix} 0.1679 \\ 0.1675 \\ 0.3264 \end{bmatrix}$$

d)

$$\mathbf{x}_t = \mathbf{x}_{t-1} + T \dot{\mathbf{x}}_t = \begin{bmatrix} 1 \\ 0 \\ 0.1 \\ 5 \\ 10 \\ 20 \\ 0.1047 \\ 0.2094 \\ 0.4189 \end{bmatrix} + 0.1 \times \begin{bmatrix} 0.0396 \\ -0.0030 \\ -0.0431 \\ 0.9167 \\ 0.3967 \\ -0.1106 \\ 0.1679 \\ 0.1675 \\ 0.3264 \end{bmatrix} = \begin{bmatrix} 1.00396 \\ -0.0003 \\ 0.0957 \\ 5.09167 \\ 10.03967 \\ 19.98894 \\ 0.1215 \\ 0.2262 \\ 0.4515 \end{bmatrix}$$

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All robot models in this section were kinematic. In this exercise, you will consider a robot with dynamics. Consider a robot that lives in a 1-D coordinate system. Its location will be denoted by  $x$ , its velocity by  $\dot{x}$ , and its acceleration by  $\ddot{x}$ . Suppose we can only control the acceleration  $\ddot{x}$ .

Develop a mathematical motion model that computes the posterior over the pose  $x'$  and the velocity  $\dot{x}'$  from an initial pose  $x$  and velocity  $\dot{x}$ , assuming that the acceleration  $\ddot{x}$  is the sum of a commanded acceleration and a zero-mean Gaussian noise term with variance  $\sigma^2$  (and assume that the actual acceleration remains constant in the simulation interval  $\Delta t$ ).

Are  $x'$  and  $\dot{x}'$  correlated in the posterior? Explain why/why not.

### ANSWER

$$\dot{x}' = \dot{x} + T\ddot{x}$$

$$\mathcal{N}(\dot{x}', \sigma_v^2) = \mathcal{N}(\dot{x} + T\ddot{x}, T\sigma^2)$$

$$x' = x + T\dot{x} + \frac{T^2}{2}\ddot{x}$$

$$\mathcal{N}(x', \sigma_p^2) = \mathcal{N}\left(x + T\dot{x} + \frac{T^2}{2}\ddot{x}, \frac{T^2}{2}\sigma^2\right)$$

Yes,  $x'$  and  $\dot{x}'$  are correlated as  $x'$  is dependent on  $\dot{x}'$ .