

CONTACT MODEL: HERTZ-MINDLIN

This is soft-sphere model which is used to calculate particle-particle or particle wall contact. In both cases calculations are similar, however, when particle-wall contact is calculated, then particle radius and mass are considered as equivalent radius R^* and mass M^* .

Velocities:

$$\begin{split} & \bar{v}_{rel} = \bar{v}_2 - \bar{v}_1 + \overline{\omega}_1 \times \overline{r_c} - \overline{\omega}_2 \times \overline{r_c}_2 \\ & \bar{v}_{rel,n} = \bar{r}_n \cdot (\bar{r}_n \cdot \bar{v}_{rel}) \\ & \bar{v}_{rel,t} = \bar{v}_{rel} - \bar{v}_{rel,n} \end{split}$$

Additional parameters:

$$\alpha = \frac{\ln(e)}{\sqrt{\pi^2 + \ln^2(e)}}$$

$$R^* = \frac{r_1 \cdot r_2}{r_1 + r_2}$$

$$M^* = \frac{m_1 \cdot m_2}{m_1 + m_2}$$

$$E^* = \left(\frac{1 - v_1^2}{E_1} + \frac{1 - v_2^2}{E_2}\right)^{-1}$$

Normal force:

$$\begin{split} \xi_n &= r_1 + r_2 - |O_2 - O_1| \\ k_n &= 2E^* \sqrt{\xi_n \cdot R^*} \\ \overline{F_n} &= -\bar{r}_n \cdot \frac{2}{3} \xi_n \cdot k_n - \bar{r}_n \cdot sgn(\bar{v}_{rel,n} \cdot \bar{r}_n) \cdot 1.8257 \cdot \alpha \cdot |\bar{v}_{rel,n}| \cdot \sqrt{k_n \cdot M^*} \end{split}$$

Tangential force:

$$\begin{split} & \Delta \bar{\xi}_t = \bar{v}_{rel,t} \cdot \Delta t \\ & k_t = 8 \cdot G^* \cdot \sqrt{R^* \cdot \xi_n} \\ & \Delta \bar{F}_t = \left[k_t \cdot \Delta \bar{\xi}_t - 1.8257 \cdot \alpha \cdot \bar{v}_{rel,t} \cdot \sqrt{k_t \cdot M^*} \right] \\ & \bar{F}_{t,pr}^{cor} = \bar{F}_{t,pr} - \bar{r}_n \cdot \left(\bar{r}_n \cdot \bar{F}_{t,pr} \right) \end{split}$$



$$\bar{F}_{t,pr}^{cor} = \bar{F}_{t,pr}^{cor} \cdot |\bar{F}_{t,pr}|/|\bar{F}_{t,pr}^{cor}|$$

$$\overline{F}_t = \overline{F}_{t,pr}^{cor} + \Delta \overline{F}_t$$

if

$$|\overline{F}_t| > \mu_{sl} \cdot |\overline{F}_n|$$

then

$$\overline{F}_t = \mu_{sl} \cdot |\overline{F}_n| \cdot \frac{\overline{F}_t}{|\overline{F}_t|}$$

Rolling friction:

$$\overline{M}_{ro,1} = -\mu_{ro} \cdot |\overline{F}_n| \cdot r_1 \cdot \frac{\overline{\omega}_1}{|\overline{\omega}_1|}$$

$$\overline{M}_{ro,2} = -\mu_{ro} \cdot |\overline{F}_n| \cdot r_2 \cdot \frac{\overline{\omega}_2}{|\overline{\omega}_2|}$$

Summarized forces and moments acting on particle (wall):

$$\bar{F}_{tot} = \bar{F}_n + \bar{F}_t$$

$$\bar{F}_1 = \bar{F}_n + \bar{F}_t$$

$$\bar{F}_2 = -\bar{F}_n - \bar{F}_t$$

$$\overline{M}_{tot,1} = \overline{r_n} \times \overline{F}_t \cdot r_1 + \overline{M}_{ro,1}$$

$$\overline{M}_{tot,2} = -\overline{r_n} \times \overline{F}_t \cdot r_2 + \overline{M}_{ro,2}$$

Literature

Hertz H. (1882). Über die Berührung fester elastischer Körper. Journal die reine und angewandte Mathematik, 92, 156-171.

Tsuji Y., Tanaka T., Ishida T. (1992). Lagrangian numerical simulation of plug flow of cohesionless particles in horizontal pipe. *Powder Technology, 71 239-250.*



| Symbol | Description |
|-----------------------------------------------|----------------------------------------------------------|
| $\Delta ar{ar{\xi}}_t$ | Tangential displacement in the current step [m] |
| e | Restitution coefficient [-] |
| E * | Equivalent Young's modulus [Pa] |
| E_1, E_2 | Young's moduli of contact partners [Pa] |
| \overline{F}_n , \overline{F}_t | Force in normal and tangential directions [N] |
| $\overline{F}_{t,pr}$ | Tangential force on previous iteration [N] |
| G^* | Equivalent shear modulus [Pa] |
| $ar{M}_{ro}$ | Moment due to the rolling friction [N] |
| m_1, m_2 | Particle masses [kg] |
| M * | Equivalent mass [kg] |
| 0 ₁ , 0 ₂ | Centers of contact partners [m] |
| μ_{ro}, μ_{sl} | Coefficient of rolling friction and sliding friction [-] |
| \overline{v}_{rel} | Relative velocity [m/s] |
| $\overline{v}_1,\overline{v}_2$ | Translational velocities of contact partners [m/s] |
| r_1, r_2 | Particle radii [m] |
| R* | Equivalent radius [m] |
| $ar{r_c}$ | Contact vector [m] |
| \bar{r}_n | Normalized contact vector [-] |
| $\overline{\omega}_1,\overline{\omega}_2$ | Rotation velocities of particles [rad/s] |
| ξ_n | Normal overlap [m] |