Property	Unit	Model equations	Input parameters	ARD (%) ^{c)}		Referen
				Reported	This study	
Cetane number (CN)	-					
Model 1		Global FAMEs mixture correlation : o $CN = 61.1 + 0.088 \cdot w_{14:0} + 0.133 \cdot w_{16:0} + 0.152 \cdot w_{18:0} - 0.101 \cdot w_{16:1} - 0.039 \cdot w_{18:1} - 0.243 \cdot w_{18:2} - 0.395 \cdot w_{18:3}$ (1.1) $R^2 = 0.88$ Performs better at: b $w_{18:1} > 17.82$; $w_{16:0} \le 25$ and $w_{18:0} \le 16$	w _i , weight prop. of the C14:0, C16:0, C16:1, C18:0, C18:1, C18:2, and C18:3 FAMEs.	3.18 (1.98- 4.02); N=19	11.75, N=274/ 9.91, N=6	(Bamgb oye and Hansen, 2008; Tong et al., 2011)
Model 2		CNs of individual FAMEs (cetane number of the i^{th} FAME in the mixture) : $^{e^j}$ $\varphi_i = -52.974 + (13.767 - 1.202 \cdot ndb_i^2 + 0.152 \cdot ndb_i^2) \cdot nc_i - 0.351 \cdot nc_i^2$ (1.2) $R^2 = 0.946$ To obtain the global CN for FAMEs mixture, Linear mixing rule (Modified Grunberg-Nissan model) is applied as follows : $CN = \sum_i^n w_i \cdot \varphi_i$ (1.3)	ndb _i , numb. of double bonds of the <i>i</i> th FAME; nc _i , numb. of carbon atoms of the <i>i</i> th FAME; w _i , weight prop. of the <i>i</i> th FAME.	6.5 (1.5- 25.1); N=11	11.78, N=274/ 5.34, N=6	(Lapuert a et al., 2009; Tong et al., 2011)
Model 3		CNs of individual FAMEs (cetane number of the i^{th} FAME in the mixture) : $ \varphi_i = 58.1 + 2.8 \cdot (\frac{nc_i - 9}{2}) - 15.9 \cdot ndb_i $ (1.4) Linear mixing rule : cf . (1.3) Performs better at: $ 14 < w_{18:2} \le 29 \text{ and } w_{20:0} > 1 $	ndb _i , numb. of double bonds of the <i>i</i> th FAME; nc _i , numb. of carbon atoms of the <i>i</i> th FAME; w _i , weight prop. of the <i>i</i> th FAME.	5.55; N=35	11, N=274/ 11.39, N=6	(Klopfen stein, 1985; Su et al., 2011)
Model 4		CNs of individual FAMEs (cetane number of the $i^{\rm th}$ FAME in the mixture) :	nc _i , numb. of carbon atoms of the i th FAME; w _i , weight prop. of the i th FAME.	0.96 (0.02- 2.98); N=19	11.26, N=274/ 5.14, N=6	(Tong et al., 2011)

		$\varphi_{i}(\text{C n}:0) = -107.71 + 31.126 \cdot nc_{i} - 2.042 \cdot nc_{i}^{2} + 0.0499 \cdot nc_{i}^{3}$ $R^{2} = 0.9835$ $\varphi_{i}(\text{C n}:1,2,3) = 109 - 9.292 \cdot nc_{i} + 0.354 \cdot nc_{i}^{2}$ $R^{2} = 0.9058$ Linear mixing rule: $CN = 1.068 \cdot \sum_{i}^{n} \left(w_{i} \cdot \varphi_{i} \right) - 6.747 \text{ (1.6)}$ Performs better at: $w_{18:1} > 18 \text{ and } w_{18:0} \le 6$				
Model 5		CNs of individual FAMEs (cetane number of the i^{th} FAME in the mixture) : $\varphi_i = -7.8 + 0.302 \cdot M_i - 20 \cdot ndb_i$ (1.7) Linear mixing rule : $CN = \sum_i^n x_i \cdot \varphi_i \text{ , where: } x_i = \frac{\frac{W_i}{M_i}}{\sum_i^n \left(\frac{W_i}{M_i}\right)}$ (1.8) Performs better at: $x_{18:1} > 0.3$ and $x_{20:0} \le 0.03$	ndb _i , numb. of double bonds of the i th FAME; w _i , weight prop. of the i th FAME; x _i , mol. mass fraction of the i th FAME; M _i , mol. weight of the i th FAME.	3.24 (2.4- 5.85); N=5	11.43, N=274/ 5.2, N=6	(Ramíre z- Verduzc o, 2012)
Cold Filter Plugging Point (CFPP)	°C					
Model 1		Global FAMEs mixture correlation : $CFPP = 0.511 \cdot w_{16:0} - 7.823$, with 0 <w<sub>16:0<45 (2.1)</w<sub>	w _{16:0} , weight prop. of the C16:0.	0.88	3.9, N=20/ 2.99, N=6	(Sarin et al., 2009)
Model 2		Global FAMEs mixture correlation: $CFPP = 18.019 \cdot \overline{nc} - 0.804 \cdot w_{n:1,2,3} \textbf{(2.2)}$ Where $\overline{nc} = \frac{\sum_{i}^{n} x_{i} \cdot nc_{i}}{\sum_{i}^{n} x_{i}} \textbf{(2.3)}, \text{ with } x_{i} \text{ as defined in equation (1.8)}$	w _{n:1,2,3} , weight prop. of the unsaturated FAMEs; nc, weighted avg. no. of carbon atoms.	0.83	4.6, N=20/ 5.26, N=6	(Su et al., 2011)
Model 3		Global FAMEs mixture correlation : $CFPP = (3.1417 \cdot LCSF) - 16.477$ (2.4)	w _i , weight prop. of the saturated	n.d.	8.41, N=20/	(Ramos et al.,

		Where the long-chain saturated factor (LCSF) of the mixture is defined as: $LCSF = 0.1 \cdot w_{16:0} + 0.5 \cdot w_{18:0} + 1 \cdot w_{20:0} + 1.5 \cdot w_{22:0} + 2 \cdot w_{24:0}$ (2.5)	FAMEs.		5.91, N=6	2009)
Cloud point (CP)	°C					
Model 1		Global FAMEs mixture correlation : $CP = 0.526 \cdot w_{16:0} - 4.992$, with 0< $w_{16:0}$ <45 (3.1) $R^2 = 0.963$	$W_{16:0}$, weight prop. of the C16:0.	n.d.		(Sarin et al., 2009)
Model 2		Global FAMEs mixture correlation : $CP = 18.134 \cdot \overline{nc} - 0.79 \cdot w_{n:1,2,3}$ (3.2), with \overline{nc} as defined in equation (2.3)	w _{n:1,2,3} , weight prop. of the unsaturated FAMEs; nc, weighted avg. no. of carbon atoms.	n.d.		(Su et al., 2011)
Density (ρ) ,	g/cm³					
20°C						
Model 1		$\rho \text{s of individual FAMEs (density of the } i^{\text{th}} \text{ FAME in the mixture)}:$ $\rho_i = 851.4714 + \frac{250.718 \cdot ndb_i + 280.899}{1.214 + \text{nc}_i} \text{ (4.1)}$ $R^2 = 0.969$ Linear mixing rule: $\rho = \sum_i^n w_i \cdot \rho_i \text{ (4.2)}$	ndb _i , numb. of double bonds of the i th FAME; nc _i , numb. of carbon atoms of the i th FAME; w _i , weight prop. of the i th FAME.	0.66 (0.02- 5.31); N=32	1.16, N=79/ 0.65, N=6	(García et al., 2013; Lapuert a et al., 2009)
Model 2		$ ho$ s of individual FAMEs (density of the i^{th} FAME in the mixture) : $ \rho_i = 0.8463 + \frac{4.9}{M_i} + 0.0118 \cdot ndb_i $ (4.3) Linear mixing rule : $ \rho = \sum_i^n x_i \cdot \rho_i $ (4.4)	ndb _i , numb. of double bonds of the i th FAME; x _i , mol. mass fraction of the i th FAME; M _i , mol. weight of the i th FAME;	0.47 (0.24- 0.67); N=5	1.4, N=79/ 1, N=6	(Ramíre z- Verduzc o, 2012)
Flash point (FP)	°C					
Model 1		Global FAMEs mixture correlation : $FP = 23.362 \cdot \overline{nc} + 4.854 \cdot \overline{ndb}$ (5.1)	nc, weighted avg. no. of carbon atoms; ndb, weighted avg. no. of double bonds;	1.81	14.47, N=45/ 22.49, N=6	(Su et al., 2011)

		Where $\overline{ndb} = \frac{\sum_{i}^{n} x_{i} \cdot ndb_{i}}{\sum_{i}^{n} x_{i}}$ (5.2), and \overline{nc} as defined in equation (2.3) Performs better at: $\overline{nc} > 17.6$ and $FP \le 170$ °C	x _i , mol. mass fraction of the i th FAME;			
Model 2		FPs of individual FAMEs (flash point of the i^{th} FAME in the mixture) : $\theta_i = (0.3544 \cdot T_{b_i}^{1.14711} \cdot nc_i^{-0.07677}) - 273.15$ (5.2) Linear mixing rule : $FP = \sum_i^n w_i \cdot \theta_i$ (5.3)	nc_i , numb. of carbon atoms of the i^{th} FAME; T_{bi} , normal ebullition point of the i^{th} FAME. w_i , weight prop. of the i^{th} FAME.		18, N=49/ 12.4, N=6	(Catoire, 2006)
Higher heating value (HHV)	MJ/kg					
Model 1		HHVs of individual FAMEs (higher heating value of the i^{th} FAME in the mixture) : $\delta_i = 46.19 - \frac{1794}{M_i} - 0.21 nc_i \text{(6.1)}$ Linear mixing rule : $HHV = \sum_i^n x_i \delta_i \text{(6.2)}$	x _i , mol. mass fraction of the i th FAME; M _i , mol. weight of the i th FAME.	1.92	0.87, N=38/ 0.49, N=6	(Ramíre z- Verduzc o, 2012)
lodine value (IV)	g I ₂ /100 g					
Model 1		Global FAMEs mixture correlation (slightly tuned in this study) : $IV = 89.79 - 1.11 \cdot w_{10:0} - 0.85 \cdot w_{12:0} - 0.97 \cdot w_{14:0} - 0.43 \cdot w_{16:0} \\ -0.59 \cdot w_{16:1} - 0.81 \cdot w_{18:0} - 0.11 \cdot w_{18:1} \\ +0.77 \cdot w_{18:2} + 1.49 \cdot w_{18:3} - 0.8 \cdot w_{20:0} \\ R^2 = 0.898$ Performs better at: $w_{14:0} \le 17; \ w_{12:0} \le 44; \ w_{18:0} \le 18; \ w_{16:0} \le 26; \ \text{and} \ w_{18:0} > 10$	<i>w_i</i> , weight prop. of the C10-20:0, C16:1 and C18:1-3 FAMEs.	1.79 (- 0.26, 3.37); N=10	11.08, N=158/ 3.75, N=5*	(Gopina th et al., 2009)
Model 2		Global FAMEs mixture correlation : $IV = \sum_{i}^{n} 100 \left(\frac{253.81 \cdot w_{i} \cdot ndb_{i}}{M_{i}} \right) $ (7.2)	ndb _i , numb. of double bonds of the i th FAME; w _i , weight prop. of the i th FAME;	n.d.	8.29, N=158/ 2.96, N=5*	(Knothe, 2002)

			x _i , mol. mass fraction of the i th FAME; M _i , mol. weight of the i th FAME.		
Model 3		Global FAMEs mixture correlation (slightly tuned in this study) : $IV = w_{n:1} + 1.5 \cdot w_{n:2} + 2.51 \cdot w_{n:3}$ (7.3)	w _{n:1} , weight prop. of the 12.24); monounsaturated FAMEs; w _{n:2} , w _{n:3} , weight prop. of the ployunsaturated FAMEs.	5, 10, N=158/ 7.44, N=5*	(Kyriakid is and Katsiloul is, 2000)
Induction period (IP)	h				
Model 1		$IP = 6.1924 + 0.85242 \cdot w_{8:0} - 1.31462 \cdot w_{10:0} + 0.24307 \cdot w_{12:0} + 0.23174 \cdot w_{14:0} + 0.15171 \cdot w_{16:0} - 0.13884 \cdot w_{18:0} + 0.01139 \cdot w_{18:1} - 0.07447 \cdot w_{18:2} - 0.06931 \cdot w_{18:3} - 0.67224 \cdot w_{20:0} - 0.05735 \cdot w_{20:1} - 0.07329 \cdot w_{22:1}$	w _i , weight prop. of the C8-20:0, C18:1- 3, C20:1 and C22:1 FAMEs.	22, N=55/ 13.9, N=6	(Barrada s Filho et al., 2015)
Model 2		Global FAMEs mixture correlation : $IP = \frac{117.9295}{(w_{18:2} + w_{18:3})} + 2.5905 \textbf{(8.1)}$ Conditions: $0 < (w_{18:2} + w_{18:3}) < 100$	w _i , weight prop. of the C18:2, and C18:3 FAMEs.	28, N=50/-	(Park et al., 2008)
Model 3		Global FAMEs mixture correlation: $OS = 0.27 \cdot w_{n:0} + 0.31 \cdot w_{n:1} - 0.09 \cdot w_{n:2,3}$ (8.2) $R^2 = 0.88$ Conditions: $7.2 \le w_{n:0} \le 92.9$; $5.9 \le w_{n:1} \le 83.1$; and $1.2 \le w_{n:2,3} \le 61.3$ Global FAMEs mixture correlation: $OS = 49.0 \cdot w_{n:2,3}^{-0.50}$ (8.3) $R^2 = 0.91$ Conditions: $1.2 \le w_{n:2,3} \le 61.3$	w _{n:0} , weight prop. of the saturated FAMEs; w _{n:1} , weight prop. of the monounsaturated FAMEs; w _{n:2,3} , weight prop. of the ployunsaturated FAMEs.	42.6, N=24/ 60, N=6	(Serrano et al., 2014)

Model 4		Global FAMEs mixture correlation : $OS = -0.0384 \cdot DU + 7.770 \textbf{(8.4)}$ $R^2 = 0.6421$ Where the degree of unsaturation (<i>DU</i>) is defined as: $DU = 1 \cdot w_{n:1} + 2 \cdot w_{n:2} + 3 \cdot w_{n:3} \textbf{(8.5)}$	w _{n:1} , weight prop. of the monounsaturated FAMEs; w _{n:2} , w _{n:3} , weight prop. of the ployunsaturated FAMEs.	n.d.	20.5, N=50/-	(Wang et al., 2012)
Pour point (PP)	°C					
Model 1		Global FAMEs mixture correlation : $PP = 0.571 \cdot w_{16:0} - 12.24$ (9.1), with 0 < $w_{16:0}$ < 45 $R^2 = 0.863$	w _{16:0} , weight prop. of the C16:0.			(Sarin et al., 2009)
Model 2		Global FAMEs mixture correlation : $PP = 18.880 \cdot \overline{nc} - w_{n:1,2,3}$ (9.2)	nc, weighted avg. no. of carbon atoms; w _{n:1,2,3} , weight prop. of the unsaturated FAMEs.			(Su et al., 2011)
Saponification value (SV)	g KOH/100g					
Model 1		Global FAMEs mixture correlation (slightly tuned in this study) : $241.85 + 0.08 \cdot w_{10.0} + 0.38 \cdot w_{12.0} + 0.02 \cdot w_{14.0} - 0.17 \cdot w_{16.0} \\ -1.67 \cdot w_{16.1} - 0.47 \cdot w_{18.0} - 0.45 \cdot w_{18.1} - 0.42 \cdot w_{18.2} \\ -0.41 \cdot w_{18.3} - 0.46 \cdot w_{20.0} $ (10.1) $R^2 = 0.715$	w _i , weight prop. of the C10-20:0, C16:1 and C18:1-3 FAMEs.	1.13 (0.19- 2.29); N=10	2.25, N=125/ 4.68, N=6	(Gopina th et al., 2009)
Model 2		Global FAMEs mixture correlation : $SV = \sum_{i}^{n} \left(\frac{561.06 \cdot w_{i}}{M_{i}} \right) $ (10.2)	w _i , weight prop. of the i th FAME; M _i , mol. weight of the i th FAME.	n.d.	5.2, N=125/ 0.52, N=5	(Knothe, 2002)
Kinematic viscosity (η), 40°C	mm²/s					
Model 1		η s of individual FAMEs (kinematic viscosity of of the i^{th} FAME in the mixture) : $\operatorname{Ln}(\eta_i)_{Cn:0} = a \cdot nc_i^b + \frac{c \cdot nc_i^d}{e \cdot \operatorname{Ln}(nc_i) + f + T} \textbf{(11.1)}$	ndb _i , numb. of double bonds of the <i>i</i> th FAME;	1.33; N=247	5.33, N=183/ 6.73, N=5	(Chavarr ia- Hernand

	Individual monounsaturated FAMEs : $\operatorname{Ln}(\eta_i)_{Cn:1} = g \cdot n c_i^h + \frac{i \cdot n c_i^j}{k+T} \textbf{(11.2)}$ Individual polyunsaturated FAMEs : $\operatorname{Ln}(\eta_i)_{Cn:2,3} = g \cdot (n c_i - n d b_i^l)^h + \frac{i \cdot (n c_i - n d b_i^l)^j}{k+T} \textbf{(11.3)}$ with $T = 313.15 \text{ K}$ Linear mixing rule : $\operatorname{Ln}(\eta) = \sum_i^n x_i \cdot \operatorname{Ln}(\eta_i) \textbf{(11.4)}$	nc _i , numb. of carbon atoms of the <i>i</i> th FAME; w _i , weight prop. of the <i>i</i> th FAME; Values of parameters a - l given by the reference; x _i , mol. mass fraction of the <i>i</i> th FAME.			ez and Pacheco - Catalán, 2014)
Model 2	η s of individual FAMEs (kinematic viscosity of of the i^{th} FAME in the mixture) : $\operatorname{Ln}(\eta_i) = -12.503 + 2.496 \cdot \operatorname{Ln}(M_i) - 0.178 \cdot ndb_i$ (11.5) Linear mixing rule : cf. (11.4)	ndb _i , numb. of double bonds of the <i>i</i> th FAME; <i>M</i> _i , mol. weight of the <i>i</i> th FAME.	1.68	5.37, N=183/ 6.81, N=6	(Ramíre z Verduzc o, 2013)
Model 3	Global FAMEs mixture correlation : $\eta = A \cdot \overline{nc} + B \cdot \overline{ndb} + C \qquad (11.6)$ Performs better at: $\eta \le 4.77 \text{ mm}^2/\text{s}$	nc, weighted avg. no. of carbon atoms; ndb, weighted avg. no. of double bonds;	5.45	11.37, N=176/ 10.82, N=6	(Su et al., 2011)

^{*} Coconut oil value out of range

 φ_i , cetane number of the i^{th} FAME; M_i , molecular weight of the i^{th} FAME; ndb_i , number of double bonds of the i^{th} FAME; nc_i , number of carbon atoms of the i^{th} FAME; w_i , weight proportion of the i^{th} FAME; $w_{i6:0}$, weight proportion of C14:0 methyl-ester; $w_{i6:0}$, weight proportion of C16:0 methyl-ester; $w_{i6:0}$, weight proportion of C18:1 methyl-ester; $w_{i6:0}$, weight proportion of C18:2 methyl-ester; $w_{i8:2}$, weight proportion of C18:3 methyl-ester; $m_{i8:2}$, weight proportion of C18:3 methyl-ester; $m_{i8:3}$, weight proportion of C18:3 methyl-ester;

 ρ_{i} , density of the i^{th} FAME;

Barradas Filho, A.O., Barros, A.K.D., Labidi, S., Viegas, I.M.A., Marques, D.B., Romariz, A.R.S., De Sousa, R.M., Marques, A.L.B., Marques, E.P., 2015. Application of artificial neural networks to predict viscosity, iodine value and induction period of biodiesel focused on the study of oxidative stability. *Fuel* 145, 127–135.

Catoire, L., 2006. Estimation of Closed Cup Flash Points of Combustible Solvent Blends. J. Phys. Chem. Ref. Data 35, 9.

Chavarria-Hernandez, J.C., Pacheco-Catalán, D.E., 2014. Predicting the kinematic viscosity of FAMEs and biodiesel: Empirical models. Fuel 124, 212-220.

García, M., Alba, J.-J., Gonzalo, A., Sánchez, J.L., Arauzo, J., 2013. Density of alkyl esters and its mixtures: A comparison and improvement of predictive models. Fuel 103, 232-238.

Gopinath, a., Puhan, S., Nagarajan, G., 2009. Theoretical modeling of iodine value and saponification value of biodiesel fuels from their fatty acid composition. Renew. Energy 34, 1806-1811.

Klopfenstein, W.E., 1985. Effect of molecular weights of fatty acid esters on cetane numbers as diesel fuels. J. Am. Oil Chem. Soc. 62, 1029-1031.

Knothe, G., 2002. Structure indices in FA chemistry. How relevant is the iodine value? J. Am. Oil Chem. Soc. 79, 847-854.

Kyriakidis, N.B., Katsiloulis, T., 2000. Calculation of iodine value from measurements of fatty acid methyl esters of some oils: Comparison with the relevant American Oil Chemists Society method. J. Am. Oil Chem. Soc. 77, 1235–1238.

Lapuerta, M., Rodríguez-Fernández, J., Mora, E. de, 2009. Correlation for the estimation of the cetane number of biodiesel fuels and implications on the iodine number. Energy Policy 37, 4337-4344.

Park, J.-Y., Kim, D.-K., Lee, J.-P., Park, S.-C., Kim, Y.-J., Lee, J.-S., 2008. Blending effects of biodiesels on oxidation stability and low temperature flow properties. Bioresour. Technol. 99, 1196–203.

Ramírez Verduzco, L.F., 2013. Density and viscosity of biodiesel as a function of temperature: Empirical models. Renew. Sustain. Energy Rev. 19, 652-665.

Ramírez-Verduzco, L., 2012. Predicting cetane number, kinematic viscosity, density and higher heating value of biodiesel from its fatty acid methyl ester composition. Fuel 91, 102-111.

Ramos, M., Fernández, C., Casas, A., Ramos, M. J., Fernández, C. M., Casas, A., Rodríguez, L., Pérez, Á., 2009. Influence of fatty acid composition of raw materials on biodiesel properties. Bioresour. Technol. 100, 261–268.

Sarin, A., Arora, R., Singh, N.P., Sarin, R., Malhotra, R.K., Kundu, K., 2009. Effect of blends of Palm-Jatropha-Pongamia biodiesels on cloud point and pour point. Energy 34, 2016-2021.

Serrano, M., Oliveros, R., Sánchez, M., Andrea, M., Mercedes, M., Aracil, J., 2014. Influence of blending vegetable oil methyl esters on biodiesel fuel properties: Oxidative stability and cold flow properties properties: Oxidative stability and cold flow properties. Energy 65, 109-115.

Su, Y.-C., Liu, Y.A., Diaz Tovar, C.A., Gani, R., 2011. Selection of Prediction Methods for Thermophysical Properties for Process Modeling and Product Design of Biodiesel Manufacturing. Ind. Eng. Chem. Res. 50, 6809-6836.

Tong, D., Hu, C., Jiang, K., Li, Y., 2011. Cetane number prediction of biodiesel from the composition of the fatty acid methyl esters. J. Am. Oil Chem. Soc. 88, 415-423.

Wang, L., Yu, H., He, X., Liu, R., 2012. Influence of fatty acid composition of woody biodiesel plants on the fuel properties. J. Fuel Chem. Technol. 40, 397-404.