On the Stefan Problem with Internal Heat Generation and Prescribed Heat Flux Conditions at the Boundary

Sidney Williams University of Idaho

L. Barannyk, O. Ogidan, J. Crepeau University of Idaho

A. Sakhnov Kutateladze Institute of Thermophysics SB RAS

ASME Summer Heat Transfer Conference July 2019

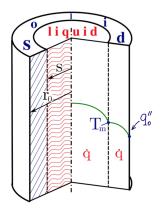
Applications

- Nuclear accident/meltdown scenario analysis
- Metal casting/materials processing industry
- Cryosurgical applications
- Geophysical modeling

Objective

Find an analytic solution to the Stefan problem (solid-liquid phase change) with internal heat generation, and fixed heat flux in both cylindrical and plane wall geometries

Problem Geometries



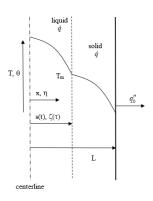


Figure: Cylindrical, and Plane Wall Schematic

Problem Assumptions

- The internal heat generation and the thermophysical properties of the materials are equal and constant in both the solid and liquid phases.
- The melting temperature T_m of the material is fixed and known.
- The phase change occurs at a single temperature T_m and there is no "mushy zone" at the interface in between phases.
- The heat transfer is by conduction. Convection in the liquid phase is neglected.

Governing Equations

Conduction Equation

$$\frac{1}{r}\frac{\partial}{\partial r}\left(r\frac{\partial T}{\partial r}\right) + \frac{\dot{q}}{k} = \frac{1}{\alpha}\frac{\partial T}{\partial t}$$

Interface Equation

$$-k_{liq} \frac{\partial T_{liq}(r,t)}{\partial r} \bigg|_{r=s} + \rho_{sol} \Delta h_f \frac{ds(t)}{dt} = -k_{sol} \frac{\partial T_{sol}(r,t)}{\partial r} \bigg|_{r=s}$$

$$T = T(r,t)$$

$$0 \le s \le r_0$$

$$t \ge 0$$

Boundary and Initial Conditions

BCs and IC in the liquid phase

$$\begin{split} \frac{\partial T_{liq}(r,t)}{\partial r}\bigg|_{r=0} &= 0,\\ T_{liq}(s(t),t) &= T_m, \quad T_{liq}(r,0) = \phi_{liq}(r) \end{split}$$

BCs and IC in the solid phase

$$T_{sol}(s(t), t) = T_m,$$

$$-k \frac{\partial T_{sol}(r, t)}{\partial r} \Big|_{r=r_0} = q_0'', \quad T_{sol}(r, 0) = \phi_{sol}(r)$$

Nondimensional Variables

$$\eta = \frac{r}{r_0}, \quad \zeta = \frac{s(t)}{r_0}, \quad \tau = \frac{\alpha t}{r_0^2}$$

$$\theta(\eta, \tau) = \frac{T(r, t) - T_m}{T^*}$$

$$T^* = \frac{\alpha \rho_{sol} \Delta h_f}{k_{sol}}, \quad \dot{Q} = \frac{\dot{q} r_o^2}{\alpha \rho_{sol} \Delta h_f}, \quad Q'' = \frac{q'' r_0}{k_{sol} T^*}$$

Dimensionless Governing Equations

Conduction Equation

$$\frac{1}{\eta} \frac{\partial}{\partial \eta} \left(\eta \frac{\partial \theta(\eta, \tau)}{\partial \eta} \right) + \dot{Q} = \frac{\partial \theta(\eta, \tau)}{\partial \tau},$$

Interface Equation

$$\left. \frac{\partial \theta_{liq}(\eta, \tau)}{\partial \eta} \right|_{\eta = \zeta} + \frac{d\zeta(\tau)}{d\tau} = \left. \frac{\partial \theta_{sol}(\eta, \tau)}{\partial \eta} \right|_{\eta = \zeta}$$

$$0 \le \zeta \le 1$$
$$\tau > 0$$

Dimensionless Boundary and Initial Conditions

BCs and IC in the liquid phase:

$$\begin{split} \frac{\partial \theta_{liq}(0,\tau)}{\partial \eta} &= 0\\ \theta_{liq}(\zeta(\tau),\tau) &= 0, \theta_{liq}(\eta,0) = \Phi_{liq}(\eta) \end{split}$$

BCs and IC in the solid phase:

$$\begin{split} \theta_{sol}(\zeta(\tau),\tau) &= 0 \\ \frac{\partial \theta_{sol}(1,\tau)}{\partial \eta} &= -Q'', \quad \theta_{sol}(\eta,0) = \Phi_{sol}(\eta) \end{split}$$

Solution in liquid phase

$$\theta_{liq}(\eta,\tau) = \sum_{n=1}^{\infty} A_n e^{-\lambda_n^2 \tau} J_0(\lambda_n \eta) + \frac{\zeta^2 - \eta^2}{4} \dot{Q}$$

where

$$A_n = \frac{\int_0^{\zeta} [\Phi_{liq}(\eta) - \theta_{liq,ss}(\eta)] J_0(\lambda_n \eta) \eta \, d\eta}{\int_0^{\zeta} J_0^2(\lambda_n \eta) \eta \, d\eta}$$
$$\lambda_n = \frac{z_{0n}}{\zeta(\tau)}, \quad n = 1, 2, \dots$$

Solution in Solid Phase

The full solution in solid phase is:

$$\theta_{sol}(\eta, \tau) = \theta_{sol,tr}(\eta, \tau) + \theta_{sol,ss}(\eta), \quad \zeta(\tau) < \eta < 1$$

$$\theta_{sol}(\eta,\tau) = \sum_{n=1}^{\infty} B_n \tilde{f}_n(\tilde{\lambda}_n \eta) e^{-\tilde{\lambda}_n^2 \tau} + \frac{\dot{Q}}{4} \left[\zeta^2 - \eta^2 \right] + \left(\frac{\dot{Q}}{2} - Q'' \right) \ln \frac{\eta}{\zeta}$$

where

$$B_n = \frac{\int_{\zeta(\tau)}^{1} (\Phi_{sol}(\eta) - \theta_{sol,ss}(\eta)) \tilde{f}_n(\tilde{\lambda}_n \eta) \eta \, d\eta}{\int_{\zeta(\tau)}^{1} [\tilde{f}_n(\tilde{\lambda}_n \eta)]^2 \eta \, d\eta}$$

The eigenvalues λ_n are the roots of

$$Y_1(\lambda)J_0(\zeta\lambda) - Y_0(\zeta\lambda)J_1(\lambda) = 0$$

$$\tilde{f}_n(\tilde{\lambda}_n\eta) = J_0(\tilde{\lambda_n}\eta) - \frac{J_1(\tilde{\lambda_n})}{Y_1(\tilde{\lambda_n})}Y_0(\tilde{\lambda_n}\eta): \quad \text{associated e'functions}$$

Interface Equation

The interface equation is:

$$\left. \frac{\partial \theta_{liq}(\eta,\tau)}{\partial \eta} \right|_{\eta=\zeta} + \frac{d\zeta(\tau)}{d\tau} = \left. \frac{\partial \theta_{sol}(\eta,\tau)}{\partial \eta} \right|_{\eta=\zeta}$$

Hence we have:

$$\frac{d\zeta(\tau)}{d\tau} = \sum_{n=1}^{\infty} A_n \lambda_n e^{-\lambda^2 \tau} J_1(\lambda_n \zeta) + \sum_{n=1}^{\infty} B_n \tilde{\lambda_n} \bar{f_n}(\zeta \tilde{\lambda_n}) e^{-\tilde{\lambda_n^2} \tau} + \left(\frac{\dot{Q}}{2} - Q''\right) \frac{1}{\zeta}$$

where

$$ar{f}_n(ilde{\lambda_n}\eta) = -J_1(ilde{\lambda_n}\eta) + rac{J_1(ilde{\lambda_n})}{Y_1(ilde{\lambda_n})}Y_1(ilde{\lambda_n}\eta)$$

Quasi-Static Interface Equation

$$\frac{d\zeta(\tau)}{d\tau} = \left(\frac{\dot{Q}}{2} - Q''\right)\frac{1}{\zeta}$$

Melting: $Q'' < \frac{\dot{Q}}{2}$.

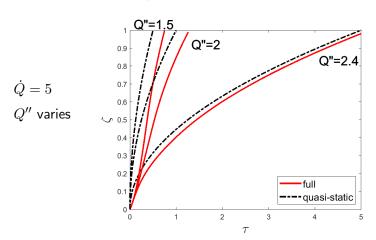
Solidification: $Q'' > \frac{\dot{Q}}{2}$.

J. Crepeau, A. Siahpush, Approximate solutions to the Stefan problem with internal heat generation, *Heat and Mass Transfer* **44** (7) (2008).

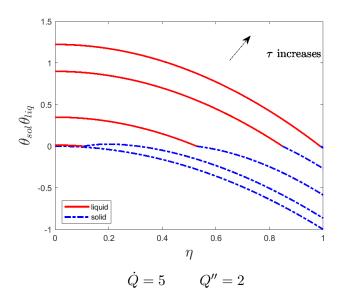
Interface Evolution for Melting

Initial conditions for melting:

At
$$\tau = 0$$
, $\Phi_{liq}(\eta) = 1$, $\Phi_{sol}(\eta) = 1 - \eta^2$, $\zeta(\tau) = 0$



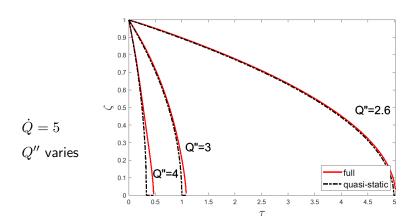
Temperature Evolution During Melting



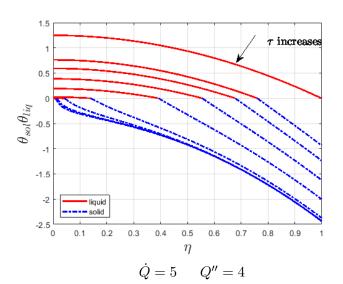
Interface Evolution for Solidification

Initial conditions for solidification:

$$\text{At} \quad \tau=0, \quad \Phi_{liq}(\eta)=\frac{Q}{4}(1-\eta^2)+1, \quad \Phi_{sol}(\eta)=1, \quad \zeta(\tau)=1$$



Temperature Evolution for Solidification



Conclusions

Defined the Governing Equations

Solution Through Classical Techniques

Interface Equation with Quasi-Static Approximation

Numerical Results