Nonfragile Output Feedback Tracking Control for Markov Jump Fuzzy Systems Based on Integral Reinforcement Learning Scheme

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Abstract—In this article, a novel integral reinforcement learning (RL)-based nonfragile output feedback tracking control algorithm is proposed for uncertain Markov jump nonlinear systems presented by the Takagi-Sugeno fuzzy model. The problem of nonfragile control is converted into solving the zero-sum games, where the control input and uncertain disturbance input can be regarded as two rival players. Based on the RL architecture, an offline parallel output feedback tracking learning algorithm is first designed to solve fuzzy stochastic coupled algebraic Riccati equations for Markov jump fuzzy systems. Furthermore, to overcome the requirement of a precise system information and transition probability, an online parallel integral RL-based algorithm is designed. Besides, the tracking object is achieved and the stochastically asymptotic stability, and expected \mathcal{H}_{∞} performance for considered systems is ensured via the Lyapunov stability theory and stochastic analysis method. Furthermore, the effectiveness of the proposed control algorithm is verified by a robot arm system.

Index Terms—Fuzzy tracking control, integral reinforcement learning (RL), Markov jump fuzzy systems (MJFSs), nonfragile control.

I. INTRODUCTION

ARKOV jump systems (MJSs) are a kind of random jumping system composed of many interconnected subsystems, in which the Markov process characterizes the jumping among the subsystems. In the last few decades, since MJSs could be capable of modeling many practical physical systems, where their structures or parameters

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change randomly, such systems have attracted lots of attention [1], [2], [3], [4], [5], [6], [7], [8]. On the other front, it should be mentioned that nonlinearities exist in many physical systems. The Takagi-Sugeno (T-S) fuzzy model is an effective method to approximate these nonlinearities [9], [10], [11]. Combining MJSs and T-S fuzzy model, a broader type of system, namely, Markov jump fuzzy systems (MJFSs), have received significantly increasing attention and numerous important results have emerged [12], [13], [14], [15], [16]. To be specific, by virtue of the linear matrix inequality technique, Wu et al. [17] investigated the problem of nonfragile guaranteed cost controller design for MJFSs with time-varying delays. The problems of \mathcal{H}_{∞} control and filtering for Markov jump nonlinear singularly perturbed systems were studied in [18]. In [19], the finite-time asynchronous filtering issue for MJFSs with incomplete transition rate was addressed.

Besides, in the era of the fourth industrial revolution, artificial intelligent methods have attracted lots of attention and gradually becomes one key focus in the control field [20], [21], [22], [23], [24]. Through interaction with the environment, reinforcement learning (RL) methods can remove the curse of dimensionality effectively in the traditional dynamic programming method [25], [26], [27]. On the other hand, the RL method has been successfully employed to solve the optimal control policy issue [28], in which optimal solution can be converted into algebraic Riccati equation or Hamilton-Jacobi-Bellman equation. Furthermore, the optimal tracking control has become an important problem in robot engineering and aircraft transportation field [29], [30], [31], where adaptive dynamic programming and the RL method were widely introduced to approximate the optimal policy. Mohammadi et al. [32] investigated the optimal tracking controller design problem for nonlinear continuous-time systems, where the integral RL (IRL) method was introduced to determine the control input. Optimal tracking control of switched systems was studied in [33]. By virtue of the IRL technology, Zhang et al. [34] developed a parallel tracking control algorithm for fuzzy interconnected systems. Furthermore, the above-mentioned works are both based on the state feedback control. However, it is not easy to measure the full states of the systems in some practical situations. The static output feedback control strategy allows flexibility and simplicity of implementation, which is extremely important in

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current controller design applications. Hence, it is of great significance to study output feedback tracking control design in the framework of RL.

What is more, inaccuracies or uncertainties may exist in many practical applications because of the effect of the highly complex working environment of control systems [35], [36], [37], [38], [39], [40]. A smaller controller gain fluctuations may cause the control system to be unstable or fail to guarantee the expected performance [41], [42], [43]. Therefore, it is necessary to investigate the nonfragile control problem. In [44], a resilient controller was designed by solving zero-sum games, where cyber defenders and denial-of-service attackers were two rival players. Nevertheless, the research on these points is quietly few, let alone with the RL algorithm, which motivates our current investigation.

In summary, by employing the IRL technology and the strategy of output feedback, we devote ourselves to designing a nonfragile tracking controller for MJFSs based on the T-S fuzzy model. The main contributions are listed as follows.

- 1) For the first attempt, an offline parallel fuzzy nonfragile output feedback tracking learning control algorithm and an online IRL-based fuzzy nonfragile output feedback tracking control algorithm are designed for MJFSs presented by the T–S fuzzy model. Moreover, the system information can be partially unknown in the proposed online algorithm.
- 2) A nonfragile fuzzy output feedback tracking controller is developed by solving a class of zero-sum games, where the control policy and disturbance policy that have different impacts on the system performance are regarded as two rival players, which provides new insights to design the nonfragile tracking learning controller.
- 3) By designing two kinds of learning algorithms, a set of fuzzy stochastic coupled algebraic Riccati equations (FSCAREs) is solved. Moreover, the stochastic stability of the presented online IRL-based algorithm is verified by the Lyapunov stability theory. Furthermore, the applicability to the real engineering systems of the proposed method is proven by a robot arm system model.

The remainder of this article is organized as follows. Based on the T-S fuzzy model, the system and controller model are elaborated in Section II. In Section III, an offline learning algorithm and an IRL tracking algorithm are presented for MJFSs. A robot arm example is provided in Section IV to demonstrate the effectiveness of the proposed method. In Section V, we conclude this article. Moreover, the structure of the nonfragile output-feedback tracking learning control scheme is presented in Fig. 1.

Notations: The notations used in this article are standard. $\mathbb{E}\{\cdot\}$ denotes mathematical expectation. \mathcal{M}^T means the transpose of the matrix \mathcal{M} ; $\mathcal{M} > 0$ represents that matrix \mathcal{M} is positive definite. \mathbf{R} , \mathbf{R}^n , and $\mathbf{R}^{n \times m}$ denote the set of real numbers, the *n*-dimensional Euclidean space, and the set of all real matrices, respectively. Symbol $exp(\cdot)$ represents a function as $\exp([\varsigma_1,\ldots,\varsigma_d]) = [\exp(\varsigma_1),\ldots,\exp(\varsigma_d)].$

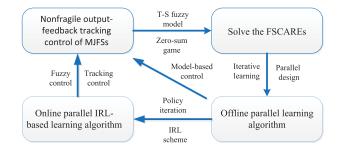


Fig. 1. Structure of the nonfragile output-feedback tracking learning control

II. PRELIMINARIES

A. System Description

Consider a class of continuous-time MJFSs uncertainties.

Plant Rule α : **IF** $\theta_1(\ell)$ is $R_{\alpha 1}$, $\theta_2(\ell)$ is $R_{\alpha 2}, \ldots, \theta_g(\ell)$ is $R_{\alpha g}$ THEN

$$\dot{x}(\ell) = (A_{\alpha\eta(\ell)} + \Delta A_{\alpha\eta(\ell)}(\ell))x(\ell)
+ (B_{\alpha\eta(\ell)} + \Delta B_{\alpha\eta(\ell)}(\ell))\mu(\ell)
y(\ell) = C_{\alpha\eta(\ell)}x(\ell)$$
(1)

where $\alpha \in \mathbb{M}\{1, 2, ..., m\}$, and m is the number of **IF-THEN** rules of system. $R_{\alpha a}$ with a = 1, ..., g is the fuzzy set. $\theta(\ell) = [\theta_1(\ell), \dots, \theta_g(\ell)]^T$ is the premise variable. $x(\ell) \in \mathbf{R}^{n_x}$, $u(\ell) \in \mathbf{R}^{n_u}$, and $y(\ell) \in \mathbf{R}^{n_y}$ represent system state, control input, and system output, respectively. $A_{\alpha\eta(\ell)}$, $B_{\alpha\eta(\ell)}$, and $C_{\alpha\eta(\ell)}$ are system matrices. $\Delta A_{\alpha\eta(\ell)}$ and $\Delta B_{\alpha\eta(\ell)}$ denote time-varying uncertainties. $\{\eta(\ell)\}\$ is a continuous-time Markov process, which takes values in a set $\mathbb{S} = \{1, 2, \dots, S\}$ with the transition probability rate matrix $\Pi \triangleq [\pi_{ij}]_{S \times S}$ is given by

$$\Pr\{\eta(\ell+\Delta) = j | \eta(\ell) = i\} = \begin{cases} \pi_{ij}\Delta + o(\Delta), & i \neq j \\ 1 - \pi_{ii}\Delta + o(\Delta), & i = j \end{cases}$$

where $\Delta > 0$, $\lim_{\Delta \to 0} o(\Delta) \Delta^{-1} = 0$, for $i \neq j$, $\pi_{ij} \geq 0$ is the transition rate from mode i at time t to mode j at time $t + \Delta$ and $\pi_{ii} = -\sum_{j=1, j \neq i}^{S} \pi_{ij}$. Fuzzy weighting functions are defined as

$$f_{\alpha}(\theta(\ell)) \triangleq \frac{\prod_{z=1}^{g} R_{\alpha z}(\theta_{z}(\ell))}{\sum_{\alpha=1}^{m} \prod_{z=1}^{g} R_{\alpha z}(\theta_{z}(\ell))}$$

where $R_{\alpha z}(\theta_z(\ell))$ is the membership degree of $\theta_z(\ell)$ in the fuzzy rule α . It follows that:

$$f_{\alpha}(\theta(\ell)) \ge 0, \sum_{\alpha=1}^{m} f_{\alpha}(\theta(\ell)) = 1.$$

To simplify the notation, for $\forall \alpha \in \mathbb{M}, \ \eta(\ell) = i \in \mathbb{S}$, we denote $A_{\alpha i} \stackrel{\triangle}{=} A_{\alpha \eta(\ell)}$, $B_{\alpha i} \stackrel{\triangle}{=} B_{\alpha \eta(\ell)}$ and $C_{\alpha i} \stackrel{\triangle}{=} C_{\alpha \eta(\ell)}$. Based on (1), the overall system dynamic can be obtained as follows:

$$\dot{x}(\ell) = \sum_{\alpha=1}^{m} f_{\alpha}(\theta(\ell))[(A_{\alpha i} + \Delta A_{\alpha i}(\ell))x(\ell) + (B_{\alpha i} + \Delta B_{\alpha i}(\ell))\mu(\ell)]$$

$$y(\ell) = \sum_{\alpha=1}^{m} f_{\alpha}(\theta(\ell))C_{\alpha i}x(\ell)$$
(2)

where $\Delta A_{\alpha i}(\ell)$ and $\Delta B_{\alpha i}(\ell)$ are considered as the following form:

$$[\Delta A_{\alpha i}(\ell) \quad \Delta B_{\alpha i}(\ell)] = H_{\alpha i} T(\ell) [D_{1\alpha i} \quad D_{2\alpha i}]$$

where $H_{\alpha i}$, $D_{1\alpha i}$, and $D_{2\alpha i}$ are constant matrices. The unknown time-varying matrix $T(\ell)$ satisfies $T^{\mathrm{T}}(\ell)T(\ell) \leq I$.

Define the desired reference trajectory as the following form:

$$\dot{x}_r(\ell) = Fx_r(\ell), \ y_r(\ell) = Gx_r(\ell) \tag{3}$$

where $x_r \in \mathbf{R}^{n_{x_r}}$ and $y_r \in \mathbf{R}^{n_{y_r}}$ are system state and system output of reference trajectory system, respectively. F and G are constant matrices.

Let $X(\ell) \triangleq [x^{\mathrm{T}}(\ell) \ x_r^{\mathrm{T}}(\ell)]^{\mathrm{T}} \in \mathbf{R}^n$, $n = n_x + n_{x_r}$, and $Y(\ell) \triangleq [y^{\mathrm{T}}(\ell) \ y_r^{\mathrm{T}}(\ell)]^{\mathrm{T}} \in \mathbf{R}^{n_y + n_{y_r}}$. From (2) and (3), we can deduce

$$\dot{X}(\ell) = \sum_{\alpha=1}^{m} f_{\alpha}(\theta(\ell)) \left\{ \left(\mathbb{A}_{\alpha i} + \mathcal{I} \Delta A_{\alpha i}(\ell) \mathcal{I}^{T} \right) X(\ell) + \left(\mathbb{B}_{\alpha i} + \mathcal{I} \Delta B_{\alpha i}(\ell) \right) \mu(\ell) \right\}
Y(\ell) = \sum_{\alpha=1}^{m} f_{\alpha}(\theta(\ell)) \left\{ \mathbb{C}_{\alpha i} X(\ell) \right\}$$
(4)

where

$$\mathbb{A}_{\alpha i} \triangleq \begin{bmatrix} A_{\alpha i} & 0 \\ 0 & F \end{bmatrix}, \ \mathbb{B}_{\alpha i} \triangleq \begin{bmatrix} B_{\alpha i} \\ 0 \end{bmatrix}$$
$$\mathbb{C}_{\alpha i} \triangleq \begin{bmatrix} C_{\alpha i} & 0 \\ 0 & G \end{bmatrix}, \ \mathcal{I} \triangleq \begin{bmatrix} I & 0 \end{bmatrix}^{\mathrm{T}}.$$

Then, the tracking error is defined as

$$y_e(\ell) \triangleq y(\ell) - y_r(\ell) = \mathbb{C}_{0i}X(\ell)$$

where $\mathbb{C}_{0i} \triangleq \sum_{\alpha=1}^{m} f_{\alpha}(\theta(\ell)) \mathbb{C}_{0\alpha i}$ and $\mathbb{C}_{0\alpha i} \triangleq [C_{\alpha i} - G]$. Control Rule α : IF $\theta_1(\ell)$ is $R_{\alpha 1}$, $\theta_2(\ell)$ is $R_{\alpha 2}$, ..., $\theta_g(\ell)$ is $R_{\alpha g}$, THEN

$$\mu(\ell) = (K_{\alpha i} + \Delta K_{\alpha i})Y(\ell)$$

where $K_{\alpha i}$ is controller gain and $\Delta K_{\alpha i} \triangleq \tilde{N}_{\alpha i} T(\ell) \tilde{M}_{\alpha i}$ denotes controller gain uncertainties, where $\tilde{N}_{\alpha i}$ and $\tilde{M}_{\alpha i}$ are known matrices.

Then, we can deduce the overall controller as

$$\mu(\ell) = \sum_{\alpha=1}^{m} f_{\alpha}(\theta(\ell)) (K_{\alpha i} + \Delta K_{\alpha i}) Y(\ell)$$
$$= \check{K}_{i} Y(\ell)$$

where $\check{K}_i \stackrel{\triangle}{=} \sum_{\alpha=1}^m f_{\alpha}(\theta(\ell))(K_{\alpha i} + \Delta K_{\alpha i}).$

Substituting $\mu(\ell)$ to (4), it yields the following system equation:

$$\dot{X}(\ell) = \sum_{\alpha=1}^{m} f_{\alpha}(\theta(\ell)) (\mathbb{A}_{\alpha i} X(\ell) + \mathbb{B}_{\alpha i} u(\ell) + \mathbb{E}_{\alpha i} w(\ell))$$
 (5)

where $u(\ell) \triangleq \sum_{\alpha=1}^{m} f_{\alpha}(\theta(\ell)) K_{\alpha i} Y(\ell)$, $w(\ell) \triangleq (\mathcal{I} H_{\alpha i} T(\ell) (D_{1\alpha i} \mathcal{I}^{T} + D_{2\alpha i} K_{i} \mathbb{C}_{\alpha i}) + \mathbb{B}_{\alpha i} \Delta K_{i} \mathbb{C}_{\alpha i}) X(\ell)$ denote the impact of system and controller uncertainties on the system. $\mathbb{E}_{\alpha i}$ is the identity matrix.

Remark 1: It is noticed that the system parameter uncertainties and the gain fluctuation are considered as $w(\ell)$, which may

worsen the system performance. Furthermore, when $T(\ell) = 0$, we can deduce $w(\ell) = 0$, which means that uncertainties and the gain fluctuation are not occur. Thus, inspired by [44], system parameter uncertainties and nonfragile control problems can be discussed within the framework of zero-sum games theory.

B. Control Design With Zero-Sum Games

The overall performance index is defined as

$$V(X(\ell), i) = \mathbb{E}\left\{\int_{\ell}^{\infty} e^{-\delta(\tau - \ell)} ((\mathbb{C}_{0i}X(\tau))^{\mathrm{T}} Q(\mathbb{C}_{0i}X(\tau)) + u^{\mathrm{T}}(\tau)u(\tau) - \gamma^{2}w^{\mathrm{T}}(\tau)w(\tau))\mathrm{d}\tau | X(\ell), i \right\}. (6)$$

The solvability of zero-sum games problem can be described as

$$\begin{split} V(X(\ell), i) &= \min_{u(\ell)} \max_{w(\ell)} \mathbb{E} \left\{ \int_{\ell}^{\infty} \mathcal{U}(X, u, w) \mathrm{d}\tau | X(\ell), i \right\} \\ &= \max_{w(\ell)} \min_{u(\ell)} \mathbb{E} \left\{ \int_{\ell}^{\infty} \mathcal{U}(X, u, w) \mathrm{d}\tau | X(\ell), i \right\} \end{split}$$

where $\mathcal{U}(X, u, w) \triangleq e^{-\delta(\tau - \ell)} [(\mathbb{C}_{0i}X(\tau))^{\mathrm{T}}Q(\mathbb{C}_{0i}X(\tau)) + u^{\mathrm{T}}(\tau)u(\tau) - \gamma^{2}w^{\mathrm{T}}(\tau)w(\tau)].$

By employing the parallel distributed compensation scheme, the mode-dependent feedback control policies and performance index under fuzzy rule can be developed as follows.

Control Rule α : **IF** $\theta_1(\ell)$ is $R_{\alpha 1}$, $\theta_2(\ell)$ is $R_{\alpha 2}$, ..., $\theta_g(\ell)$ is $R_{\alpha g}$, **THEN**

$$u_{\alpha}(\ell) = K_{\alpha i} Y(\ell)$$

$$w_{\alpha}(\ell) = K_{w\alpha i} X(\ell)$$

$$V_{\alpha}(X(\ell), i) = \mathbb{E}\{\int_{\ell}^{\infty} \mathcal{U}(X, u_{\alpha}, w_{\alpha}) d\tau | X(\ell), i \}.$$
 (7)

Therefore, we have overall control policies expressed as

$$u(\ell) = \sum_{\alpha=1}^{m} f_{\alpha}(\theta(\ell)) K_{\alpha i} Y(\ell) = K_{i} Y(\ell)$$

$$w(\ell) = \sum_{\alpha=1}^{m} f_{\alpha}(\theta(\ell)) K_{w\alpha i} X(\ell) = K_{wi} X(\ell).$$
(8)

Inserting the control policies (8) into (5), it yields

$$\dot{X}(\ell) = (\bar{\mathbb{A}}_i + \bar{\mathbb{B}}_i K_i \bar{\mathbb{C}}_i + \bar{\mathbb{E}}_i K_{wi}) X(\ell) \tag{9}$$

where $\bar{\mathbb{A}}_i \triangleq \sum_{\alpha=1}^m f_{\alpha}(\theta(\ell)) \mathbb{A}_{\alpha i}, \bar{\mathbb{B}}_i \triangleq \sum_{\alpha=1}^m f_{\alpha}(\theta(\ell)) \mathbb{B}_{\alpha i}, \bar{\mathbb{C}}_i \triangleq \sum_{\alpha=1}^m f_{\alpha}(\theta(\ell)) \mathbb{C}_{\alpha i}, \bar{\mathbb{E}}_i \triangleq \sum_{\alpha=1}^m f_{\alpha}(\theta(\ell)) \mathbb{E}_{\alpha i}.$

Before further presentation, the following definitions and lemmas are introduced.

Definition 1 [3]: The continuous-time MJSs (9) with $w(\ell) \equiv 0$ are stochastically stable, if there exists a control $u(\ell)$ satisfying

$$\lim_{T \to \infty} \mathbb{E} \{ \int_0^T X^T(\ell, u) X(\ell, u) d\ell | X_0, \eta_0 \} \le X_0^T \mathbb{M} X_0$$

where $M = M^T$ is a symmetric positive-definite matrix.

Definition 2 [45]: The continuous-time MJSs (9) are stochastically stable along with an \mathcal{H}_{∞} performance index, if for all X_0 , η_0 , and nonzero w, the following inequality holds:

$$\mathbb{E}\left\{\int_{t}^{\infty} e^{-\delta(\tau-\ell)} (y_{e}^{\mathsf{T}} Q y_{e} + u^{\mathsf{T}} u) d\tau\right\}$$

$$\leq \gamma^{2} \int_{t}^{\infty} e^{-\delta(\tau-\ell)} w^{\mathsf{T}} w d\tau.$$

Lemma 1 [34]: Given \mathbb{S} , $\mathbb{S}_{\alpha} > 0$ be symmetrical positivedefinite matrices, which meet $SS_{\alpha} = S_{\alpha}S$. Then, SS_{α} and $S_{\alpha}S$ are positive definite.

Lemma 2 [44]: Let $V(\ell) = x^{T}(\ell)SZSx(\ell)$ and $V_{\alpha}(\ell) =$ $x^{\mathrm{T}}(\ell)SZS_{\alpha}x(\ell)$, where $S, S_{\alpha} > 0$ are symmetrical, $SS_{\alpha} = S_{\alpha}S$ and $Z^{T} = Z$ are the symmetric matrix. One can deduce that $V(\ell) = \sigma V_{\alpha}(\ell), \, \sigma > 0$ is a constant.

Lemma 3: Considering the MJFSs (9), both the overall performance index $V(X(\ell), i)$ and the fuzzy-based performance index $V_{\alpha}(X(\ell), i)$ can be expressed as the quadratic form $V(X(\ell), i) = X^{T}(\ell)P_{i}X(\ell)$ and $V_{\alpha}(X(\ell), i) =$ $X^{\mathrm{T}}(\ell)P_{\alpha i}X(\ell)$.

Proof: For the control policies u_{α} and w_{α} , the performance index $V_{\alpha}(X(\ell), i)$ can be developed as

$$\begin{split} V_{\alpha}(X(\ell),i) &= \mathbb{E}\bigg\{\int_{\ell}^{\infty} \mathcal{U}(X,u_{\alpha},w_{\alpha})\mathrm{d}\tau | X(\ell),i\bigg\} \\ &= \mathbb{E}\bigg\{\int_{0}^{\infty} e^{-\delta\tau} \big[X^{\mathrm{T}}(\tau+\ell)\mathbb{C}_{0\alpha i}^{\mathrm{T}}Q\mathbb{C}_{0\alpha i}X(\tau+\ell) \\ &+ X^{\mathrm{T}}(\tau+\ell)\mathbb{C}_{\alpha i}^{\mathrm{T}}K_{\alpha}^{\mathrm{T}}K_{\alpha}\mathbb{C}_{\alpha i}X(\tau+\ell) \\ &- \gamma^{2}X^{\mathrm{T}}(\tau+\ell)K_{w\alpha}^{\mathrm{T}}K_{w\alpha}X(\tau+\ell)\bigg]\mathrm{d}\tau | X(\ell),i\bigg\} \end{split}$$

which implies

$$V_{\alpha}(X(\ell), i) = X^{T}(\ell) \left(\mathbb{E} \left\{ \int_{0}^{\infty} e^{-\delta \tau} \left[\exp^{T}(\Gamma_{i}\tau) (\mathbb{C}_{0\alpha i}^{T} Q \mathbb{C}_{0\alpha i} + \mathbb{C}_{\alpha i}^{T} K_{\alpha i}^{T} K_{\alpha i} \mathbb{C}_{\alpha i} - \gamma^{2} K_{w\alpha i}^{T} K_{w\alpha i} \right] \right.$$

$$\times d\tau |X(\ell), i \right\} X(\ell)$$

$$= X^{T}(\ell) P_{\alpha i} X(\ell)$$

where $\Gamma_i = \mathbb{A}_{\alpha i} + \mathbb{B}_{\alpha i} K_{\alpha i} \mathbb{C}_{\alpha i} + \mathbb{E}_{\alpha i} K_{w\alpha i}$, $P_{\alpha i} = \mathbb{E} \{ \int_0^\infty e^{-\delta \tau} [\exp^T(\Gamma_i \tau) (\mathbb{C}_{0\alpha i}^T \mathcal{Q} \mathbb{C}_{0\alpha i} + \mathbb{C}_{\alpha i}^T K_{\alpha i}^T K_{\alpha i} \mathbb{C}_{\alpha i} - \gamma^2 K_{\alpha i}^T K_{\alpha i} K_{w\alpha i})] d\tau |X(\ell), i\}$. Similarly, one can deduce that $V(X(\ell), i) = X^{\mathrm{T}}(\ell)P_iX(\ell)$. This end the proof.

III. MAIN RESULTS

In this section, the problem of nonfragile output feedback tracking control for MJFSs is converted to solving a set of zero-sum games. Two kinds of learning algorithms are presented to solve FSCAREs, respectively. Furthermore, the equivalence of solutions of offline Algorithm 1 and online Algorithm 2 is proved. Besides, the stability is proved by the Lyapunov stability theory.

A. Problem Transformation

Theorem 1: Considering the MJFSs (9) in the α th rule, the solution optimal matrix $P_{\alpha i}$ of $V_{\alpha}(X(\ell), i)$ satisfies the

Algorithm 1: Offline Parallel Output Feedback Nonfragile Tracking Control Algorithm for MJFSs

- Select a sequence $P_{\alpha}(0) = (P_{\alpha 1}(0), \dots, P_{\alpha m}(0))$ for every rule. Start with initial admissible feedback matrices $K_{\alpha i}(0)$, $K_{w\alpha i}(0)$ and $L_{\alpha i}(0)$.
- - Parallel evaluates $P_{\alpha i}(\lambda + 1)$ from

$$(\tilde{\mathbb{A}}_{\alpha i} + \mathbb{B}_{\alpha i} K_{\alpha i}(\lambda) \mathbb{C}_{\alpha i} + \mathbb{E}_{\alpha i} K_{w\alpha i}(\lambda) - 0.5\delta I)^{\mathrm{T}}$$

$$P_{\alpha i}(\lambda + 1) + P_{\alpha i}(\lambda + 1) (\tilde{\mathbb{A}}_{\alpha i} + \mathbb{B}_{\alpha i} K_{\alpha i}(\lambda)$$

$$\times \mathbb{C}_{\alpha i} + \mathbb{E}_{\alpha i} K_{w\alpha i}(\lambda) - 0.5\delta I)$$

$$= -\mathbb{C}_{0i}^{\mathrm{T}} Q \mathbb{C}_{0i} - \mathbb{C}_{\alpha i}^{\mathrm{T}} K_{\alpha i}^{\mathrm{T}}(\lambda) K_{\alpha i}(\lambda) \mathbb{C}_{\alpha i}$$

$$+ \gamma^{2} K_{w\alpha i}^{\mathrm{T}}(\lambda) K_{w\alpha i}(\lambda) - \sum_{j \neq i}^{S} \pi_{ij} P_{\alpha j}(\lambda)$$
(11)

Parallel policy is updated by

$$K_{\alpha i}(\lambda + 1) = -(\mathbb{B}_{\alpha i}^{T} P_{\alpha i}(\lambda + 1) + L_{\alpha i}(\lambda))$$

$$\times \mathbb{C}_{\alpha i}^{T} (\mathbb{C}_{\alpha i} \mathbb{C}_{\alpha i}^{T})^{-1}$$

$$K_{w\alpha i}(\lambda + 1) = (1/\gamma^{2}) \mathbb{E}_{\alpha i}^{T} P_{\alpha i}(\lambda + 1)$$

$$L_{\alpha i}(\lambda + 1) = K_{\alpha i}(\lambda + 1) \mathbb{C}_{\alpha i} - \mathbb{B}_{i}^{T} P_{\alpha i}(\lambda + 1)$$
(12)

5 until $\max_{\alpha i} ||P_{\alpha i}(\lambda + 1) - P_{\alpha i}(\lambda)|| < \epsilon, \epsilon > 0$ is a small constant;

Algorithm 2: Online Parallel IRL-Based Output Feedback Nonfragile Tracking Control Algorithm for MJFSs

- 1 Initialization
- Select a sequence $P_{\alpha}(0) = (P_{\alpha 1}(0), \dots, P_{\alpha m}(0))$ for every rule and given inital admissible feedback matrices $K_{\alpha i}(0)$ $K_{w\alpha i}(0)$ and $L_{\alpha i}(0)$. Let $\Delta \ell$ be a small enough positive constant, and $\lambda = 1$.
- 3 Procedure

```
while \max_{\alpha i} \|P_{\alpha i}(\lambda + 1) - P_{\alpha i}(\lambda)\| > \epsilon, \ \epsilon > 0 is a small constant do
                       for for all \eta(\ell) = i \in \mathbb{S} do
                                     for for all \alpha \in \mathbb{M} do
                                                  Evaluate matrix P_{\alpha i} from
                                                 \begin{split} & X^{\mathsf{T}}(\ell) P_{\alpha i}(\lambda) X(\ell) - e^{-\delta \Delta \ell} X^{\mathsf{T}}(\ell + \Delta \ell) P_{\alpha i}(\lambda) X(\ell + \Delta \ell) \\ &= \int_{\ell}^{\ell + \Delta \ell} e^{-\delta (\tau - \ell)} X^{\mathsf{T}}(\tau) (\mathbb{C}_{0\alpha i}^{\mathsf{T}} Q \mathbb{C}_{0\alpha i} + \mathbb{C}_{\alpha i}^{\mathsf{T}} K_{\alpha i} K_{\alpha i} \mathbb{C}_{\alpha i} - \gamma^2 K_{w\alpha i}^{\mathsf{T}} K_{w\alpha i} X(\tau)) \mathrm{d}\tau \end{split}
                                                  Update control policies by
 10
                                                  K_{\alpha i}(\lambda + 1) = -\left(\mathbb{B}_{\alpha i}^{\mathsf{T}} P_{\alpha i}(\lambda) + L_{\alpha i}(\lambda)\right) \mathbb{C}_{\alpha i}^{\mathsf{T}} \left(\mathbb{C}_{\alpha i} \mathbb{C}_{\alpha i}^{\mathsf{T}}\right)^{-1}
11
                                                   K_{w\alpha i}(\lambda + 1) = (1/\gamma^2) \mathbb{E}_{\alpha i}^{\mathrm{T}} P_{\alpha i}(\lambda)
 12
                                                  L_{\alpha i}(\lambda + 1) = K_{\alpha i}(\lambda + 1)\mathbb{C}_{\alpha i} - \mathbb{B}_{i}^{T}P_{\alpha i}(\lambda)
Update the feedback control policies as
 13
 14
                                                  u_{\alpha i}(\ell) = K_{\alpha i}(\lambda + 1) Y(\ell)
 15
                                                  w_{\alpha i}(\ell) = K_{w\alpha i}(\lambda + 1)X(\ell)
16
                       end
18
19
                       Set \lambda = \lambda + 1
20 end
21 Use the overall control policies with
```

22 $u(\ell) = \sum_{\alpha=1}^{m} f_{\alpha}(\theta(\ell)) K_{\alpha i} Y(\ell)$ 23 $w(\ell) = \sum_{\alpha=1}^{m} f_{\alpha}(\theta(\ell)) K_{w\alpha i} X(\ell)$ 23 $w(\ell) = \sum_{\alpha=1}^{m} f_{\alpha}(\theta(\ell)) K_{w\alpha i} X(\ell)$ 24 End Procedure

following FSCAREs:

$$\mathbb{A}_{\alpha i}^{\mathsf{T}} P_{\alpha i} + P_{\alpha i} \mathbb{A}_{\alpha i} - \delta P_{\alpha i} - P_{\alpha i} \mathbb{B}_{\alpha i} \mathbb{B}_{\alpha i}^{\mathsf{T}} P_{\alpha i}
+ \left(1/\gamma^{2} \right) P_{\alpha i} \mathbb{E}_{\alpha i} \mathbb{E}_{\alpha i}^{\mathsf{T}} P_{\alpha i} + \mathbb{C}_{0\alpha i}^{\mathsf{T}} Q \mathbb{C}_{0\alpha i}
+ L_{\alpha i}^{\mathsf{T}} L_{\alpha i} + \sum_{i=1}^{S} \pi_{ij} P_{\alpha j} = 0$$
(10)

and corresponding optimal control policies are obtained as $u_{\alpha}(\ell) = K_{\alpha i} Y(\ell)$ and $w_{\alpha}(\ell) = K_{w\alpha i} X(\ell)$, where $K_{\alpha i} = -(\mathbb{B}_{i}^{\mathrm{T}} P_{\alpha i} + L_{\alpha i}) \mathbb{C}_{\alpha i}^{\mathrm{T}} (\mathbb{C}_{\alpha i} \mathbb{C}_{\alpha i}^{\mathrm{T}})^{-1}$ and $K_{w\alpha i} = (1/\gamma^{2}) \mathbb{E}_{\alpha i}^{\mathrm{T}} P_{\alpha i}$.

Proof: See Appendix A.

Remark 2: According to [23], the output feedback optimal control design problem may not have a global optimal solution. Thus, the matrix $L_{\alpha i}$ is employed in this article to show the difference between the optimal state-feedback control gain and the proposed output-feedback control gain for MJFSs.

To solve FSCAREs (10), a novel offline parallel algorithm and an IRL-based online parallel algorithm are designed in the following part.

B. Offline Parallel Algorithm Design

In this part, an offline parallel output feedback tracking algorithm is proposed for MJFSs. By mathematical transformation, (10) can be rewritten as

$$\begin{split} & \left[\tilde{\mathbb{A}}_{\alpha i} + \mathbb{B}_{\alpha i} K_{\alpha i} \mathbb{C}_{\alpha i} + \mathbb{E}_{\alpha i} K_{w \alpha i} - 0.5 \delta I \right]^{\mathsf{T}} P_{\alpha i} \\ & + P_{\alpha i} \left[\tilde{\mathbb{A}}_{\alpha i} + \mathbb{B}_{\alpha i} K_{\alpha i} \mathbb{C}_{\alpha i} + \mathbb{E}_{\alpha i} K_{w \alpha i} - 0.5 \delta I \right] \\ & = -\mathbb{C}_{0 \alpha i}^{\mathsf{T}} Q \mathbb{C}_{0 \alpha i} - \mathbb{C}_{\alpha i}^{\mathsf{T}} K_{\alpha i}^{\mathsf{T}} K_{\alpha i} \mathbb{C}_{\alpha i} + \gamma^{2} K_{w \alpha i}^{\mathsf{T}} K_{w \alpha i} \\ & - \sum_{i=1, i \neq i}^{S} \pi_{ij} P_{\alpha j} \end{split}$$

where $\tilde{\mathbb{A}}_{\alpha i} = \mathbb{A}_{\alpha i} + ((\pi_{ii}/2)I)$, matrices $P_{\alpha i}$ and $P_{\alpha j}$ are symmetric positive definite. Using parallel Lyapunov (11) to evaluate the matrix $P_{\alpha i}$, a parallel two-step learning method is proposed in Algorithm 1.

Remark 3: Due to the existence of the term $\sum_{j=1}^{S} \pi_{ij} P_{\alpha j}$, the existing algorithm cannot be directly used to solve $P_{\alpha i}$ from FSCAREs (10). Thus, we transform $\sum_{j=1}^{S} \pi_{ij} P_{\alpha j}$ into $\sum_{j\neq i}^{S} \pi_{ij} P_{\alpha j} + \pi_{ii} P_{\alpha i}$ and rewrite $\tilde{\mathbb{A}}_{\alpha i}$ as $\mathbb{A}_{\alpha i} + ((\pi_{ii}/2)I_n)$. Based on this transformation, $P_{\alpha i}$ can be parallel evaluated from (11).

Note that the system dynamics and the exact information of stationary transition probability are required in Algorithm 1, which may be difficult to meet in practical applications.

C. Online Parallel IRL-Based Algorithm Design

To relax the requirement of exact information of stationary transition probability and system dynamic $\mathbb{A}_{\alpha i}$ of MJFSs, a novel IRL-based output feedback tracking nonfragile control algorithm is designed to solving a class of FSCAREs.

Considering MJFSs (9) and performance index (7), we have the following integral Bellman equation:

$$X^{\mathrm{T}}(\ell)P_{\alpha i}X(\ell) - e^{-\delta\Delta\ell}X^{\mathrm{T}}(\ell + \Delta\ell)P_{\alpha i}X(\ell + \Delta\ell)$$

$$= \int_{\ell}^{\ell + \Delta\ell} e^{-\delta(\tau - \ell)}X^{\mathrm{T}}(\tau)(\mathbb{C}_{0\alpha i}^{\mathrm{T}}Q\mathbb{C}_{0\alpha i} + \mathbb{C}_{\alpha i}^{\mathrm{T}}K_{\alpha i}^{\mathrm{T}}K_{\alpha i}\mathbb{C}_{\alpha i}$$

$$- \gamma^{2}K_{w\alpha i}^{\mathrm{T}}K_{w\alpha i})X(\tau)\mathrm{d}\tau. \tag{13}$$

Note that stationary transition probability and system dynamic are avoided in (13). In the following, we will prove that the solution obtained by (13) is equal to the solution of Lyapunov (11) in Algorithm 1.

Theorem 2: For every fuzzy rule α , the positive-define matrix $P_{\alpha i}$ calculated from (13) in Algorithm 2 is equal to the solution by solving the Lyapunov (11) in Algorithm 1.

Proof: See Appendix B.

Based on integral Bellman (13), we present a novel IRL-based nonfragile output feedback tracking control method for MJFSs, which is shown in Algorithm 2.

Remark 4: Compared with Algorithm 1, the proposed IRL-based algorithm exhibits the following distinct advantages.

- 1) The computational burden is reduced. The main computation is to solve (13) by using the least square method. The calculation process is shown in the following.
- 2) In Algorithm 2, the requirement of accurate dynamic information can be avoided in the process of learning.

In the following, we show the computation method to implement Algorithm 2, where the matrix $P_{\alpha i}(\lambda)$ is obtained from the following equality:

$$\begin{split} X^{\mathrm{T}}(\ell)P_{\alpha i}(\lambda)X(\ell) &- e^{-\delta\Delta\ell}X^{\mathrm{T}}(\ell+\Delta\ell)P_{\alpha i}(\lambda+1)X(\ell+\Delta\ell) \\ &= \int_{\ell}^{\ell+\Delta\ell} e^{-\delta(\tau-\ell)}X^{\mathrm{T}}(\tau)(\mathbb{C}_{0\alpha i}^{\mathrm{T}}Q\mathbb{C}_{0\alpha i} + \mathbb{C}_{\alpha i}^{\mathrm{T}}K_{\alpha i}^{\mathrm{T}}(\lambda) \\ &\times K_{\alpha i}(\lambda)\mathbb{C}_{\alpha i} - \gamma^{2}K_{w\alpha i}^{\mathrm{T}}(\lambda)K_{w\alpha i}(\lambda)X(\tau))\mathrm{d}\tau \end{split}$$

and introduce batch least squares method to obtain the solution of matrix $P_{\alpha i}^{\lambda}$. Define the following operators:

$$\begin{split} \bar{P}_{\alpha i}^{\lambda} &= \operatorname{vecs}(P_{\alpha i}(\lambda)) \in \mathbf{R}^{n(n+1)/2} \\ &\triangleq \left[P_{\alpha i}^{\lambda 11} \ 2P_{\alpha i}^{\lambda 12} \ \dots \ P_{\alpha i}^{\lambda 22} \ \dots \ 2P_{\alpha i}^{\lambda 2n} \ \dots \ P_{\alpha i}^{\lambda nn} \right]^{\mathrm{T}} \\ \bar{X}(\ell) &\triangleq \left[X_{1}^{2} \ X_{1}X_{2} \ \dots \ X_{2}^{2} \ \dots \ X_{2}X_{n} \ \dots \ X_{n}^{2} \right]^{\mathrm{T}}. \\ &\in \mathbf{R}^{n(n+1)/2} \end{split}$$

Then, one can deduce

$$X^{\mathrm{T}}(\ell)P_{\alpha i}^{\lambda}X(\ell) = (\bar{P}_{\alpha i}^{\lambda})^{\mathrm{T}}\bar{X}(\ell).$$

Furthermore, the parallel policy evaluation (13) can be rewritten as

$$(\bar{P}_{\alpha i}^{\lambda})^{\mathrm{T}} \tilde{X}(\ell) = v(X(\ell), K_{\alpha i}^{\lambda}, K_{w\alpha i}^{\lambda})$$

where $\tilde{X}(\ell) = \bar{X}(\ell) - e^{-\delta \Delta \ell} \bar{X}(\ell + \Delta \ell)$ and $v(X(\ell), K_{\alpha i}^{\lambda}, K_{w\alpha i}^{\lambda}) = \int_{\ell}^{\ell + \Delta \ell} e^{-\delta(\tau - \ell)} X^{\mathrm{T}}(\tau) (\mathbb{C}_{0\alpha i}^{\mathrm{T}} Q \mathbb{C}_{0\alpha i} + \mathbb{C}_{\alpha i}^{\mathrm{T}} K_{\alpha i}^{\mathrm{T}}(\lambda) K_{\alpha i}(\lambda) \mathbb{C}_{\alpha i} - \gamma^{2} K_{w\alpha i}^{\mathrm{T}}(\lambda) K_{w\alpha i}(\lambda) X(\tau)) d\tau.$

By using the least squares method, we need to collect $N \ge n(n+1)/2$ data and matrix $\bar{P}_{\alpha i}^{\lambda}$ can be solved by

$$\bar{P}_{\alpha i}^{\lambda} = \left(\tilde{X}^{\lambda} \left(\tilde{X}^{\lambda}\right)^{\mathrm{T}}\right)^{-1} \tilde{X}^{\lambda} \left(\Theta_{\alpha i}^{\lambda}\right)$$

where

$$\begin{split} \tilde{X}^{\lambda} &= \begin{bmatrix} \tilde{X}_{1}^{\lambda} & \tilde{X}_{2}^{\lambda} & \dots & \tilde{X}_{N}^{\lambda} \end{bmatrix}^{\mathrm{T}} \in \mathbf{R}^{\frac{n(n+1)}{2} \times N} \\ \Theta_{\alpha i}^{\lambda} &= \begin{bmatrix} v \left(X_{1}^{\lambda}(\ell), K_{\alpha i}^{\lambda}, K_{w \alpha i}^{\lambda} \right) & v \left(X_{2}^{\lambda}(\ell), K_{\alpha i}^{\lambda}, K_{w \alpha i}^{\lambda} \right) \\ & \dots & v \left(X_{N}^{\lambda}(\ell), K_{\alpha i}^{\lambda}, K_{w \alpha i}^{\lambda} \right) \end{bmatrix}^{\mathrm{T}} \in \mathbf{R}^{N}. \end{split}$$

Finally, the obtained matrix $P_{\alpha i}^{\lambda}$ can be employed to compute $K_{\alpha i}^{\lambda+1}$ and $K_{w\alpha i}^{\lambda+1}$.

Remark 5: Note that matrix $P_{\alpha i}$ has n(n+1)/2 unknown independent elements, thus, we need at least $N \ge n(n+1)/2$ sampled data to evaluate $P_{\alpha i}$ by least squares method. $\Delta \ell$ can be regarded as control policy update interval, where stationary

transition probability π_{ij} and system dynamic $\mathbb{A}_{\alpha i}$ are avoided by collecting system state and control input information. As shown in [45], the value of $\Delta \ell$ may have little influence on the convergence of Algorithm 2. It is necessary to select a big enough $\Delta \ell$ to learn the matrix $P_{\alpha i}$, which can precise reflect the jumping characteristics on system data.

D. Stability Analysis

From Algorithm 2, the overall fuzzy control policies are obtained. The following theorem will prove that overall fuzzy control policies integrated by local fuzzy control policies can make MJFSs (9) stochastically asymptotically stable with an \mathcal{H}_{∞} performance.

Theorem 3: Consider the performance index with quadratic from $V(X(\ell), i) = X^{T}(\ell)P_{i}X(\ell)$, where $P_{i} > 0$ is symmetric, then, system (9) is stochastically asymptotically stable with \mathcal{H}_{∞} performance if there exist matrices \bar{K}_{i} , \bar{K}_{wi} , and L_{i} such that

$$\bar{K}_i \bar{\mathbb{C}}_i = -(\bar{\mathbb{B}}_i^{\mathrm{T}} P_i + L_i)$$
$$\bar{K}_{wi} = (1/\gamma^2) \bar{\mathbb{E}}_i^{\mathrm{T}} P_i$$

where $P_i = P_i^{\rm T}$ is the solution of

$$\begin{split} \left(\tilde{\mathbb{A}}_{i}-0.5\delta I\right)^{\mathrm{T}}P_{i}+P_{i}\Big(\tilde{\mathbb{A}}_{i}-0.5\delta I\Big)+\sum_{j=1,j\neq i}^{S}\pi_{ij}P_{j}\\ &+\mathbb{C}_{0i}^{\mathrm{T}}Q\mathbb{C}_{0i}-P_{i}\bar{\mathbb{B}}_{i}\bar{\mathbb{B}}_{i}^{\mathrm{T}}P_{i}+\frac{1}{\gamma^{2}}P_{i}\bar{\mathbb{E}}_{i}\bar{\mathbb{E}}_{i}^{\mathrm{T}}P_{i}+L_{i}^{\mathrm{T}}L_{i}=0\\ \text{with } \bar{K}_{i}=\sum_{\alpha=1}^{m}f_{\alpha}(\theta(\ell))K_{\alpha i}=-\sum_{\alpha=1}^{m}f_{\alpha}(\theta(\ell))(\mathbb{B}_{\alpha i}^{\mathrm{T}}P_{\alpha i}+L_{\alpha i})\quad\mathbb{C}_{\alpha i}^{\mathrm{T}}\mathbb{C}_{\alpha i}\mathbb{C}_{\alpha i}^{\mathrm{T}}\Big)^{-1},\ \bar{K}_{w i}=\sum_{\alpha=1}^{m}f_{\alpha}(\theta(\ell))K_{w \alpha i}=\sum_{\alpha=1}^{m}f_{\alpha}(\theta(\ell))(1/\gamma^{2})\mathbb{E}_{\alpha i}^{\mathrm{T}}P_{\alpha i}. \end{split}$$

Proof: See Appendix C.

Remark 6: Compared with the existing related control methods, the method proposed in this article has the following features

- Compared with [46] and [47] that investigate MJSs by using the RL method, the nonlinearity, system uncertainty, and controller gain fluctuation are employed in this article simultaneously, which are not involved in [46] and [47]. The system model considered in this article is more general. Moreover, we first develop two kinds of nonfragile output feedback tracking learning algorithms for MJFSs.
- 2) Although the nonfragile control problem is solved in [7] and [12] for MJSs by utilizing the linear matrix inequality and matrix scaling techniques, it may bring some conservatism. In this article, we regard control input and the impact of system parameter uncertainties and the controller gain fluctuation as two hostile players and transform the nonfragile control into solving the zero-sum games for MJFSs.
- 3) The core characteristic distinguishing this article and [14], [17] lies in that the requirement of system dynamic $\mathbb{A}_{\alpha i}$ and stationary transition probability π_{ij} are avoided in the proposed method by using the IRL scheme. Thus, the presented control method for MJFSs is more practical.

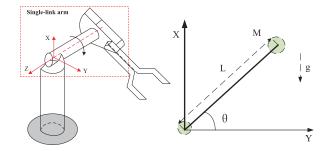


Fig. 2. Single-link robot arm.

TABLE I
PARAMETER VALUES OF SINGLE-LINK ROBOT ARM SYSTEM

Mode	Parameter M	Parameter J	Parameter L	Parameter g
1	1	1	0.5	9.81
2	2	2	0.5	9.81

IV. SIMULATION

In this section, a single-link robot arm model is adopted to verify the availability of the main results. We assume that the reference trajectory system has the following form:

$$\dot{x}_r(\ell) = Fx_r(\ell) = \begin{bmatrix} 0 & 1 \\ -1 & 0 \end{bmatrix} x_r(\ell)$$
$$y_r(\ell) = Gx_r(\ell) = \begin{bmatrix} 1 & 1 \end{bmatrix} x_r(\ell)$$

where $\dot{x}_r(\ell) = [x_{1r}^{\rm T}(\ell) \ x_{2r}^{\rm T}(\ell)]^{\rm T}$ and the initial state $\dot{x}_r(0) = [1 \ 1]^{\rm T}$.

The single-link robot arm system is presented in Fig. 2, in which the dynamic equation is given by

$$\ddot{\vartheta}(\ell) = -\frac{MgL}{\mathbb{T}}\sin(\vartheta(\ell)) - \frac{\mathbb{D}(\ell)}{\mathbb{T}}\dot{\vartheta}(\ell) + \frac{1}{\mathbb{T}}u(\ell)$$

where $u(\ell)$, $\vartheta(\ell)$, \mathbb{J} , g, L, M, and $\mathbb{D}(\ell)$ represent control input, the angle position, the total inertia, acceleration of gravity, the length of the arm, load mass, and the damping, respectively. The values of parameters $\mathbb{D}(\ell)$ are selected with its nominal value $\mathbb{D}=2$ and the other parameters are presented in Table I with two modes. The transition probability rate matrix is given as follows:

$$\Pi = \begin{bmatrix} -0.3 & 0.3\\ 0.5 & -0.5 \end{bmatrix}.$$

Let $x_1(\ell) = \vartheta(\ell)$ and $x_2(\ell) = \dot{\vartheta}(\ell)$. Under the condition $-179.4270^{\circ} < \vartheta(\ell) < 179.4270^{\circ}$, the nonlinear function $\sin(x_1(\ell))$ can be described as

$$\sin(x_1(\ell)) = f_1(x_1(\ell)) \cdot x_1(\ell) + f_2(x_1(\ell)) \cdot \xi \cdot x_1(\ell)$$

where $\xi = 10^{-2}/\pi$. Then, $f_1(x_1(\ell))$ and $f_2(x_1(\ell))$ can be obtained as

$$f_1(x_1(\ell)) = \begin{cases} \frac{\sin(x_1(\ell)) - \xi x_1(\ell)}{x_1(\ell)(1 - \xi)}, & x_1(\ell) \neq 0\\ 1, & x_1(\ell) = 0 \end{cases}$$

$$f_2(x_1(\ell)) = 1 - f_1(x_1(\ell)).$$

Then, MJFSs can be represented as the following T–S fuzzy model.

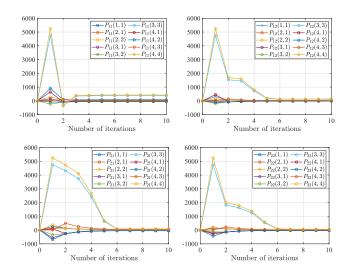


Fig. 3. Convergence of matrices P_{11} , P_{12} , P_{21} , and P_{22}

Plant Rule 1:

IF $x_1(\ell)$ is "around 0 rad" **THEN**

$$\dot{x}(\ell) = (A_{1i} + \Delta A_{1i}(\ell))x(\ell) + (B_{1i} + \Delta B_{1i}(\ell))u(\ell) y(\ell) = C_{1i}x(\ell).$$

Plant Rule 2:

IF $x_1(\ell)$ is "around π rad or $-\pi$ rad" **THEN**

$$\dot{x}(\ell) = (A_{2i} + \Delta A_{2i}(\ell))x(\ell) + (B_{2i} + \Delta B_{2i}(\ell))u(\ell)$$

$$y(\ell) = C_{2i}x(\ell)$$

where $x(\ell) = [x_1^T(\ell) \ x_2^T(\ell)]^T$

$$A_{11} = \begin{bmatrix} 0 & 1 \\ -gL & -\mathbb{D}_0 \end{bmatrix}, A_{12} = \begin{bmatrix} 0 & 1 \\ -gL & -0.5\mathbb{D}_0 \end{bmatrix}$$

$$A_{21} = \begin{bmatrix} 0 & 1 \\ -gL/\pi & -\mathbb{D}_0 \end{bmatrix}, A_{22} = \begin{bmatrix} 0 & 1 \\ -gL/\pi & -0.5\mathbb{D}_0 \end{bmatrix}$$

$$B_{11} = B_{21} = \begin{bmatrix} 0 \\ 1 \end{bmatrix}, B_{12} = B_{22} = \begin{bmatrix} 0 \\ 0.5 \end{bmatrix}$$

$$C_{\alpha i} = \begin{bmatrix} 1 & 1 \end{bmatrix}, H_{\alpha i} = \tilde{N}_{\alpha i} = 0.01$$

$$T(\ell) = \begin{cases} \sin(\ell), & 0 \le \ell \le 2 \\ 0, & \ell > 2 \end{cases}$$

$$D_{1\alpha i} = \begin{bmatrix} 0.1 & 0.2 \\ 0.3 & 0.4 \end{bmatrix}, D_{2\alpha i} = \begin{bmatrix} 0.1 \\ 0.2 \end{bmatrix}$$

$$\tilde{M}_{\alpha i} = \begin{bmatrix} 0.1 & 0.2 & 0.1 & 0.2 \end{bmatrix}, i = 1, 2, \alpha = 1, 2.$$

We select Q = 500, $\delta = 0.1$, $\gamma = 100$. The initial state is $X(0) = \begin{bmatrix} 2.2 & -3 & 1 & 1 \end{bmatrix}^T$. The simulation is employed using the system data at every 0.05 s. The control policies are considered to update at every 2 s. By applying parallel Algorithm 1, the output feedback tracking control gains are obtained as

$$K_{11} = \begin{bmatrix} 17.9173 & -21.4952 \end{bmatrix}$$

 $K_{12} = \begin{bmatrix} 19.8191 & -22.2238 \end{bmatrix}$
 $K_{21} = \begin{bmatrix} 20.5846 & -21.9922 \end{bmatrix}$
 $K_{22} = \begin{bmatrix} 21.2753 & -22.4877 \end{bmatrix}$

Furthermore, along with the learning process in Algorithm 2, the parameter matrices P_{11} , P_{12} , P_{21} , and P_{22} are presented in Fig. 3, where both stability and

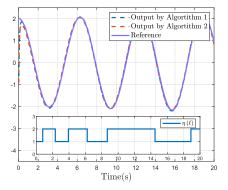


Fig. 4. Tracking trajectories by Algorithms 1 and 2.

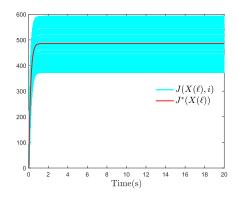


Fig. 5. Monte Carlo simulation.

convergence of the IRL-based Algorithm 2 are achieved. And the gains of controller are obtained without using the system dynamic $\mathbb{A}_{\alpha i}$ and transition probability π_{ij} , which are presented as follows:

$$K_{11} = \begin{bmatrix} 18.3226 & -21.4508 \end{bmatrix}$$

 $K_{12} = \begin{bmatrix} 19.6216 & -22.0838 \end{bmatrix}$
 $K_{21} = \begin{bmatrix} 20.7476 & -22.2003 \end{bmatrix}$
 $K_{22} = \begin{bmatrix} 21.0660 & -22.2516 \end{bmatrix}$.

By using the control gains calculated from Algorithms 1 and 2, the system tracking trajectories are shown in Fig. 4, respectively, where the reference trajectories get well tracked. Moreover, the mode evaluation of the Markov chain during the learning process is also depicted in Fig. 4. It indicates the validity and practicability of the proposed learning method. Moreover, based on the control policies obtained from Algorithm 2, we perform 1000 Monte Carlo experiments in Fig. 5 to show the convergence of mode-based performance index $J(X(\ell), i)$ and overall optimal performance index $J^*(X(\ell), i)$.

V. CONCLUSION

A novel online IRL-based nonfragile output feedback tracking control algorithm has been first proposed for MJFSs. The proposed online algorithm does not require the information of all the system dynamics. Moreover, by considering the control policy and disturbance as two rival players, the problem of nonfragile control can be converted into the issue of zero-sum

games. Two kinds of learning algorithms have been developed for solving the FSCAREs for MJFSs. For the proposed algorithm, stochastic stability has been proven via the Lyapunov stability theory. In addition, we have applied the designed algorithm in an application, and the simulation results have demonstrated the effectiveness. In our future work, we will attempt to apply the obtained results to semi-Markov systems or hidden-Markov systems.

APPENDIX A PROOF OF THEOREM 1

Proof: Together with Lemma 3 and weak infinitesimal operator \mathcal{L} , we have

$$\mathcal{L}V_{a}(X(\ell), i)$$

$$= \lim_{\Delta \ell \to 0} \frac{1}{\Delta \ell} [\mathbb{E}\{V_{a}(X(\ell + \Delta \ell), i + \Delta \ell) | X(\ell), i\}$$

$$- V_{a}(X(\ell), i)]$$

$$= X^{T}(\ell) [(\mathbb{A}_{\alpha i} + \mathbb{B}_{\alpha i} K_{\alpha i} \mathbb{C}_{\alpha i} + \mathbb{E}_{\alpha i} K_{w\alpha i})^{T} P_{\alpha i}$$

$$+ P_{\alpha i} (\mathbb{A}_{\alpha i} + \mathbb{B}_{\alpha i} K_{\alpha i} \mathbb{C}_{\alpha i} + \mathbb{E}_{\alpha i} K_{w\alpha i})$$

$$+ \sum_{j=1}^{S} \pi_{ij} P_{\alpha j} [X(\ell)]$$

$$= -X^{T}(\ell) \Big[\mathbb{C}_{0\alpha i}^{T} Q \mathbb{C}_{0\alpha i} + \mathbb{C}_{\alpha i}^{T} K_{\alpha i}^{T} K_{\alpha i} \mathbb{C}_{\alpha i}$$

$$- \gamma^{2} K_{w\alpha i}^{T} K_{w\alpha i} - \delta P_{\alpha i} \Big] X(\ell)$$

which implies the following Bellman equation:

$$(\mathbb{A}_{\alpha i} + \mathbb{B}_{\alpha i} K_{\alpha i} \mathbb{C}_{\alpha i} + \mathbb{E}_{\alpha i} K_{w \alpha i})^{\mathrm{T}} P_{\alpha i}$$

$$+ P_{\alpha i} (\mathbb{A}_{\alpha i} + \mathbb{B}_{\alpha i} K_{\alpha i} \mathbb{C}_{\alpha i} + \mathbb{E}_{\alpha i} K_{w \alpha i}) + \sum_{j=1}^{S} \pi_{ij} P_{\alpha j} - \delta P_{\alpha i}$$

$$+ \mathbb{C}_{0i}^{\mathrm{T}} Q \mathbb{C}_{0i} + \mathbb{C}_{\alpha i}^{\mathrm{T}} K_{\alpha i}^{\mathrm{T}} K_{\alpha i} \mathbb{C}_{\alpha i} - \gamma^{2} K_{w \alpha i}^{\mathrm{T}} K_{w \alpha i} = 0.$$

$$(14)$$

Based on the Bellman's optimization principle, we can further obtain the optimal policy as $u_{\alpha}(\ell) = -\mathbb{B}_{\alpha i}^{T} P_{\alpha i} \mathbb{C}_{\alpha i} X(\ell)$ and $w_{\alpha}(\ell) = (1/\gamma^{2})\mathbb{E}_{\alpha i}^{T} P_{\alpha i} X(\ell)$. From (14), we have

$$\begin{split} & \mathbb{A}_{\alpha i}^{\mathsf{T}} P_{\alpha i} + P_{\alpha i} \mathbb{A}_{\alpha i} - \delta P_{\alpha i} - P_{\alpha i} \mathbb{B}_{\alpha i} \mathbb{B}_{\alpha i}^{\mathsf{T}} P_{\alpha i} \\ & + (1/\gamma^2) P_{\alpha i} \mathbb{E}_{\alpha i} \mathbb{E}_{\alpha i}^{\mathsf{T}} P_{\alpha i} + \mathbb{C}_{0\alpha i}^{\mathsf{T}} Q \mathbb{C}_{0\alpha i} \\ & + L_{\alpha i}^{\mathsf{T}} L_{\alpha i} + \sum_{j=1}^{S} \pi_{ij} P_{\alpha j} = 0 \end{split}$$

where equation $K_{\alpha i}\mathbb{C}_{\alpha i}=-(\mathbb{B}_{\alpha i}^{\mathrm{T}}P_{\alpha i}+L_{\alpha i})$ is used. This completes the proof.

APPENDIX B PROOF OF THEOREM 2

Proof: Dividing both sides of (13) with $\Delta \ell$, we have

$$\begin{split} & \lim_{\Delta\ell \to 0} \frac{1}{\Delta\ell} \bigg[\int_{\ell}^{\ell + \Delta\ell} e^{-\delta(\tau - \ell)} \big[X^{\mathrm{T}}(\ell) \mathbb{C}_{0\alpha i}^{\mathrm{T}} Q \mathbb{C}_{0\alpha i} X(\ell) \\ & + u_{\alpha}^{\mathrm{T}}(\ell) u_{\alpha}(\ell) - \gamma^2 w_{\alpha}^{\mathrm{T}}(\ell) w_{\alpha}(\ell) \bigg] \mathrm{d}\tau \\ & = X^{\mathrm{T}}(\ell) \mathbb{C}_{0\alpha i}^{\mathrm{T}} Q \mathbb{C}_{0\alpha i} X(\ell) + u_{\alpha}^{\mathrm{T}}(\ell) u_{\alpha}(\ell) \\ & - \gamma^2 w^{\mathrm{T}}(\ell) w_{\alpha}(\ell). \end{split}$$

On the other hand, we have

$$\lim_{\Delta\ell \to 0} \frac{1}{\Delta\ell} \Big[\mathbb{E} \Big\{ e^{-\delta\Delta\ell} X^{\mathsf{T}}(\ell + \Delta\ell) P_{\alpha i} X(\ell + \Delta\ell) \\ - X^{\mathsf{T}}(\ell) P_{\alpha i} X(\ell) \Big\} \Big]$$

$$= -X^{\mathsf{T}}(\ell) \Big\{ [\mathbb{A}_{\alpha i} + \mathbb{B}_{\alpha i} K_{\alpha i} \mathbb{C}_{\alpha i} + \mathbb{E}_{\alpha i} K_{w\alpha i}]^{\mathsf{T}} P_{\alpha i} \\ + P_{\alpha i} [\mathbb{A}_{\alpha i} + \mathbb{B}_{\alpha i} K_{\alpha i} \mathbb{C}_{\alpha i} + \mathbb{E}_{\alpha i} K_{w\alpha i}] \\ + \sum_{j=1}^{S} \pi_{ij} P_{\alpha j} - \delta P_{\alpha i} \Big\} X(\ell)$$

Thus, the matrix $P_{\alpha i}$ calculated from (13) is equal to the solution by solving (11). This completes the proof.

APPENDIX C PROOF OF THEOREM 3

Proof: For the system (9), $V(X(\ell), i)$ is selected as the overall stochastic quadratic Lyapunov function. Consider the weak infinitesimal operator \mathcal{L} , we have

$$\mathcal{L}V(X(\ell), i) = X^{\mathrm{T}}(\ell) \left[\left[\tilde{\mathbb{A}}_i + \bar{\mathbb{B}}_i K_i \bar{\mathbb{C}}_i + \bar{\mathbb{E}}_i K_{wi} \right]^{\mathrm{T}} P_i \right]$$

$$+ P_i \left[\tilde{\mathbb{A}}_i + \bar{\mathbb{B}}_i K_i \bar{\mathbb{C}}_i + \bar{\mathbb{E}}_i K_{wi} \right] + \sum_{j=1, j \neq i}^{S} \pi_{ij} P_j X(\ell).$$
 (15)

According to the optimal principle, we can deduce that

$$\mathcal{L}V(X(\ell),i) = X^{\mathrm{T}}(\ell) \left[\left(\tilde{\mathbb{A}}_{i} - 0.5\delta I \right)^{\mathrm{T}} P_{i} + P_{i} \left(\tilde{\mathbb{A}}_{i} - 0.5\delta I \right) \right]$$

$$- \tilde{\mathbb{C}}_{i}^{\mathrm{T}} \bar{K}_{i}^{\mathrm{T}} \left(\bar{K}_{i} \tilde{\mathbb{C}}_{i} + L_{i} \right) - \left(\bar{K}_{i} \tilde{\mathbb{C}}_{i} + L_{i} \right)^{\mathrm{T}} \bar{K}_{i} \tilde{\mathbb{C}}_{i}$$

$$+ 2\gamma^{2} \bar{K}_{wi}^{\mathrm{T}} \bar{K}_{wi} + \sum_{j=1, j \neq i}^{S} \pi_{ij} P_{j} X(\ell)$$

$$= -X^{\mathrm{T}}(\ell) \left[\tilde{\mathbb{C}}_{0i}^{\mathrm{T}} Q \tilde{\mathbb{C}}_{0i} + \tilde{\mathbb{C}}_{i}^{\mathrm{T}} \bar{K}_{i}^{\mathrm{T}} \bar{K}_{i} \tilde{\mathbb{C}}_{i} - \gamma^{2} \bar{K}_{wi}^{\mathrm{T}} \bar{K}_{wi} X(\ell) \right]$$

$$(16)$$

By using Lemmas 1 and 2, there exists $\sigma \in (0, 2)$ satisfying

$$X^{\mathrm{T}}(\ell) \Big[\bar{\mathbb{C}}_{i}^{\mathrm{T}} \bar{K}_{i}^{\mathrm{T}} \bar{K}_{i} \bar{\mathbb{C}}_{i} - \gamma^{2} \bar{K}_{wi}^{\mathrm{T}} \bar{K}_{wi} \Big] X(\ell)$$

$$= \sigma X^{\mathrm{T}}(\ell) \Big[\bar{\mathbb{C}}_{i}^{\mathrm{T}} \bar{K}_{i}^{\mathrm{T}} K_{i} \bar{\mathbb{C}}_{i} - \gamma^{2} \bar{K}_{wi}^{\mathrm{T}} K_{wi} \Big] X(\ell). \tag{17}$$

Then, combining (15)–(17) can further become

$$-2\sigma \left(\bar{\mathbb{C}}_{i}^{\mathsf{T}}\bar{K}_{i}^{\mathsf{T}}\bar{K}_{i}\bar{\mathbb{C}}_{i} - \gamma^{2}\bar{K}_{wi}^{\mathsf{T}}\bar{K}_{wi}\right)\right]X(\ell)$$

$$+\sigma X^{\mathsf{T}}(\ell)\left[\bar{\mathbb{C}}_{0i}^{\mathsf{T}}Q\bar{\mathbb{C}}_{0i} + \bar{\mathbb{C}}_{i}^{\mathsf{T}}\bar{K}_{i}^{\mathsf{T}}\bar{K}_{i}\bar{\mathbb{C}}_{i} - \gamma^{2}\bar{K}_{wi}^{\mathsf{T}}\bar{K}_{wi}\right]X(\ell)\right\}$$

$$= -\frac{1}{\rho}X^{\mathsf{T}}(\ell)\left[\bar{\mathbb{C}}_{0i}^{\mathsf{T}}Q_{1}\bar{\mathbb{C}}_{0i} + \bar{\mathbb{C}}_{i}^{\mathsf{T}}\bar{K}_{i}^{\mathsf{T}}\bar{K}_{i}\bar{\mathbb{C}}_{i} - \gamma^{2}\bar{K}_{wi}^{\mathsf{T}}\bar{K}_{wi}\right]X(\ell)$$

$$(18)$$

where $\rho = \sigma/(2 - \sigma)$ and $Q_1 = \rho Q$.

When $w(\ell) \equiv 0$, there is $\mathcal{L}V(X(\ell), i) \leq 0$, which ensures the stochastically asymptotic stability of the system.

Multiplying $e^{-\delta \ell}$ to both sides of (18) and integrating both sides in [0, T], then, one can deduce that

$$\begin{split} & \mathbb{E} \bigg\{ \int_0^{\mathsf{T}} e^{-\delta \ell} \big(X^{\mathsf{T}}(\ell) \bar{\mathbb{C}}_{0i}^{\mathsf{T}} Q_1 \bar{\mathbb{C}}_{0i} X(\ell) + u^{\mathsf{T}}(\ell) u(\ell) \big) d\ell \bigg\} \\ & \leq \mathbb{E} \bigg\{ \gamma^2 \int_0^{\mathsf{T}} e^{-\delta \ell} w^{\mathsf{T}}(\ell) w(\ell) d\ell \bigg\} \end{split}$$

taking $T \to \infty$, which matches the Definition 2. This completes the proof.

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