

Mixing Langevin + ElastoHydroDynamic of cylinder

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1 Theoretical Framework

1.1 Fundamentals

Gibbs-Boltzmann distribution The Boltzmann distribution is a probability distribution that gives the probability of a certain state as a function of that state's energy and temperature of the system to which the distribution is applied. It is given as

$$p_i = \frac{\exp(-\beta \varepsilon_i)}{\sum_{j=1}^M \exp(-\beta \varepsilon_j)}$$

Langevin equation The original Langevin equation describes Brownian motion, the apparently random movement of a particle in a fluid due to collisions with molecules of the fluid,

$$m \frac{dv}{dt} = -\lambda v + \eta(t)$$

where v is the velocity of the particle, and m is the mass. The force acting on the particle is written as a sum of a viscous force proportional to the particles's velocity, and a noise term $\eta(t)$ representing the effect of the collisions with the molecules of the fluid. The force $\eta(t)$ has a Gaussian probability distribution with correlation function $\langle \eta_i(t) \eta_j(t') \rangle = 2\lambda k_B T \delta_{ij} \delta(t - t')$

There are two common choices of discretization: the Itô and the Stratonovich conventions. Discretization of the Langevin equation:

$$\frac{x_{t+\Delta} - x_t}{\Delta} = -V'(x_t) + \xi_t$$

with an associated discretization of the correlations:

$$\langle f[x(t)] \rangle \rightarrow \langle f(x_t) \rangle \quad \langle f[x(t)] \xi(t) \rangle \rightarrow \langle f(x_t) \xi_t \rangle \quad \langle f[x(t)] \dot{x}(t) \rangle \rightarrow \left\langle f(x_t) \frac{x_{t+\Delta} - x_t}{\Delta} \right\rangle$$

which leads to **Itô's chain rule**:

$$\frac{d}{dt} \langle f[x(t)] \rangle = \left\langle f'[x(t)] \frac{dx}{dt} \right\rangle + T \langle f''[x(t)] \rangle$$

Fokker-Planck equation In one spatial dimension x , for an Itô process driven by the standard Wiener process W_t and described by the stochastic differential equation (SDE)

$$dX_t = \mu(X_t, t)dt + \sigma(X_t, t)dW_t$$

with drift $\mu(X_t, t)$ and diffusion coefficient $D(X_t, t) = \sigma^2(X_t, t)/2$, the Fokker-Planck equation for the probability density $p(x, t)$ of the random variable X_t is

$$\frac{\partial}{\partial t} p(x, t) = -\frac{\partial}{\partial x} [\mu(x, t)p(x, t)] + \frac{\partial^2}{\partial x^2} [D(x, t)p(x, t)]$$

Derivation from the over-damped Langevin equation

Let $\mathbb{P}(x, t)$ be the probability density density function to find a particle in $[x, x + dx]$ at time t , and let x satisfy:

$$\dot{x}(t) = -V'(x) + \xi(t)$$

if f is a function, we have:

$$\frac{d}{dt} \langle f[x(t)] \rangle = \frac{d}{dt} \int \mathbb{P}(x, t) f(x) dx = \int \frac{\partial \mathbb{P}(x, t)}{\partial t} f(x) dx$$

but using Itô's chain rule:

$$\frac{d}{dt} \langle f[x(t)] \rangle = \left\langle f'[x(t)] \frac{dx}{dt} \right\rangle + T \langle f''[x(t)] \rangle$$

with Langevin's equation

$$\frac{d}{dt} \langle f[x(t)] \rangle = \langle f'[x(t)] \{-V'[x(t)] + \xi(t)\} \rangle + T \langle f''[x(t)] \rangle$$

since $\langle f'[x(t)] \xi(t) \rangle = 0$, we have

$$\frac{d}{dt} \langle f[x(t)] \rangle = \int \left[\frac{df(x)}{dx} \left(-\frac{dV(x)}{dx} \right) + T \frac{d^2 f(x)}{dx^2} \right] \mathbb{P}(x, t) dx$$

performing an integration by parts, and using that $\mathbb{P}(x, t)$ is a probability density vanishing at $x \rightarrow \infty$:

$$\int \frac{\partial \mathbb{P}(x, t)}{\partial t} f(x) dx = \int \frac{\partial}{\partial x} \left[\frac{dV(x)}{dx} + T \frac{\partial}{\partial x} \right] \mathbb{P}(x, t) f(x) dx$$

this is true for any function f , thus

$$\boxed{\frac{\partial \mathbb{P}(x, t)}{\partial t} = \frac{\partial}{\partial x} \left[\frac{dV(x)}{dx} + T \frac{\partial}{\partial x} \right] \mathbb{P}(x, t)}$$

It could be written as $\partial_t \mathbb{P}(x, t) = -H_{FP} \mathbb{P}(x, t)$ with H_{FP} the Fokker-Planck operator shown above.

1.2 Salez2015: Elastohydrodynamics of a sliding, spinning and sedimenting cylinder near a soft wall

arxiv: 1412.0162; Journal of Fluid Mechanics, 779 181 (2015)

This article describes the sedimentation, sliding, and spinning motions of a cylinder near a thin compressible elastic wall by thin-film lubrication dynamics. Below is the illustration.

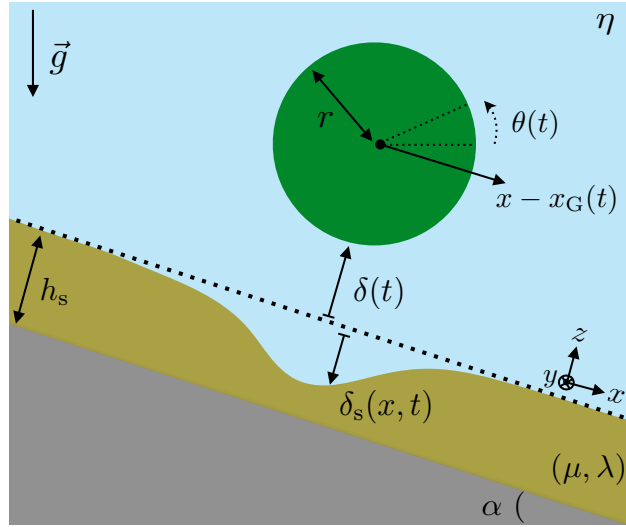


FIG. 1: Schematic of the system. A negatively buoyant cylinder (green) falls down under the acceleration of gravity \vec{g} , inside a viscous fluid (blue), in the vicinity of a thin soft wall (brown). The ensemble lies atop a tilted, infinitely rigid support (grey).

The deformation of the soft wall reads:

$$\delta_s(x, t) = -\frac{h_s p(x, t)}{2\mu + \lambda} \quad (\text{Salez2015.2})$$

as well as the dimensionless parameters: $z = Zr\epsilon$, $h = Hr\epsilon$, $\delta = \Delta r\epsilon$, $x = Xr\sqrt{2\epsilon}$, $x_G = X_G r\sqrt{2\epsilon}$, $\theta = \Theta\sqrt{2\epsilon}$, $t = Tr\sqrt{2\epsilon}/c$, $u = Uc$, and $p = P\eta c\sqrt{2}/(r\epsilon^{3/2})$; a free fall velocity scale $c = \sqrt{2gr\rho^*/\rho}$

and one dimensionless parameter ξ measures the ratio of the free fall time $\sqrt{\rho r \epsilon / (\rho^* g)}$ and the typical lubrication damping time $m \epsilon^{3/2} / \eta$ over which the inertia of the cylinder vanishes.

$$\xi = \frac{3\sqrt{2}\eta}{r^{3/2}\epsilon\sqrt{\rho\rho^*g}}\kappa = \frac{2h_s\eta\sqrt{g\rho^*}}{r^{3/2}\epsilon^{5/2}(2\mu + \lambda)\sqrt{\rho}}$$

With perturbation theory in first-order correction of κ , the soft compressible wall gives

$$\ddot{X}_G + \frac{2\epsilon\xi}{3} \frac{\dot{X}_G}{\sqrt{\Delta}} + \frac{\kappa\epsilon\xi}{6} \left[\frac{19}{4} \frac{\dot{\Delta}\dot{X}_G}{\Delta^{7/2}} - \frac{\dot{\Delta}\dot{\Theta}}{\Delta^{7/2}} + \frac{1}{2} \frac{\ddot{\Theta} - \ddot{X}_G}{\Delta^{5/2}} \right] - \sqrt{\frac{\epsilon}{2}} \sin \alpha = 0 \quad (\text{Salez2015.50})$$

$$\ddot{\Delta} + \xi \frac{\dot{\Delta}}{\Delta^{3/2}} + \frac{\kappa\xi}{4} \left[21 \frac{\dot{\Delta}^2}{\Delta^{9/2}} - \frac{(\dot{\Theta} - \dot{X}_G)^2}{\Delta^{7/2}} - \frac{15}{2} \frac{\ddot{\Delta}}{\Delta^{7/2}} \right] + \cos \alpha = 0 \quad (\text{Salez2015.51})$$

$$\ddot{\Theta} + \frac{4\epsilon\xi}{3} \frac{\dot{\Theta}}{\sqrt{\Delta}} + \frac{\kappa\epsilon\xi}{3} \left[\frac{19}{4} \frac{\dot{\Delta}\dot{\Theta}}{\Delta^{7/2}} - \frac{\dot{\Delta}\dot{X}_G}{\Delta^{7/2}} + \frac{1}{2} \frac{\ddot{X}_G - \ddot{\Theta}}{\Delta^{5/2}} \right] = 0 \quad (\text{Salez2015.52})$$

where Δ refers to z and X_G refers to x after the scaling. For the plan case, we set $\alpha = 0$.

1.3 David's note: Determining noise from deterministic forces

Here is the note of David Dean, considering the Brownian motion but only in two dimension (Δ, X). The rotation had been neglected ($\dot{\Theta} = 0$), and the second derivatives in the first-order correction of κ as well. To be clear, Fokker-Planck equation would be carefully discussed. Other personal comments are also written in Italic.

Consider the following deterministic equations (α refers to Δ, X these two directions)

$$dX_\alpha = V_\alpha dt \quad (\text{David.1})$$

and (\mathbf{X}, \mathbf{V} refer to the position and the velocity, respectively)

$$dV_\alpha = -U_\alpha dt - \nabla \phi(\mathbf{X}) dt \quad (\text{David.2})$$

We assume that U_α are generated by hydrodynamic interactions which do not however affect the equilibrium Gibbs-Boltzmann distribution which is

$$P_{eq}(\mathbf{X}, \mathbf{V}) = \frac{1}{Z} \exp \left(-\frac{\beta \mathbf{V}^2}{2} - \beta \phi(\mathbf{X}) \right) \quad (\text{David.3})$$

Exploit the Fokker-Planck operator (\dots refers the similar terms about X_α)

$$\frac{\partial P}{\partial t} = -H_{FP}P = \frac{\partial}{\partial x} \left[\frac{dV}{dx} P + T \frac{\partial}{\partial x} P \right] = \frac{\partial}{\partial V_\alpha} \left[(U_\alpha + \nabla_\alpha \phi) P + T \gamma_{\alpha\beta} \frac{\partial P}{\partial V_\beta} \right] + \frac{\partial}{\partial X_\alpha} [\dots]$$

Note $\frac{\partial P}{\partial X_\alpha} = P \left(-\beta \frac{\partial \phi}{\partial X_\alpha} \right)$ and $\frac{\partial P}{\partial V_\alpha} = P (-\beta V_\alpha)$. Consider the gravity $\phi(\mathbf{X}) = -mg\Delta$, and then we could derive the eq. *David.4*, regarding k_B as 1

$$\begin{aligned} \frac{\partial}{\partial X_\alpha} \left[\frac{dV}{dx} P + T \frac{\partial}{\partial x} P \right] &= \frac{\partial}{\partial X_\alpha} \left[\frac{dV}{dX_\alpha} P + T \frac{\partial}{\partial X_\alpha} P + T \frac{\partial}{\partial V_\alpha} P \right] \\ &= \frac{\partial}{\partial X_\alpha} \left[(\nabla_\alpha \phi) P + T \cdot P \left(-\beta \frac{\partial \phi}{\partial X_\alpha} \right) + T \frac{\partial}{\partial V_\alpha} P \right] = \frac{\partial}{\partial X_\alpha} \left[T \frac{\partial}{\partial V_\alpha} P \right] \\ &= \frac{\partial}{\partial X_\alpha} [T \cdot P (-\beta V_\alpha)] = -\frac{\partial}{\partial X_\alpha} V_\alpha P \end{aligned}$$

The Fokker Planck equation at finite temperature which introduces white noise and possibly temperature dependent drifts is $\phi(\mathbf{X})$ is

$$\frac{\partial P}{\partial t} = \frac{\partial}{\partial V_\alpha} \left[T \gamma_{\alpha\beta} \frac{\partial P}{\partial V_\beta} + U_\alpha P + \frac{\partial \phi}{\partial X_\alpha} P \right] - \frac{\partial}{\partial X_\alpha} V_\alpha P \quad (\text{David.4})$$

The last two terms would vanish since

$$\begin{aligned} \frac{\partial}{\partial V_\alpha} \left(\frac{\partial \phi}{\partial X_\alpha} P \right) &= \left(\frac{\partial}{\partial V_\alpha} \frac{\partial \phi}{\partial X_\alpha} \right) \cdot P + \frac{\partial \phi}{\partial X_\alpha} \cdot \frac{\partial P}{\partial V_\alpha} = \frac{\partial \phi}{\partial X_\alpha} \cdot P (-\beta V_\alpha) \\ \frac{\partial}{\partial X_\alpha} V_\alpha P &= \left(\frac{\partial V_\alpha}{\partial X_\alpha} \right) P + V_\alpha \left(\frac{\partial P}{\partial X_\alpha} \right) = V_\alpha \cdot P \cdot \left(-\beta \frac{\partial \phi}{\partial X_\alpha} \right) \end{aligned}$$

Therefore, at equilibrium $\frac{\partial P}{\partial t} = 0$

$$\frac{\partial P}{\partial t} = \frac{\partial}{\partial V_\alpha} \left[T \gamma_{\alpha\beta} \frac{\partial P}{\partial V_\beta} + U_\alpha P \right] = \frac{\partial}{\partial V_\alpha} [T \gamma_{\alpha\beta} P \cdot (-\beta V_\beta) + U_\alpha P] = \frac{\partial}{\partial V_\alpha} [(U_\alpha - \gamma_{\alpha\beta} V_\beta) \cdot P] = 0$$

We obtain the GB distribution for the steady state if

$$U_\alpha = \gamma_{\alpha\beta} V_\beta \quad (\text{David.5})$$

We have for small velocities that

$$U_\alpha = \lambda_{\alpha\beta}(\mathbf{X}) V_\beta + \Lambda_{\alpha\beta\gamma}(\mathbf{X}) V_\beta V_\gamma \quad (\text{David.6})$$

and so we find

$$\gamma_{\alpha\beta} V_\beta = \lambda_{\alpha\beta}(\mathbf{X}) V_\beta + \Lambda_{\alpha\beta\gamma}(\mathbf{X}) V_\beta V_\gamma \quad (\text{David.7})$$

Written this way the term $\lambda_{\alpha\beta}(\mathbf{X})$ is just the friction tensor in the absence of any elastic effects. We can thus write

$$\gamma_{\alpha\beta} = \lambda_{\alpha\beta} + \gamma_{2\alpha\beta} \quad (\text{David.8})$$

and we write

$$\gamma_{2\alpha\beta} = \Gamma_{\alpha\beta\gamma} V_\gamma \quad (\text{David.9})$$

and

$$\Gamma_{\alpha\beta\gamma}(\mathbf{X})V_\beta V_\gamma = \Lambda_{\alpha\beta\gamma}(\mathbf{X})V_\beta V_\gamma \quad (\text{David.10})$$

where we without loss of generality take $\Lambda_{\alpha\beta\gamma} = \Lambda_{\alpha\gamma\beta}$, which then gives

$$\Gamma_{\alpha\beta\gamma} + \Gamma_{\alpha\gamma\beta} = 2\Lambda_{\alpha\beta\gamma} \quad (\text{David.11})$$

We have to solve this system with the constraint that $\Gamma_{\alpha\beta\gamma}V_\gamma = \Gamma_{\beta\alpha\gamma}V_\gamma$. In Thomas' problem (*see subsection 1.2*) we have

$$\begin{aligned} \ddot{\Delta} + \xi \frac{\dot{\Delta}}{\Delta^{3/2}} + \frac{\kappa\xi}{4} \left[21 \frac{\dot{\Delta}^2}{\Delta^{9/2}} - \frac{(\dot{\Theta} - \dot{X}_G)^2}{\Delta^{7/2}} - \frac{15}{2} \frac{\ddot{\Delta}}{\Delta^{7/2}} \right] + \cos \alpha &= 0 \\ \ddot{X}_G + \frac{2\varepsilon\xi}{3} \frac{\dot{X}_G}{\sqrt{\Delta}} + \frac{\kappa\varepsilon\xi}{6} \left[\frac{19}{4} \frac{\dot{\Delta}\dot{X}_G}{\Delta^{7/2}} - \frac{\dot{\Delta}\dot{\Theta}}{\Delta^{7/2}} + \frac{1}{2} \frac{\ddot{\Theta} - \ddot{X}_G}{\Delta^{5/2}} \right] - \sqrt{\frac{\varepsilon}{2}} \sin \alpha &= 0 \end{aligned}$$

where Δ refers to z and X_G refers to x . Note $\dot{\Delta} = -U_z$ and $\dot{X}_G = -U_x$, we write

$$U_z = \xi \frac{V_z}{Z^{3/2}} + \frac{21\kappa\xi}{4} \frac{V_z^2}{Z^{9/2}} - \frac{\kappa\xi}{4} \frac{V_x^2}{Z^{7/2}} \quad (\text{David.12})$$

$$U_x = 2\xi\varepsilon \frac{V_x}{3Z^{1/2}} + \frac{19\kappa\xi\varepsilon}{24} \frac{V_z V_x}{Z^{7/2}} \quad (\text{David.13})$$

Note $\dot{\Delta} = V_z$ and $\dot{X}_G = V_x$, we could extract the relevant coefficients. But Attention! Here $\dot{\Theta}$ was assumed 0, and the second derivatives in first-order correlation had been ignored.

Form this we find that

$$\begin{aligned} \sum_{\alpha\beta} \Lambda_{z\alpha\beta} V_\alpha V_\beta &= \frac{21\kappa\xi}{4} \frac{V_z^2}{Z^{9/2}} - \frac{\kappa\xi}{4} \frac{V_x^2}{Z^{7/2}} \\ \sum_{\alpha\beta} \Lambda_{x\alpha\beta} V_\alpha V_\beta &= \frac{19\kappa\xi\varepsilon}{24} \frac{V_z V_x}{Z^{7/2}} \end{aligned} \quad (\text{David.14})$$

This gives the set of equations

$$\Gamma_{zzz} = \frac{21\kappa\xi}{4Z^{9/2}} \quad (\text{David.15})$$

$$\Gamma_{zxx} = -\frac{\kappa\xi}{4Z^{7/2}} \quad (\text{David.16})$$

$$\Gamma_{zxz} + \Gamma_{zzx} = 0 \quad (\text{David.17})$$

$$\Gamma_{xzz} = 0 \quad (\text{David.18})$$

$$\Gamma_{xxz} = 0 \quad (\text{David.19})$$

$$\Gamma_{xxz} + \Gamma_{xzx} = \frac{19\kappa\xi\varepsilon}{24Z^{7/2}} \quad (\text{David.20})$$

The symmetry $\Gamma_{\alpha\beta\gamma} = \Gamma_{\beta\alpha\gamma}$ now gives

$$\Gamma_{xxz} = \frac{19\kappa\xi\varepsilon}{24Z^{7/2}} - \Gamma_{xzx} = \frac{19\kappa\xi\varepsilon}{24Z^{7/2}} - \Gamma_{zxx} = \frac{\kappa\xi}{Z^{7/2}} \left(\frac{19\varepsilon}{24} + \frac{1}{4} \right) \quad (\text{David.21})$$

as well as

$$\Gamma_{zxx} = \Gamma_{zzx} = 0 \quad (\text{David.22})$$

The Langevin equation corresponding to this is, using the Itô convention,

$$\frac{dV_\alpha}{dt} = -U_\alpha - \frac{\partial\phi(\mathbf{X})}{\partial X_\alpha} + T \frac{\partial\gamma_{\alpha\beta}}{\partial V_\beta} + \eta_\alpha(t) \quad (\text{David.23})$$

which can be written as

$$\frac{dV_\alpha}{dt} = -U_\alpha - \frac{\partial\phi(\mathbf{X})}{\partial X_\alpha} + T\Gamma_{\alpha\beta\beta} + \eta_\alpha(t) \quad (\text{David.24})$$

where we use the Einstein summation convention and the noise correlator is given by

$$\langle \eta_\alpha(t) \eta_\beta(t') \rangle = 2T\gamma_{\alpha\beta} \delta(t - t') = 2T [\lambda_{\alpha\beta}(\mathbf{X}) + \Gamma_{\alpha\beta\gamma}(\mathbf{X}) V_\gamma] \delta(t - t') \quad (\text{David.25})$$

Putting this together we find (from eq. [David.24](#)) with all $\Gamma_{\alpha\beta\beta}$ only depending on Δ, X .

$$\begin{aligned} \frac{dV_z}{dt} &= -V'(Z) - \xi \frac{V_z}{Z^{3/2}} - \frac{21\kappa\xi}{4} \frac{V_z^2}{Z^{9/2}} + \frac{\kappa\xi V_x^2}{4Z^{7/2}} + T \left[\frac{21\kappa\xi}{4Z^{9/2}} - \frac{\kappa\xi}{4Z^{7/2}} \right] + \eta_z(t) \\ \frac{dV_x}{dt} &= -2\xi\varepsilon \frac{V_x}{3Z^{1/2}} - \frac{19\kappa\xi V_z V_x}{24Z^{7/2}} + \eta_x(t) \end{aligned} \quad (\text{David.26})$$

1.4 New Coefficients: $\lambda_{\alpha\beta}, \Gamma_{\alpha\beta\gamma}$ in 3D (Δ, X, Θ)

In this part, we would renew coefficients for the motion in 3D (Δ, X, Θ). Based on the previous subsection, we could repeat the calculation by Fokker-Planck operator, finding the similar results with additional terms about Θ .

For the sake of convenience, we re-write Thomas' differential equations (see subsection [1.2](#)) with \dot{v}_i , (and X refers to X_G)

$$\begin{aligned} -U_Z &= \dot{v}_\Delta = \ddot{\Delta} = F_\Delta(\Delta, v_\Delta, v_X, v_\Theta, \dot{v}_\Delta) \\ -U_X &= \dot{v}_X = \ddot{X} = F_X(\Delta, v_\Delta, v_X, v_\Theta, \dot{v}_X, \dot{v}_\Theta) \\ -U_\Theta &= \dot{v}_\Theta = \ddot{\Theta} = F_\Theta(\Delta, v_\Delta, v_X, v_\Theta, \dot{v}_X, \dot{v}_\Theta) \end{aligned} \quad (1)$$

However, we'd like to derive equations for each \dot{v} only depending on Δ and v , without \dot{v} . Therefore, we have to find the proper expression for each \dot{v}_i .

Consider the second derivative in the eq. [Salez2015.51](#),

$$\ddot{\Delta} + a_1 \frac{\dot{\Delta}}{\Delta^{3/2}} + a_2 \frac{\dot{\Delta}^2}{\Delta^{9/2}} + a_3 \frac{\dot{\Theta}^2}{\Delta^{7/2}} + a_3 \frac{\dot{X}^2}{\Delta^{7/2}} + a_4 \frac{\dot{\Theta}\dot{X}}{\Delta^{7/2}} + a_5 \frac{\ddot{\Delta}}{\Delta^{7/2}} + a_6 = 0 \quad (2)$$

$$\ddot{\Delta} = (a_1 \frac{\dot{\Delta}}{\Delta^{3/2}} + a_2 \frac{\dot{\Delta}^2}{\Delta^{9/2}} + a_3 \frac{\dot{\Theta}^2}{\Delta^{7/2}} + a_3 \frac{\dot{X}^2}{\Delta^{7/2}} + a_4 \frac{\dot{\Theta}\dot{X}}{\Delta^{7/2}} + a_6) \times \frac{-1}{1 + a_5/\Delta^{7/2}} \quad (3)$$

We know that $a_1 = \xi$, $a_2 = \frac{21\kappa\xi}{4}$, $a_3 = -\frac{\kappa\xi}{4}$, $a_4 = \frac{\kappa\xi}{2}$, $a_5 = -\frac{15\kappa\xi}{8}$, $a_6 = \cos(\alpha = 0) = 1$. After simple calculation, we could obtain \dot{v}_Δ (\dot{v}_z) namely $\ddot{\Delta}$

$$-\dot{v}_\Delta = U_z = \frac{8\Delta^{9/2} + 2\xi(-\Delta\kappa v_X^2 + 4\Delta^3 v_z + 21\kappa v_z^2 + 2\Delta\kappa v_X v_\theta - \Delta\kappa v_\theta^2)}{8\Delta^{9/2} - 15\Delta\kappa\xi} \quad (4)$$

Similarly, we write the eqs [Salez2015.50](#) and [Salez2015.52](#) as

$$\ddot{X} + b_1 \frac{\dot{X}}{\sqrt{\Delta}} + b_2 \frac{\dot{\Delta}\dot{X}}{\Delta^{7/2}} + b_3 \frac{\dot{\Delta}\dot{\Theta}}{\Delta^{7/2}} + b_4 \frac{\ddot{\Theta}}{\Delta^{5/2}} + b_5 \frac{\ddot{X}}{\Delta^{5/2}} + b_6 = 0 \quad (5)$$

$$\ddot{\Theta} + c_1 \frac{\dot{\Theta}}{\sqrt{\Delta}} + c_2 \frac{\dot{\Delta}\dot{\Theta}}{\Delta^{7/2}} + c_3 \frac{\dot{\Delta}\dot{X}}{\Delta^{7/2}} + c_4 \frac{\ddot{X}}{\Delta^{5/2}} + c_5 \frac{\ddot{\Theta}}{\Delta^{5/2}} + c_6 = 0 \quad (6)$$

with all coefficients we need: $b_1 = \frac{2\varepsilon\xi}{3}$, $b_2 = \frac{19\kappa\xi\varepsilon}{24}$, $b_3 = -\frac{\kappa\xi\varepsilon}{6}$, $b_4 = \frac{\kappa\xi\varepsilon}{12}$, $b_5 = -\frac{\kappa\xi\varepsilon}{12}$, $b_6 = \sin(\alpha = 0) = 0$; and $c_1 = \frac{4\varepsilon\xi}{3}$, $c_2 = \frac{19\kappa\xi\varepsilon}{12}$, $c_3 = -\frac{\kappa\xi\varepsilon}{3}$, $c_4 = \frac{\kappa\xi\varepsilon}{6}$, $c_5 = -\frac{\kappa\xi\varepsilon}{6}$, $c_6 = 0$. For this system of linear equations, the coefficient matrix has full rank.

$$\begin{pmatrix} 1 + (b_5) & (b_4) \\ (c_4) & 1 + (c_5) \end{pmatrix} \begin{pmatrix} \ddot{X} \\ \ddot{\Theta} \end{pmatrix} = \begin{pmatrix} (b_1 + b_2 + b_3 + b_6) \\ (c_1 + c_2 + c_3 + c_6) \end{pmatrix}$$

Then we could solve $\ddot{X} = \dot{v}_X$ and $\ddot{\Theta} = \dot{v}_\Theta$ directly

$$-\dot{v}_X = U_X = \frac{\varepsilon\xi \left(\kappa \left(16\Delta^3 \varepsilon\xi + \left(-24\Delta^{5/2} + 23\varepsilon\kappa\xi \right) v_z \right) v_\theta + v_X \left(-4\varepsilon\kappa^2\xi v_z + \left(6\Delta^{5/2} - \varepsilon\kappa\xi \right) (16\Delta^3 + 19\kappa v_\theta) \right) \right)}{36(4\Delta^6 - \Delta^{7/2}\varepsilon\kappa\xi)} \quad (7)$$

$$-\dot{v}_\Theta = U_\Theta = \frac{\varepsilon\xi \left(\left(16\Delta^3 \left(12\Delta^{5/2} - \varepsilon\kappa\xi \right) + \kappa \left(228\Delta^{5/2} - 23\varepsilon\kappa\xi \right) v_z \right) v_\theta + \kappa v_X \left(\left(-48\Delta^{5/2} + 4\varepsilon\kappa\xi \right) v_z + \varepsilon\xi (16\Delta^3 + 19\kappa v_\theta) \right) \right)}{36(4\Delta^6 - \Delta^{7/2}\varepsilon\kappa\xi)} \quad (8)$$

Compare with the eq. [1](#), we finally remove the second derivatives inside each expression

$$\begin{aligned} \dot{v}_\Delta &= F_\Delta(\Delta, v_\Delta, v_X, v_\Theta) \\ \dot{v}_X &= F_X(\Delta, v_\Delta, v_X, v_\Theta) \\ \dot{v}_\Theta &= F_\Theta(\Delta, v_\Delta, v_X, v_\Theta) \end{aligned} \quad (9)$$

See eqs [David.5](#) ~ [David.9](#), we could extract these $\lambda_{\alpha\beta}$ by

$$\lambda_{\alpha\beta} = \text{Coefficient}[U_\alpha, v_\beta] - \text{Coefficient}[U_\alpha, v_\beta v_\gamma] \times v_\gamma \quad (10)$$

and $\Gamma_{\alpha\beta\beta}$ by

$$\Gamma_{\alpha\beta\beta} = \text{Coefficient}[U_\alpha, v_\beta v_\beta] \quad (11)$$

As for $\Gamma_{\alpha\beta\gamma}$, we should resolve them by

$$2\Lambda_{\alpha\beta\gamma} = \text{Coefficient}[U_\alpha, v_\beta v_\gamma] = \Gamma_{\alpha\beta\gamma} + \Gamma_{\alpha\gamma\beta} \quad (12)$$

as well as the constraint $\Gamma_{\alpha\beta\gamma} = \Gamma_{\beta\alpha\gamma}$.

After some calculations with the help of *Mathematica*, we list all $\lambda_{\alpha\beta}$

$$\begin{aligned} \lambda_{zz} &= \frac{8\Delta^2\xi}{8\Delta^{7/2} - 15\kappa\xi} \\ \lambda_{xx} &= -\frac{4\epsilon\xi \left(-6\Delta^{5/2} + \epsilon\kappa\xi\right)}{36\Delta^3 - 9\sqrt{\Delta}\epsilon\kappa\xi} \\ \lambda_{\theta\theta} &= -\frac{4\epsilon\xi \left(-12\Delta^{5/2} + \epsilon\kappa\xi\right)}{36\Delta^3 - 9\sqrt{\Delta}\epsilon\kappa\xi} \end{aligned} \quad (13)$$

$$\lambda_{x\theta} = \lambda_{\theta x} = \frac{4\epsilon^2\kappa\xi^2}{36\Delta^3 - 9\sqrt{\Delta}\epsilon\kappa\xi} \quad (14)$$

$$\lambda_{zx} = \lambda_{xz} = \lambda_{z\theta} = \lambda_{\theta z} = 0 \quad (15)$$

and then $\Gamma_{\alpha\beta\gamma}$

$$\begin{aligned} \Gamma_{zzz} &= \frac{42\kappa\xi}{8\Delta^{9/2} - 15\Delta\kappa\xi} \\ \Gamma_{xzx} = \Gamma_{zxx} &= \frac{2\kappa\xi}{-8\Delta^{7/2} + 15\kappa\xi} \end{aligned} \quad (16)$$

$$\begin{aligned} \Gamma_{\theta z\theta} = \Gamma_{z\theta\theta} &= \frac{2\kappa\xi}{-8\Delta^{7/2} + 15\kappa\xi} \\ \Gamma_{zxz} = \Gamma_{zzx} = \Gamma_{zz\theta} = \Gamma_{z\theta z} &= 0 \end{aligned} \quad (17)$$

$$\Gamma_{xzz} = \Gamma_{xxz} = \Gamma_{\theta zz} = \Gamma_{\theta\theta\theta} = 0 \quad (18)$$

$$\Gamma_{\theta xx} = \Gamma_{x\theta x} = \Gamma_{x\theta\theta} = \Gamma_{\theta x\theta} = 0 \quad (19)$$

$$\begin{aligned}
\Gamma_{xxz} &= \frac{1}{9} \kappa \xi \left(\frac{18}{8\Delta^{7/2} - 15\kappa\xi} + \frac{\epsilon^2 \kappa \xi}{-4\Delta^6 + \Delta^{7/2} \epsilon \kappa \xi} \right) \\
\Gamma_{xx\theta} &= \frac{19\epsilon \kappa \xi \left(-6\Delta^{5/2} + \epsilon \kappa \xi \right)}{-144\Delta^6 + 36\Delta^{7/2} \epsilon \kappa \xi} \\
\Gamma_{\theta\theta x} &= \frac{19\epsilon^2 \kappa^2 \xi^2}{36(4\Delta^6 - \Delta^{7/2} \epsilon \kappa \xi)} \\
\Gamma_{\theta\theta z} &= \frac{\epsilon \kappa \xi \left(-228\Delta^{5/2} + 23\epsilon \kappa \xi \right)}{-144\Delta^6 + 36\Delta^{7/2} \epsilon \kappa \xi}
\end{aligned} \tag{20}$$

$$\begin{aligned}
\Gamma_{zx\theta} = \Gamma_{xz\theta} &= -\frac{25}{18\Delta} - \frac{19\epsilon \kappa \xi}{72\Delta^{7/2}} + \frac{2\kappa\xi}{8\Delta^{7/2} - 15\kappa\xi} + \frac{50\Delta^{3/2}}{36\Delta^{5/2} - 9\epsilon \kappa \xi} \\
\Gamma_{z\theta x} = \Gamma_{\theta zx} &= \frac{25}{18\Delta} + \frac{19\epsilon \kappa \xi}{72\Delta^{7/2}} + \frac{2\kappa\xi}{8\Delta^{7/2} - 15\kappa\xi} + \frac{50\Delta^{3/2}}{9(-4\Delta^{5/2} + \epsilon \kappa \xi)} \\
\Gamma_{x\theta z} = \Gamma_{\theta xz} &= \frac{2}{15} - \frac{1}{2\Delta} - \frac{3\epsilon \kappa \xi}{8\Delta^{7/2}} + \frac{16}{15\left(-8 + \frac{15\kappa\xi}{\Delta^{7/2}}\right)} + \frac{1}{2\Delta - \frac{\epsilon \kappa \xi}{2\Delta^{3/2}}}
\end{aligned} \tag{21}$$

1.5 $\gamma_{\alpha\beta}$ and linear approximation of κ

Since $\gamma_{\alpha\beta} = \lambda_{\alpha\beta} + \Gamma_{\alpha\beta\gamma} V_\gamma$, we have

$$\begin{aligned}
\gamma_{zz} &= \frac{8\Delta^2 \xi}{8\Delta^{7/2} - 15\kappa\xi} + \frac{42\kappa\xi v_z}{8\Delta^{9/2} - 15\Delta\kappa\xi} \\
&= \frac{\xi}{\Delta^{3/2}} + \left(\frac{15\xi^2}{8\Delta^5} + \frac{21\xi v_z}{4\Delta^{9/2}} \right) \kappa + \left(\frac{225\xi^3}{64\Delta^{17/2}} + \frac{315\xi^2 v_z}{32\Delta^8} \right) \kappa^2 + O[\kappa]^3
\end{aligned} \tag{22}$$

$$\begin{aligned}
\gamma_{zx} = \gamma_{xz} &= \frac{2\kappa\xi v_X}{-8\Delta^{7/2} + 15\kappa\xi} + \left(-\frac{25}{18\Delta} - \frac{19\epsilon \kappa \xi}{72\Delta^{7/2}} + \frac{2\kappa\xi}{8\Delta^{7/2} - 15\kappa\xi} + \frac{50\Delta^{3/2}}{36\Delta^{5/2} - 9\epsilon \kappa \xi} \right) v_\theta \\
&= -\frac{(\xi(3v_X - 3v_\theta - \epsilon v_\theta)) \kappa}{12\Delta^{7/2}} + \frac{5\xi^2(-27v_X + 27v_\theta + 5\Delta\epsilon^2 v_\theta) \kappa^2}{288\Delta^7} + O[\kappa]^3
\end{aligned} \tag{23}$$

$$\begin{aligned}
\gamma_{z\theta} = \gamma_{\theta z} &= \left(\frac{25}{18\Delta} + \frac{19\epsilon \kappa \xi}{72\Delta^{7/2}} + \frac{2\kappa\xi}{8\Delta^{7/2} - 15\kappa\xi} + \frac{50\Delta^{3/2}}{9(-4\Delta^{5/2} + \epsilon \kappa \xi)} \right) v_X + \frac{2\kappa\xi v_\theta}{-8\Delta^{7/2} + 15\kappa\xi} \\
&= -\frac{(\xi(-3v_X + \epsilon v_X + 3v_\theta)) \kappa}{12\Delta^{7/2}} - \frac{5(\xi^2(-27v_X + 5\Delta\epsilon^2 v_X + 27v_\theta)) \kappa^2}{288\Delta^7} + O[\kappa]^3
\end{aligned} \tag{24}$$

$$\begin{aligned}
\gamma_{xx} &= -\frac{4\epsilon\xi(-6\Delta^{5/2} + \epsilon\kappa\xi)}{36\Delta^3 - 9\sqrt{\Delta}\epsilon\kappa\xi} + \frac{1}{9}\kappa\xi\left(\frac{18}{8\Delta^{7/2} - 15\kappa\xi} + \frac{\epsilon^2\kappa\xi}{-4\Delta^6 + \Delta^{7/2}\epsilon\kappa\xi}\right)v_z + \frac{19\epsilon\kappa\xi(-6\Delta^{5/2} + \epsilon\kappa\xi)v_\theta}{-144\Delta^6 + 36\Delta^{7/2}\epsilon\kappa\xi} \\
&= \frac{2\epsilon\xi}{3\sqrt{\Delta}} + \frac{(4\sqrt{\Delta}\epsilon^2\xi^2 + 18\xi v_z + 57\epsilon\xi v_\theta)\kappa}{72\Delta^{7/2}} + \left(\frac{\epsilon^3\xi^3}{72\Delta^{11/2}} - \frac{(-135 + 8\Delta\epsilon^2)\xi^2 v_z}{288\Delta^7} + \frac{19\epsilon^2\xi^2 v_\theta}{288\Delta^6}\right)\kappa^2 + O[\kappa]^3
\end{aligned} \tag{25}$$

$$\begin{aligned}
\gamma_{\theta\theta} &= -\frac{4\epsilon\xi(-12\Delta^{5/2} + \epsilon\kappa\xi)}{36\Delta^3 - 9\sqrt{\Delta}\epsilon\kappa\xi} + \frac{19\epsilon^2\kappa^2\xi^2 v_X}{36(4\Delta^6 - \Delta^{7/2}\epsilon\kappa\xi)} + \kappa\xi\left(\frac{23\epsilon}{36\Delta^{7/2}} + \frac{2}{8\Delta^{7/2} - 15\kappa\xi} + \frac{34\epsilon}{36\Delta^{7/2} - 9\Delta\epsilon\kappa\xi}\right)v_z \\
&= \frac{4\epsilon\xi}{3\sqrt{\Delta}} + \left(\frac{2\epsilon^2\xi^2}{9\Delta^3} + \frac{(3 + 19\epsilon)\xi v_z}{12\Delta^{7/2}}\right)\kappa + \left(\frac{\epsilon^3\xi^3}{18\Delta^{11/2}} + \frac{19\epsilon^2\xi^2 v_X}{144\Delta^6} + \frac{(135 + 68\Delta\epsilon^2)\xi^2 v_z}{288\Delta^7}\right)\kappa^2 + O[\kappa]^3
\end{aligned} \tag{26}$$

$$\begin{aligned}
\gamma_{x\theta} = \gamma_{\theta x} &= \frac{4\epsilon^2\kappa\xi^2}{36\Delta^3 - 9\sqrt{\Delta}\epsilon\kappa\xi} + \left(\frac{2}{15} - \frac{1}{2\Delta} - \frac{3\epsilon\kappa\xi}{8\Delta^{7/2}} + \frac{16}{15\left(-8 + \frac{15\kappa\xi}{\Delta^{7/2}}\right)} + \frac{1}{2\Delta - \frac{\epsilon\kappa\xi}{2\Delta^{3/2}}}\right)v_z \\
&= \left(\frac{\epsilon^2\xi^2}{9\Delta^3} - \frac{(\xi + \epsilon\xi)v_z}{4\Delta^{7/2}}\right)\kappa + \left(\frac{\epsilon^3\xi^3}{36\Delta^{11/2}} + \frac{(-15 + \Delta\epsilon^2)\xi^2 v_z}{32\Delta^7}\right)\kappa^2 + O[\kappa]^3
\end{aligned} \tag{27}$$

Finally, we have obtained the all components of $\gamma_{\alpha\beta}$.

$$\boldsymbol{\gamma} = \begin{pmatrix} \gamma_{zz} & \gamma_{zx} & \gamma_{z\theta} \\ \gamma_{xz} & \gamma_{xx} & \gamma_{x\theta} \\ \gamma_{\theta z} & \gamma_{\theta x} & \gamma_{\theta\theta} \end{pmatrix}$$

As we could see, this is a symmetric matrix. In addition, only three diagonal elements, namely $\gamma_{zz}, \gamma_{xx}, \gamma_{\theta\theta}$ have zero-order term of κ , which describes the compliance. In genenral, this parameter is about $10^{-4} \sim 10^{-3}$. Hence we just consider the first-order correction in the following calculations.

Up to now, we have elucidated the drift force. Indeed, there exist the external potential (like gravity) and white noises at the same time.

$$\dot{v}_i = F_i + T F_i^{drift} + \eta_i \tag{28}$$

Since three components are coupled, the equation turns to

$$\begin{pmatrix} \dot{v}_\Delta \\ \dot{v}_X \\ \dot{v}_\Theta \end{pmatrix} = - \begin{pmatrix} \gamma_{zz} & \gamma_{zx} & \gamma_{z\theta} \\ \gamma_{xz} & \gamma_{xx} & \gamma_{x\theta} \\ \gamma_{\theta z} & \gamma_{\theta x} & \gamma_{\theta\theta} \end{pmatrix} \begin{pmatrix} v_\Delta \\ v_X \\ v_\Theta \end{pmatrix} + \begin{pmatrix} \eta_\Delta \\ \eta_X \\ \eta_\Theta \end{pmatrix} \tag{29}$$

where the noise correlator has been shown in the eq. [David.25](#):

$$\langle \eta_\alpha(t) \eta_\beta(t') \rangle = 2T \gamma_{\alpha\beta} \delta(t - t') = 2T [\lambda_{\alpha\beta}(\mathbf{X}) + \Gamma_{\alpha\beta\gamma}(\mathbf{X}) V_\gamma] \delta(t - t')$$

So we'd like to find the expression of $\gamma^{1/2}$.

Suppose that

$$\gamma = \Psi + \kappa \Phi + O[\kappa]^2 \quad (30)$$

where Ψ is zero-order matrix of κ , and Φ the first-order one. So $\gamma^{1/2}$ would show a form such as $\gamma^{1/2} \approx \psi + \kappa \chi$,

$$\gamma = \gamma^{1/2} \gamma^{1/2} = (\psi + \kappa \chi)(\psi + \kappa \chi) = \psi \psi + \kappa(\psi \chi + \chi \psi) + O[\kappa]^2$$

we have $\Phi = \chi \psi + \psi \chi$, and $\psi = \sqrt{\Psi}$. Note Ψ is a symmetric matrix and all non-diagonal elements are equal to 0.

$$\Psi = \begin{pmatrix} \lambda_1 & 0 & 0 \\ 0 & \lambda_2 & 0 \\ 0 & 0 & \lambda_3 \end{pmatrix} = \begin{pmatrix} \frac{\xi}{\Delta^{3/2}} & 0 & 0 \\ 0 & \frac{2\epsilon\xi}{3\sqrt{\Delta}} & 0 \\ 0 & 0 & \frac{4\epsilon\xi}{3\sqrt{\Delta}} \end{pmatrix} \quad (31)$$

Then we could solve all components of χ

$$\begin{aligned} \chi_{11} &= \frac{3\xi (5\xi + 14\sqrt{\Delta}v_z)}{16\Delta^5 \sqrt{\frac{\xi}{\Delta^{3/2}}}} \\ \chi_{22} &= \frac{\xi (18v_z + \epsilon (4\sqrt{\Delta}\epsilon\xi + 57v_\theta))}{48\sqrt{6}\Delta^{7/2} \sqrt{\frac{\epsilon\xi}{\sqrt{\Delta}}}} \\ \chi_{33} &= \frac{\xi (8\sqrt{\Delta}\epsilon^2\xi + (9 + 57\epsilon)v_z)}{48\sqrt{3}\Delta^{7/2} \sqrt{\frac{\epsilon\xi}{\sqrt{\Delta}}}} \end{aligned} \quad (32)$$

$$\begin{aligned} \chi_{12} = \chi_{21} &= \frac{\xi (-3v_X + (3 + \epsilon)v_\theta)}{4\Delta^{7/2} \left(3\sqrt{\frac{\xi}{\Delta^{3/2}}} + \sqrt{6}\sqrt{\frac{\epsilon\xi}{\sqrt{\Delta}}} \right)} \\ \chi_{13} = \chi_{31} &= -\frac{\xi (3v_\theta + (\epsilon - 3)v_X)}{4\Delta^{7/2} \left(3\sqrt{\frac{\xi}{\Delta^{3/2}}} + 2\sqrt{3}\sqrt{\frac{\epsilon\xi}{\sqrt{\Delta}}} \right)} \\ \chi_{23} = \chi_{32} &= \frac{\xi (4\sqrt{\Delta}\epsilon^2\xi - 9(1 + \epsilon)v_z)}{12\sqrt{3} (2 + \sqrt{2}) \Delta^{7/2} \sqrt{\frac{\epsilon\xi}{\sqrt{\Delta}}}} \end{aligned} \quad (33)$$