# CE 3111.103

Lab 4: BJT Amplifiers – Part I

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### Objective

The physical meaning of the low-frequency small-signal parameters of BJT, the transfer function for two of the three BJT amplifier configurations and the meaning of biasing for transistor circuits, and how to bias a BJT in the forward-active region (FAR).

## **Experimental Results**

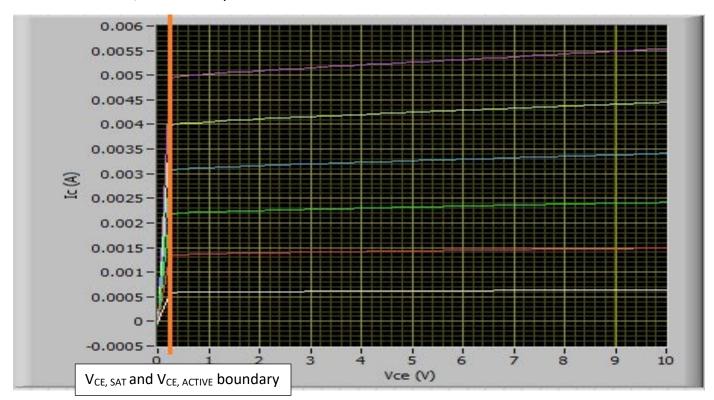
- BJT Small Signal Parameters
  - $\circ$  g<sub>m</sub>, β<sub>0</sub>, r<sub>π</sub>, r<sub>0</sub> calculations:

$$g_{\rm m} = \frac{0.00227A - 0.0006A}{4.97V - 4.99V} = -0.0835$$

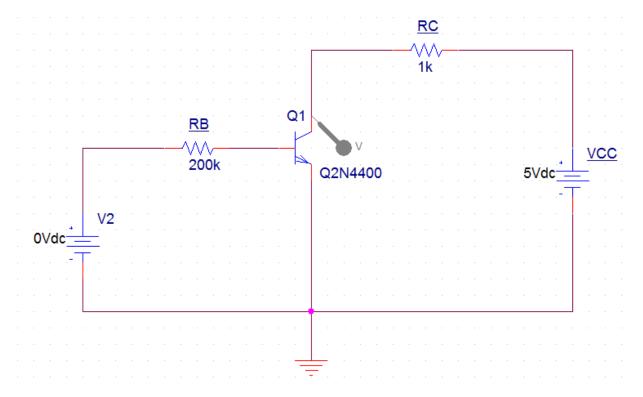
• 
$$r_{\pi} = \frac{4.97V - 4.99V}{(30 - 10) \times 10^{-6}} = 1000\Omega$$

• 
$$r_0 = \frac{3V - 2V}{0.0015A - 0.0014A} = 10000\Omega$$

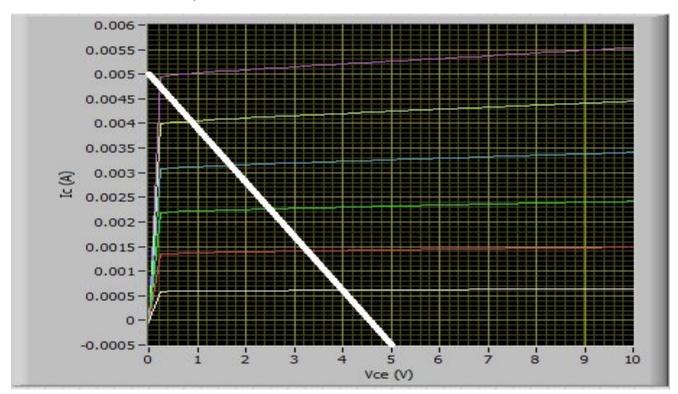
VCE,SAT boundary



- CE amplifier
  - o Circuit:



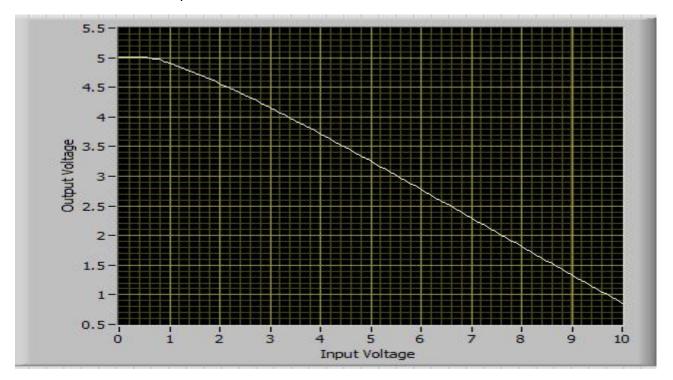
o Load line Graph



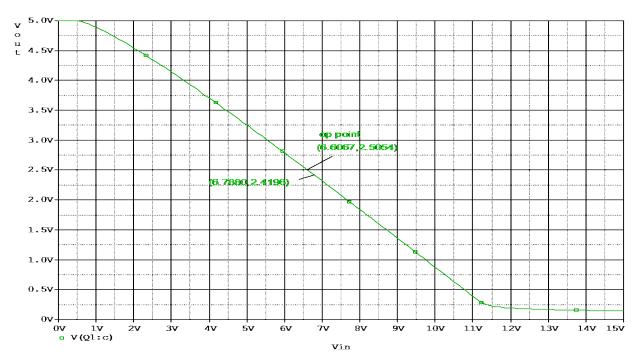
• Load line: 
$$I_C = \frac{V_{CC} - V_{CE}}{R_C} = \frac{5V - V_{CE}}{1000}$$

o Transfer function \*step g was omitted during the lab

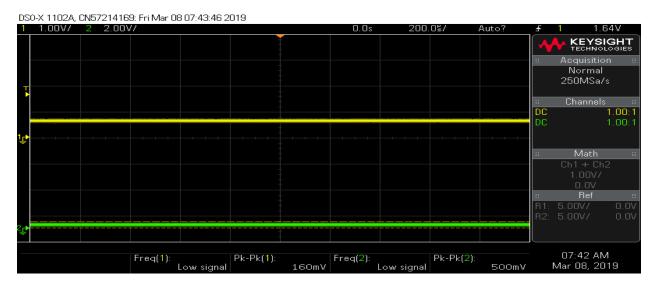
Step b



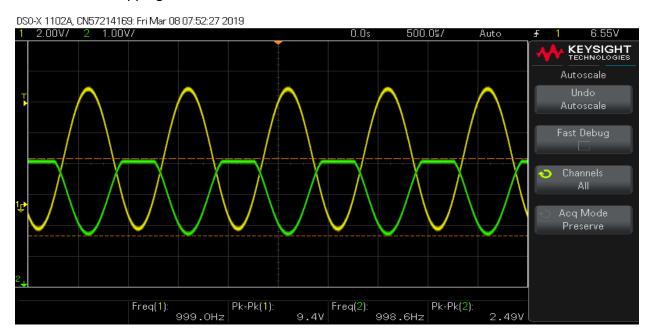
- $(V_{in,min}, V_{out,max})=(0.8, 4.9), (V_{in,max}, V_{out,min})=(10, 0.85), (V_{in,middle}, V_{out,middle})=(5.4, 2.875)$
- $V_{\text{out,middle}})=(5.4, 2.875)$   $V_{out} = \frac{0.85 4.9}{10 0.8} = -0.4402$
- Simulated curve



- (V<sub>in,min</sub>, V<sub>out,max</sub>)=(0.6, 4.9), (V<sub>in,max</sub>, V<sub>out,min</sub>)=(11.3, 0.6), (V<sub>in,middle</sub>, V<sub>out,middle</sub>)=(6.6067, 2.5054)
- $\frac{v_{out}}{v_{in}} = \frac{2.4196 2.5054}{6.7880 6.6067} = \frac{0.0858}{0.1813} = 0.4732$
- Small signal gain picture in step e

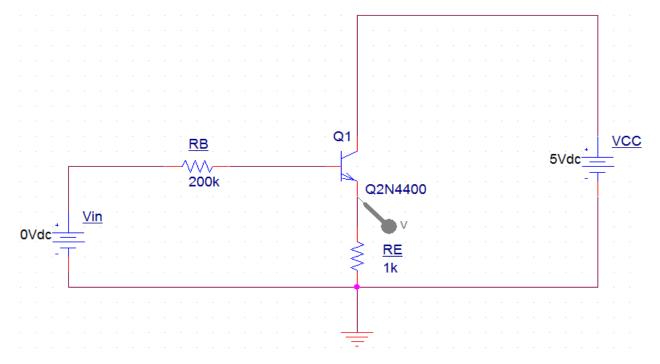


- The collector voltage
- I<sub>c</sub>=0.002632A V<sub>CE</sub>=2.5V
- $Av = \frac{500mV}{1100mV} = 0.4545$
- Clipping

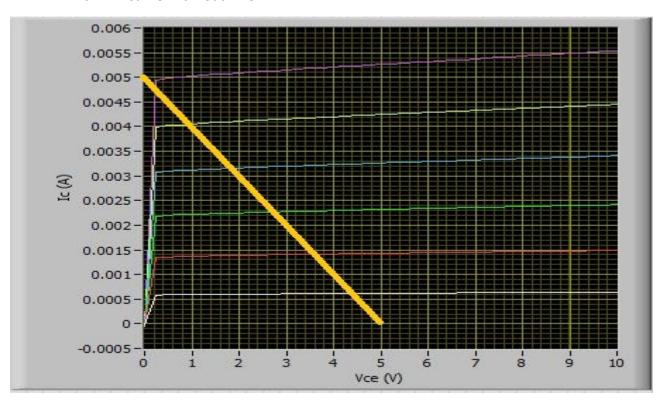


Clipping occurs because of the negative gain characteristic of the amplifier, and the transfer function rules the  $V_{out}$  decreases as  $V_{in}$  increases.

- Emitter Follower
  - o Circuit



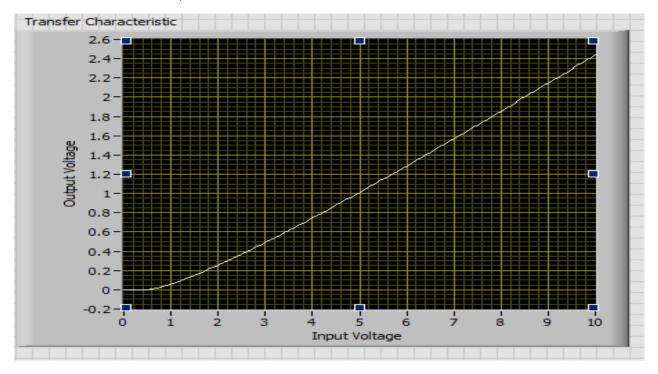
#### o I-V curve with load line



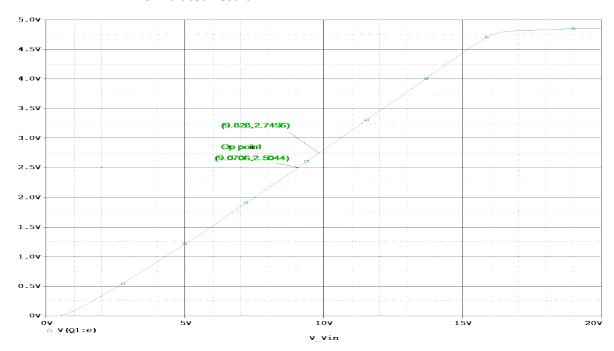
• Load Line: 
$$I_E = \frac{V_{CC} - V_{EC}}{R_E} = \frac{5V - V_{EC}}{1000}$$

### Transfer function \*step g was omitted during the lab

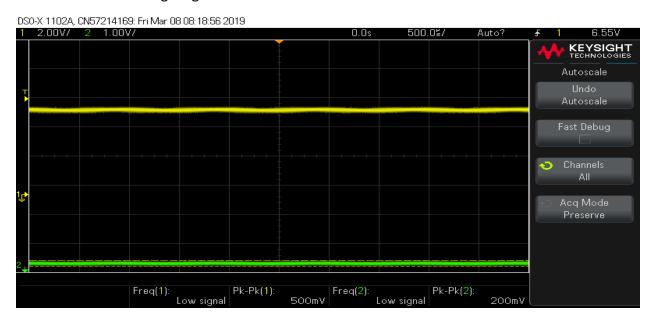
Step b



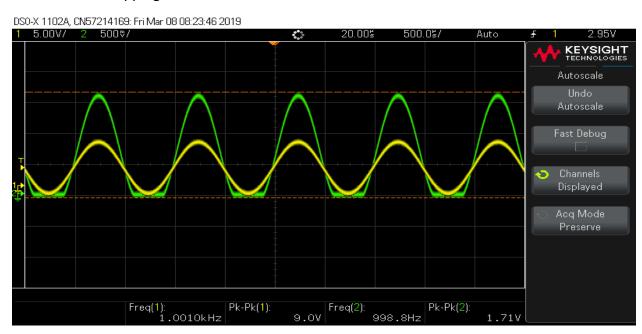
- (V<sub>in,min</sub>, V<sub>out,max</sub>)=(0.6, 0.01), (V<sub>in,max</sub>, V<sub>out,min</sub>)=(10, 2.45), (V<sub>in,middle</sub>, V<sub>out,middle</sub>)=(5.4, 1.15)
- $V_{\text{out,middle}})=(5.4, 1.15)$   $\frac{V_{out}}{V_{in}} = \frac{2.45-0.01}{10-0.6} = 0.2595$
- Simulated result



- (V<sub>in,min</sub>, V<sub>out,max</sub>)=(0.5, 0.01), (V<sub>in,max</sub>, V<sub>out,min</sub>)=(16, 4.75), (V<sub>in,middle</sub>, V<sub>out,middle</sub>)=(9.0706,2.5044)
- GAIN= $\frac{4.75-0.01}{16-0.5} = \frac{0.2452}{0.7574} = 0.3058$
- Discrepancy in gain due to different range of V<sub>in</sub> between the experiment and simulation
- o Small signal gain



- I<sub>c</sub>=0.000010943A V<sub>CE</sub>=2.5V
- Av= $\frac{200mV}{650mV}$ =0.3077
- Clipping



Clipping occurs because of the positive gain characteristic of the amplifier, and the transfer function rules the  $V_{out}$  increases as  $V_{in}$  increases.

# **Analysis**

1. The linear portion (Forward active region) of the transfer function for both CE amplifier and the emitter follower can be sketched by hand. Pspice adds the ability to simulate the saturation, early effect and the cut off regions of a BJT.

2.

a. For CE emitter

 $I_c = \beta I_B$ , The edge of saturation point is when  $V_{BE} = V_{CE}$ 

$$\frac{V_{in} - V_{BE}}{R_R} = \beta \frac{V_{CC} - V_{CE}}{R_C} \Rightarrow \frac{V_{in} - V_{BE}}{R_R} = \beta \frac{V_{CC} - V_{BE}}{R_C} \Rightarrow \frac{6.58V - 2.5V}{R_R} = 83.5 \frac{5 - 2.5}{1000}$$

$$R_B = 19.544\Omega$$

$$I_c = \frac{V_{CC} - V_{CE,SAT}}{R_C} = \frac{5V - 0.2V}{1000} = 4.8mA$$

$$I_c = \beta I_B$$

$$I_B = \frac{4.8 \text{mA}}{83.5} = 5.749 \times 10^{-5} A$$

$$R_B = \frac{V_{in} - V_{BE}}{I_B} = \frac{5 - 0.7}{57.49 \mu A} = 102287.5 \Omega$$

$$19.544 \le R_R \le 102287.5$$

b. For Emitter follower

$$\frac{V_{in} - V_{BE}}{R_B} = \beta \left(\frac{V_{CC} - V_{CE}}{R_E}\right) \left(\frac{\beta}{\beta + 1}\right) \rightarrow \frac{V_{in} - V_{BE}}{R_B} = \beta \frac{V_{CC} - V_{BE}}{R_C} (0.98) \rightarrow \frac{5.85V - 2.5V}{R_B} = 83.5 \frac{5 - 2.5}{1000}$$

$$R_B = 16.0479\Omega$$

$$I_E = \frac{V_{CC} - V_{CE,SAT}}{R_E} = \frac{5V - 0.2V}{1000} = 4.8mA$$

$$I_c = \frac{4.8 \text{mA}}{84.5/83.5} = 0.0047432A$$

$$I_B = \frac{0.0047432A}{83.5} = 5.6804 \times 10^{-5} A$$

$$R_B = \frac{V_{in} - V_{BE}}{I_B} = \frac{5 - 0.7}{56.804 \text{uA}} = 75698.89\Omega$$

$$16.0479 \le R_B \le 75698.89$$