

(答案需有完整計算過程及標示必要的向量符號)

1. 給定一長直圓柱，長 5 m 及半徑 $a = 0.005$ m，表面均勻分布電荷 $+5\mu\text{C}$ 。此圓柱外部有一同軸圓柱殼，長 5 m 及半徑 $b = 0.01$ m，表面均勻分布電荷 $-2.5\mu\text{C}$ ，其剖面圖如圖 1 所示。可忽略邊緣效應，請計算所有區域之電場 \vec{E} 。(16%)
2. 給定一長直同軸線，其內、外導體半徑分別為 $r_i = 0.5$ cm 及 $r_o = 1$ cm，導體間填充有同軸之橡膠(相對介電常數 $\epsilon_{rr} = 3.2$)及聚苯乙烯(相對介電常數 $\epsilon_{rp} = 2.6$)，圖 2 所示為剖面圖，其中 $r_p = 0.75$ cm。為避免介電崩潰，介質能承受之最大電場強度需低於其介電強度之 25%，橡膠及聚苯乙烯之介電強度分別為 25×10^6 V/m 及 20×10^6 V/m。(a)請分別計算橡膠層及聚苯乙烯層各自所能承受之最大電場強度值 E (8%)，(b)請決定此同軸線內、外導體間最大允許工作電壓 V (8%)。
3. 給定一個厚介質球殼，內半徑為 a ，外半徑為 b ，具有極化向量 $\vec{P} = \hat{a}_R \frac{k}{R}$ ，其中 k 為常數，假設無自由電荷。(a)請計算束縛電荷密度 ρ_{pv} 及 ρ_{ps} 。(6%) (b)請計算總束縛電荷 Q_p 。($Q_p = Q_{pv} + Q_{ps}$) (5%)。 (c)計算所有區域之電場 \vec{E} 。(5%)
4. 給定同心導體球殼及導體球，導體球殼半徑 $b = 30$ cm，導體球半徑 $a = 8$ cm，兩導體間填充有兩層不同介質，兩介質之相對介電常數分別為 $\epsilon_{r1} = 5$ 及 $\epsilon_{r2} = 10$ ，兩層介質相接處半徑 $c = 20$ cm，如圖 3 所示。請計算其電容 C 。(16%)
5. 給定兩垂直連接導體板，兩板分別朝 $+x$ 軸及 $+y$ 軸方向無限延伸，也同時朝 z 軸方向無限延伸，擺置一 100 nC 之電荷 Q 於位置 $(3, 4, 0)$ 處，如圖 4 所示，周圍為自由空間。(a)請計算於位置 $(3, 5, 0)$ 之電位 V 及電場 \vec{E} 。(8%) (b)請計算此兩導體板位於 $z = 0$ 處之表面電荷密度 ρ_s 。(8%)
6. 給定一中空圓柱電阻器，此材料電導率為 σ ，長度為 L ，內、外徑分別為 r_a 及 r_b ，如圖 5 所示。假設電流朝徑向方向流動，請計算中空圓柱內、外表面間之電阻值 R 。(20%)

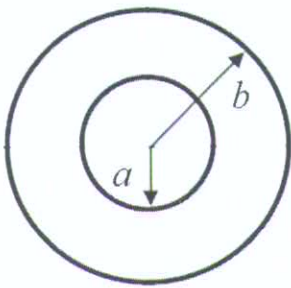


圖 1

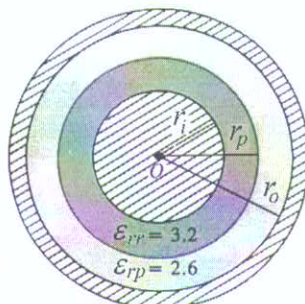


圖 2

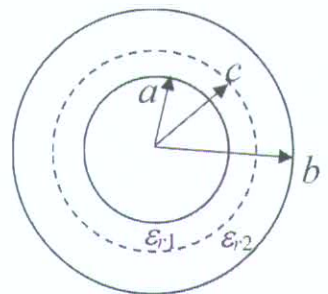


圖 3

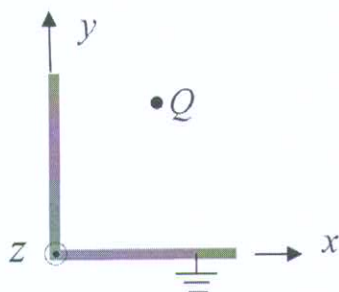


圖 4

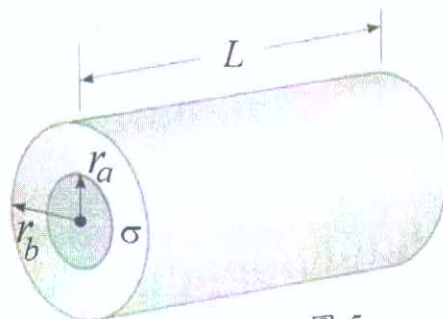


圖 5

1. 因具有对称性, 可选高斯面, 套用高斯定律

• For $r < a$:

$$\oint_S \vec{E} \cdot d\vec{S} = \frac{Q}{\epsilon_0} \Rightarrow 2\pi r L E_r = \frac{0}{\epsilon_0}$$
$$\Rightarrow E_r = 0 \Rightarrow \underline{\vec{E} = 0} \quad \#$$

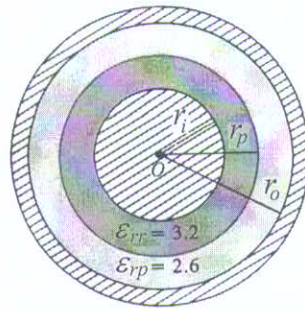
• For $a < r < b$:

$$\oint_S \vec{E} \cdot d\vec{S} = \frac{Q}{\epsilon_0} \Rightarrow 2\pi r L E_r = \frac{q_a}{\epsilon_0}$$
$$\Rightarrow E_r = \frac{q_a}{2\pi r L \epsilon_0} = \frac{5 \times 10^{-6}}{2\pi r \times 5 \times \frac{1}{36\pi} \times 10^{-9}}$$
$$= \frac{1.8 \times 10^4}{r}$$
$$\underline{\vec{E} = a\hat{r} \frac{1.8 \times 10^4}{r} \text{ V/m}} \quad \#$$

• For $r > b$:

$$\oint_S \vec{E} \cdot d\vec{S} = \frac{Q}{\epsilon_0}$$
$$2\pi r L E_r = \frac{q_a + q_b}{\epsilon_0}$$
$$\Rightarrow E_r = \frac{q_a + q_b}{2\pi r L \epsilon_0} = \frac{5 \times 10^{-6} - 2.5 \times 10^{-6}}{2\pi r \times 5 \times \frac{1}{36\pi} \times 10^{-9}}$$
$$= \frac{9 \times 10^3}{r}$$
$$\underline{\vec{E} = a\hat{r} \frac{9 \times 10^3}{r} \text{ V/m}} \quad \#$$

2.



圖二

Solution :

(a) 參考課本 Example 3-12, $r_i = 0.5 \text{ cm}$ 、 $r_o = 1 \text{ cm}$ 及 $r_p = 0.75 \text{ cm}$ 。

橡膠層 25% 介電強度 $\rightarrow 0.25 \times 25 \times 10^6 = 6.25 \times 10^6 \text{ V/m}$

聚苯乙烯層 25% 介電強度 $\rightarrow 0.25 \times 20 \times 10^6 = 5 \times 10^6 \text{ V/m}$

$$\text{Max. } E_r = \frac{\rho_l}{2\pi\epsilon_o} \left(\frac{1}{3.2r_i} \right) \Rightarrow \frac{\rho_l}{2\pi\epsilon_o} = 6.25 \times 10^6 \times 3.2r_i = 10^5 \text{ V/m}$$

$$\text{Max. } E_p = \frac{\rho_l}{2\pi\epsilon_o} \left(\frac{1}{2.6r_p} \right) \Rightarrow \frac{\rho_l}{2\pi\epsilon_o} = 5 \times 10^6 \times 2.6r_p = 0.975 \times 10^5 \text{ V/m}$$

(b)

由 $\text{Max. } E_p$ 決定可承受之最大 $\rho_l / 2\pi\epsilon_o \Rightarrow \frac{\rho_l}{2\pi\epsilon_o} = 0.975 \times 10^5 \text{ V/m}$

參考課本 Example 3-12,

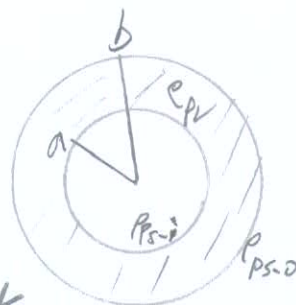
$$\begin{aligned} V_{\max} &= \frac{\rho_l}{2\pi\epsilon_o} \left(\frac{1}{\epsilon_{rp}} \ln \frac{r_o}{r_p} + \frac{1}{\epsilon_{rr}} \ln \frac{r_p}{r_i} \right) \\ &= 0.975 \times 10^5 \left(\frac{1}{2.6} \ln 1.333 + \frac{1}{3.2} \ln 1.5 \right) = 2.31 \times 10^4 \text{ V} \end{aligned}$$

3.

sol):

$$(a) \quad \vec{P} = a_{\hat{R}} \frac{K}{R}$$

$$\rho_{PV} = -\nabla \cdot \vec{P} = -\frac{1}{R^2} \frac{\partial}{\partial R} (R^2 \frac{K}{R}) = \underline{-\frac{K}{R^2}} \quad \#$$



$$\rho_{PS-outer} = \vec{P} \cdot \hat{a}_n = a_{\hat{R}} \frac{K}{b} \cdot \hat{a}_R = \underline{\frac{K}{b}} \quad \#$$

$$\rho_{PS-inner} = \vec{P} \cdot \hat{a}_n = a_{\hat{R}} \frac{K}{a} \cdot (-\hat{a}_R) = \underline{-\frac{K}{a}} \quad \#$$

$$(b) \quad Q_P = Q_{PV} + Q_{PS} = \int_V \rho_{PV} dV + \oint_S \rho_{PS-outer} ds + \oint_S \rho_{PS-inner} ds$$

$$= \int_0^{2\pi} \int_0^\pi \int_a^b \left(-\frac{K}{R^2}\right) R^2 \sin\theta dR d\theta d\phi + \int_0^{2\pi} \int_0^\pi \frac{K}{b} b^2 \sin\theta d\theta d\phi$$

$$+ \int_0^{2\pi} \int_0^\pi \left(-\frac{K}{a}\right) a^2 \sin\theta d\theta d\phi$$

$$= -4\pi K R \Big|_a^b + 4\pi b K - 4\pi a K$$

$$= -4\pi K (b-a) + 4\pi b K - 4\pi a K$$

$$= 0$$

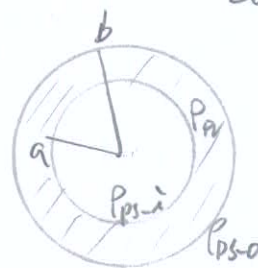
$$\underline{\hspace{2cm}} \quad \#$$

(c) 具對稱性, 可選高斯面, 套用高斯定律 $\oint_S \vec{E} \cdot d\vec{S} = \frac{Q+Q_p}{\epsilon_0}$

• for $R < a$, 無自由及束縛電荷 $\Rightarrow Q=0 \Rightarrow \vec{E}=0$ *

• for $R > b$, 無自由電荷, 束縛電荷淨量 $Q_p=0$
 $\Rightarrow \vec{E}=0$ *

• for $a < R < b$,



Method 1:

$$Q_p = \oint P_{ps-inner} dS + \int_0^{2\pi} \int_0^\pi \int_a^R P_{pv} dv$$

$$= 4\pi a^2 \left(-\frac{K}{a}\right) + 4\pi (-K) R \Big|_a^R$$

$$= -4\pi a K - 4\pi K (R-a)$$

$$= -4\pi K R$$

$$\therefore \oint_S \vec{E} \cdot d\vec{S} = \frac{Q+Q_p}{\epsilon_0}, \text{ 假設 } \vec{E} = \hat{a}_R E_R$$

$$4\pi R^2 E_R = -4\pi K R / \epsilon_0$$

$$E_R = \frac{-K}{R \epsilon_0}$$

$$\therefore \vec{E} = \hat{a}_R \left(\frac{-K}{R \epsilon_0} \right)$$

Method 2: 由 $\vec{D} = \epsilon_0 \vec{E} + \vec{P}$

$\therefore a < R < b$ 無自由電荷 Q

$$\therefore \vec{E} = -\frac{\vec{P}}{\epsilon_0}$$

$$\therefore \oint_S \vec{D} \cdot d\vec{S} = Q \Rightarrow \vec{D}=0$$

$$= -\hat{a}_R \frac{K}{R \epsilon_0}$$

4.

Sol): 假设导体球上有电荷 Q
球壳上为 $-Q$.

由高斯定律 $\oint \vec{D} \cdot d\vec{S} = Q$

$$\Rightarrow 4\pi R^2 D = Q$$

$$\Rightarrow D = \frac{Q}{4\pi R^2}$$

$$\therefore \vec{E} = \vec{a}_R \frac{Q}{4\pi \epsilon R^2}, \quad \epsilon_1 = \epsilon_0 \epsilon_{r1}, \quad \epsilon_2 = \epsilon_0 \epsilon_{r2}$$

$$V_{ab} = - \left[\int_b^c \vec{a}_R \frac{Q}{4\pi \epsilon_2 R^2} \cdot \vec{a}_R dR + \int_c^a \vec{a}_R \frac{Q}{4\pi \epsilon_1 R^2} \cdot \vec{a}_R dR \right]$$

$$= \frac{Q}{4\pi \epsilon_2} \frac{1}{R} \Big|_b^c + \frac{Q}{4\pi \epsilon_1} \frac{1}{R} \Big|_c^a$$

$$= \frac{Q}{4\pi \epsilon_2} \left(\frac{1}{c} - \frac{1}{b} \right) + \frac{Q}{4\pi \epsilon_1} \left(\frac{1}{a} - \frac{1}{c} \right)$$

$$\therefore C = \frac{Q}{V_{ab}} = \frac{1}{\frac{1}{4\pi \epsilon_2} \left(\frac{1}{c} - \frac{1}{b} \right) + \frac{1}{4\pi \epsilon_1} \left(\frac{1}{a} - \frac{1}{c} \right)}$$

$$= \frac{10^{-9}}{\frac{9}{10} \left(\frac{1}{0.2} - \frac{1}{0.3} \right) + \frac{9}{5} \left(\frac{1}{0.08} - \frac{1}{0.2} \right)}$$

$$= \frac{10^{-9}}{1.5 + 13.5} = \underline{\underline{6.67 \times 10^{-11} \text{ F}}}$$

5. Soln):

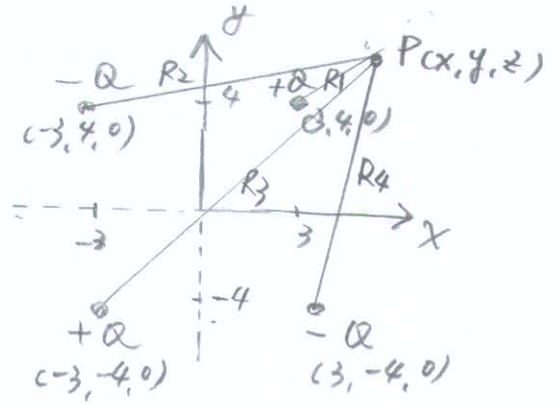
(a) 擺 = 果負鏡像電荷

$$R_1 = [(x-3)^2 + (y-4)^2 + z^2]^{1/2}$$

$$R_2 = [(x+3)^2 + (y-4)^2 + z^2]^{1/2}$$

$$R_3 = [(x+3)^2 + (y+4)^2 + z^2]^{1/2}$$

$$R_4 = [(x-3)^2 + (y+4)^2 + z^2]^{1/2}$$



At $P(3, 5, 0) \Rightarrow R_1 = 1, R_2 = 6.08, R_3 = 10.82, R_4 = 9$

$$V = \frac{Q}{4\pi\epsilon_0 R} \Rightarrow V = \frac{100 \times 10^{-9}}{4\pi \times \frac{1}{36\pi} \times 10^{-9}} \left(\frac{1}{R_1} - \frac{1}{R_2} + \frac{1}{R_3} - \frac{1}{R_4} \right)$$

$$= 900 \left(1 - \frac{1}{6.08} + \frac{1}{10.82} - \frac{1}{9} \right)$$

$$= 735.2 \text{ V}$$

$$\vec{E} = -\nabla V = -\hat{a}_x \frac{\partial V}{\partial x} - \hat{a}_y \frac{\partial V}{\partial y} - \hat{a}_z \frac{\partial V}{\partial z}, V = 900 \left(\frac{1}{R_1} - \frac{1}{R_2} + \frac{1}{R_3} - \frac{1}{R_4} \right)$$

$$= -900 \left[-\frac{x-3}{R_1^3} + \frac{x+3}{R_2^3} - \frac{x+3}{R_3^3} + \frac{x-3}{R_4^3} \right] \hat{a}_x$$

$$- 900 \left[-\frac{y-4}{R_1^3} + \frac{y-4}{R_2^3} - \frac{y+4}{R_3^3} + \frac{y+4}{R_4^3} \right] \hat{a}_y$$

$$= -19.76 \hat{a}_x + 891.28 \hat{a}_y$$

(b). 水平板 ($y=0$):

$$R_1 = [(x-3)^2 + 16]^{1/2} = R_4, R_2 = [(x+3)^2 + 16]^{1/2} = R_3$$

$$\vec{E} = -900 \left[\frac{\rho}{R_1^3} - \frac{\rho}{R_2^3} \right] \hat{a}_y = -900 \left[\frac{\rho}{[(x-3)^2 + 16]^{3/2}} - \frac{\rho}{[(x+3)^2 + 16]^{3/2}} \right] \hat{a}_y$$

$$\rho_s = \epsilon_0 E_n = -6.37 \times 10^{-8} \left[\frac{1}{[(x-3)^2 + 16]^{3/2}} - \frac{1}{[(x+3)^2 + 16]^{3/2}} \right]$$

三、垂直板 ($x=0$):

$$R_1 = [9 + (y-4)^2]^{1/2} = R_2$$

$$R_3 = [9 + (y+4)^2]^{1/2} = R_4$$

$$\vec{E} = -900 \left[\frac{6}{[9 + (y-4)^2]^{3/2}} - \frac{6}{[9 + (y+4)^2]^{3/2}} \right] \hat{a}_x$$

$$P_5 = \epsilon_0 E_n = -4.77 \times 10^{-8} \left[\frac{1}{[9 + (y-4)^2]^{3/2}} - \frac{1}{[9 + (y+4)^2]^{3/2}} \right]$$

6.

Sol): 假設 $r=r_a$ 表面之電位 $V=V_0$,
 而 $r=r_b$ 之電位 $V=0$, $\nabla^2 V = 0$ $\because \frac{\partial^2 V}{\partial \phi^2} = 0, \frac{\partial^2 V}{\partial z^2} = 0$

$$\therefore \frac{d}{dr} \left(r \frac{dV}{dr} \right) = 0 \Rightarrow V = C_1 \ln r + C_2$$

代入邊界條件:

$$V_0 = C_1 \ln r_a + C_2 \quad \text{--- (1)}$$

$$0 = C_1 \ln r_b + C_2 \quad \text{--- (2)}$$

$$\text{由 (1) - (2)} \quad V_0 = C_1 (\ln r_a - \ln r_b) = C_1 \ln \frac{r_a}{r_b}$$

$$\therefore C_1 = \frac{V_0}{\ln \frac{r_a}{r_b}} \quad \text{代入 (2)}$$

$$C_2 = -C_1 \ln r_b = -\frac{V_0 \ln r_b}{\ln \frac{r_a}{r_b}}$$

$$\begin{aligned} \therefore V &= C_1 \ln r + C_2 = \frac{V_0 \ln r}{\ln \frac{r_a}{r_b}} - \frac{V_0 \ln r_b}{\ln \frac{r_a}{r_b}} \\ &= V_0 \frac{\ln \frac{r}{r_b}}{\ln \frac{r_a}{r_b}} \end{aligned}$$

$$\vec{J} = \sigma \vec{E} = -\sigma \nabla V = -\hat{a}_r \sigma \frac{\partial V}{\partial r} = -\hat{a}_r \frac{\sigma V_0}{r \ln \frac{r_a}{r_b}}$$

$$I = \int_S \vec{J} \cdot d\vec{S} = \int_S \left(-\hat{a}_r \frac{\sigma V_0}{r \ln \frac{r_a}{r_b}} \right) \cdot \hat{a}_r r d\phi dz$$

$$= -\frac{\sigma V_0 2\pi L}{\ln \frac{r_a}{r_b}}$$

$$R = \frac{V_0}{I} = \frac{V_0}{-\frac{\sigma V_0 2\pi L}{\ln \frac{r_a}{r_b}}} = \frac{\ln \frac{r_a}{r_b}}{-\sigma 2\pi L}$$

$$= \frac{\ln \frac{r_b}{r_a}}{\sigma 2\pi L}$$

~~~~~ \*