## Radiation 6: Self-viewing radiation

radiation-6-self. pdf

In cases where the constructed domain is not convex, some raidiation will not continue to infinity, but instead stite another partien of the domain boundary.

consider a differential area dA at T, with normal Ti, which receives radiation from dA at F\*, with normal Ti\*. The dispacement from T\*

day on

$$\vec{d} = \vec{r} - \vec{r}^*. \qquad (r6.1)$$

Let the nameds make angle of and of with the correcting line of the displacement. It is well known that the view factor from SA\* to JA, which is, the proportion of radiation which leaves SA\* and strikes JA, is given by

Thus, to account for self-viewing vadiation, the boundary condition (cos) must be modified to

$$\vec{R} \cdot \vec{\nabla} \vec{T} = -cT^{+} + \int \frac{cT^{*+} \cos \theta}{T d^{*2}} dA^{+}$$
(6.3)

Mere the integral is taken over all elements dAt which can see the element dA at the local position it under consideration. The ratio R between the new integral term and the existing term in (76-3) is given by

$$R = \frac{1}{T^4} \int \frac{T^{*4} \cos \theta^* \cos \theta}{T d^{*2}} dA^*$$

$$(6.4)$$

NOW observe that

$$\cos \theta^* = \frac{\vec{n}^* \cdot \vec{J}^*}{d^*}$$

$$\cos \theta = \frac{\vec{n} \cdot (-\vec{d}^{+})}{\vec{d}^{+}}$$

$$COSG^*COSG = \frac{(\overrightarrow{n}^* \cdot \overrightarrow{d}^*)(-\overrightarrow{n} \cdot \overrightarrow{d}^*)}{d^{*2}}$$

$$R = \frac{1}{74} \int \frac{T^{*4}(\vec{n}^* \cdot \vec{d}^*)(-\vec{n} \cdot \vec{d}^*)}{T d^{*4}} dA^*$$

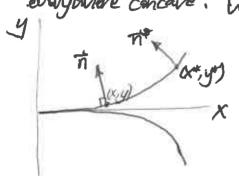
(r6.8)

specific

We now consider some coses:

## 1. Plane source spite

Consider the spite y = y(x) from radiation-1-planespot, which is everywhere concave. We have the following a where primes dende x-differentiation:



$$\vec{n} = \frac{-\sqrt{a_x + a_y}}{\sqrt{1 + y'^2}} \qquad (r6.9)$$

There Are,

$$-\pi \cdot \vec{d}^* = \frac{+(x-x^*)y'-(y-y^*)}{\sqrt{|+y'|^2}} \cdot (r6.1)$$



Also 
$$dA^{*} = dS^{*}dZ^{*} = \sqrt{1+y'^{*2}} dX^{*}dZ^{*}$$
 (r.6+3)

If we are constructing a domain with traced boundaries taten from the interval from X, to Xz, we therefore have

$$R = \frac{1}{T^{4}} \int_{-\infty}^{\infty} \frac{(x-x^{4})y^{14} + (y-y^{4})[(x-x^{4})y' - (y-y^{4})] \sqrt{1+y^{4}}^{2}}{(x-x^{4})^{2} + (y-y^{4})^{2} + (y-y^{4})^{2}} \sqrt{1+y^{4}}^{2} \sqrt{1+y^{4}}^{2}} \sqrt{1+y^{4}}^{2} \sqrt{1+y^{4}}^{2}}$$

$$R = \frac{1}{7^{4}} \int_{K_{1}}^{K_{2}} \frac{7^{4+} \left[ -(x+^{4})y'^{4} + (y-y^{4}) \right] (x-x'^{4})y' - (y-y^{4})}{2[(x-x^{4})^{2} + (y-y^{4})^{2}]^{3/2} \sqrt{(x+y')^{2}}}$$
(6.15)

whose we have used

$$\int_{-\infty}^{\infty} \frac{ds}{\pi (\rho^2 + \zeta^2)^2} = \frac{1}{2 [\rho^2]^{\frac{3}{2}}}.$$
 (66.6)

A crude upper bound for (F6-15) can be estimated by Taylor remainders.

Observe that

$$y = y^* + (x - x^*)y'^* + \frac{(x - x^*)^2}{2!}y_c^{K*}$$
 (r6.17)

$$y^{+} = y + (x^{+} - x)y' + (x^{+} - x)^{2}y''$$
(F618)

where  $y_c'' = y''|_{x=x_c''}$  is  $y_c'' = y''|_{x=x_c}$ , for some  $x_c$  and  $x_c$  between  $x^*$  and x. Therefore

$$-(x-x^*)y'' + (y-y^*) = \frac{(x-x^*)^2}{2!}y''' + (y-y^*) = \frac{(x-x^*)^2}{2!}y'' + (y-y^*)^2 +$$

so we have

$$R = \frac{1}{74} \int_{X_{1}}^{K_{2}} \frac{7^{44} (x - x^{4})^{2} y_{1}^{14} (x - x^{4})^{2} y_{2}^{14} dx^{4}}{2 \cdot 2! 2! \left[ (x - x^{4})^{2} + (y - y^{4})^{2} \right]^{3/2} \left[ i + y^{1/2} \right]}$$

$$= \frac{1}{87^{4} \left[ i + y^{1/2} \right]_{X_{1}}^{K_{2}} \frac{7^{44} (x - x^{4})^{4} y_{1}^{14} y_{2}^{14} y_{2}^{14} dx^{4}}{\left[ (x - x^{4})^{2} + (y - y^{4})^{2} \right]^{3/2}}$$

$$(F6.21)$$

Grudely, we have the upper bound

$$R \leq \frac{y_{\text{max}}^{11}}{87^{4}/1+y^{12}} \int_{K_{1}}^{K_{2}} \frac{T^{44}(x-x^{4})^{4}}{[(x-x^{4})^{2}+(y-y^{2})^{2}]^{2}}$$

$$(26.22)$$

where  $y'''_{max} = \max_{x_i \in x_i \in x_i} y''$ . The bound (x6-22) has a derivative-free integrand, but still requires testing an integral, for an ultra-onde bound which requires not taking an integral, note that

$$y-y^{*} = (x-x^{*}) y 6^{*}$$

$$(y-y^{*})^{2} \ge (x-x^{*})^{2} y_{min}^{*}$$

$$(x-x^{*})^{2} + (y-y^{*})^{2} \ge (x-x^{*})^{2} (1+y_{min}^{*})^{2}$$

therefore

$$R \leq \frac{y_{max}^{2}}{8 T_{min} / 1 + y_{min}^{2}} | x_{1} | \frac{(x - x^{4})^{2} (x + y_{min}^{2})}{(x - x^{4})^{2} (1 + y_{min}^{2})} | x_{2} | x_{1} | x_{2} | x_{1} | x_{2} | x_{2} | x_{1} | x_{2} | x_{2} | x_{1} | x_{2} |$$

Since we only considering  $x_1 \le x \le x_2$ , and integraling over  $x_1 \le x^+ \le x_2$ , we have (x-x\*) < (x-x1). (r6.25) Thorefore

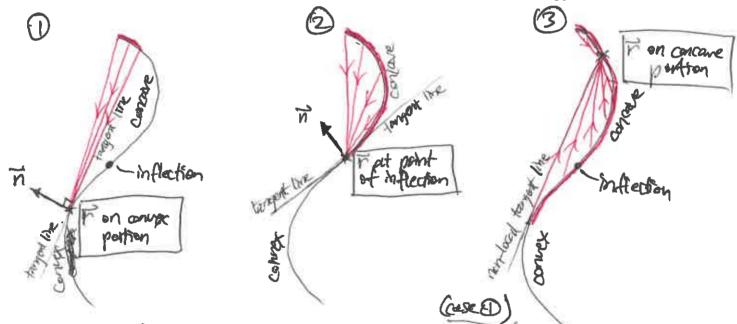
R = (K2-X1)2 (Tmaye/Tmin)4 y x 2 8 (1+4/min<sup>2</sup>)2

r6.26

2. Mn-convex lens

one superisor sails that it halld be good to aduate R for the non-convex less-like domaine for the castine simple (B=1) case, see Page 155, Sec. 3.3.2 in radiation-5-come, put

But that studion is actually quite complicated; there is self-vicing even unto the convex portrans; this is best seen with an exaggerated sketch;



We see that If it is on the anex portion of the loss, the self wanty solden for vato R & probably les than for one @ 23, but between @40 it is undear which has greater R, In paraicular for one 1 the local point is received radiation from both the entire concave portion,

but also some of the conjex portion too,

The simplest way forward is to do a bounding on y = y = ye, where ye is the end of the land t x(y) | g=ye = 11/2, -inflection (ki, yi) and (si, yi) is the larest part (in the top half of the loss) which is visible to the and Let primes denote y-differentiation. The tangett like through (xv, yw) meats the andpoint (2, ye), therefore  $X_V + (y_e - y_V)X_V' = \pi/2$ (F628) x(y) + (ye-y) x(y) = 11/2 (F6.29) determines yh. Now for x=x(y), we have instead of (6.9),  $\vec{n} = \frac{-\vec{q}_x + \chi' \vec{q}_y}{\sqrt{\chi'' + 1}}$ (F&30) so we with {y' -1, 1 - x} unto (615), and get  $R = \frac{1}{7^4} \left[ \frac{(3^2 - x^4) + (y - y^4) + (y - y^4)^2 - (y - y^4) x'^4 }{2 \left[ (x - x^4)^2 + (y - y^4)^2 \right]^{2/2} \sqrt{x'^2 + 1}} \right] dy^4$ and so R = 1 (y=y+)2 | x(= (Q-y+)2 | X(= dy+
8 (y-y+)2)3/2 (Q+y)3/2 | x(2+1)3/2 | x(2+1) 1x/2 <- (Truck) + 1x11 |2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1/2 | 1 R = (4-4)2 (Trus/Frank 1/2 (max)2 (r6.32) very ondely.

r6-5