## Finite Difference Method

CENG6202: Advanced Computational Methods in Geotechnical Engineering

Yared W. Bekele, PhD Fall Semester 2019

#### Contents

- Introduction
- 2 Basic Principles
  - Derivatives as Difference Equations
  - Difference Equations for Partial Derivatives
  - Solving Differential Equations
- One-dimensional Problems
  - Steady-state Groundwater Flow
  - Consolidation
- Two-dimensional Problems
  - Steady-state Groundwater Flow



#### **Contents**

- Introduction
- 2 Basic Principles
  - Derivatives as Difference Equations
  - Difference Equations for Partial Derivatives
  - Solving Differential Equations
- One-dimensional Problems
  - Steady-state Groundwater Flow
  - Consolidation
- 4 Two-dimensional Problems
  - Steady-state Groundwater Flow



# The Finite Difference Method (FDM) is one of the most widely used computational methods in engineering.

- The governing mathematical equation is nonlinear and can't be linearized without affecting the result.
- The computational domain is complex.
- The boundary conditions are of mixed types.
- The boundary conditions are time-dependent.
- The material property is non-homogeneous or anisotropic

The Finite Difference Method (FDM) is one of the most widely used computational methods in engineering.

- The governing mathematical equation is nonlinear and can't be linearized without affecting the result.
- The computational domain is complex.
- The boundary conditions are of mixed types.
- The boundary conditions are time-dependent...
- The material property is non-homogeneous or anisotropic



The Finite Difference Method (FDM) is one of the most widely used computational methods in engineering.

- The governing mathematical equation is nonlinear and can't be linearized without affecting the result.
- The computational domain is complex.
- The boundary conditions are of mixed types.
- The boundary conditions are time-dependent.
- The material property is non-homogeneous or anisotropic.

The Finite Difference Method (FDM) is one of the most widely used computational methods in engineering.

- The governing mathematical equation is nonlinear and can't be linearized without affecting the result.
- The computational domain is complex.
- The boundary conditions are of mixed types.
- The boundary conditions are time-dependent.
- The material property is non-homogeneous or anisotropic.



The Finite Difference Method (FDM) is one of the most widely used computational methods in engineering.

- The governing mathematical equation is nonlinear and can't be linearized without affecting the result.
- The computational domain is complex.
- The boundary conditions are of mixed types.
- The boundary conditions are time-dependent.
- The material property is non-homogeneous or anisotropic.



The Finite Difference Method (FDM) is one of the most widely used computational methods in engineering.

- The governing mathematical equation is nonlinear and can't be linearized without affecting the result.
- The computational domain is complex.
- The boundary conditions are of mixed types.
- The boundary conditions are time-dependent.
- The material property is non-homogeneous or anisotropic.



The Finite Difference Method (FDM) is one of the most widely used computational methods in engineering.

- The governing mathematical equation is nonlinear and can't be linearized without affecting the result.
- The computational domain is complex.
- The boundary conditions are of mixed types.
- The boundary conditions are time-dependent.
- The material property is non-homogeneous or anisotropic.



# FDM is based on approximations that allow replacing differential equations by **finite difference equations**.

- Divide the computational domain into a grid of nodes
- Approximate the governing differential equation by an equivalent finite difference equation with respect to the grid points.
- Solve the finite difference equations for the unknowns subject to the boundary and/or initial conditions.

FDM is based on approximations that allow replacing differential equations by **finite difference equations**.

- Divide the computational domain into a grid of nodes.
- Approximate the governing differential equation by an equivalent finite difference equation with respect to the grid points.
- Solve the finite difference equations for the unknowns subject to the boundary and/or initial conditions.

FDM is based on approximations that allow replacing differential equations by **finite difference equations**.

- 1 Divide the computational domain into a grid of nodes.
- Approximate the governing differential equation by an equivalent finite difference equation with respect to the grid points.
- Solve the finite difference equations for the unknowns subject to the boundary and/or initial conditions.

FDM is based on approximations that allow replacing differential equations by **finite difference equations**.

- 1 Divide the computational domain into a grid of nodes.
- Approximate the governing differential equation by an equivalent finite difference equation with respect to the grid points.
- Solve the finite difference equations for the unknowns subject to the boundary and/or initial conditions.

FDM is based on approximations that allow replacing differential equations by **finite difference equations**.

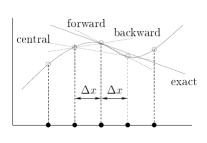
- 1 Divide the computational domain into a grid of nodes.
- Approximate the governing differential equation by an equivalent finite difference equation with respect to the grid points.
- Solve the finite difference equations for the unknowns subject to the boundary and/or initial conditions.

#### **Contents**

- Introduction
- 2 Basic Principles
  - Derivatives as Difference Equations
  - Difference Equations for Partial Derivatives
  - Solving Differential Equations
- One-dimensional Problems
  - Steady-state Groundwater Flow
  - Consolidation
- Two-dimensional Problems
  - Steady-state Groundwater Flow



Consider a real-valued function f(x). The first derivative of f at x=a may be approximated in different ways for  $h=\Delta x$ .



Forward Difference Equation:

$$f'(a) \approx \frac{f(a+h) - f(a)}{h}$$

Central Difference Equation:

$$f'(a) \approx \frac{f(a+h) - f(a-h)}{2h}$$

$$f'(a) \approx \frac{f(a) - f(a-h)}{h}$$

#### →Derivatives as Difference Equations

Consider a real-valued function f(x). The first derivative of f at x=a may be approximated in different ways for  $h=\Delta x$ .

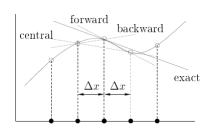
#### Forward Difference Equation:

$$f'(a) \approx \frac{f(a+h) - f(a)}{h}$$

Central Difference Equation:

$$f'(a) \approx \frac{f(a+h) - f(a-h)}{2h}$$

$$f'(a) \approx \frac{f(a) - f(a-h)}{h}$$



Consider a real-valued function f(x). The first derivative of f at x=a may be approximated in different ways for  $h=\Delta x$ .

# $\begin{array}{c|c} \text{forward} \\ \text{backward} \\ \hline \Delta x & \Delta x \end{array} \quad \text{exact}$

#### Forward Difference Equation:

$$f'(a) \approx \frac{f(a+h) - f(a)}{h}$$

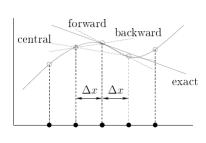
#### Central Difference Equation:

$$f'(a) \approx \frac{f(a+h) - f(a-h)}{2h}$$

$$f'(a) \approx \frac{f(a) - f(a-h)}{h}$$

#### →Derivatives as Difference Equations

Consider a real-valued function f(x). The first derivative of f at x=a may be approximated in different ways for  $h=\Delta x$ .



#### Forward Difference Equation:

$$f'(a) \approx \frac{f(a+h) - f(a)}{h}$$

#### Central Difference Equation:

$$f'(a) \approx \frac{f(a+h) - f(a-h)}{2h}$$

$$f'(a) \approx \frac{f(a) - f(a-h)}{h}$$



## The accuracy of the three approximations can be compared by looking at the Taylor series expansion of f.

Taylor series expansion of f(x) at a point a:

$$f(x) = \sum_{n=0}^{\infty} \frac{(x-a)^n}{n!} f^n(a) = f(a) + \frac{x-a}{1!} f'(a) + \frac{(x-a)^2}{2!} f''(a) + \cdots$$

Series expansions at x = a + h and x = a - h:

$$f(a+h) = f(a) + hf'(a) + \frac{h^2}{2!}f''(a) + \frac{h^3}{3!}f'''(a) + \cdots$$
$$f(a-h) = f(a) - hf'(a) + \frac{h^2}{2!}f''(a) - \frac{h^3}{3!}f'''(a) + \cdots$$

The accuracy of the three approximations can be compared by looking at the Taylor series expansion of f.

Taylor series expansion of f(x) at a point a:

$$f(x) = \sum_{n=0}^{\infty} \frac{(x-a)^n}{n!} f^n(a) = f(a) + \frac{x-a}{1!} f'(a) + \frac{(x-a)^2}{2!} f''(a) + \cdots$$

Series expansions at x = a + h and x = a - h:

$$f(a+h) = f(a) + hf'(a) + \frac{h^2}{2!}f''(a) + \frac{h^3}{3!}f'''(a) + \cdots$$
$$f(a-h) = f(a) - hf'(a) + \frac{h^2}{2!}f''(a) - \frac{h^3}{3!}f'''(a) + \cdots$$

The accuracy of the three approximations can be compared by looking at the Taylor series expansion of f.

Taylor series expansion of f(x) at a point a:

$$f(x) = \sum_{n=0}^{\infty} \frac{(x-a)^n}{n!} f^n(a) = f(a) + \frac{x-a}{1!} f'(a) + \frac{(x-a)^2}{2!} f''(a) + \cdots$$

Series expansions at x = a + h and x = a - h:

$$f(a+h) = f(a) + hf'(a) + \frac{h^2}{2!}f''(a) + \frac{h^3}{3!}f'''(a) + \cdots$$
$$f(a-h) = f(a) - hf'(a) + \frac{h^2}{2!}f''(a) - \frac{h^3}{3!}f'''(a) + \cdots$$

Based on the previous series expansions, f'(a) may be written as

$$f'(a) = \frac{f(a+h) - f(a)}{h} - \frac{h}{2!}f''(a) + \frac{h^2}{3!}f'''(a) + \cdots$$

$$f'(a) = \frac{f(a+h) - f(a-h)}{2h} - \frac{h^2}{3!}f'''(a) + \cdots$$

$$f'(a) = \frac{f(a) - f(a-h)}{h} + \frac{h}{2!}f''(a) - \frac{h^2}{3!}f'''(a) + \cdots$$

The orders of these approximations with respect to h:

$$f'(a) = \frac{f(a+h) - f(a)}{h} + \mathcal{O}(h)$$

$$f'(a) = \frac{f(a+h) - f(a-h)}{2h} + \mathcal{O}(h^2)$$

$$f'(a) = \frac{f(a) - f(a-h)}{h} + \mathcal{O}(h)$$

#### →Derivatives as Difference Equations

Based on the previous series expansions, f'(a) may be written as

$$f'(a) = \frac{f(a+h) - f(a)}{h} - \frac{h}{2!}f''(a) + \frac{h^2}{3!}f'''(a) + \cdots$$

$$f'(a) = \frac{f(a+h) - f(a-h)}{2h} - \frac{h^2}{3!}f'''(a) + \cdots$$

$$f'(a) = \frac{f(a) - f(a-h)}{h} + \frac{h}{2!}f''(a) - \frac{h^2}{3!}f'''(a) + \cdots$$

The orders of these approximations with respect to h:

$$f'(a) = \frac{f(a+h) - f(a)}{h} + \mathcal{O}(h)$$

$$f'(a) = \frac{f(a+h) - f(a-h)}{2h} + \mathcal{O}(h^2)$$

$$f'(a) = \frac{f(a) - f(a-h)}{h} + \mathcal{O}(h)$$

Higher order derivatives are derived in a similar way from the Taylor series expansions.

For example, the second derivative is given by

$$f''(a) = \frac{f(a+h) - 2f(a) + f(a-h)}{h^2} + \mathcal{O}(h^2)$$

This approximation is sometimes referred to as the **Symmetric Difference Equation**.

Higher order derivatives are derived in a similar way from the Taylor series expansions.

For example, the second derivative is given by

$$f''(a) = \frac{f(a+h) - 2f(a) + f(a-h)}{h^2} + \mathcal{O}(h^2)$$

This approximation is sometimes referred to as the **Symmetric Difference Equation**.

Higher order derivatives are derived in a similar way from the Taylor series expansions.

For example, the second derivative is given by

$$f''(a) = \frac{f(a+h) - 2f(a) + f(a-h)}{h^2} + \mathcal{O}(h^2)$$

This approximation is sometimes referred to as the **Symmetric Difference Equation**.

#### → Difference Equations for Partial Derivatives

Many physical quantities are functions of two or more variables.

Consider f(t,x), a function of time and one-dimensional space. Parital derivative of f with respect to x for  $a=x_0$  and  $h=\Delta x$ :

$$f'(t, x_o) = \frac{f(t, x_o + \Delta x) - f(t, x_o)}{\Delta x}$$

For discrete values of  $x=(x_1,x_2,\cdots,x_N)$ , and discrete levels of  $t=(t_0,t_1,t_2,\cdots,t_n)$  the derivative at a point  $(t_n,x_i)$  is

$$f'(t_n, x_i) = \frac{f(t_n, x_{i+1}) - f(t_n, x_i)}{\Delta x} = \frac{f_{i+1}^n - f_i^n}{\Delta x}$$

$$\dot{f}(t_n, x_i) = \frac{f_i^{n+1} - f_i^r}{\Delta t}$$

Consider f(t,x), a function of time and one-dimensional space. Parital derivative of f with respect to x for  $a=x_0$  and  $h=\Delta x$ :

$$f'(t, x_o) = \frac{f(t, x_o + \Delta x) - f(t, x_o)}{\Delta x}$$

For discrete values of  $x=(x_1,x_2,\cdots,x_N)$ , and discrete levels of  $t=(t_0,t_1,t_2,\cdots,t_n)$  the derivative at a point  $(t_n,x_i)$  is

$$f'(t_n, x_i) = \frac{f(t_n, x_{i+1}) - f(t_n, x_i)}{\Delta x} = \frac{f_{i+1}^n - f_i^n}{\Delta x}$$

$$\dot{f}(t_n, x_i) = \frac{f_i^{n+1} - f_i^n}{\Delta t}$$



Consider f(t,x), a function of time and one-dimensional space. Parital derivative of f with respect to x for  $a=x_{\rm o}$  and  $h=\Delta x$ :

$$f'(t, x_{o}) = \frac{f(t, x_{o} + \Delta x) - f(t, x_{o})}{\Delta x}$$

For discrete values of  $x=(x_1,x_2,\cdots,x_N)$ , and discrete levels of  $t=(t_0,t_1,t_2,\cdots,t_n)$  the derivative at a point  $(t_n,x_i)$  is

$$f'(t_n, x_i) = \frac{f(t_n, x_{i+1}) - f(t_n, x_i)}{\Delta x} = \frac{f_{i+1}^n - f_i^n}{\Delta x}$$

$$\dot{f}(t_n, x_i) = \frac{f_i^{n+1} - f_i^n}{\Delta t}$$



Consider f(t,x), a function of time and one-dimensional space. Parital derivative of f with respect to x for  $a=x_0$  and  $h=\Delta x$ :

$$f'(t, x_o) = \frac{f(t, x_o + \Delta x) - f(t, x_o)}{\Delta x}$$

For discrete values of  $x=(x_1,x_2,\cdots,x_N)$ , and discrete levels of  $t=(t_0,t_1,t_2,\cdots,t_n)$  the derivative at a point  $(t_n,x_i)$  is

$$f'(t_n, x_i) = \frac{f(t_n, x_{i+1}) - f(t_n, x_i)}{\Delta x} = \frac{f_{i+1}^n - f_i^n}{\Delta x}$$

$$\dot{f}(t_n, x_i) = \frac{f_i^{n+1} - f_i^n}{\Delta t}$$



Consider f(t,x), a function of time and one-dimensional space. Parital derivative of f with respect to x for  $a=x_0$  and  $h=\Delta x$ :

$$f'(t, x_{o}) = \frac{f(t, x_{o} + \Delta x) - f(t, x_{o})}{\Delta x}$$

For discrete values of  $x=(x_1,x_2,\cdots,x_N)$ , and discrete levels of  $t=(t_0,t_1,t_2,\cdots,t_n)$  the derivative at a point  $(t_n,x_i)$  is

$$f'(t_n, x_i) = \frac{f(t_n, x_{i+1}) - f(t_n, x_i)}{\Delta x} = \frac{f_{i+1}^n - f_i^n}{\Delta x}$$

$$\dot{f}(t_n, x_i) = \frac{f_i^{n+1} - f_i^n}{\Delta t}$$



### Basic Principles

→Difference Equations for Partial Derivatives

Partial Derivative	Difference Equation	Туре	Accuracy
$f' = \frac{\partial f}{\partial x}$	$\frac{f_{i+1}^n - f_i^n}{\Delta x}$	Forward	$\mathcal{O}(\Delta x)$
$f' = \frac{\partial f}{\partial x}$	$\frac{f_i^n - f_{i-1}^n}{\Delta x}$	Backward	$\mathcal{O}(\Delta x)$
$f' = \frac{\partial f}{\partial x}$	$\frac{f_{i+1}^n - f_{i-1}^n}{2\Delta x}$	Central	$\mathcal{O}(\Delta x^2)$
	$\frac{f_{i+1}^n - 2f_i^n + f_{i-1}^n}{\Delta x^2}$	Symmetric	$\mathcal{O}(\Delta x^2)$
$\dot{f} = \frac{\partial f}{\partial t}$	$\frac{f_i^{n+1} - f_i^n}{\Delta t}$	Forward	$\mathcal{O}(\Delta t)$
	$\frac{f_i^n - f_i^{n-1}}{\Delta t}$	Backward	$\mathcal{O}(\Delta t)$
	$\frac{f_i^{n+1} - f_i^{n-1}}{2\Delta t}$	Central	$\mathcal{O}(\Delta t^2)$
	$\frac{f_i^{n+1} - 2f_i^n + f_i^{n-1}}{\Delta t^2}$	Symmetric	$\mathcal{O}(\Delta t^2)$

## Basic Principles →Difference Equations for Partial Derivatives

Partial Derivative	Difference Equation	Туре	Accuracy
$f' = \frac{\partial f}{\partial x}$	$\frac{f_{i+1}^n - f_i^n}{\Delta x}$	Forward	$\mathcal{O}(\Delta x)$
$f' = \frac{\partial f}{\partial x}$	$\frac{f_i^n - f_{i-1}^n}{\Delta x}$	Backward	$\mathcal{O}(\Delta x)$
$f' = \frac{\partial f}{\partial x}$	$\frac{f_{i+1}^n - f_{i-1}^n}{2\Delta x}$	Central	$\mathcal{O}(\Delta x^2)$
$f'' = \frac{\partial^2 f}{\partial x^2}$	$\frac{f_{i+1}^n - 2f_i^n + f_{i-1}^n}{\Delta x^2}$	Symmetric	$\mathcal{O}(\Delta x^2)$
$\dot{f} = \frac{\partial f}{\partial t}$	$\frac{f_i^{n+1} - f_i^n}{\Delta t}$	Forward	$\mathcal{O}(\Delta t)$
	$\frac{f_i^n - f_i^{n-1}}{\Delta t}$	Backward	$\mathcal{O}(\Delta t)$
	$\frac{f_i^{n+1} - f_i^{n-1}}{2\Delta t}$	Central	$\mathcal{O}(\Delta t^2)$
	$\frac{f_i^{n+1} - 2f_i^n + f_i^{n-1}}{\Delta t^2}$	Symmetric	$\mathcal{O}(\Delta t^2)$

## Basic Principles

→Difference Equations for Partial Derivatives

Partial Derivative	Difference Equation	Туре	Accuracy
$f' = \frac{\partial f}{\partial x}$	$\frac{f_{i+1}^n - f_i^n}{\Delta x}$	Forward	$\mathcal{O}(\Delta x)$
$f' = \frac{\partial f}{\partial x}$	$\frac{f_i^n - f_{i-1}^n}{\Delta x}$	Backward	$\mathcal{O}(\Delta x)$
$f' = \frac{\partial f}{\partial x}$	$\frac{f_{i+1}^n - f_{i-1}^n}{2\Delta x}$	Central	$\mathcal{O}(\Delta x^2)$
$f'' = \frac{\partial^2 f}{\partial x^2}$	$\frac{f_{i+1}^n - 2f_i^n + f_{i-1}^n}{\Delta x^2}$	Symmetric	$\mathcal{O}(\Delta x^2)$
$\dot{f} = \frac{\partial f}{\partial t}$	$\frac{f_i^{n+1} - f_i^n}{\Delta t}$	Forward	$\mathcal{O}(\Delta t)$
$\dot{f} = \frac{\partial f}{\partial t}$	$\frac{f_i^n - f_i^{n-1}}{\Delta t}$	Backward	$\mathcal{O}(\Delta t)$
$\dot{f} = \frac{\partial f}{\partial t}$	$\frac{f_i^{n+1} - f_i^{n-1}}{2\Delta t}$	Central	$\mathcal{O}(\Delta t^2)$
	$\frac{f_i^{n+1} - 2f_i^n + f_i^{n-1}}{\Delta t^2}$	Symmetric	$\mathcal{O}(\Delta t^2)$

# Basic Principles

→Difference Equations for Partial Derivatives

Partial Derivative	Difference Equation	Туре	Accuracy
$f' = \frac{\partial f}{\partial x}$	$\frac{f_{i+1}^n - f_i^n}{\Delta x}$	Forward	$\mathcal{O}(\Delta x)$
$f' = \frac{\partial f}{\partial x}$	$\frac{f_i^n - f_{i-1}^n}{\Delta x}$	Backward	$\mathcal{O}(\Delta x)$
$f' = \frac{\partial f}{\partial x}$	$\frac{f_{i+1}^n - f_{i-1}^n}{2\Delta x}$	Central	$\mathcal{O}(\Delta x^2)$
$f'' = \frac{\partial^2 f}{\partial x^2}$	$\frac{f_{i+1}^n - 2f_i^n + f_{i-1}^n}{\Delta x^2}$	Symmetric	$\mathcal{O}(\Delta x^2)$
$\dot{f} = \frac{\partial f}{\partial t}$	$\frac{f_i^{n+1} - f_i^n}{\Delta t}$	Forward	$\mathcal{O}(\Delta t)$
$\dot{f} = \frac{\partial f}{\partial t}$	$\frac{f_i^n - f_i^{n-1}}{\Delta t}$	Backward	$\mathcal{O}(\Delta t)$
$\dot{f} = \frac{\partial f}{\partial t}$	$\frac{f_i^{n+1} - f_i^{n-1}}{2\Delta t}$	Central	$\mathcal{O}(\Delta t^2)$
$\ddot{f} = \frac{\partial^2 f}{\partial t^2}$	$\frac{f_i^{n+1} - 2f_i^n + f_i^{n-1}}{\Delta t^2}$	Symmetric	$\mathcal{O}(\Delta t^2)$

Various problems in geotechnical engineering are mathematically described in terms of differential equations. Some examples include:

Groundwater Flow: General for confined aquifers

$$\frac{\partial}{\partial x} \left( k_x \frac{\partial h}{\partial x} \right) + \frac{\partial}{\partial y} \left( k_y \frac{\partial h}{\partial y} \right) + \frac{\partial}{\partial z} \left( k_z \frac{\partial h}{\partial z} \right) = S_s \frac{\partial h}{\partial z}$$

Various problems in geotechnical engineering are mathematically described in terms of differential equations. Some examples include:

Groundwater Flow: General for confined aquifers

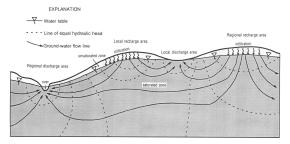
$$\frac{\partial}{\partial x} \left( k_x \frac{\partial h}{\partial x} \right) + \frac{\partial}{\partial y} \left( k_y \frac{\partial h}{\partial y} \right) + \frac{\partial}{\partial z} \left( k_z \frac{\partial h}{\partial z} \right) = S_s \frac{\partial h}{\partial t}$$

#### → Solving Differential Equations

Various problems in geotechnical engineering are mathematically described in terms of differential equations. Some examples include:

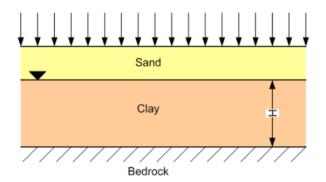
**Groundwater Flow**: General for confined aquifers

$$\frac{\partial}{\partial x} \left( k_x \frac{\partial h}{\partial x} \right) + \frac{\partial}{\partial y} \left( k_y \frac{\partial h}{\partial y} \right) + \frac{\partial}{\partial z} \left( k_z \frac{\partial h}{\partial z} \right) = S_{\rm s} \frac{\partial h}{\partial t}$$



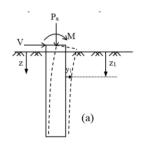
#### Consolidation:

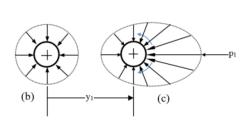
$$\frac{\partial u}{\partial t} - c_{\mathbf{v}} \frac{\partial^2 u}{\partial z^2} = 0$$



#### **Laterally Loaded Piles:**

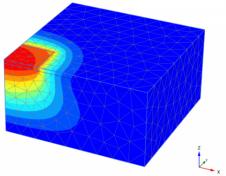
$$E_{\rm p}I_{\rm p}\frac{d^4y}{dx^4} + P_{\rm x}\frac{d^2y}{dx^2} + E_{\rm py}y - W = 0$$





## **Coupled Deformation and Flow:**

$$\nabla \cdot (\boldsymbol{\sigma}' + u\boldsymbol{I}) + \rho \boldsymbol{b} = \boldsymbol{0}$$
$$\nabla \cdot \dot{\boldsymbol{u}} + c \frac{\partial u}{\partial t} + \nabla \cdot \boldsymbol{v}_{w} = 0$$



# Initial Conditions (ICs):

- Specify the values of field variables at the start of a simulation.
- Usually specified for time dependent variables at t=0.

# Boundary Conditions (BCs):

- Define the values of field variables or functions of field variables at the boundaries of the computational domain.
- Boundary types depend on spatial dimension:
   1D Point, 2D Edge, 3D Face

## Initial Conditions (ICs):

- Specify the values of field variables at the start of a simulation.
- Usually specified for time dependent variables at t=0.

# Boundary Conditions (BCs):

- Define the values of field variables or functions of field variables at the boundaries of the computational domain.
- Boundary types depend on spatial dimension:
   1D Point, 2D Edge, 3D Face

 Dirichlet BCs: specify the value of the unknown function on a given boundary in the form

$$f=ar{f} \quad {\rm on} \; \Gamma_{\rm D}$$

where  $\Gamma_D$  is the boundary on which the condition is specified.

Neumann BCs: specify the normal derivative of the unknown function on a given boundary i.e.

$$\frac{\partial f}{\partial n} = q \quad \text{on } \Gamma_{\mathcal{N}}$$

where n is the normal to the boundary  $\Gamma_{
m N}.$ 

 Robin BCs: define a linear combination of Dirichlet and Neumann conditions in the form

$$\alpha f + \beta \frac{\partial f}{\partial n} = r \quad \text{on } \Gamma_{\mathbf{R}}$$

where lpha and eta are constants.



Oirichlet BCs: specify the value of the unknown function on a given boundary in the form

$$f=ar{f}\quad {
m on}\ \Gamma_{
m D}$$

where  $\Gamma_{\rm D}$  is the boundary on which the condition is specified.

Neumann BCs: specify the normal derivative of the unknown function on a given boundary i.e.

$$\frac{\partial f}{\partial n} = q \quad \text{on } \Gamma_{N}$$

where n is the normal to the boundary  $\Gamma_N$ .

 Robin BCs: define a linear combination of Dirichlet and Neumann conditions in the form

$$\alpha f + \beta \frac{\partial f}{\partial n} = r \quad \text{on } \Gamma_{\mathbf{R}}$$

where  $\alpha$  and  $\beta$  are constants.



• **Dirichlet BCs**: specify the value of the unknown function on a given boundary in the form

$$f=\bar{f}\quad \text{on }\Gamma_{\rm D}$$

where  $\Gamma_D$  is the boundary on which the condition is specified.

Neumann BCs: specify the normal derivative of the unknown function on a given boundary i.e.

$$\frac{\partial f}{\partial n} = q \quad \text{on } \Gamma_{\mathcal{N}}$$

where n is the normal to the boundary  $\Gamma_N$ .

On Robin BCs: define a linear combination of Dirichlet and Neumann conditions in the form

$$\alpha f + \beta \frac{\partial f}{\partial n} = r \quad \text{on } \Gamma_{\mathbf{R}}$$

where  $\alpha$  and  $\beta$  are constants.



• **Dirichlet BCs**: specify the value of the unknown function on a given boundary in the form

$$f=ar{f}\quad {
m on}\ \Gamma_{
m D}$$

where  $\Gamma_D$  is the boundary on which the condition is specified.

Neumann BCs: specify the normal derivative of the unknown function on a given boundary i.e.

$$\frac{\partial f}{\partial n} = q \quad \text{on } \Gamma_{\mathbf{N}}$$

where n is the normal to the boundary  $\Gamma_N$ .

**Robin BCs**: define a linear combination of Dirichlet and Neumann conditions in the form

$$\alpha f + \beta \frac{\partial f}{\partial n} = r \quad \text{on } \Gamma_{\mathbf{R}}$$

where  $\alpha$  and  $\beta$  are constants.



**Spatial Discretization**: The computational domain over which we aim to solve the PDE is divided into a grid mesh with the required grid spacing. Depending on the spatial dimension of the problem, the grid required may be 1D, 2D or 3D.

**Temporal Discretization**: If there are time dependent quantities in the differential equation, the next step is to perform temporal discretization of these to obtain difference equations.

**Solving the Problem**: The individual equations at all the grid points in the spatially discretized domain are assembled to form a system of equations of the form

$$Ax = b$$

which may be solved using the appropriate solution method.



**Spatial Discretization**: The computational domain over which we aim to solve the PDE is divided into a grid mesh with the required grid spacing. Depending on the spatial dimension of the problem, the grid required may be 1D, 2D or 3D.

**Temporal Discretization**: If there are time dependent quantities in the differential equation, the next step is to perform temporal discretization of these to obtain difference equations.

**Solving the Problem**: The individual equations at all the grid points in the spatially discretized domain are assembled to form a system of equations of the form

$$Ax = b$$

which may be solved using the appropriate solution method.



**Spatial Discretization**: The computational domain over which we aim to solve the PDE is divided into a grid mesh with the required grid spacing. Depending on the spatial dimension of the problem, the grid required may be 1D, 2D or 3D.

**Temporal Discretization**: If there are time dependent quantities in the differential equation, the next step is to perform temporal discretization of these to obtain difference equations.

**Solving the Problem**: The individual equations at all the grid points in the spatially discretized domain are assembled to form a system of equations of the form

$$Ax = b$$

which may be solved using the appropriate solution method.



# **Contents**

- Introduction
- 2 Basic Principles
  - Derivatives as Difference Equations
  - Difference Equations for Partial Derivatives
  - Solving Differential Equations
- One-dimensional Problems
  - Steady-state Groundwater Flow
  - Consolidation
- 4 Two-dimensional Problems
  - Steady-state Groundwater Flow



Governing equation in 3D:

$$k_x \frac{\partial^2 h}{\partial x^2} + k_y \frac{\partial^2 h}{\partial y^2} + k_z \frac{\partial^2 h}{\partial z^2} = Q$$

One-dimensional equivalent:

$$k\frac{\partial^2 h}{\partial x^2} = Q$$



Governing equation in 3D:

$$k_x \frac{\partial^2 h}{\partial x^2} + k_y \frac{\partial^2 h}{\partial y^2} + k_z \frac{\partial^2 h}{\partial z^2} = Q$$

One-dimensional equivalent:

$$k\frac{\partial^2 h}{\partial x^2} = Q$$



Governing equation in 3D:

$$k_x \frac{\partial^2 h}{\partial x^2} + k_y \frac{\partial^2 h}{\partial y^2} + k_z \frac{\partial^2 h}{\partial z^2} = Q$$

One-dimensional equivalent:

$$k\frac{\partial^2 h}{\partial x^2} = Q$$

#### 

Governing equation in 3D:

$$k_x \frac{\partial^2 h}{\partial x^2} + k_y \frac{\partial^2 h}{\partial y^2} + k_z \frac{\partial^2 h}{\partial z^2} = Q$$

One-dimensional equivalent:

$$k\frac{\partial^2 h}{\partial x^2} = Q$$



 $\hookrightarrow$ Steady-state Flow

Spatial discretization: Divide the domain into a desired number of sub-domains, say  $N\colon$ 

$$0 \xrightarrow{x_0 \quad x_1 \quad \cdots \quad x_{i-1} \quad x_i \quad x_{i+1} \quad \cdots \quad x_{N-1} \quad x_N} 1$$

The grid spacing in this case is

$$\Delta x = \frac{1}{N}$$

Hydraulic head values at grid points:

$$h(x_i) = h_i, \qquad i = 0, 1, \cdots, N$$

$$h(x_0) = h_0$$
$$h(x_N) = h_N$$

Spatial discretization: Divide the domain into a desired number of sub-domains, say N:

$$0 \xrightarrow{x_0 \quad x_1 \quad \cdots \quad x_{i-1} \quad x_i \quad x_{i+1} \quad \cdots \quad x_{N-1} \quad x_N}$$

The grid spacing in this case is

$$\Delta x = \frac{1}{N}$$

Hydraulic head values at grid points:

$$h(x_i) = h_i, \qquad i = 0, 1, \cdots, N$$

$$h(x_0) = h_0$$
$$h(x_N) = h_N$$

# One-dimensional Problems

 $\hookrightarrow$ Steady-state Flow

Spatial discretization: Divide the domain into a desired number of sub-domains, say  $N\colon$ 

$$0 \xrightarrow{x_0 \quad x_1 \quad \cdots \quad x_{i-1} \quad x_i \quad x_{i+1} \quad \cdots \quad x_{N-1} \quad x_N}$$

The grid spacing in this case is

$$\Delta x = \frac{1}{N}$$

Hydraulic head values at grid points:

$$h(x_i) = h_i, \qquad i = 0, 1, \cdots, N$$

$$h(x_0) = h_0$$
$$h(x_N) = h_N$$



# One-dimensional Problems

 $\hookrightarrow$ Steady-state Flow

Spatial discretization: Divide the domain into a desired number of sub-domains, say  $N\colon$ 

$$0 \xrightarrow{\qquad \qquad } 1$$

$$x_0 \quad x_1 \quad \cdots \quad x_{i-1} \quad x_i \quad x_{i+1} \quad \cdots \quad x_{N-1} \quad x_N$$

The grid spacing in this case is

$$\Delta x = \frac{1}{N}$$

Hydraulic head values at grid points:

$$h(x_i) = h_i, \qquad i = 0, 1, \cdots, N$$

$$h(x_0) = h_0$$
$$h(x_N) = h_N$$



$$\frac{\partial^2 h}{\partial x^2} = \frac{h_{i+1} - 2h_i + h_{i-1}}{\Delta x^2}$$

Discrete form of original equation, in terms of grid point values

$$k \frac{h_{i+1} - 2h_i + h_{i-1}}{(\Delta x)^2} = Q_i$$

Solution for N=2:

Difference equation at internal grid point (assuming  $Q_1=0$ )

$$h_2 - 2h_1 + h_0 = 0$$

$$h_1 = \frac{h_2 + h_0}{2}$$

$$\frac{\partial^2 h}{\partial x^2} = \frac{h_{i+1} - 2h_i + h_{i-1}}{\Delta x^2}$$

Discrete form of original equation, in terms of grid point values

$$k \frac{h_{i+1} - 2h_i + h_{i-1}}{(\Delta x)^2} = Q_i$$

Solution for N=2:

Difference equation at internal grid point (assuming  $Q_1=0$ )

$$h_2 - 2h_1 + h_0 = 0$$

$$h_1 = \frac{h_2 + h_0}{2}$$



$$\frac{\partial^2 h}{\partial x^2} = \frac{h_{i+1} - 2h_i + h_{i-1}}{\Delta x^2}$$

Discrete form of original equation, in terms of grid point values

$$k \frac{h_{i+1} - 2h_i + h_{i-1}}{(\Delta x)^2} = Q_i$$

Solution for N=2:

Difference equation at internal grid point (assuming  $Q_1=0$ )

$$h_2 - 2h_1 + h_0 = 0$$

$$h_1 = \frac{h_2 + h_0}{2}$$



$$\frac{\partial^2 h}{\partial x^2} = \frac{h_{i+1} - 2h_i + h_{i-1}}{\Delta x^2}$$

Discrete form of original equation, in terms of grid point values

$$k \frac{h_{i+1} - 2h_i + h_{i-1}}{(\Delta x)^2} = Q_i$$

Solution for N=2:

Difference equation at internal grid point (assuming  $Q_1=0$ )

$$h_2 - 2h_1 + h_0 = 0$$

$$h_1 = \frac{h_2 + h_0}{2}$$



#### **Solution for arbitrary** N:

Difference equations at unknown nodes  $i = 1, 2, \dots, N-1$ :

$$i = 1 k \frac{h_2 - 2h_1 + h_0}{(\Delta x)^2} = Q_1$$

$$i = 2 k \frac{h_3 - 2h_2 + h_1}{(\Delta x)^2} = Q_2$$

$$\vdots \vdots$$

$$i = N - 1 k \frac{h_N - 2h_{N-1} + h_{N-2}}{(\Delta x)^2} = Q_{N-1}$$

#### **Solution for arbitrary** N:

In matrix form:

$$\frac{k}{(\Delta x)^2} \begin{bmatrix} 1 & -2 & 1 & & & & \\ & 1 & -2 & 1 & & & \\ & & 1 & -2 & 1 & & \\ & & & \ddots & \ddots & \ddots & \\ & & & & 1 & -2 & 1 \\ & & & & & 1 & -2 & 1 \end{bmatrix} \begin{bmatrix} h_0 \\ h_1 \\ h_2 \\ h_3 \\ \vdots \\ h_{N-1} \\ h_N \end{bmatrix} = \begin{bmatrix} Q_1 \\ Q_2 \\ Q_3 \\ \vdots \\ Q_{N-1} \end{bmatrix}$$

#### **Solution for arbitrary** N:

Considering known boundary conditions:

$$\frac{k}{(\Delta x)^2} \begin{bmatrix} -2 & 1 & & & & \\ 1 & -2 & 1 & & & \\ & 1 & -2 & 1 & & \\ & & \ddots & \ddots & \ddots & \\ & & & 1 & -2 & 1 \\ & & & & 1 & -2 \end{bmatrix} \begin{pmatrix} h_1 \\ h_2 \\ h_3 \\ \vdots \\ h_{N-1} \end{pmatrix} = \begin{pmatrix} Q_1 - \frac{k}{(\Delta x)^2} h_0 \\ Q_2 \\ Q_3 \\ \vdots \\ Q_{N-1} - \frac{k}{(\Delta x)^2} h_N \end{pmatrix}$$

which is a linear equation system of the form

$$Ax = b$$

# One-dimensional Problems

 $\hookrightarrow$ Consolidation

Governing equation for one-dimensional consolidation

$$\frac{\partial u}{\partial t} - c_{\rm v} \frac{\partial^2 u}{\partial z^2} = 0$$

Coefficient of consolidation

$$c_{\rm v} = \frac{k}{m_{\rm v} \gamma_{\rm w}}$$

# One-dimensional Problems

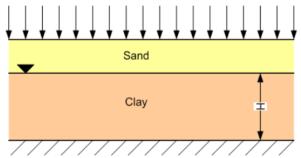
 $\hookrightarrow$ Consolidation

Governing equation for one-dimensional consolidation:

$$\frac{\partial u}{\partial t} - c_{\mathbf{v}} \frac{\partial^2 u}{\partial z^2} = 0$$

Coefficient of consolidation

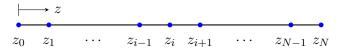
$$c_{\rm v} = \frac{k}{m_{\rm v} \gamma_{\rm w}}$$



#### $\hookrightarrow$ Consolidation

#### **Spatial Discretization**:

Consider a 1D domain sub-divided into N elements.



For a uniform grid spacing and domain depth/length d, we have

$$\Delta z = \frac{d}{N}$$

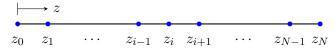
**Temporal Discretization**: For a simulation from time  $t_0$  to  $t_n$ , choosing a uniform time step  $\Delta t$  implies n time steps such that

$$t_n = n\Delta t$$



#### **Spatial Discretization**:

Consider a 1D domain sub-divided into N elements.



For a uniform grid spacing and domain depth/length d, we have

$$\Delta z = \frac{d}{N}$$

**Temporal Discretization**: For a simulation from time  $t_0$  to  $t_n$ , choosing a uniform time step  $\Delta t$  implies n time steps such that

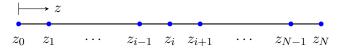
$$t_n = n\Delta t$$



#### $\hookrightarrow$ Consolidation

#### **Spatial Discretization**:

Consider a 1D domain sub-divided into N elements.

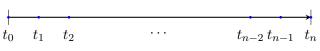


For a uniform grid spacing and domain depth/length d, we have

$$\Delta z = \frac{d}{N}$$

**Temporal Discretization**: For a simulation from time  $t_{\rm o}$  to  $t_n$ , choosing a uniform time step  $\Delta t$  implies n time steps such that

$$t_n = n\Delta t$$



The excess pore pressure is a function of both time and space:

$$u = u(t, z)$$

The partial derivative with respect to time may be approximated as a difference equation in different ways, resulting in different solution methods.

- Explicit Method: forward difference approximation in time.
- Implicit Method: backward difference approximation in time.
- 3 Crank-Nicolson Method: central difference approximation in time.

The excess pore pressure is a function of both time and space:

$$u = u(t, z)$$

The partial derivative with respect to time may be approximated as a difference equation in different ways, resulting in different solution methods.

- Explicit Method: forward difference approximation in time.
- ② Implicit Method: backward difference approximation in time.
- Crank-Nicolson Method: central difference approximation in time.

The excess pore pressure is a function of both time and space:

$$u = u(t, z)$$

The partial derivative with respect to time may be approximated as a difference equation in different ways, resulting in different solution methods.

- Explicit Method: forward difference approximation in time.
- Implicit Method: backward difference approximation in time.
- Crank-Nicolson Method: central difference approximation in time.

Forward difference approximation for time derivative

$$\frac{\partial u}{\partial t} = \frac{u_i^{n+1} - u_i^n}{\Delta t}$$

Symmetric difference approximation for spatial derivative

$$\frac{\partial^2 u}{\partial z^2} = \frac{u_{i+1}^n - 2u_i^n + u_{i-1}^n}{\Delta z^2}$$

$$\frac{u_i^{n+1} - u_i^n}{\Delta t} - c_{\rm v} \frac{u_{i+1}^n - 2u_i^n + u_{i-1}^n}{\Delta z^2} = 0$$

## Forward difference approximation for time derivative

$$\frac{\partial u}{\partial t} = \frac{u_i^{n+1} - u_i^n}{\Delta t}$$

Symmetric difference approximation for spatial derivative

$$\frac{\partial^2 u}{\partial z^2} = \frac{u_{i+1}^n - 2u_i^n + u_{i-1}^n}{\Delta z^2}$$

$$\frac{u_i^{n+1} - u_i^n}{\Delta t} - c_{\mathbf{v}} \frac{u_{i+1}^n - 2u_i^n + u_{i-1}^n}{\Delta z^2} = 0$$

Forward difference approximation for time derivative

$$\frac{\partial u}{\partial t} = \frac{u_i^{n+1} - u_i^n}{\Delta t}$$

Symmetric difference approximation for spatial derivative

$$\frac{\partial^2 u}{\partial z^2} = \frac{u_{i+1}^n - 2u_i^n + u_{i-1}^n}{\Delta z^2}$$

$$\frac{u_i^{n+1} - u_i^n}{\Delta t} - c_v \frac{u_{i+1}^n - 2u_i^n + u_{i-1}^n}{\Delta z^2} = 0$$

Forward difference approximation for time derivative

$$\frac{\partial u}{\partial t} = \frac{u_i^{n+1} - u_i^n}{\Delta t}$$

Symmetric difference approximation for spatial derivative

$$\frac{\partial^2 u}{\partial z^2} = \frac{u_{i+1}^n - 2u_i^n + u_{i-1}^n}{\Delta z^2}$$

$$\frac{u_i^{n+1} - u_i^n}{\Delta t} - c_{\mathbf{v}} \frac{u_{i+1}^n - 2u_i^n + u_{i-1}^n}{\Delta z^2} = 0$$

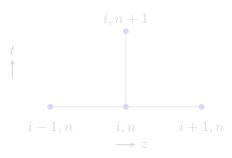
Solving for pore water pressure at time step  $t_{n+1}$  gives

$$u_i^{n+1} = u_i^n + \kappa \left( u_{i+1}^n - 2u_i^n + u_{i-1}^n \right)$$

where

$$\kappa = c_{\rm v} \frac{\Delta t}{\Delta z^2}$$

Stencil for the explicit method



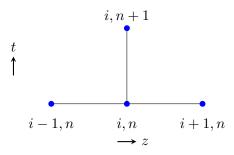
Solving for pore water pressure at time step  $t_{n+1}$  gives

$$u_i^{n+1} = u_i^n + \kappa \left( u_{i+1}^n - 2u_i^n + u_{i-1}^n \right)$$

where

$$\kappa = c_{\rm v} \frac{\Delta t}{\Delta z^2}$$

Stencil for the explicit method



## Stability and Convergence:

The explicit method is numerically stable and convergent when

$$\kappa \leq \frac{1}{2}$$

Thus, the time step used must satisfy

$$\Delta t \leq \frac{\Delta z^2}{2c_{\rm v}}$$

### Accuracy:

First-order in time,  $\mathcal{O}(\Delta t)$ , and second-order in space,  $\mathcal{O}(\Delta z^2)$ .

Backward difference approximation for time derivative

$$\frac{\partial u}{\partial t} = \frac{u_i^n - u_i^{n-1}}{\Delta t}$$

Symmetric difference approximation for spatial derivative

$$\frac{\partial^2 u}{\partial z^2} = \frac{u_{i+1}^n - 2u_i^n + u_{i-1}^n}{\Delta z^2}$$

$$\frac{u_i^n - u_i^{n-1}}{\Delta t} - c_{\mathbf{v}} \frac{u_{i+1}^n - 2u_i^n + u_{i-1}^n}{\Delta z^2} = 0$$

Backward difference approximation for time derivative

$$\frac{\partial u}{\partial t} = \frac{u_i^n - u_i^{n-1}}{\Delta t}$$

Symmetric difference approximation for spatial derivative

$$\frac{\partial^2 u}{\partial z^2} = \frac{u_{i+1}^n - 2u_i^n + u_{i-1}^n}{\Delta z^2}$$

$$\frac{u_i^n - u_i^{n-1}}{\Delta t} - c_{\mathbf{v}} \frac{u_{i+1}^n - 2u_i^n + u_{i-1}^n}{\Delta z^2} = 0$$

Backward difference approximation for time derivative

$$\frac{\partial u}{\partial t} = \frac{u_i^n - u_i^{n-1}}{\Delta t}$$

Symmetric difference approximation for spatial derivative

$$\frac{\partial^2 u}{\partial z^2} = \frac{u_{i+1}^n - 2u_i^n + u_{i-1}^n}{\Delta z^2}$$

$$\frac{u_i^n - u_i^{n-1}}{\Delta t} - c_{\mathbf{v}} \frac{u_{i+1}^n - 2u_i^n + u_{i-1}^n}{\Delta z^2} = 0$$

Backward difference approximation for time derivative

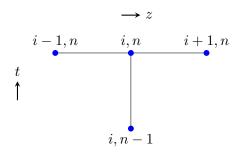
$$\frac{\partial u}{\partial t} = \frac{u_i^n - u_i^{n-1}}{\Delta t}$$

Symmetric difference approximation for spatial derivative

$$\frac{\partial^2 u}{\partial z^2} = \frac{u_{i+1}^n - 2u_i^n + u_{i-1}^n}{\Delta z^2}$$

$$\frac{u_i^n - u_i^{n-1}}{\Delta t} - c_{\mathbf{v}} \frac{u_{i+1}^n - 2u_i^n + u_{i-1}^n}{\Delta z^2} = 0$$

#### Stencil for the implicit method



The pore pressure at node i at time step  $t_n$  depends on the pore pressure values of the neighboring nodes at the same time step.  $\Rightarrow$  We can not solve for  $u_i^n$  directly.

#### Solution for N=3:

Assume the pore pressures at the boundary nodes are known.

Finite difference equations at unknown interior nodes

$$\frac{u_1^n - u_1^{n-1}}{\Delta t} - c_v \frac{u_2^n - 2u_1^n + u_0^n}{\Delta z^2} = 0$$

$$\frac{u_2^n - u_2^{n-1}}{\Delta t} - c_v \frac{u_3^n - 2u_2^n + u_1^n}{\Delta z^2} = 0$$

Equations to be solved for unknowns  $u_1^n$  and  $u_2^n$ 

$$(1+2\kappa)u_1^n - \kappa u_2^n = \kappa u_0^n + u_1^{n-1}$$
$$-\kappa u_1^n + (1+2\kappa)u_2^n = \kappa u_3^n + u_2^{n-1}$$

$$\begin{bmatrix} 1+2\kappa & -\kappa \\ -\kappa & 1+2\kappa \end{bmatrix} \begin{Bmatrix} u_1^n \\ u_2^n \end{Bmatrix} = \begin{Bmatrix} \kappa u_0^n + u_1^{n-1} \\ \kappa u_3^n + u_2^{n-1} \end{Bmatrix}$$

#### Solution for N=3:

Assume the pore pressures at the boundary nodes are known.

Finite difference equations at unknown interior nodes

$$\frac{u_1^n - u_1^{n-1}}{\Delta t} - c_v \frac{u_2^n - 2u_1^n + u_0^n}{\Delta z^2} = 0$$

$$\frac{u_2^n - u_2^{n-1}}{\Delta t} - c_v \frac{u_3^n - 2u_2^n + u_1^n}{\Delta z^2} = 0$$

Equations to be solved for unknowns  $u_1^n$  and  $u_2^n$ 

$$(1+2\kappa)u_1^n - \kappa u_2^n = \kappa u_0^n + u_1^{n-1}$$
$$-\kappa u_1^n + (1+2\kappa)u_2^n = \kappa u_3^n + u_2^{n-1}$$

$$\begin{bmatrix} 1+2\kappa & -\kappa \\ -\kappa & 1+2\kappa \end{bmatrix} \begin{Bmatrix} u_1^n \\ u_2^n \end{Bmatrix} = \begin{Bmatrix} \kappa u_0^n + u_1^{n-1} \\ \kappa u_3^n + u_2^{n-1} \end{Bmatrix}$$

#### Solution for N=3:

Assume the pore pressures at the boundary nodes are known.

Finite difference equations at unknown interior nodes

$$\frac{u_1^n - u_1^{n-1}}{\Delta t} - c_v \frac{u_2^n - 2u_1^n + u_0^n}{\Delta z^2} = 0$$

$$\frac{u_2^n - u_2^{n-1}}{\Delta t} - c_v \frac{u_3^n - 2u_2^n + u_1^n}{\Delta z^2} = 0$$

Equations to be solved for unknowns  $u_1^n$  and  $u_2^n$ 

$$(1+2\kappa)u_1^n - \kappa u_2^n = \kappa u_0^n + u_1^{n-1}$$
$$-\kappa u_1^n + (1+2\kappa)u_2^n = \kappa u_3^n + u_2^{n-1}$$

$$\begin{bmatrix} 1+2\kappa & -\kappa \\ -\kappa & 1+2\kappa \end{bmatrix} \begin{Bmatrix} u_1^n \\ u_2^n \end{Bmatrix} = \begin{Bmatrix} \kappa u_0^n + u_1^{n-1} \\ \kappa u_3^n + u_2^{n-1} \end{Bmatrix}$$

# One-dimensional Problems

→Consolidation: Implicit Method

#### Solution for N=3:

Assume the pore pressures at the boundary nodes are known.

Finite difference equations at unknown interior nodes

$$\frac{u_1^n - u_1^{n-1}}{\Delta t} - c_v \frac{u_2^n - 2u_1^n + u_0^n}{\Delta z^2} = 0$$

$$\frac{u_2^n - u_2^{n-1}}{\Delta t} - c_v \frac{u_3^n - 2u_2^n + u_1^n}{\Delta z^2} = 0$$

Equations to be solved for unknowns  $u_1^n$  and  $u_2^n$ 

$$(1+2\kappa)u_1^n - \kappa u_2^n = \kappa u_0^n + u_1^{n-1}$$
$$-\kappa u_1^n + (1+2\kappa)u_2^n = \kappa u_3^n + u_2^{n-1}$$

$$\begin{bmatrix} 1+2\kappa & -\kappa \\ -\kappa & 1+2\kappa \end{bmatrix} \begin{Bmatrix} u_1^n \\ u_2^n \end{Bmatrix} = \begin{Bmatrix} \kappa u_0^n + u_1^{n-1} \\ \kappa u_3^n + u_2^{n-1} \end{Bmatrix}$$

### **Solution for arbitrary** N:

Assume the pore pressures at the boundary nodes are known.

Finite difference equation

$$-\kappa u_{i-1}^n + (1+2\kappa)u_i^n - \kappa u_{i+1}^n = u_i^{n-1}$$

## **Solution for arbitrary** N:

Assume the pore pressures at the boundary nodes are known.

Finite difference equation

$$-\kappa u_{i-1}^n + (1+2\kappa)u_i^n - \kappa u_{i+1}^n = u_i^{n-1}$$

### **Solution for arbitrary** N:

Assume the pore pressures at the boundary nodes are known.

Finite difference equation

$$-\kappa u_{i-1}^n + (1+2\kappa)u_i^n - \kappa u_{i+1}^n = u_i^{n-1}$$

Finite difference equation at the unknown interior nodes

$$\begin{split} i &= 1 & -\kappa u_0^n + (1+2\kappa)u_1^n - \kappa u_2^n = u_1^{n-1} \\ i &= 2 & -\kappa u_1^n + (1+2\kappa)u_2^n - \kappa u_3^n = u_2^{n-1} \\ \vdots & \vdots & \vdots \\ i &= N-2 & -\kappa u_{N-3}^n + (1+2\kappa)u_{N-2}^n - \kappa u_{N-1}^n = u_{N-2}^{n-1} \\ i &= N-1 & -\kappa u_{N-2}^n + (1+2\kappa)u_{N-1}^n - \kappa u_N^n = u_{N-1}^{n-1} \end{split}$$

### **Solution for arbitrary** N:

Assume the pore pressures at the boundary nodes are known.

Finite difference equation

$$-\kappa u_{i-1}^n + (1+2\kappa)u_i^n - \kappa u_{i+1}^n = u_i^{n-1}$$

## **Solution for arbitrary** N:

Assume the pore pressures at the boundary nodes are known.

Finite difference equation

$$-\kappa u_{i-1}^n + (1+2\kappa)u_i^n - \kappa u_{i+1}^n = u_i^{n-1}$$

Matrix form considering boundary conditions

## One-dimensional Problems

→ Consolidation: Implicit Method

### Stability and Convergence:

The implicit method is numerically stable and convergent.

### Accuracy:

First-order in time,  $\mathcal{O}(\Delta t)$ , and second-order in space,  $\mathcal{O}(\Delta z^2)$ .

# One-dimensional Problems

→Consolidation: Crank-Nicolson Method

Central difference approximation for time derivative at  $(t_{n+\frac{1}{2}},z_i)$ 

$$\frac{\partial u}{\partial t} = \frac{u_i^{n+1} - u_i^n}{2\frac{\Delta t}{2}} = \frac{u_i^{n+1} - u_i^n}{\Delta t}$$

Finite difference approximation for spatial derivative at  $(t_{n+\frac{1}{2}},z_i)$ 

$$\frac{\partial^2 u}{\partial z^2} = \frac{u_{i+1}^{n+\frac{1}{2}} - 2u_i^{n+\frac{1}{2}} + u_{i-1}^{n+\frac{1}{2}}}{\Delta z^2}$$

$$u_i^{n+\frac{1}{2}} \approx \frac{1}{2} \left( u_i^n + u_i^{n+1} \right)$$

$$\Rightarrow \frac{\partial^2 u}{\partial z^2} = \frac{1}{2} \left( \frac{u_{i+1}^{n+1} - 2u_i^{n+1} + u_{i-1}^{n+1}}{\Delta z^2} + \frac{u_{i+1}^n - 2u_i^n + u_{i-1}^n}{\Delta z^2} \right)$$

Central difference approximation for time derivative at  $(t_{n+\frac{1}{2}},z_i)$ 

$$\frac{\partial u}{\partial t} = \frac{u_i^{n+1} - u_i^n}{2\frac{\Delta t}{2}} = \frac{u_i^{n+1} - u_i^n}{\Delta t}$$

Finite difference approximation for spatial derivative at  $(t_{n+\frac{1}{2}},z_i)$ 

$$\frac{\partial^2 u}{\partial z^2} = \frac{u_{i+1}^{n+\frac{1}{2}} - 2u_i^{n+\frac{1}{2}} + u_{i-1}^{n+\frac{1}{2}}}{\Delta z^2}$$

$$u_i^{n+\frac{1}{2}} \approx \frac{1}{2} \left( u_i^n + u_i^{n+1} \right)$$

$$\Rightarrow \frac{\partial^2 u}{\partial z^2} = \frac{1}{2} \left( \frac{u_{i+1}^{n+1} - 2u_i^{n+1} + u_{i-1}^{n+1}}{\Delta z^2} + \frac{u_{i+1}^n - 2u_i^n + u_{i-1}^n}{\Delta z^2} \right)$$

Central difference approximation for time derivative at  $(t_{n+\frac{1}{2}},z_i)$ 

$$\frac{\partial u}{\partial t} = \frac{u_i^{n+1} - u_i^n}{2\frac{\Delta t}{2}} = \frac{u_i^{n+1} - u_i^n}{\Delta t}$$

Finite difference approximation for spatial derivative at  $(t_{n+\frac{1}{2}},z_i)$ 

$$\frac{\partial^2 u}{\partial z^2} = \frac{u_{i+1}^{n+\frac{1}{2}} - 2u_i^{n+\frac{1}{2}} + u_{i-1}^{n+\frac{1}{2}}}{\Delta z^2}$$

$$u_i^{n+\frac{1}{2}} \approx \frac{1}{2} \left( u_i^n + u_i^{n+1} \right)$$

$$\Rightarrow \frac{\partial^2 u}{\partial z^2} = \frac{1}{2} \left( \frac{u_{i+1}^{n+1} - 2u_i^{n+1} + u_{i-1}^{n+1}}{\Delta z^2} + \frac{u_{i+1}^n - 2u_i^n + u_{i-1}^n}{\Delta z^2} \right)$$

Central difference approximation for time derivative at  $(t_{n+\frac{1}{2}},z_i)$ 

$$\frac{\partial u}{\partial t} = \frac{u_i^{n+1} - u_i^n}{2\frac{\Delta t}{2}} = \frac{u_i^{n+1} - u_i^n}{\Delta t}$$

Finite difference approximation for spatial derivative at  $(t_{n+\frac{1}{2}},z_i)$ 

$$\frac{\partial^2 u}{\partial z^2} = \frac{u_{i+1}^{n+\frac{1}{2}} - 2u_i^{n+\frac{1}{2}} + u_{i-1}^{n+\frac{1}{2}}}{\Delta z^2}$$

$$u_i^{n+\frac{1}{2}} \approx \frac{1}{2} \left( u_i^n + u_i^{n+1} \right)$$

$$\Rightarrow \frac{\partial^2 u}{\partial z^2} = \frac{1}{2} \left( \frac{u_{i+1}^{n+1} - 2u_i^{n+1} + u_{i-1}^{n+1}}{\Delta z^2} + \frac{u_{i+1}^n - 2u_i^n + u_{i-1}^n}{\Delta z^2} \right)$$

Central difference approximation for time derivative at  $(t_{n+\frac{1}{2}},z_i)$ 

$$\frac{\partial u}{\partial t} = \frac{u_i^{n+1} - u_i^n}{2\frac{\Delta t}{2}} = \frac{u_i^{n+1} - u_i^n}{\Delta t}$$

Finite difference approximation for spatial derivative at  $(t_{n+\frac{1}{2}},z_i)$ 

$$\frac{\partial^2 u}{\partial z^2} = \frac{u_{i+1}^{n+\frac{1}{2}} - 2u_i^{n+\frac{1}{2}} + u_{i-1}^{n+\frac{1}{2}}}{\Delta z^2}$$

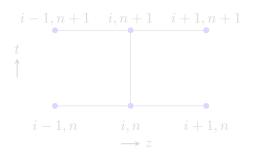
$$u_i^{n+\frac{1}{2}} \approx \frac{1}{2} \left( u_i^n + u_i^{n+1} \right)$$

$$\Rightarrow \frac{\partial^2 u}{\partial z^2} = \frac{1}{2} \left( \frac{u_{i+1}^{n+1} - 2u_i^{n+1} + u_{i-1}^{n+1}}{\Delta z^2} + \frac{u_{i+1}^n - 2u_i^n + u_{i-1}^n}{\Delta z^2} \right)$$

### Final finite difference equation

$$\frac{u_i^{n+1} - u_i^n}{\Delta t} - \frac{c_{\mathbf{v}}}{2} \left( \frac{u_{i+1}^{n+1} - 2u_i^{n+1} + u_{i-1}^{n+1}}{\Delta z^2} + \frac{u_{i+1}^n - 2u_i^n + u_{i-1}^n}{\Delta z^2} \right) = 0$$

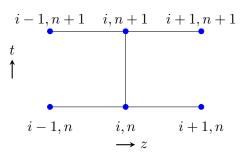
Stencil for the Crank-Nicolson method



Final finite difference equation

$$\frac{u_i^{n+1} - u_i^n}{\Delta t} - \frac{c_{\mathbf{v}}}{2} \left( \frac{u_{i+1}^{n+1} - 2u_i^{n+1} + u_{i-1}^{n+1}}{\Delta z^2} + \frac{u_{i+1}^n - 2u_i^n + u_{i-1}^n}{\Delta z^2} \right) = 0$$

Stencil for the Crank-Nicolson method



## One-dimensional Problems

→Consolidation: Crank-Nicolson Method

Simplified finite difference equation with unknowns on the LHS

$$-\frac{\kappa}{2}u_{i-1}^{n+1} + (1+\kappa)u_i^{n+1} - \frac{\kappa}{2}u_{i+1}^{n+1} = \frac{\kappa}{2}u_{i-1}^n + (1-\kappa)u_i^n + \frac{\kappa}{2}u_{i+1}^n$$

Solution for arbitrary N:

Simplified finite difference equation with unknowns on the LHS

$$-\frac{\kappa}{2}u_{i-1}^{n+1} + (1+\kappa)u_i^{n+1} - \frac{\kappa}{2}u_{i+1}^{n+1} = \frac{\kappa}{2}u_{i-1}^n + (1-\kappa)u_i^n + \frac{\kappa}{2}u_{i+1}^n$$

## **Solution for arbitrary** N:

Finite difference equation at the unknown interior nodes

$$\begin{split} -\frac{\kappa}{2}u_0^{n+1} + (1+\kappa)u_1^{n+1} - \frac{\kappa}{2}u_2^{n+1} &= \frac{\kappa}{2}u_0^n + (1-\kappa)u_1^n + \frac{\kappa}{2}u_2^n \\ -\frac{\kappa}{2}u_1^{n+1} + (1+\kappa)u_2^{n+1} - \frac{\kappa}{2}u_3^{n+1} &= \frac{\kappa}{2}u_1^n + (1-\kappa)u_2^n + \frac{\kappa}{2}u_3^n \\ & \vdots & \vdots & \vdots \\ -\frac{\kappa}{2}u_{N-3}^{n+1} + (1+\kappa)u_{N-2}^{n+1} - \frac{\kappa}{2}u_{N-1}^{n+1} &= \frac{\kappa}{2}u_{N-3}^n + (1-\kappa)u_{N-2}^n + \frac{\kappa}{2}u_{N-1}^n \\ -\frac{\kappa}{2}u_{N-2}^{n+1} + (1+\kappa)u_{N-1}^{n+1} - \frac{\kappa}{2}u_N^{n+1} &= \frac{\kappa}{2}u_{N-2}^n + (1-\kappa)u_{N-1}^n + \frac{\kappa}{2}u_N^n \end{split}$$

Simplified finite difference equation with unknowns on the LHS

$$-\frac{\kappa}{2}u_{i-1}^{n+1} + (1+\kappa)u_i^{n+1} - \frac{\kappa}{2}u_{i+1}^{n+1} = \frac{\kappa}{2}u_{i-1}^n + (1-\kappa)u_i^n + \frac{\kappa}{2}u_{i+1}^n$$

## **Solution for arbitrary** N:

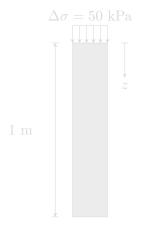
In matrix form

$$\begin{bmatrix} 1+\kappa & -\frac{\kappa}{2} \\ -\frac{\kappa}{2} & 1+\kappa & -\frac{\kappa}{2} \\ & \ddots & \ddots & \ddots \\ & & \ddots & \ddots & \ddots \\ & & & -\frac{\kappa}{2} & 1+\kappa & -\frac{\kappa}{2} \\ & & & -\frac{\kappa}{2} & 1+\kappa & -\frac{\kappa}{2} \\ & & & -\frac{\kappa}{2} & 1+\kappa \end{bmatrix} \begin{bmatrix} u_1^{n+1} \\ u_2^{n+1} \\ \vdots \\ u_{N-2}^{n+1} \\ u_{N-1}^{n+1} \end{bmatrix} = \begin{bmatrix} b_1 + \frac{\kappa}{2} u_0^{n+1} \\ b_2 \\ \vdots \\ b_{N-2} \\ b_{N-1} + \frac{\kappa}{2} u_N^{n+1} \end{bmatrix}$$

where

$$b_{i} = \frac{\kappa}{2}u_{i-1}^{n} + (1 - \kappa)u_{i}^{n} + \frac{\kappa}{2}u_{i+1}^{n}$$

Consider a 1 m thick soil subjected to a surcharge load of 50 kPa.



Coefficient of consolidation:

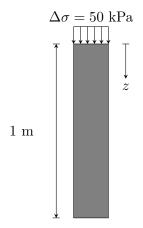
$$c_v = 2 \times 10^{-6} \text{ m}^2/\text{s}$$

Dimensionless time

$$T = \frac{c_{\rm v} t}{H^2}$$

Solve for the excess pore pressure as a function of time using the explicit, implicit and Crank-Nicolson methods.

Consider a 1 m thick soil subjected to a surcharge load of 50 kPa.



Coefficient of consolidation:

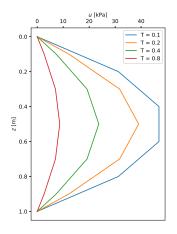
$$c_v = 2 \times 10^{-6} \text{ m}^2/\text{s}$$

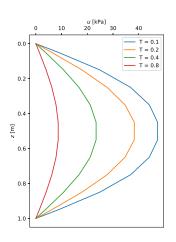
Dimensionless time

$$T = \frac{c_{\rm v}t}{H^2}$$

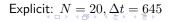
Solve for the excess pore pressure as a function of time using the explicit, implicit and Crank-Nicolson methods.

 $\hookrightarrow$ Consolidation: Example



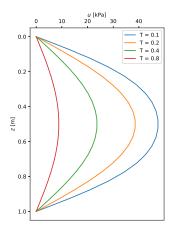


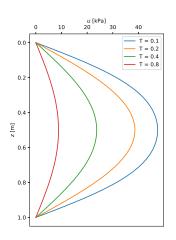
Explicit:  $N = 10, \Delta t = 2500$ 





→Consolidation: Example



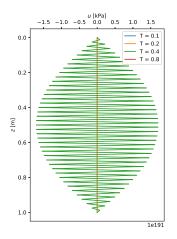


Explicit:  $N = 40, \Delta t = 156$ 



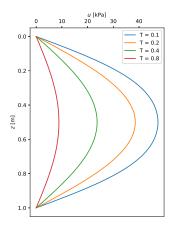


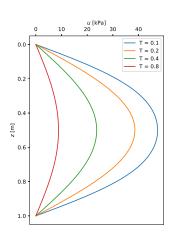
→Consolidation: Example



Explicit:  $N=80, \Delta t=50$ 

 $\hookrightarrow$ Consolidation: Example





Implicit:  $N = 80, \Delta t = 200$ 

Crank-Nicolson:  $N=80, \Delta t=100$ 

## **Contents**

- Introduction
- 2 Basic Principles
  - Derivatives as Difference Equations
  - Difference Equations for Partial Derivatives
  - Solving Differential Equations
- One-dimensional Problems
  - Steady-state Groundwater Flow
  - Consolidation
- 4 Two-dimensional Problems
  - Steady-state Groundwater Flow



Steady-state groundwater flow in two-dimensions: The governing differential equation is

$$k_x \frac{\partial^2 h}{\partial x^2} + k_y \frac{\partial^2 h}{\partial y^2} = Q$$

For an isotropic material and neglecting source/sink terms

$$\frac{\partial^2 h}{\partial x^2} + \frac{\partial^2 h}{\partial y^2} = 0$$

Steady-state groundwater flow in two-dimensions: The governing differential equation is

$$k_x \frac{\partial^2 h}{\partial x^2} + k_y \frac{\partial^2 h}{\partial y^2} = Q$$

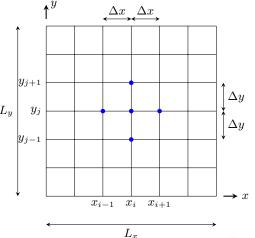
For an isotropic material and neglecting source/sink terms

$$\frac{\partial^2 h}{\partial x^2} + \frac{\partial^2 h}{\partial y^2} = 0$$

→Steady-state Flow

#### Spatial Discretization:

 $N_x$  and  $N_y$  elements with grid spacing of  $\Delta x$  and  $\Delta y$ , respectively.



$$\Delta x = \Delta y$$

Grid spacings are calculated from

$$\Delta x = rac{L_x}{N_x}$$
 and  $\Delta y = rac{L_y}{N_y}$ 

Notation for hydrauclic head at point  $(x_i, j_j)$ 

$$h(x_i, y_j) = h_{i,j}$$

for  $i=0,1,\cdots,N_x$  and  $j=0,1,\cdots,N_y$ .

$$h_{0,j}=h_{N,j}=\bar{h}_1\quad\text{and}\quad h_{i,0}=h_{i,N}=\bar{h}_2$$

$$\Delta x = \Delta y$$

Grid spacings are calculated from

$$\Delta x = \frac{L_x}{N_x} \quad \text{and} \quad \Delta y = \frac{L_y}{N_y}$$

Notation for hydrauclic head at point  $(x_i, j_j)$ 

$$h(x_i, y_j) = h_{i,j}$$

for  $i=0,1,\cdots,N_x$  and  $j=0,1,\cdots,N_y$ .

$$h_{0,j}=h_{N,j}=\bar{h}_1\quad\text{and}\quad h_{i,0}=h_{i,N}=\bar{h}_2$$

$$\Delta x = \Delta y$$

Grid spacings are calculated from

$$\Delta x = \frac{L_x}{N_x} \quad \text{and} \quad \Delta y = \frac{L_y}{N_y}$$

Notation for hydrauclic head at point  $(x_i, j_j)$ 

$$h(x_i, y_j) = h_{i,j}$$

for 
$$i=0,1,\cdots,N_x$$
 and  $j=0,1,\cdots,N_y$ .

$$h_{0,j} = h_{N,j} = \bar{h}_1$$
 and  $h_{i,0} = h_{i,N} = \bar{h}_2$ 

$$\Delta x = \Delta y$$

Grid spacings are calculated from

$$\Delta x = \frac{L_x}{N_x} \quad \text{and} \quad \Delta y = \frac{L_y}{N_y}$$

Notation for hydrauclic head at point  $(x_i, j_j)$ 

$$h(x_i, y_j) = h_{i,j}$$

for  $i=0,1,\cdots,N_x$  and  $j=0,1,\cdots,N_y$ .

$$h_{0,j}=h_{N,j}=\bar{h}_1\quad\text{and}\quad h_{i,0}=h_{i,N}=\bar{h}_2$$

Finite difference approximations for spatial derivatives

$$\begin{split} \frac{\partial^2 h}{\partial x^2} &= \frac{h_{i+1,j} - 2h_{i,j} + h_{i-1,j}}{\Delta x^2} \\ \frac{\partial^2 h}{\partial y^2} &= \frac{h_{i,j+1} - 2h_{i,j} + h_{i,j-1}}{\Delta y^2} \end{split}$$

Based on the governing equation, we get

$$\frac{h_{i+1,j} - 2h_{i,j} + h_{i-1,j}}{\Delta x^2} + \frac{h_{i,j+1} - 2h_{i,j} + h_{i,j-1}}{\Delta y^2} = 0$$

For a uniform grid where  $\Delta x = \Delta y$ 

$$h_{i,j-1} + h_{i-1,j} - 4h_{i,j} + h_{i+1,j} + h_{i,j+1} = 0$$

Finite difference approximations for spatial derivatives

$$\begin{split} \frac{\partial^2 h}{\partial x^2} &= \frac{h_{i+1,j} - 2h_{i,j} + h_{i-1,j}}{\Delta x^2} \\ \frac{\partial^2 h}{\partial y^2} &= \frac{h_{i,j+1} - 2h_{i,j} + h_{i,j-1}}{\Delta y^2} \end{split}$$

Based on the governing equation, we get

$$\frac{h_{i+1,j} - 2h_{i,j} + h_{i-1,j}}{\Delta x^2} + \frac{h_{i,j+1} - 2h_{i,j} + h_{i,j-1}}{\Delta y^2} = 0$$

For a uniform grid where  $\Delta x = \Delta y$ 

$$h_{i,j-1} + h_{i-1,j} - 4h_{i,j} + h_{i+1,j} + h_{i,j+1} = 0$$

Finite difference approximations for spatial derivatives

$$\begin{split} \frac{\partial^2 h}{\partial x^2} &= \frac{h_{i+1,j} - 2h_{i,j} + h_{i-1,j}}{\Delta x^2} \\ \frac{\partial^2 h}{\partial y^2} &= \frac{h_{i,j+1} - 2h_{i,j} + h_{i,j-1}}{\Delta y^2} \end{split}$$

Based on the governing equation, we get

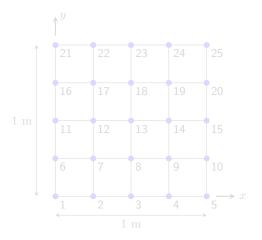
$$\frac{h_{i+1,j} - 2h_{i,j} + h_{i-1,j}}{\Delta x^2} + \frac{h_{i,j+1} - 2h_{i,j} + h_{i,j-1}}{\Delta y^2} = 0$$

For a uniform grid where  $\Delta x = \Delta y$ 

$$h_{i,j-1} + h_{i-1,j} - 4h_{i,j} + h_{i+1,j} + h_{i,j+1} = 0$$

## Solution for $N_x = N_y = 4$ :

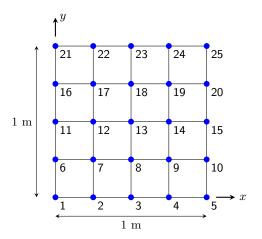
Consider a  $1 \text{ m} \times 1 \text{ m}$  grid divided into 4 elements.



←Steady-state Flow

Solution for  $N_x = N_y = 4$ :

Consider a  $1~\mathrm{m}\times1~\mathrm{m}$  grid divided into 4 elements.



Assume that the boundary conditions are

$$h=10$$
 for  $y=1$   
 $h=0$  for  $x=0, x=1$  and  $y=0$ 

Finite difference equations for nodes 7, 8 and 9

$$-4h_7 + h_8 + h_{12} = 0$$
$$h_7 - 4h_8 + h_9 + h_{13} = 0$$
$$h_8 - 4h_9 + h_{14} = 0$$

Finite difference equations for nodes 12, 13 and 14

$$h_7 - 4h_{12} + h_{13} + h_{17} = 0$$
  
$$h_8 + h_{12} - 4h_{13} + h_{14} + h_{18} = 0$$
  
$$h_9 + h_{13} - 4h_{14} + h_{19} = 0$$

Assume that the boundary conditions are

$$h=10$$
 for  $y=1$   
 $h=0$  for  $x=0, x=1$  and  $y=0$ 

Finite difference equations for nodes 7, 8 and 9

$$-4h_7 + h_8 + h_{12} = 0$$
$$h_7 - 4h_8 + h_9 + h_{13} = 0$$
$$h_8 - 4h_9 + h_{14} = 0$$

Finite difference equations for nodes 12, 13 and 14

$$h_7 - 4h_{12} + h_{13} + h_{17} = 0$$
  
$$h_8 + h_{12} - 4h_{13} + h_{14} + h_{18} = 0$$
  
$$h_9 + h_{13} - 4h_{14} + h_{19} = 0$$

Assume that the boundary conditions are

$$h=10$$
 for  $y=1$   
 $h=0$  for  $x=0, x=1$  and  $y=0$ 

Finite difference equations for nodes 7, 8 and 9

$$-4h_7 + h_8 + h_{12} = 0$$
$$h_7 - 4h_8 + h_9 + h_{13} = 0$$
$$h_8 - 4h_9 + h_{14} = 0$$

Finite difference equations for nodes 12, 13 and 14

$$h_7 - 4h_{12} + h_{13} + h_{17} = 0$$
  
$$h_8 + h_{12} - 4h_{13} + h_{14} + h_{18} = 0$$
  
$$h_9 + h_{13} - 4h_{14} + h_{19} = 0$$

Finite difference equations for nodes 17, 18 and 19

$$h_{12} - 4h_{17} + h_{18} = -10$$

$$h_{13} + h_{17} - 4h_{18} + h_{19} = -10$$

$$h_{14} + h_{18} - 4h_{19} = -10$$

Assembling the equations into a matrix form gives

 $\hookrightarrow$ Steady-state Flow

Finite difference equations for nodes 17, 18 and 19

$$h_{12} - 4h_{17} + h_{18} = -10$$
$$h_{13} + h_{17} - 4h_{18} + h_{19} = -10$$
$$h_{14} + h_{18} - 4h_{19} = -10$$

Assembling the equations into a matrix form gives

$$\begin{bmatrix} -4 & 1 & 0 & 1 & 0 & 0 & 0 & 0 & 0 \\ 1 & -4 & 1 & 0 & 1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 1 & -4 & 0 & 0 & 1 & 0 & 0 & 0 & 0 \\ \hline 1 & 0 & 0 & 1 & -4 & 0 & 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 1 & -4 & 1 & 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 & 1 & -4 & 0 & 0 & 1 \\ \hline 0 & 0 & 0 & 1 & 0 & 0 & -4 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 & 0 & 1 & -4 & 1 \\ 0 & 0 & 0 & 0 & 0 & 1 & 0 & 1 & -4 & 1 \\ 0 & 0 & 0 & 0 & 0 & 1 & 0 & 1 & -4 & 1 \\ \end{bmatrix} \begin{bmatrix} h_7 \\ h_8 \\ h_9 \\ h_{12} \\ h_{13} \\ h_{14} \\ h_{17} \\ h_{18} \\ h_{19} \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \\ -10 \\ -10 \\ -10 \\ -10 \end{bmatrix}$$

The final equation system is of the form

$$Ax = b$$

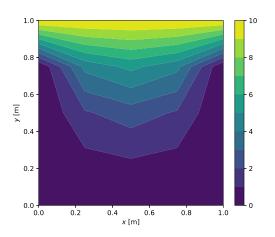
where

$$A = \begin{bmatrix} B & I & \mathbf{0} \\ \hline I & B & I \\ \hline \mathbf{0} & I & B \end{bmatrix}$$

and

$$\boldsymbol{B} = \begin{bmatrix} -4 & 1 & 0 \\ 1 & -4 & 1 \\ 0 & 1 & -4 \end{bmatrix} \quad \text{and} \quad \boldsymbol{I} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

 $\hookrightarrow$ Steady-state Flow



Solution for Nx = Ny = 4.

### Solution for an $N_x \times N_y$ grid:

$$(N_x+1)\times(N_y+1)$$

Coefficient matrix A with a similar structure:

$$A = \begin{bmatrix} B & I & 0 & \cdots & 0 \\ \hline I & B & I & \ddots & \vdots \\ \hline 0 & I & \ddots & \ddots & 0 \\ \hline \vdots & \ddots & \ddots & B & I \\ \hline 0 & \cdots & 0 & I & B \end{bmatrix}$$

$$(N_x - 1)^2 \times (N_y - 1)^2$$

### Solution for an $N_x \times N_y$ grid:

Assume that the grid is uniform in both directions i.e.  $\Delta x = \Delta y$ .

$$(N_x+1)\times(N_y+1)$$

Coefficient matrix A with a similar structure:

$$A = \begin{bmatrix} B & I & 0 & \cdots & 0 \\ \hline I & B & I & \ddots & \vdots \\ 0 & I & \ddots & \ddots & 0 \\ \vdots & \ddots & \ddots & B & I \\ \hline 0 & \cdots & 0 & I & B \end{bmatrix}$$

$$(N_x - 1)^2 \times (N_y - 1)^2$$

### Solution for an $N_x \times N_y$ grid:

Assume that the grid is uniform in both directions i.e.  $\Delta x = \Delta y$ . Number of grid points in the computational domain:

$$(N_x+1)\times(N_y+1)$$

Coefficient matrix A with a similar structure:

$$A = \begin{bmatrix} B & I & 0 & \cdots & 0 \\ \hline I & B & I & \ddots & \vdots \\ 0 & I & \ddots & \ddots & 0 \\ \vdots & \ddots & \ddots & B & I \\ \hline 0 & \cdots & 0 & I & B \end{bmatrix}$$

$$(N_x - 1)^2 \times (N_y - 1)^2$$

#### Solution for an $N_x \times N_y$ grid:

Assume that the grid is uniform in both directions i.e.  $\Delta x = \Delta y$ . Number of grid points in the computational domain:

$$(N_x+1)\times(N_y+1)$$

Coefficient matrix A with a similar structure:

$$A = \begin{bmatrix} B & I & 0 & \cdots & 0 \\ \hline I & B & I & \ddots & \vdots \\ \hline 0 & I & \ddots & \ddots & 0 \\ \hline \vdots & \ddots & \ddots & B & I \\ \hline 0 & \cdots & 0 & I & B \end{bmatrix}$$

$$(N_x - 1)^2 \times (N_y - 1)^2$$



#### Matrices $\boldsymbol{B}$ and $\boldsymbol{I}$ :

$$\boldsymbol{B} = \begin{bmatrix} -4 & 1 & 0 & \cdots & 0 \\ 1 & -4 & 1 & \ddots & \vdots \\ 0 & \ddots & \ddots & \ddots & 0 \\ \vdots & \ddots & 1 & -4 & 1 \\ 0 & \cdots & 0 & 1 & -4 \end{bmatrix} \quad \text{and} \quad \boldsymbol{I} = \begin{bmatrix} 1 & 0 & \cdots & \cdots & 0 \\ 0 & 1 & \ddots & \vdots \\ \vdots & \ddots & \ddots & \ddots & \vdots \\ \vdots & \ddots & \ddots & \ddots & \vdots \\ \vdots & \ddots & \ddots & \ddots & \vdots \\ 0 & \cdots & \cdots & 0 & 1 \end{bmatrix}$$

Sizes of matrices  $oldsymbol{B}$  and  $oldsymbol{I}$ :

$$(N_x - 1) \times (N_y - 1)$$

RHS vector b:

$$\boldsymbol{b} = \left\{ 0 \quad 0 \quad \cdots \quad 0 \quad -10 \quad \cdots \quad -10 \right\}^{\mathsf{T}}$$

#### Matrices $\boldsymbol{B}$ and $\boldsymbol{I}$ :

$$\boldsymbol{B} = \begin{bmatrix} -4 & 1 & 0 & \cdots & 0 \\ 1 & -4 & 1 & \ddots & \vdots \\ 0 & \ddots & \ddots & \ddots & 0 \\ \vdots & \ddots & 1 & -4 & 1 \\ 0 & \cdots & 0 & 1 & -4 \end{bmatrix} \quad \text{and} \quad \boldsymbol{I} = \begin{bmatrix} 1 & 0 & \cdots & \cdots & 0 \\ 0 & 1 & \ddots & \vdots \\ \vdots & \ddots & \ddots & \ddots & \vdots \\ \vdots & \ddots & \ddots & \ddots & \vdots \\ \vdots & \ddots & \ddots & 1 & 0 \\ 0 & \cdots & \cdots & 0 & 1 \end{bmatrix}$$

Sizes of matrices  $\boldsymbol{B}$  and  $\boldsymbol{I}$ :

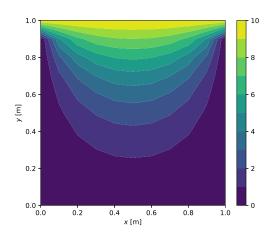
$$(N_x - 1) \times (N_y - 1)$$

RHS vector b:

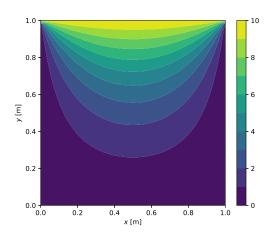
$$\boldsymbol{b} = \begin{bmatrix} 0 & 0 & \cdots & 0 & -10 & \cdots & -10 \end{bmatrix}^\mathsf{T}$$



 $\hookrightarrow$ Steady-state Flow

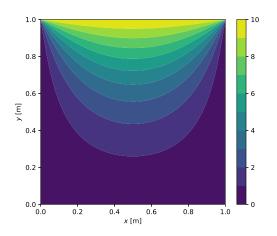


Solution for Nx = Ny = 10.



Solution for Nx = Ny = 50.

 $\hookrightarrow$ Steady-state Flow



Solution for Nx = Ny = 100.