

# SEA Project Report 1

Yi Yang

09/19/2016

This week, I re-plot driving point impedance theoretical results(virtual stiffness), codes and plots shown below:

```
1 % This program is used for obtaining bode plots of linear model
2 % Admittance Control Devices
3 s = tf('s');
4 dataID = sysID();
5 Z_h = dataID.M * s + dataID.B; % the inherent impedance of haptic devices
6 Kve = 400; % [N/m], virtual environment spring constant
7 Z_ve = Kve/s; % impedance of virtual environment
8 C = 2; % portional control law
9 Z_padm = (dataID.n * C * Z_ve + Z_h)/(dataID.n * C + 1);
10
11 % Series Elastic Actuator Device
12 k = 904; % [N/m], Physical spring constant
13 kk = k/s + dataID.b;
14 Z_e = dataID.m * s;
15 Z_psea = (Z_e * (Z_h + k * dataID.n * C/s + kk) + kk * (Z_h + dataID.n * C * Z_ve))/(Z_h + ...
16     k * dataID.n * C/s + kk);
17
18 close all; figure(1);
19 opts = bodeoptions('cstprefs');
20 opts.PhaseVisible = 'off';
21 opts.FreqUnits = 'Hz';
22 opts.Grid = 'on';
23 bodemag(Z_padm, opts);
24 hold on;
25 bodemag(Z_psea, opts);
26 bodemag(Z_ve, '--', opts);
27 legend('Admittance', 'SEA(k= 904)', 'ideal line');
28 title('Virtual Stiffness');
29 hold off;
```

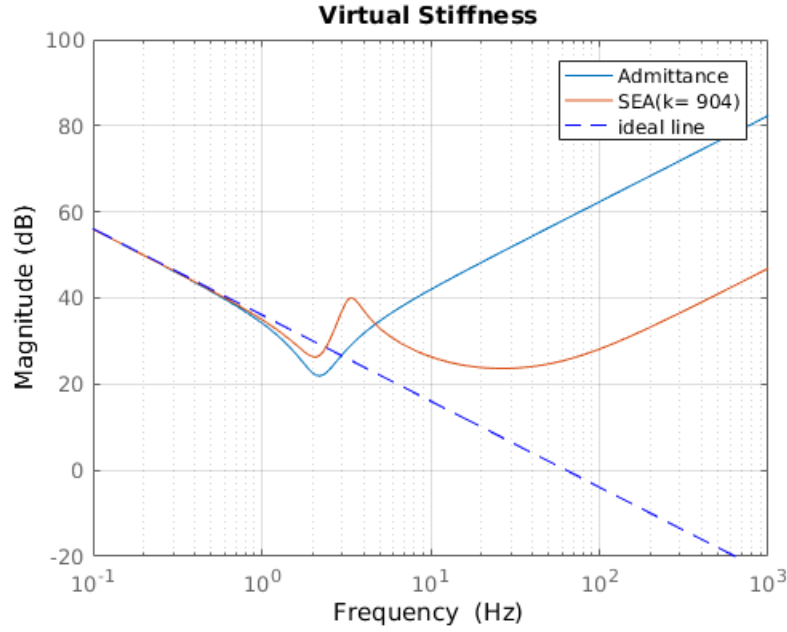


Figure 1: Driving point impedance theoretical results(virtual stiffness)

After plotting the theoretical transfer function, I want to use some real data to estimate the transfer functions and compare them with the theoretical ones. First, I input a step signal with time step size  $0.001s$ , I add a white noise ( $SNR = 10$ ) to the input signal and then apply it to the linear matlab model. By using *tffestimate* function in Matlab, I can get the transfer function for admittance and SEA schemes respectively. The codes and plots are attached below:

```

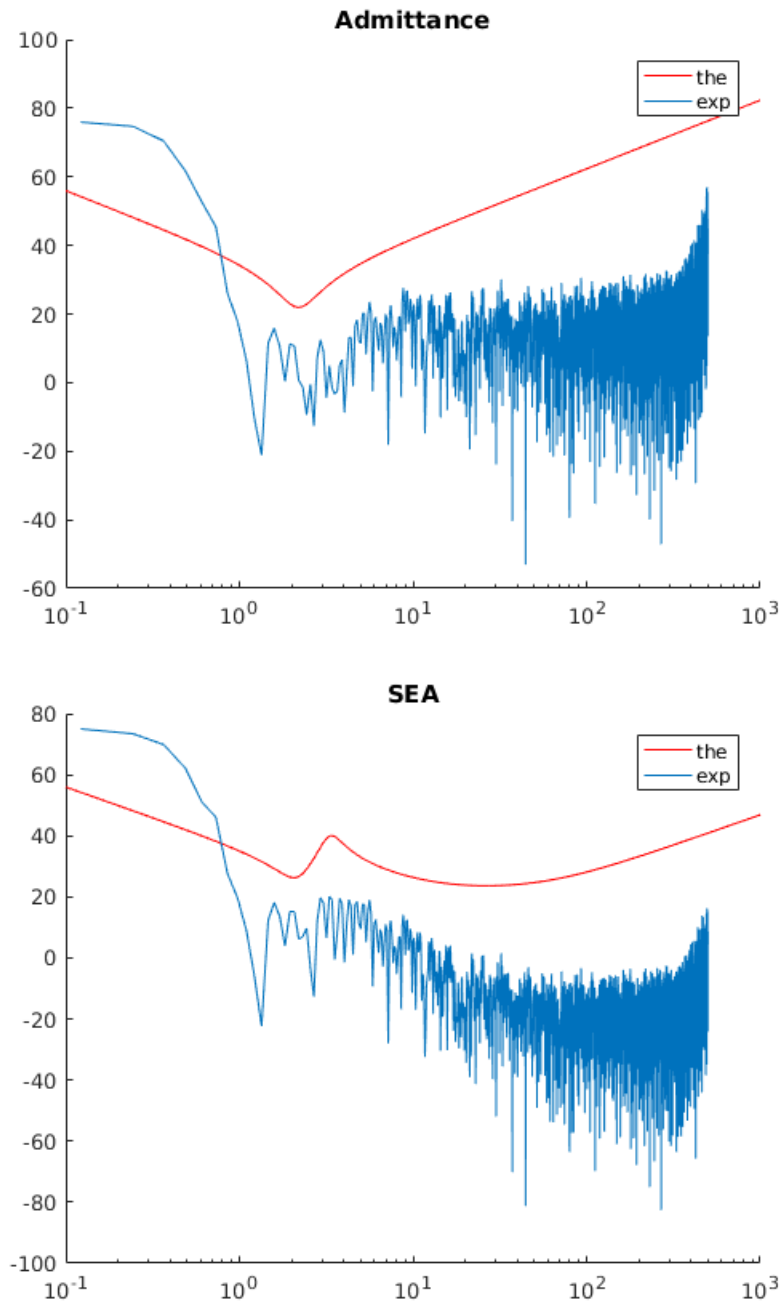
1 % This program is to generate Bode plots using the real recorded data, but
2 % the model we use is still linear Matlab model
3 % by Yi Yang
4 % Date: 9/23/2016
5 %-----
6 % Admittance Control Devices
7 clear all; close all;
8 s = tf('s');
9 dataID = sysID();
10 Z_h = dataID.M * s + dataID.B; % the inherent impedance of haptic devices
11 Kve = 400; % [N/m], virtual environment spring constant
12 Z_ve = Kve/s; % impedance of virtual environment
13 C = 2; % portional control law
14 Z_padm = (dataID.n * C * Z_ve + Z_h)/(dataID.n * C + 1);
15
16 % Series Elastic Actuator Device
17 k = 904; % [N/m], Physical spring constant
18 kk = k/s + dataID.b;
19 Z_e = dataID.m * s;
20 Z_psea = (Z_e * (Z_h + k * dataID.n * C/s + kk) + kk * (Z_h + dataID.n * C * Z_ve))/(Z_h + ...
    k * dataID.n * C/s + kk);
21
22 % Add sinusoidal signal with white noise of snr = 10 to the linear model
23 t = linspace(0, 10, 10001); % time step chosen to be ~ 0.001
24 f0 = ones(length(t), 1);
25 fi = awgn(f0, 10, 0); % the measured loadCellForceA

```

```

26 uo_adm = lsim(1/Z_padm, fi, t);
27 uo_sea = lsim(1/Z_psea, fi, t);
28 %figure(1);
29 %hold on;
30 %plot(t, uo_adm);
31 %plot(t, uo_sea);
32 %hold off;
33
34 % Now use output signal to estimate the transfer function
35 fs = 1/(t(2) - t(1));
36 NFFT = 2^(nextpow2(length(t)) - 1);
37 [TF_adm, freq1] = tfestimate(uo_adm, f0, [], [], NFFT, fs);
38 [TF_sea, freq2] = tfestimate(uo_sea, f0, [], [], NFFT, fs);
39 Z_adm_e = 1./TF_adm;
40 Z_sea_e = 1./TF_sea;
41
42 % In order to compare theoretical and test data generated curve
43 [MagTh_adm, PhaseTh_adm, FreqTh_adm] = bode(Z_padm, {2*pi*1e-1, 2*pi*1e3});
44 [MagTh_sea, PhaseTh_sea, FreqTh_sea] = bode(Z_psea, {2*pi*1e-1, 2*pi*1e3});
45 Mag_adm = zeros(length(MagTh_adm), 1);
46 Freq_adm = FreqTh_adm./(2*pi);
47 Mag_sea = zeros(length(MagTh_sea), 1);
48 Freq_sea = FreqTh_sea./(2*pi);
49 for i = 1:length(MagTh_adm)
50     Mag_adm(i, 1) = MagTh_adm(1, 1, i);
51     Mag_adm(i, 1) = 20 * log10(Mag_adm(i, 1));
52 end
53 for i = 1:length(MagTh_sea)
54     Mag_sea(i, 1) = MagTh_sea(1, 1, i);
55     Mag_sea(i, 1) = 20 * log10(Mag_sea(i, 1));
56 end
57 % opts = bodeoptions('cstprefs');
58 % opts.PhaseVisible = 'off';
59 % opts.FreqUnits = 'Hz';
60 % opts.Grid = 'on';
61 figure(2);
62 % bodemag(Z_padm, opts);
63 hold on;
64 semilogx(Freq_adm, Mag_adm, 'r');
65 semilogx(freq1, mag2db(abs(TF_adm)));
66 legend('the', 'exp');
67 set(gca, 'xscale', 'log');
68 title('Admittance')
69 hold off;
70 figure(3);
71 % bodemag(Z_ve, '--', opts);
72 hold on;
73 semilogx(Freq_sea, Mag_sea, 'r');
74 semilogx(freq2, mag2db(abs(TF_sea)));
75 set(gca, 'xscale', 'log');
76 legend('the', 'exp');
77 title('SEA');
78 hold off;

```



We can find that there is large discrepancy between theoretical curve and the curve generated by adding noise to the input signal. And I am not sure whether the method is correct to generate these results.

# Appendix

System ID is shown below:

```
1 % system Identification
2 function dataID = sysID()
3     dataID.M = 176; % [kg], Stage and motor inertia
4     dataID.B = 1051; % [kg/s], Stage damping
5     dataID.m = 0.035; % [kg], End-effector mass
6     dataID.b = 15.05; % [kg/s], End-effector damping
7     dataID.k = 1300; % [N/m], Physical spring stiffness
8     dataID.n = 41.8; % [-], Gear ratio
9 end
```