

## मोतीलाल नेहरू राष्ट्रीय प्रौद्योगिकी संस्थान इलाहाबाद

प्रयागराज-211004 भारत

### Motilal Nehru National Institute of TechnologyAllahabad Prayagraj-211004 [India]

# **DEPARTMENT OF CHEMICAL ENGINEERING**

## Mid Semester (Even) Examination 2023-24

Trogramme Name: B. Took /N. T.	ear) Sauminution	- U-						
Course Code: CHN 15111	e/MCA			Ser	neste	er:	5 <sup>th</sup>	
Branch: Chemical Engineering	Course Name: Heterogeneous Reaction Engineering							
Duration: 90 Minutes	Student Reg. No.:	2	0	2	2	2	0	6 8

Max. Marks: 20

Instructions: (Related to Questions)

- 1. Attempt all questions
- 2. Figures to the right indicate the full marks.
- 3. Symbols have their usual meanings
- 4. Assume missing data suitably, if any
- 5. Use of non-programmable scientific calculator is permitted
- Q1A first order reaction occurs in a reactor whose RTD is given in Fig. Q1 (c). Calculate the Marks CO No. conversion for the flow schemes shown in the Figs. Q1(a & b). For simplicity take  $C_0 = 1$ , k = 1,

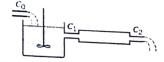
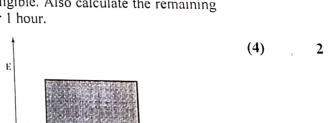


Fig. Q1(c)

Fig. Q1(a): Microfluid, early mixing at molecular level,

Fig. Q1(b): Macrofluid, early mixing of elements

Calculate the time needed to burn to completion spherical particles of graphite (radius 12 mm,  $Q_2$ bulk density 2.4 gm/cm³, surface reaction rate constant, k" = 20 cm/sec) in 12% oxygen stream at 900 °C and 1 atm. Assume gas film resistance to be negligible. Also calculate the remaining amount of graphite particles unburned and their radius after 1 hour.



Hydrogen sulfide is removed from coal gas by passing the gas through a moving bed or iron oxide particles. In the coal gas environment (consider uniform) the solids are converted from Fe<sub>2</sub>O<sub>3</sub> to FeS by the SCM/reaction control,  $\tau = 2$  hr. Find the fractional conversion of oxide to iron sulfide if the RTD of solids in the reactor is approximated by the E curves of Fig. Q3.

(4)

Fig. Q3 Gaseous A absorbs and reacts with liquid phase reactant B in a packed bed according to following reaction:

(4)

2

$$A(g \rightarrow I) + B(I) \rightarrow R(I), \qquad -r_A = kC_A C_B$$

Calculate the rate of reaction in mol/hr.m<sup>3</sup> in reactor at a point in the reactor where  $p_A = 100 \text{ Pa}$ and  $C_B = 100 \text{ mol/m}^3$ .

Additional data:  $k_{Ag}a = 0.1 \text{ mol/hr} \cdot m^2$  of reactor. Pa;  $k_{Al}a = 100 \text{ m}^3$  liquid/m³ reactor .hr;  $D_{Al} = D_{Bl} = 1.0$  $\times$  10<sup>-6</sup>  $m^2/hr$   $H_A = 1000$  Pa.  $m^3/mol$ ; k = 10  $m^3/mol.hr$ ; a = 100  $m^2/m^3$ ;  $f_l = 0.01$   $m^3$  liquid/ $m^3$  reactor.

Q 5	Discus	S ANY TWO of the following in detail:	(2×2)	
	(b)	Role of Hatta Number and Solubility data in fluid-fluid reaction system.	3	1 2
		Factors to Consider in Selecting a Contactor for fluid-fluid reaction system.		2

\*\*\*\* Good Luck \*\*\*\*

#### Course Outcomes (COs):

- 1. Ability to interpret and analyze heterogeneous reaction kinetics data.
- 2. Ability to design reactors for non-catalytic heterogeneous (fluid-particle and fluid-fluid) reactions systems.
- 3. Ability to identify the kinetics of solid catalyzed reaction systems and to design reactors containing solid catalysts.
- 4. Ability to identify kinetics of the catalyst deactivation, and to design reactors containing decaying solid catalysts.



### मोतीलाल नेहरू राश्ट्रीय प्रौद्योगिकी संस्थान इलाहाबाद

प्रयागराज-211004 भारत

### Motilal Nehru National Institute of TechnologyAllahabad Prayagraj-211004 [India]

### DEPARTMENT OF CHEMICAL ENGINEERING

End Semester (Even) Examination 2024-25

	Programme Name: B.Tech./M.Tech./MBA/M.Se/MCA		Semester:5 <sup>th</sup>			
	Cor	ourse Code: CHN 15111 Course Name: Heterogeneous Reaction		rogeneous Reaction Engi	neering	
	Bra	nnch: Chemical Engineering	Student Reg. No.:	20222	0 6	. 0
	lns	ration: 2½ Hours tructions: (Related to Questions)	Max. Marks: 40	A STATE OF THE STA		
	2	Attempt all questions I. Figures to the right indicate the full marks. I. Symbols have their usual meanings	4. Assume missing data 5. Use of non-programn	suitably, if any nable scientific calculator is	permitte	rd
Q 1	a	Gas A contacts and reacts with a spherical solid I $A(g) + B(s) - B(s)$	B according to the react $P(g) + S(s)$		Marks (4)	COs CO2
		As reaction progresses, a sharp reaction plane me product layer through which gaseous A and R me that act in series are gas film, ash layer, and react thickening of ash layer is proportional to rate or reach any thickness l, is the sum of the time need	noves forward into the soust diffuse. For this sittion step. Taking into of reaction at that instant	uation, three resistances consideration that rate of it, show that the time to		
		$t_{actual} = t_{film\_alone} + t_{actual}$	$_{sh\_alone} + t_{reaction\_alor}$	ıe		
	b	Two small samples of solids (2 mm and 4 mm di for a period of 1.0 hour. Under the condition pr converted and 2 mm particles are 87.5% converted conversion of solids and time required for conversion.	evailing in the oven 4 ed. Find the rate control	mm particles are 57.8% olling mechanism for the	(4)	CO2
Q 2	At	tempt ANY TWO of the following:				
	a	Air with gaseous A bubbles through a tank conta $A(g \to l) + 2B(l) \to R(l), -r_A = 0$	ining aqueous B. React $= kC_A C_B^2,  k = 10^6 \text{ n}$	ion occurs as follows: m <sup>6</sup> /mol <sup>2</sup> .hr	(4)	CO2
		For this system $k_{Ag}a = 0.01 \text{ mol/hr. m}^2$ . Pa; $k_{Al}a = 20.0 \text{ m/h}$ $D_{Al} = D_{Al} = 10^{-6} \text{ m}^2/\text{hr}$ ; $a = 20 \text{ m}^2/\text{m}^3$	$\text{nr; } f_l = 0.98;  H_A = 10$	<sup>5</sup> Pa. m <sup>3</sup> /mol		
		For a point in the absorber-reactor where $p_A =$ Determine following for the above system:	$5.0 \times 10^3 \text{ Pa}$ ; $C_B$	$= 1.0 \mathrm{mol/m^3}$		
	b	(i) locate the resistance to the reaction (iii) determine the behavior in the liquid film (i Researchers studied the rate of CO <sub>2</sub> absorption KHCO <sub>3</sub> . The resulting reaction can be represented	into an alkaline buffer	reaction (mol/m <sup>3</sup> .hr)	(4)	CO2
		$CO_2(g \rightarrow l) + OH^-(l) \rightarrow HCO$		$C_A C_B$		

recirculating solution kept at 20°C and close to constant C<sub>B</sub>. Find the fraction of entering CO<sub>2</sub> absorbed.

In the experiment pure CO2 at 1 atm was bubbled into a packed column irrigated by rapidly

(B)

(A)

Data Given:

Column: 
$$V_r = 0.6041 \text{ m}^3$$
  $f_l = 0.08$   $a = 120 \text{ m}^2/\text{m}^3$  Gas:  $\pi = 101 325 \text{ Pa}$   $H_A = 3500 \text{ Pa} \cdot \text{m}^3/\text{mol} \cdot \text{v}_0 = 0.0363 \text{ m}^3/\text{s}$  Hates:  $k = 0.433 \text{ m}^3/\text{mol} \cdot \text{s}$   $\mathcal{D}_{Al} = \mathcal{D}_{Bl} = 1.4 \times 10^{-9} \text{ m}^2/\text{s}$   $k_{Al}a = 0.025 \text{ s}^{-1}$ 

Consider the following three-phase (gas-liquid on solid catalysts) reaction and stoichiometry:

Three-phase (gas-liquid on solid catalysts) reaction and stoichiometry: (4) CO2
$$A(g \rightarrow l) + bB(l) \xrightarrow{\text{on catalyst} \atop \text{surface}} \text{products} \cdot \cdot \cdot b = \left(\frac{\text{mol B}}{\text{mol A}}\right)$$
CO3

$$-r'''_A = k'''_A C_A C_B$$

$$-r'''_B = k'''_B C_A C_B$$
where
$$k'''_A = k'''_B / b \cdot \cdot \cdot \operatorname{mol} A / m^3 \operatorname{cat} \cdot s$$

$$k'''_A = k'''_B / b \cdot \cdot \cdot \operatorname{mf} / \operatorname{mol} B \cdot m^3 \operatorname{cat} \cdot s$$

Gas reactant must first dissolve in the liquid, then both reactants (A & B) diffuse to the solid catalyst surface for reaction to occur. Develop overall rate equations  $(-r_A''')$  and  $(-r_B''')$  in terms of measurable concentration or partial pressure. Also, mention all the assumptions required for the same.

Define Non-dissociative and Dessociative Adsorption. Derive Langmuir adsorption isotherm equation with all necesseary assumptions for Dessociative Adsorption.

CO<sub>3</sub> (4)

The reaction of two noxious automobile exhaust products, CO and NO carried out over a copper catalyst to form environmentally acceptable products, N2 and CO2. The main reaction and its mechanism are given below:

CO<sub>3</sub> (4)

Reaction:

$$CO + NO \iff CO_2 + \frac{1}{2}N_2$$

Mechanism:

$$\begin{array}{c} \text{CO + NO} & \stackrel{\textit{Copper}}{\Longleftrightarrow} & \text{CO}_2 + \frac{1}{2} N_2 \\ & \stackrel{\text{CO+S}}{\Longleftrightarrow} & \text{CO+S} \\ & \text{NO+S} & \stackrel{\text{Po-S}}{\Longleftrightarrow} & \text{NO+S} \end{array}$$

 $NO \cdot S + CO \cdot S \longrightarrow CO_2 + N \cdot S + S$  Rate-limiting

$$\left. \begin{array}{c} N \cdot S + N \cdot S & \longleftrightarrow & N_2 \cdot S \\ N_2 \cdot S & \longleftrightarrow & N_2 + S \end{array} \right\} \qquad \qquad \text{Rapid}$$

Derive overall rate equation for the reaction using Langmuir-Hinshelwood Approach.

- A first-order catalytic reaction  $A(l) \rightarrow R(l)$  is run in a long, narrow vertical reactor with up flow of liquid through a fluidized bed of catalyst particles. Conversion is 90% at the start of operations when the catalyst particles are 5 mm in diameter. The catalyst is friable and slowly wears away, particles shrink and the fine powder produced washes out of the reactor. After a few months each of the 5-mm spheres has shrunk to 3-mm spheres. What should be the conversion at this time? Assume plug flow of liquid.
  - (i) Particles are porous and allow easy access for reactants (no resistance to pore diffusion).
  - (ii) Particles are porous and at all sizes provide a strong resistance to pore diffusion.
- b Consider a single cylindrical pore of length L, with reactant A diffusing into the pore, and reacting on the surface by a first-order reaction taking place at the walls of the pore, and product diffusing out of the pore. The catalyst used is decaying with time. Develop expression for Effectiveness factor in terms of Thiele Modulus for decaying catalyst  $(M_{T_d})$ .

CO<sub>3</sub> (4)& CO<sub>4</sub>

CO<sub>3</sub>

(4)

Discuss types of deactivation of a solid porous catalyst? Derive the performance equation for Mixed fluid/batch Solid system with deactivating catalyst. The reaction taking place in the reactor is of first order and the solid catalyst is decaying as a result of sintering.

(4)CO<sub>4</sub>

The reversible catalytic reaction,  $[A \leftrightarrow R, X_{Ae} = 0.5]$ , proceeds with decaying catalyst in a batch reactor (batch-solids, batch fluid). What can you say of the kinetics of reaction and deactivation from the following data:

(4)CO<sub>4</sub>

t, hr 0 0.25 0.5 1 2 (
$$\infty$$
)  
 $C_A$ , mol/liter 1.000 0.901 0.830 0.766 0.711 0.684

#### \*\*\*\* Good Luck \*\*\*\*

Course Outcomes (COs):

 $Q_3$ 

04

- Ability to interpret and analyze heterogeneous reaction kinetics data.
- Ability to design reactors for non-catalytic heterogeneous (fluid-particle and fluid-fluid) reactions systems.
- Ability to identify the kinetics of solid catalyzed reaction systems and to design reactors containing solid catalysts.
- Ability to identify kinetics of the catalyst deactivation, and to design reactors containing decaying solid catalysts.