

# Mixing Langevin + ElastoHydroDynamic of cylinder

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# 1 Framework Introduction

## 1.1 Theoretical Fundamentals

*Here are fundamentals used in the following parts, including Gibbs-Boltzmann distribution, Langevin equation, Fokker-Planck equation.*

**Gibbs-Boltzmann distribution** The Boltzmann distribution is a probability distribution that gives the probability of a certain state as a function of that state's energy and temperature of the system to which the distribution is applied. It is given as

$$p_i = \frac{\exp(-\beta \varepsilon_i)}{\sum_{j=1}^M \exp(-\beta \varepsilon_j)}$$

**Langevin equation** The original Langevin equation describes Brownian motion, the apparently random movement of a particle in a fluid due to collisions with molecules of the fluid,

$$m \frac{dv}{dt} = -\lambda v + \eta(t)$$

where  $v$  is the velocity of the particle, and  $m$  is the mass. The force acting on the particle is written as a sum of a viscous force proportional to the particles's velocity, and a noise term  $\eta(t)$  representing the effect of the collisions with the molecules of the fluid. The force  $\eta(t)$  has a Gaussian probability distribution with correlation function  $\langle \eta_i(t) \eta_j(t') \rangle = 2\lambda k_B T \delta_{ij} \delta(t - t')$

There are two common choices of discretization: the Itô and the Stratonovich conventions. Discretization of the Langevin equation:

$$\frac{x_{t+\Delta} - x_t}{\Delta} = -V'(x_t) + \xi_t$$

with an associated discretization of the correlations:

$$\langle f[x(t)] \rangle \rightarrow \langle f(x_t) \rangle \quad \langle f[x(t)] \xi(t) \rangle \rightarrow \langle f(x_t) \xi_t \rangle \quad \langle f[x(t)] \dot{x}(t) \rangle \rightarrow \left\langle f(x_t) \frac{x_{t+\Delta} - x_t}{\Delta} \right\rangle$$

which leads to **Itô's chain rule**:

$$\frac{d}{dt} \langle f[x(t)] \rangle = \left\langle f'[x(t)] \frac{dx}{dt} \right\rangle + T \langle f''[x(t)] \rangle$$

**Fokker-Planck equation** In one spatial dimension  $x$ , for an Itô process driven by the standard Wiener process  $W_t$  and described by the stochastic differential equation (SDE)

$$dX_t = \mu(X_t, t)dt + \sigma(X_t, t)dW_t$$

with drift  $\mu(X_t, t)$  and diffusion coefficient  $D(X_t, t) = \sigma^2(X_t, t)/2$ , the Fokker-Planck equation for the probability density  $p(x, t)$  of the random variable  $X_t$  is

$$\frac{\partial}{\partial t} p(x, t) = -\frac{\partial}{\partial x} [\mu(x, t)p(x, t)] + \frac{\partial^2}{\partial x^2} [D(x, t)p(x, t)]$$

Derivation from the over-damped Langevin equation

Let  $\mathbb{P}(x, t)$  be the probability density density function to find a particle in  $[x, x + dx]$  at time  $t$ , and let  $x$  satisfy:

$$\dot{x}(t) = -V'(x) + \xi(t)$$

if  $f$  is a function, we have:

$$\frac{d}{dt} \langle f[x(t)] \rangle = \frac{d}{dt} \int \mathbb{P}(x, t) f(x) dx = \int \frac{\partial \mathbb{P}(x, t)}{\partial t} f(x) dx$$

but using Itô's chain rule:

$$\frac{d}{dt} \langle f[x(t)] \rangle = \left\langle f'[x(t)] \frac{dx}{dt} \right\rangle + T \langle f''[x(t)] \rangle$$

with Langevin's equation

$$\frac{d}{dt} \langle f[x(t)] \rangle = \langle f'[x(t)] \{-V'[x(t)] + \xi(t)\} \rangle + T \langle f''[x(t)] \rangle$$

since  $\langle f'[x(t)] \xi(t) \rangle = 0$ , we have

$$\frac{d}{dt} \langle f[x(t)] \rangle = \int \left[ \frac{df(x)}{dx} \left( -\frac{dV(x)}{dx} \right) + T \frac{d^2 f(x)}{dx^2} \right] \mathbb{P}(x, t) dx$$

performing an integration by parts, and using that  $\mathbb{P}(x, t)$  is a probability density vanishing at  $x \rightarrow \infty$ :

$$\int \frac{\partial \mathbb{P}(x, t)}{\partial t} f(x) dx = \int \frac{\partial}{\partial x} \left[ \frac{dV(x)}{dx} + T \frac{\partial}{\partial x} \right] \mathbb{P}(x, t) f(x) dx$$

this is true for any function  $f$ , thus

$$\boxed{\frac{\partial \mathbb{P}(x, t)}{\partial t} = \frac{\partial}{\partial x} \left[ \frac{dV(x)}{dx} + T \frac{\partial}{\partial x} \right] \mathbb{P}(x, t)}$$

It could be written as  $\partial_t \mathbb{P}(x, t) = -H_{FP} \mathbb{P}(x, t)$  with  $H_{FP}$  the Fokker-Planck operator shown above.

## 1.2 Salez2015: Elastohydrodynamics of a sliding, spinning and sedimenting cylinder near a soft wall

Here we look at Thomas' publication (arxiv: 1412.0162) on *Journal of Fluid Mechanics*, 779 181 (2015). This article describes the sedimentation, sliding, and spinning motions of a cylinder near a thin compressible elastic wall by thin-film lubrication dynamics. Below is the illustration:

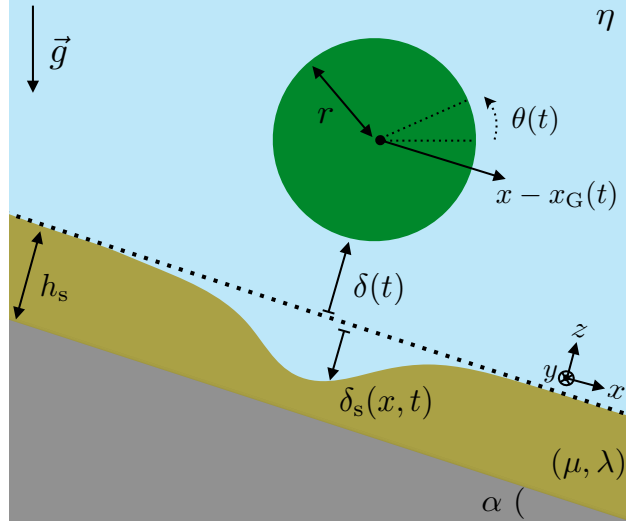


FIG. 1: Schematic of the system. A negatively buoyant cylinder (green) falls down under the acceleration of gravity  $\vec{g}$ , inside a viscous fluid (blue), in the vicinity of a thin soft wall (brown). The ensemble lies atop a tilted, infinitely rigid support (grey).

The deformation of the soft wall reads:

$$\delta_s(x, t) = -\frac{h_s p(x, t)}{2\mu + \lambda} \quad (\text{Salez2015.2})$$

as well as the dimensionless parameters:  $z = Zr\epsilon$ ,  $h = Hr\epsilon$ ,  $\delta = \Delta r\epsilon$ ,  $x = Xr\sqrt{2\epsilon}$ ,  $x_G = X_G r\sqrt{2\epsilon}$ ,  $\theta = \Theta\sqrt{2\epsilon}$ ,  $t = Tr\sqrt{2\epsilon}/c$ ,  $u = Uc$ , and  $p = P\eta c\sqrt{2}/(r\epsilon^{3/2})$ ; a free fall velocity scale  $c = \sqrt{2gr\rho^*/\rho}$  and one dimensionless parameter  $\xi$  measures the ratio of the free fall time  $\sqrt{\rho r\epsilon}/(\rho^* g)$  and the typical lubrication damping time  $m\epsilon^{3/2}/\eta$  over which the inertia of the cylinder vanishes.

$$\xi = \frac{3\sqrt{2}\eta}{r^{3/2}\epsilon\sqrt{\rho\rho^*g}}\kappa = \frac{2h_s\eta\sqrt{g\rho^*}}{r^{3/2}\epsilon^{5/2}(2\mu + \lambda)\sqrt{\rho}}$$

With perturbation theory in first-order correction of  $\kappa$ , the soft compressible wall gives

$$\ddot{X}_G + \frac{2\epsilon\xi}{3} \frac{\dot{X}_G}{\sqrt{\Delta}} + \frac{\kappa\epsilon\xi}{6} \left[ \frac{19}{4} \frac{\dot{\Delta}\dot{X}_G}{\Delta^{7/2}} - \frac{\dot{\Delta}\dot{\Theta}}{\Delta^{7/2}} + \frac{1}{2} \frac{\ddot{\Theta} - \ddot{X}_G}{\Delta^{5/2}} \right] - \sqrt{\frac{\epsilon}{2}} \sin \alpha = 0 \quad (\text{Salez2015.50})$$

$$\ddot{\Delta} + \xi \frac{\dot{\Delta}}{\Delta^{3/2}} + \frac{\kappa \xi}{4} \left[ 21 \frac{\dot{\Delta}^2}{\Delta^{9/2}} - \frac{(\dot{\Theta} - \dot{X}_G)^2}{\Delta^{7/2}} - \frac{15}{2} \frac{\ddot{\Delta}}{\Delta^{7/2}} \right] + \cos \alpha = 0 \quad (\text{Salez2015.51})$$

$$\ddot{\Theta} + \frac{4\varepsilon\xi}{3} \frac{\dot{\Theta}}{\sqrt{\Delta}} + \frac{\kappa\varepsilon\xi}{3} \left[ \frac{19}{4} \frac{\dot{\Delta}\dot{\Theta}}{\Delta^{7/2}} - \frac{\dot{\Delta}\dot{X}_G}{\Delta^{7/2}} + \frac{1}{2} \frac{\ddot{X}_G - \ddot{\Theta}}{\Delta^{5/2}} \right] = 0 \quad (\text{Salez2015.52})$$

where  $\Delta$  refers to  $z$  and  $X_G$  refers to  $x$  after the scaling. For the plan case, we set  $\alpha = 0$ .

### 1.3 David's note: Determining noise from deterministic forces

*Here is the note of David Dean, considering the Brownian motion but only in two dimension  $(\Delta, X)$ . The rotation had been neglected ( $\dot{\Theta} = 0$ ), and the second derivatives in the first-order correction of  $\kappa$  as well. To be clear, Fokker-Planck equation would be carefully discussed. Other personal comments are also written in *Italic*.*

Consider the following deterministic equations ( $\alpha$  refers to  $\Delta, X$  these two directions)

$$dX_\alpha = V_\alpha dt \quad (\text{David.1})$$

and  $(\mathbf{X}, \mathbf{V})$  refer to the position and the velocity, respectively)

$$dV_\alpha = -U_\alpha dt - \nabla \phi(\mathbf{X}) dt \quad (\text{David.2})$$

We assume that  $U_\alpha$  are generated by hydrodynamic interactions which do not however affect the equilibrium Gibbs-Boltzmann distribution which is

$$P_{eq}(\mathbf{X}, \mathbf{V}) = \frac{1}{\bar{Z}} \exp \left( -\frac{\beta \mathbf{V}^2}{2} - \beta \phi(\mathbf{X}) \right) \quad (\text{David.3})$$

*Exploit the Fokker-Planck operator ( $\dots$  refers the similar terms about  $X_\alpha$ )*

$$\frac{\partial P}{\partial t} = -H_{FP}P = \frac{\partial}{\partial x} \left[ \frac{dV}{dx} P + T \frac{\partial}{\partial x} P \right] = \frac{\partial}{\partial V_\alpha} \left[ (U_\alpha + \nabla_\alpha \phi) P + T \gamma_{\alpha\beta} \frac{\partial P}{\partial V_\beta} \right] + \frac{\partial}{\partial X_\alpha} [\dots]$$

Note  $\frac{\partial P}{\partial X_\alpha} = P \left( -\beta \frac{\partial \phi}{\partial X_\alpha} \right)$  and  $\frac{\partial P}{\partial V_\alpha} = P (-\beta V_\alpha)$ . Consider the gravity  $\phi(\mathbf{X}) = -mg\Delta$ , and then we could derive the eq. **David.4**, regarding  $k_B$  as 1

$$\begin{aligned} \frac{\partial}{\partial X_\alpha} \left[ \frac{dV}{dx} P + T \frac{\partial}{\partial x} P \right] &= \frac{\partial}{\partial X_\alpha} \left[ \frac{dV}{dX_\alpha} P + T \frac{\partial}{\partial X_\alpha} P + T \frac{\partial}{\partial V_\alpha} P \right] \\ &= \frac{\partial}{\partial X_\alpha} \left[ (\nabla_\alpha \phi) P + T \cdot P \left( -\beta \frac{\partial \phi}{\partial X_\alpha} \right) + T \frac{\partial}{\partial V_\alpha} P \right] = \frac{\partial}{\partial X_\alpha} \left[ T \frac{\partial}{\partial V_\alpha} P \right] \\ &= \frac{\partial}{\partial X_\alpha} [T \cdot P (-\beta V_\alpha)] = -\frac{\partial}{\partial X_\alpha} V_\alpha P \end{aligned}$$

The Fokker Planck equation at finite temperature which introduces white noise and possibly temperature dependent drifts is  $\phi(\mathbf{X})$  is

$$\frac{\partial P}{\partial t} = \frac{\partial}{\partial V_\alpha} \left[ T\gamma_{\alpha\beta} \frac{\partial P}{\partial V_\beta} + U_\alpha P + \frac{\partial \phi}{\partial X_\alpha} P \right] - \frac{\partial}{\partial X_\alpha} V_\alpha P \quad (\text{David.4})$$

The last two terms would vanish since

$$\frac{\partial}{\partial V_\alpha} \left( \frac{\partial \phi}{\partial X_\alpha} P \right) = \left( \frac{\partial}{\partial V_\alpha} \frac{\partial \phi}{\partial X_\alpha} \right) \cdot P + \frac{\partial \phi}{\partial X_\alpha} \cdot \frac{\partial P}{\partial V_\alpha} = \frac{\partial \phi}{\partial X_\alpha} \cdot P(-\beta V_\alpha)$$

$$\frac{\partial}{\partial X_\alpha} V_\alpha P = \left( \frac{\partial V_\alpha}{\partial X_\alpha} \right) P + V_\alpha \left( \frac{\partial P}{\partial X_\alpha} \right) = V_\alpha \cdot P \cdot \left( -\beta \frac{\partial \phi}{\partial X_\alpha} \right)$$

Therefore, at equilibrium  $\frac{\partial P}{\partial t} = 0$

$$\frac{\partial P}{\partial t} = \frac{\partial}{\partial V_\alpha} \left[ T\gamma_{\alpha\beta} \frac{\partial P}{\partial V_\beta} + U_\alpha P \right] = \frac{\partial}{\partial V_\alpha} \left[ T\gamma_{\alpha\beta} P \cdot (-\beta V_\beta) + U_\alpha P \right] = \frac{\partial}{\partial V_\alpha} \left[ (U_\alpha - \gamma_{\alpha\beta} V_\beta) \cdot P \right] = 0$$

We obtain the GB distribution for the steady state if

$$U_\alpha = \gamma_{\alpha\beta} V_\beta \quad (\text{David.5})$$

We have for small velocities that

$$U_\alpha = \lambda_{\alpha\beta}(\mathbf{X}) V_\beta + \Lambda_{\alpha\beta\gamma}(\mathbf{X}) V_\beta V_\gamma \quad (\text{David.6})$$

and so we find

$$\gamma_{\alpha\beta} V_\beta = \lambda_{\alpha\beta}(\mathbf{X}) V_\beta + \Lambda_{\alpha\beta\gamma}(\mathbf{X}) V_\beta V_\gamma \quad (\text{David.7})$$

Written this way the term  $\lambda_{\alpha\beta}(\mathbf{X})$  is just the friction tensor in the absence of any elastic effects. We can thus write

$$\gamma_{\alpha\beta} = \lambda_{\alpha\beta} + \gamma_{2\alpha\beta} \quad (\text{David.8})$$

and we write

$$\gamma_{2\alpha\beta} = \Gamma_{\alpha\beta\gamma} V_\gamma \quad (\text{David.9})$$

and

$$\Gamma_{\alpha\beta\gamma}(\mathbf{X}) V_\beta V_\gamma = \Lambda_{\alpha\beta\gamma}(\mathbf{X}) V_\beta V_\gamma \quad (\text{David.10})$$

where we without loss of generality take  $\Lambda_{\alpha\beta\gamma} = \Lambda_{\alpha\gamma\beta}$ , which then gives

$$\Gamma_{\alpha\beta\gamma} + \Gamma_{\alpha\gamma\beta} = 2\Lambda_{\alpha\beta\gamma} \quad (\text{David.11})$$

We have to solve this system with the constraint that  $\Gamma_{\alpha\beta\gamma}V_\gamma = \Gamma_{\beta\alpha\gamma}V_\gamma$ . In Thomas' problem (*see subsection 1.2*) we have

$$\ddot{\Delta} + \xi \frac{\dot{\Delta}}{\Delta^{3/2}} + \frac{\kappa\xi}{4} \left[ 21 \frac{\dot{\Delta}^2}{\Delta^{9/2}} - \frac{(\dot{\Theta} - \dot{X}_G)^2}{\Delta^{7/2}} - \frac{15}{2} \frac{\ddot{\Delta}}{\Delta^{7/2}} \right] + \cos \alpha = 0$$

$$\ddot{X}_G + \frac{2\varepsilon\xi}{3} \frac{\dot{X}_G}{\sqrt{\Delta}} + \frac{\kappa\varepsilon\xi}{6} \left[ \frac{19}{4} \frac{\dot{\Delta}\dot{X}_G}{\Delta^{7/2}} - \frac{\dot{\Delta}\dot{\Theta}}{\Delta^{7/2}} + \frac{1}{2} \frac{\ddot{\Theta} - \ddot{X}_G}{\Delta^{5/2}} \right] - \sqrt{\frac{\varepsilon}{2}} \sin \alpha = 0$$

where  $\Delta$  refers to  $z$  and  $X_G$  refers to  $x$ . Note  $\dot{\Delta} = -U_z$  and  $\dot{X}_G = -U_x$ , we write

$$U_z = \xi \frac{V_z}{Z^{3/2}} + \frac{21\kappa\xi}{4} \frac{V_z^2}{Z^{9/2}} - \frac{\kappa\xi}{4} \frac{V_x^2}{Z^{7/2}} \quad (\text{David.12})$$

$$U_x = 2\xi\varepsilon \frac{V_x}{3Z^{1/2}} + \frac{19\kappa\xi\varepsilon}{24} \frac{V_z V_x}{Z^{7/2}} \quad (\text{David.13})$$

Note  $\dot{\Delta} = V_z$  and  $\dot{X}_G = V_x$ , we could extract the relevant coefficients. But Attention! Here  $\dot{\Theta}$  was assumed 0, and the second derivatives in first-order correlation had been ignored.

Form this we find that

$$\sum_{\alpha\beta} \Lambda_{z\alpha\beta} V_\alpha V_\beta = \frac{21\kappa\xi}{4} \frac{V_z^2}{Z^{9/2}} - \frac{\kappa\xi}{4} \frac{V_x^2}{Z^{7/2}} \quad (\text{David.14})$$

$$\sum_{\alpha\beta} \Lambda_{x\alpha\beta} V_\alpha V_\beta = \frac{19\kappa\xi\varepsilon}{24} \frac{V_z V_x}{Z^{7/2}}$$

This gives the set of equations

$$\Gamma_{zzz} = \frac{21\kappa\xi}{4Z^{9/2}} \quad (\text{David.15})$$

$$\Gamma_{zxx} = -\frac{\kappa\xi}{4Z^{7/2}} \quad (\text{David.16})$$

$$\Gamma_{zxz} + \Gamma_{zzx} = 0 \quad (\text{David.17})$$

$$\Gamma_{xzz} = 0 \quad (\text{David.18})$$

$$\Gamma_{xxx} = 0 \quad (\text{David.19})$$

$$\Gamma_{xxz} + \Gamma_{xzx} = \frac{19\kappa\xi\varepsilon}{24Z^{7/2}} \quad (\text{David.20})$$

The symmetry  $\Gamma_{\alpha\beta\gamma} = \Gamma_{\beta\alpha\gamma}$  now gives

$$\Gamma_{xxz} = \frac{19\kappa\xi\varepsilon}{24Z^{7/2}} - \Gamma_{xzx} = \frac{19\kappa\xi\varepsilon}{24Z^{7/2}} - \Gamma_{zxx} = \frac{\kappa\xi}{Z^{7/2}} \left( \frac{19\varepsilon}{24} + \frac{1}{4} \right) \quad (\text{David.21})$$

as well as

$$\Gamma_{zxz} = \Gamma_{zzx} = 0 \quad (\text{David.22})$$

The Langevin equation corresponding to this is, using the Itô convention,

$$\frac{dV_\alpha}{dt} = -U_\alpha - \frac{\partial\phi(\mathbf{X})}{\partial X_\alpha} + T \frac{\partial\gamma_{\alpha\beta}}{\partial V_\beta} + \eta_\alpha(t) \quad (\text{David.23})$$

which can be written as

$$\frac{dV_\alpha}{dt} = -U_\alpha - \frac{\partial\phi(\mathbf{X})}{\partial X_\alpha} + T\Gamma_{\alpha\beta\beta} + \eta_\alpha(t) \quad (\text{David.24})$$

where we use the Einstein summation convention and the noise correlator is given by

$$\langle \eta_\alpha(t) \eta_\beta(t') \rangle = 2T\gamma_{\alpha\beta}\delta(t-t') = 2T [\lambda_{\alpha\beta}(\mathbf{X}) + \Gamma_{\alpha\beta\gamma}(\mathbf{X})V_\gamma] \delta(t-t') \quad (\text{David.25})$$

Putting this together we find (from eq. [David.24](#)) with all  $\Gamma_{\alpha\beta\beta}$  only depending on  $\Delta, X$ .

$$\begin{aligned} \frac{dV_z}{dt} &= -V'(Z) - \xi \frac{V_z}{Z^{3/2}} - \frac{21\kappa\xi}{4} \frac{V_z^2}{Z^{9/2}} + \frac{\kappa\xi V_x^2}{4Z^{7/2}} + T \left[ \frac{21\kappa\xi}{4Z^{9/2}} - \frac{\kappa\xi}{4Z^{7/2}} \right] + \eta_z(t) \\ \frac{dV_x}{dt} &= -2\xi\epsilon \frac{V_x}{3Z^{1/2}} - \frac{19\kappa\xi V_z V_x}{24Z^{7/2}} + \eta_x(t) \end{aligned} \quad (\text{David.26})$$

## 2 Further Analyses

Generally, the Brownian motion would furnish the following equation:

$$dv = \frac{f(t)}{m} dt - \gamma v dt + \sqrt{\frac{2\gamma}{\beta m}} dW(t)$$

where  $f(t)$  contains the external forces,  $\gamma$  would be a matrix rather than a constant for  $v$  is a velocity vector, the last term shows the random force.

In this section, we would first consider the second derivatives in Thomas' results, updating the  $\gamma$  matrix; then consider the effective "mass" on different directions  $(\Delta, X, \Theta)$ , showing  $\frac{1}{m}$  as an inverse matrix; finally one numerical procedure to simulate the Langevin equation.

### 2.1 New $\lambda_{\alpha\beta}, \Gamma_{\alpha\beta\gamma}$ in 3D $(\Delta, X, \Theta)$

In this part, we would renew coefficients for the motion in 3D  $(\Delta, X, \Theta)$ . Based on the previous subsection, we could repeat the calculation by Fokker-Planck operator, finding the similar results with additional terms about  $\Theta$ .

For the sake of convenience, we re-write Thomas' differential equations (see subsection [1.2](#)) with  $\dot{v}_i$ , (and  $X$  refers to  $X_G$ )

$$\begin{aligned} -U_Z &= \dot{v}_\Delta = \ddot{\Delta} = F_\Delta(\Delta, v_\Delta, v_X, v_\Theta, \dot{v}_\Delta) \\ -U_X &= \dot{v}_X = \ddot{X} = F_X(\Delta, v_\Delta, v_X, v_\Theta, \dot{v}_X, \dot{v}_\Theta) \\ -U_\Theta &= \dot{v}_\Theta = \ddot{\Theta} = F_\Theta(\Delta, v_\Delta, v_X, v_\Theta, \dot{v}_X, \dot{v}_\Theta) \end{aligned} \quad (\text{Yilin.1})$$



However, we'd like to derive equations for each  $\dot{v}$  only depending on  $\Delta$  and  $v$ , without  $\dot{v}$ . Therefore, we have to find the proper expression for each  $\dot{v}_i$ .

Consider the second derivative in the eq. [Salez2015.51](#),

$$\ddot{\Delta} + a_1 \frac{\dot{\Delta}}{\Delta^{3/2}} + a_2 \frac{\dot{\Delta}^2}{\Delta^{9/2}} + a_3 \frac{\dot{\Theta}^2}{\Delta^{7/2}} + a_3 \frac{\dot{X}^2}{\Delta^{7/2}} + a_4 \frac{\dot{\Theta}\dot{X}}{\Delta^{7/2}} + a_5 \frac{\ddot{\Delta}}{\Delta^{7/2}} + a_6 = 0 \quad (\text{Yilin.2})$$

$$\ddot{\Delta} = \left( a_1 \frac{\dot{\Delta}}{\Delta^{3/2}} + a_2 \frac{\dot{\Delta}^2}{\Delta^{9/2}} + a_3 \frac{\dot{\Theta}^2}{\Delta^{7/2}} + a_3 \frac{\dot{X}^2}{\Delta^{7/2}} + a_4 \frac{\dot{\Theta}\dot{X}}{\Delta^{7/2}} + a_6 \right) \times \frac{-1}{1 + a_5/\Delta^{7/2}} \quad (\text{Yilin.3})$$

We know that  $a_1 = \xi$ ,  $a_2 = \frac{21\kappa\xi}{4}$ ,  $a_3 = -\frac{\kappa\xi}{4}$ ,  $a_4 = \frac{\kappa\xi}{2}$ ,  $a_5 = -\frac{15\kappa\xi}{8}$ ,  $a_6 = \cos(\alpha = 0) = 1$ . After simple calculation, we could obtain  $\dot{v}_\Delta$  ( $\dot{v}_z$ ) namely  $\ddot{\Delta}$

$$-\dot{v}_\Delta = U_z = \frac{8\Delta^{9/2} + 2\xi(-\Delta\kappa v_X^2 + 4\Delta^3 v_z + 21\kappa v_z^2 + 2\Delta\kappa v_X v_\theta - \Delta\kappa v_\theta^2)}{8\Delta^{9/2} - 15\Delta\kappa\xi} \quad (\text{Yilin.4})$$

Similarly, we write the eqs [Salez2015.50](#) and [Salez2015.52](#) as

$$\ddot{X} + b_1 \frac{\dot{X}}{\sqrt{\Delta}} + b_2 \frac{\dot{\Delta}\dot{X}}{\Delta^{7/2}} + b_3 \frac{\dot{\Delta}\dot{\Theta}}{\Delta^{7/2}} + b_4 \frac{\ddot{\Theta}}{\Delta^{5/2}} + b_5 \frac{\ddot{X}}{\Delta^{5/2}} + b_6 = 0 \quad (\text{Yilin.5})$$

$$\ddot{\Theta} + c_1 \frac{\dot{\Theta}}{\sqrt{\Delta}} + c_2 \frac{\dot{\Delta}\dot{\Theta}}{\Delta^{7/2}} + c_3 \frac{\dot{\Delta}\dot{X}}{\Delta^{7/2}} + c_4 \frac{\ddot{X}}{\Delta^{5/2}} + c_5 \frac{\ddot{\Theta}}{\Delta^{5/2}} + c_6 = 0 \quad (\text{Yilin.6})$$

with all coefficients we need:  $b_1 = \frac{2\xi\xi}{3}$ ,  $b_2 = \frac{19\kappa\xi\xi}{24}$ ,  $b_3 = -\frac{\kappa\xi\xi}{6}$ ,  $b_4 = \frac{\kappa\xi\xi}{12}$ ,  $b_5 = -\frac{\kappa\xi\xi}{12}$ ,  $b_6 = \sin(\alpha = 0) = 0$ ; and  $c_1 = \frac{4\xi\xi}{3}$ ,  $c_2 = \frac{19\kappa\xi\xi}{12}$ ,  $c_3 = -\frac{\kappa\xi\xi}{3}$ ,  $c_4 = \frac{\kappa\xi\xi}{6}$ ,  $c_5 = -\frac{\kappa\xi\xi}{6}$ ,  $c_6 = 0$ . For this system of linear equations, the coefficient matrix has full rank.

$$\begin{pmatrix} 1 + (b_5) & (b_4) \\ (c_4) & 1 + (c_5) \end{pmatrix} \begin{pmatrix} \ddot{X} \\ \ddot{\Theta} \end{pmatrix} = \begin{pmatrix} (b_1 + b_2 + b_3 + b_6) \\ (c_1 + c_2 + c_3 + c_6) \end{pmatrix}$$

Then we could solve  $\ddot{X} = \dot{v}_X$  and  $\ddot{\Theta} = \dot{v}_\Theta$  directly

$$-\dot{v}_X = U_X = \frac{\epsilon\xi \left( \kappa \left( 16\Delta^3 \epsilon\xi + \left( -24\Delta^{5/2} + 23\epsilon\kappa\xi \right) v_z \right) v_\theta + v_X \left( -4\epsilon\kappa^2\xi v_z + \left( 6\Delta^{5/2} - \epsilon\kappa\xi \right) (16\Delta^3 + 19\kappa v_\theta) \right) \right)}{36(4\Delta^6 - \Delta^{7/2}\epsilon\kappa\xi)} \quad (\text{Yilin.7})$$

$$-\dot{v}_\Theta = U_\Theta = \frac{\epsilon\xi \left( \left( 16\Delta^3 \left( 12\Delta^{5/2} - \epsilon\kappa\xi \right) + \kappa \left( 228\Delta^{5/2} - 23\epsilon\kappa\xi \right) v_z \right) v_\theta + \kappa v_X \left( \left( -48\Delta^{5/2} + 4\epsilon\kappa\xi \right) v_z + \epsilon\xi (16\Delta^3 + 19\kappa v_\theta) \right) \right)}{36(4\Delta^6 - \Delta^{7/2}\epsilon\kappa\xi)} \quad (\text{Yilin.8})$$

Compare with the eq. [Yilin.1](#), we finally remove the second derivatives inside each expression

$$\begin{aligned}\dot{v}_\Delta &= F_\Delta(\Delta, v_\Delta, v_X, v_\Theta) \\ \dot{v}_X &= F_X(\Delta, v_\Delta, v_X, v_\Theta) \\ \dot{v}_\Theta &= F_\Theta(\Delta, v_\Delta, v_X, v_\Theta)\end{aligned}\tag{Yilin.9}$$

See eqs [David.5](#) ~ [David.9](#), we could extract these  $\lambda_{\alpha\beta}$  by

$$\lambda_{\alpha\beta} = \text{Coefficient}[U_\alpha, v_\beta] - \text{Coefficient}[U_\alpha, v_\beta v_\gamma] \times v_\gamma\tag{Yilin.10}$$

and  $\Gamma_{\alpha\beta\beta}$  by

$$\Gamma_{\alpha\beta\beta} = \text{Coefficient}[U_\alpha, v_\beta v_\beta]\tag{Yilin.11}$$

As for  $\Gamma_{\alpha\beta\gamma}$ , we should resolve them by

$$2\Lambda_{\alpha\beta\gamma} = \text{Coefficient}[U_\alpha, v_\beta v_\gamma] = \Gamma_{\alpha\beta\gamma} + \Gamma_{\alpha\gamma\beta}\tag{Yilin.12}$$

as well as the constraint  $\Gamma_{\alpha\beta\gamma} = \Gamma_{\beta\alpha\gamma}$ .

After some calculations verified by *Mathematica*, we list all  $\lambda_{\alpha\beta}$

$$\begin{aligned}\lambda_{zz} &= \frac{8\Delta^2\xi}{8\Delta^{7/2} - 15\kappa\xi} \\ \lambda_{xx} &= -\frac{4\epsilon\xi \left(-6\Delta^{5/2} + \epsilon\kappa\xi\right)}{36\Delta^3 - 9\sqrt{\Delta}\epsilon\kappa\xi}\end{aligned}\tag{Yilin.13}$$

$$\begin{aligned}\lambda_{\theta\theta} &= -\frac{4\epsilon\xi \left(-12\Delta^{5/2} + \epsilon\kappa\xi\right)}{36\Delta^3 - 9\sqrt{\Delta}\epsilon\kappa\xi} \\ \lambda_{x\theta} = \lambda_{\theta x} &= \frac{4\epsilon^2\kappa\xi^2}{36\Delta^3 - 9\sqrt{\Delta}\epsilon\kappa\xi}\end{aligned}\tag{Yilin.14}$$

$$\lambda_{zx} = \lambda_{xz} = \lambda_{z\theta} = \lambda_{\theta z} = 0\tag{Yilin.15}$$

and then  $\Gamma_{\alpha\beta\gamma}$

$$\begin{aligned}\Gamma_{zzz} &= \frac{42\kappa\xi}{8\Delta^{9/2} - 15\Delta\kappa\xi} \\ \Gamma_{xzx} = \Gamma_{zxx} &= \frac{2\kappa\xi}{-8\Delta^{7/2} + 15\kappa\xi}\end{aligned}\tag{Yilin.16}$$

$$\begin{aligned}\Gamma_{\theta z\theta} = \Gamma_{z\theta\theta} &= \frac{2\kappa\xi}{-8\Delta^{7/2} + 15\kappa\xi} \\ \Gamma_{zxz} = \Gamma_{zzx} = \Gamma_{zz\theta} = \Gamma_{z\theta z} &= 0\end{aligned}\tag{Yilin.17}$$

$$\Gamma_{xzz} = \Gamma_{xxx} = \Gamma_{\theta zz} = \Gamma_{\theta\theta\theta} = 0\tag{Yilin.18}$$

$$\Gamma_{\theta xx} = \Gamma_{x\theta x} = \Gamma_{x\theta\theta} = \Gamma_{\theta x\theta} = 0 \quad (\text{Yilin.19})$$

$$\begin{aligned} \Gamma_{xxz} &= \frac{1}{9}\kappa\xi \left( \frac{18}{8\Delta^{7/2} - 15\kappa\xi} + \frac{\epsilon^2\kappa\xi}{-4\Delta^6 + \Delta^{7/2}\epsilon\kappa\xi} \right) \\ \Gamma_{xx\theta} &= \frac{19\epsilon\kappa\xi \left( -6\Delta^{5/2} + \epsilon\kappa\xi \right)}{-144\Delta^6 + 36\Delta^{7/2}\epsilon\kappa\xi} \\ \Gamma_{\theta\theta x} &= \frac{19\epsilon^2\kappa^2\xi^2}{36(4\Delta^6 - \Delta^{7/2}\epsilon\kappa\xi)} \\ \Gamma_{\theta\theta z} &= \frac{\epsilon\kappa\xi \left( -228\Delta^{5/2} + 23\epsilon\kappa\xi \right)}{-144\Delta^6 + 36\Delta^{7/2}\epsilon\kappa\xi} \end{aligned} \quad (\text{Yilin.20})$$

$$\begin{aligned} \Gamma_{zx\theta} = \Gamma_{xz\theta} &= -\frac{25}{18\Delta} - \frac{19\epsilon\kappa\xi}{72\Delta^{7/2}} + \frac{2\kappa\xi}{8\Delta^{7/2} - 15\kappa\xi} + \frac{50\Delta^{3/2}}{36\Delta^{5/2} - 9\epsilon\kappa\xi} \\ \Gamma_{z\theta x} = \Gamma_{\theta zx} &= \frac{25}{18\Delta} + \frac{19\epsilon\kappa\xi}{72\Delta^{7/2}} + \frac{2\kappa\xi}{8\Delta^{7/2} - 15\kappa\xi} + \frac{50\Delta^{3/2}}{9(-4\Delta^{5/2} + \epsilon\kappa\xi)} \\ \Gamma_{x\theta z} = \Gamma_{\theta xz} &= \frac{2}{15} - \frac{1}{2\Delta} - \frac{3\epsilon\kappa\xi}{8\Delta^{7/2}} + \frac{16}{15\left(-8 + \frac{15\kappa\xi}{\Delta^{7/2}}\right)} + \frac{1}{2\Delta - \frac{\epsilon\kappa\xi}{2\Delta^{3/2}}} \end{aligned} \quad (\text{Yilin.21})$$

## 2.2 $\gamma_{\alpha\beta}$ and linear approximation of $\kappa$

Since  $\gamma_{\alpha\beta} = \lambda_{\alpha\beta} + \Gamma_{\alpha\beta\gamma}V_\gamma$ , we have

$$\begin{aligned} \gamma_{zz} &= \frac{8\Delta^2\xi}{8\Delta^{7/2} - 15\kappa\xi} + \frac{42\kappa\xi v_z}{8\Delta^{9/2} - 15\Delta\kappa\xi} \\ &= \frac{\xi}{\Delta^{3/2}} + \left( \frac{15\xi^2}{8\Delta^5} + \frac{21\xi v_z}{4\Delta^{9/2}} \right) \kappa + \left( \frac{225\xi^3}{64\Delta^{17/2}} + \frac{315\xi^2 v_z}{32\Delta^8} \right) \kappa^2 + O[\kappa]^3 \end{aligned} \quad (\text{Yilin.22})$$

$$\begin{aligned} \gamma_{zx} = \gamma_{xz} &= \frac{2\kappa\xi v_X}{-8\Delta^{7/2} + 15\kappa\xi} + \left( -\frac{25}{18\Delta} - \frac{19\epsilon\kappa\xi}{72\Delta^{7/2}} + \frac{2\kappa\xi}{8\Delta^{7/2} - 15\kappa\xi} + \frac{50\Delta^{3/2}}{36\Delta^{5/2} - 9\epsilon\kappa\xi} \right) v_\theta \\ &= -\frac{(\xi(3v_X - 3v_\theta - \epsilon v_\theta))\kappa}{12\Delta^{7/2}} + \frac{5\xi^2(-27v_X + 27v_\theta + 5\Delta\epsilon^2 v_\theta)\kappa^2}{288\Delta^7} + O[\kappa]^3 \end{aligned} \quad (\text{Yilin.23})$$

$$\begin{aligned} \gamma_{z\theta} = \gamma_{\theta z} &= \left( \frac{25}{18\Delta} + \frac{19\epsilon\kappa\xi}{72\Delta^{7/2}} + \frac{2\kappa\xi}{8\Delta^{7/2} - 15\kappa\xi} + \frac{50\Delta^{3/2}}{9(-4\Delta^{5/2} + \epsilon\kappa\xi)} \right) v_X + \frac{2\kappa\xi v_\theta}{-8\Delta^{7/2} + 15\kappa\xi} \\ &= -\frac{(\xi(-3v_X + \epsilon v_X + 3v_\theta))\kappa}{12\Delta^{7/2}} - \frac{5(\xi^2(-27v_X + 5\Delta\epsilon^2 v_X + 27v_\theta))\kappa^2}{288\Delta^7} + O[\kappa]^3 \end{aligned} \quad (\text{Yilin.24})$$

$$\begin{aligned}
\gamma_{xx} &= -\frac{4\epsilon\xi(-6\Delta^{5/2} + \epsilon\kappa\xi)}{36\Delta^3 - 9\sqrt{\Delta}\epsilon\kappa\xi} + \frac{1}{9}\kappa\xi\left(\frac{18}{8\Delta^{7/2} - 15\kappa\xi} + \frac{\epsilon^2\kappa\xi}{-4\Delta^6 + \Delta^{7/2}\epsilon\kappa\xi}\right)v_z + \frac{19\epsilon\kappa\xi(-6\Delta^{5/2} + \epsilon\kappa\xi)v_\theta}{-144\Delta^6 + 36\Delta^{7/2}\epsilon\kappa\xi} \\
&= \frac{2\epsilon\xi}{3\sqrt{\Delta}} + \frac{(4\sqrt{\Delta}\epsilon^2\xi^2 + 18\xi v_z + 57\epsilon\xi v_\theta)\kappa}{72\Delta^{7/2}} + \left(\frac{\epsilon^3\xi^3}{72\Delta^{11/2}} - \frac{(-135 + 8\Delta\epsilon^2)\xi^2 v_z}{288\Delta^7} + \frac{19\epsilon^2\xi^2 v_\theta}{288\Delta^6}\right)\kappa^2 + O[\kappa]^3
\end{aligned}
\tag{Yilin.25}$$

$$\begin{aligned}
\gamma_{\theta\theta} &= -\frac{4\epsilon\xi(-12\Delta^{5/2} + \epsilon\kappa\xi)}{36\Delta^3 - 9\sqrt{\Delta}\epsilon\kappa\xi} + \frac{19\epsilon^2\kappa^2\xi^2 v_X}{36(4\Delta^6 - \Delta^{7/2}\epsilon\kappa\xi)} + \kappa\xi\left(\frac{23\epsilon}{36\Delta^{7/2}} + \frac{2}{8\Delta^{7/2} - 15\kappa\xi} + \frac{34\epsilon}{36\Delta^{7/2} - 9\Delta\epsilon\kappa\xi}\right)v_z \\
&= \frac{4\epsilon\xi}{3\sqrt{\Delta}} + \left(\frac{2\epsilon^2\xi^2}{9\Delta^3} + \frac{(3 + 19\epsilon)\xi v_z}{12\Delta^{7/2}}\right)\kappa + \left(\frac{\epsilon^3\xi^3}{18\Delta^{11/2}} + \frac{19\epsilon^2\xi^2 v_X}{144\Delta^6} + \frac{(135 + 68\Delta\epsilon^2)\xi^2 v_z}{288\Delta^7}\right)\kappa^2 + O[\kappa]^3
\end{aligned}
\tag{Yilin.26}$$

$$\begin{aligned}
\gamma_{x\theta} = \gamma_{\theta x} &= \frac{4\epsilon^2\kappa\xi^2}{36\Delta^3 - 9\sqrt{\Delta}\epsilon\kappa\xi} + \left(\frac{2}{15} - \frac{1}{2\Delta} - \frac{3\epsilon\kappa\xi}{8\Delta^{7/2}} + \frac{16}{15\left(-8 + \frac{15\kappa\xi}{\Delta^{7/2}}\right)} + \frac{1}{2\Delta - \frac{\epsilon\kappa\xi}{2\Delta^{3/2}}}\right)v_z \\
&= \left(\frac{\epsilon^2\xi^2}{9\Delta^3} - \frac{(\xi + \epsilon\xi)v_z}{4\Delta^{7/2}}\right)\kappa + \left(\frac{\epsilon^3\xi^3}{36\Delta^{11/2}} + \frac{(-15 + \Delta\epsilon^2)\xi^2 v_z}{32\Delta^7}\right)\kappa^2 + O[\kappa]^3
\end{aligned}
\tag{Yilin.27}$$

As we could see,  $\gamma_{\alpha\beta}$  is a symmetric matrix.

$$\boldsymbol{\gamma} = \begin{pmatrix} \gamma_{zz} & \gamma_{zx} & \gamma_{z\theta} \\ \gamma_{xz} & \gamma_{xx} & \gamma_{x\theta} \\ \gamma_{\theta z} & \gamma_{\theta x} & \gamma_{\theta\theta} \end{pmatrix}$$

In addition, only three diagonal elements, namely  $\gamma_{zz}, \gamma_{xx}, \gamma_{\theta\theta}$  have zero-order term of  $\kappa$ , which describes the compliance. In genenral, this parameter is about  $10^{-4} \sim 10^{-3}$ . Right now, we could write the equation of motion as:

$$\dot{v}_i = \frac{F_i}{m} - \gamma_{ij}v_j + \eta_i
\tag{Yilin.28}$$

where  $F_i$  contains the force due to external potentials (gravity and buoyant force), as well as the spurious drift force, which originates from the derivative of  $\gamma_{\alpha\beta}$ , equal to  $\frac{\partial\gamma_{\alpha\beta}}{\partial v_\beta} = \Gamma_{\alpha\beta\beta}$ . See eqs

**Yilin.16**, we could easily obtain non-zero components:

$$\begin{aligned}\frac{\partial \gamma_{zz}}{\partial v_z} &= \Gamma_{zzz} = \frac{42\kappa\xi}{8\Delta^{9/2} - 15\Delta\kappa\xi} \approx \frac{21\kappa\xi}{4\Delta^{9/2}} + \frac{315\kappa^2\xi^2}{32\Delta^8} \\ \frac{\partial \gamma_{zx}}{\partial v_x} &= \Gamma_{zxx} = \frac{2\kappa\xi}{15\kappa\xi - 8\Delta^{7/2}} \approx -\frac{\kappa\xi}{4\Delta^{7/2}} - \frac{15\kappa^2\xi^2}{32\Delta^7} \\ \frac{\partial \gamma_{z\theta}}{\partial v_\theta} &= \Gamma_{z\theta\theta} = \frac{2\kappa\xi}{15\kappa\xi - 8\Delta^{7/2}} \approx -\frac{\kappa\xi}{4\Delta^{7/2}} - \frac{15\kappa^2\xi^2}{32\Delta^7}\end{aligned}$$

Other  $\Gamma_{\alpha\beta\gamma}$ s are all equal to 0. Thus there is only a spurious force on  $\Delta$  direction.

To be exact:

$$\begin{pmatrix} \dot{v}_\Delta \\ \dot{v}_X \\ \dot{v}_\Theta \end{pmatrix} = \begin{pmatrix} F_\Delta \\ F_X \\ F_\Theta \end{pmatrix} - \begin{pmatrix} \gamma_{zz} & \gamma_{zx} & \gamma_{z\theta} \\ \gamma_{xz} & \gamma_{xx} & \gamma_{x\theta} \\ \gamma_{\theta z} & \gamma_{\theta x} & \gamma_{\theta\theta} \end{pmatrix} \begin{pmatrix} v_\Delta \\ v_X \\ v_\Theta \end{pmatrix} + \begin{pmatrix} \eta_\Delta \\ \eta_X \\ \eta_\Theta \end{pmatrix} \quad (\text{Yilin.29})$$

As for the noise correlator, it has been shown in the eq. **David.25**:

$$\langle \eta_\alpha(t) \eta_\beta(t') \rangle = 2T \gamma_{\alpha\beta} \delta(t - t') = 2T [\lambda_{\alpha\beta}(\mathbf{X}) + \Gamma_{\alpha\beta\gamma}(\mathbf{X}) V_\gamma] \delta(t - t')$$

So we'd like to find the expression of  $\gamma^{1/2}$ . Suppose that

$$\gamma = \Psi + \kappa\Phi + O[\kappa]^2 \quad (\text{Yilin.30})$$

where  $\Psi$  is zero-order matrix of  $\kappa$ , and  $\Phi$  the first-order one. Also,  $\gamma^{1/2}$  show a form such as  $\gamma^{1/2} \approx \psi + \kappa\chi$ ,

$$\gamma = \gamma^{1/2} \gamma^{1/2} = (\psi + \kappa\chi)(\psi + \kappa\chi) = \psi\psi + \kappa(\psi\chi + \chi\psi) + O[\kappa]^2$$

we have  $\Phi = \chi\psi + \psi\chi$ , and  $\psi = \sqrt{\Psi}$ . Note  $\Psi$  is a symmetric matrix and all non-diagonal elements are equal to 0.

$$\Psi = \begin{pmatrix} \lambda_z & 0 & 0 \\ 0 & \lambda_x & 0 \\ 0 & 0 & \lambda_\theta \end{pmatrix} = \begin{pmatrix} \frac{\xi}{\Delta^{3/2}} & 0 & 0 \\ 0 & \frac{2\epsilon\xi}{3\sqrt{\Delta}} & 0 \\ 0 & 0 & \frac{4\epsilon\xi}{3\sqrt{\Delta}} \end{pmatrix} \quad (\text{Yilin.31})$$

Also,  $\chi$  is a symmetric matrix, with diagonal components as:

$$\begin{aligned}\chi_{zz} &= \frac{3\xi(5\xi + 14\sqrt{\Delta}v_z)}{16\Delta^5\sqrt{\frac{\xi}{\Delta^{3/2}}}} \\ \chi_{xx} &= \frac{\xi(18v_z + \epsilon(4\sqrt{\Delta}\epsilon\xi + 57v_\theta))}{48\sqrt{6}\Delta^{7/2}\sqrt{\frac{\epsilon\xi}{\sqrt{\Delta}}}} \\ \chi_{\theta\theta} &= \frac{\xi(8\sqrt{\Delta}\epsilon^2\xi + (9 + 57\epsilon)v_z)}{48\sqrt{3}\Delta^{7/2}\sqrt{\frac{\epsilon\xi}{\sqrt{\Delta}}}}\end{aligned} \quad (\text{Yilin.32})$$

and non-diagonal elements

$$\begin{aligned}
\chi_{zx} = \chi_{xz} &= \frac{\xi(-3v_X + (3 + \epsilon)v_\theta)}{4\Delta^{7/2} \left( 3\sqrt{\frac{\xi}{\Delta^{3/2}}} + \sqrt{6}\sqrt{\frac{\epsilon\xi}{\sqrt{\Delta}}} \right)} \\
\chi_{z\theta} = \chi_{\theta z} &= -\frac{\xi(3v_\theta + (\epsilon - 3)v_X)}{4\Delta^{7/2} \left( 3\sqrt{\frac{\xi}{\Delta^{3/2}}} + 2\sqrt{3}\sqrt{\frac{\xi\epsilon}{\sqrt{\Delta}}} \right)} \\
\chi_{x\theta} = \chi_{\theta x} &= \frac{\xi(4\sqrt{\Delta}\epsilon^2\xi - 9(1 + \epsilon)v_z)}{12\sqrt{3}(2 + \sqrt{2})\Delta^{7/2}\sqrt{\frac{\epsilon\xi}{\sqrt{\Delta}}}}
\end{aligned} \tag{Yilin.33}$$

## 2.3 Mass vector

We always regarded the mass as 1 in the previous parts, while it should be carefully distinguished later. For  $z, x$  components,  $m_\alpha = m = \pi r^2 \rho$  namely the mass of the column (per unit length). However,  $m_\Theta = mr^2/2$  refers to the moment of inertia. Taking that into account, we compare these two versions (Note we re-write  $U_\alpha$  as  $F_\alpha$  on the left side)

$m_\alpha = 1$	$m_\alpha = (m, m, mr^2/2)$
$dX_\alpha = V_\alpha dt$	$\dot{x}_\alpha = v_\alpha$
$dV_\alpha = -F_\alpha dt - \nabla_\alpha \phi(\mathbf{X}) dt$	$m_\alpha \cdot \dot{v}_\alpha = F_{h\alpha}(\mathbf{v}, \dot{\mathbf{v}}, \mathbf{x}) - \nabla_\alpha \phi(\mathbf{x})$
$F_\alpha = \gamma_{\alpha\beta} V_\beta = \lambda_{\alpha\beta} V_\beta + \Gamma_{\alpha\beta\gamma} V_\beta V_\gamma$	$F_{h\alpha}(\mathbf{v}, \dot{\mathbf{v}}, \mathbf{x}) = F_{1h\alpha}(\mathbf{v}, \mathbf{x}) + F_{2h\alpha\beta}(\mathbf{x}) \dot{v}_\beta$
	$M_{\alpha\beta} = \delta_{\alpha\beta} \cdot m_\alpha - F_{2h\alpha\beta}(\mathbf{x})$
	$M_{\alpha\beta} \dot{v}_\beta = F_{1h\alpha}(\mathbf{v}, \mathbf{x}) - \nabla_\alpha \phi(\mathbf{x})$

Since  $F_{h\alpha}(\mathbf{v}, \dot{\mathbf{v}}, \mathbf{x}) = F_{1h\alpha}(\mathbf{v}, \mathbf{x}) + F_{2h\alpha\beta}(\mathbf{x}) \dot{v}_\beta$ , we could extract  $F_{1h\alpha}(\mathbf{v}, \mathbf{x})$  and  $F_{2h\alpha\beta}(\mathbf{x})$  by

$$-\frac{F_{hZ}}{m_Z} = -\dot{v}_z = -\ddot{\Delta} = a_1 \frac{\dot{\Delta}}{\Delta^{3/2}} + a_2 \frac{\dot{\Delta}^2}{\Delta^{9/2}} + a_3 \frac{\dot{\Theta}^2}{\Delta^{7/2}} + a_3 \frac{\dot{X}^2}{\Delta^{7/2}} + a_4 \frac{\dot{\Theta}\dot{X}}{\Delta^{7/2}} + a_5 \frac{\ddot{\Delta}}{\Delta^{7/2}} + a_6 \tag{Yilin.34}$$

thus

$$\begin{aligned}
F_{1hZ} &= -m_Z \left( a_1 \frac{\dot{\Delta}}{\Delta^{3/2}} + a_2 \frac{\dot{\Delta}^2}{\Delta^{9/2}} + a_3 \frac{\dot{\Theta}^2}{\Delta^{7/2}} + a_3 \frac{\dot{X}^2}{\Delta^{7/2}} + a_4 \frac{\dot{\Theta}\dot{X}}{\Delta^{7/2}} + a_6 \right) \\
F_{2hZZ} &= -\frac{m_Z a_5}{\Delta^{7/2}} \quad F_{2hZX} = 0 \quad F_{2hZ\Theta} = 0
\end{aligned} \tag{Yilin.35}$$

Similarly, there are cross terms for  $X, \Theta$  components

$$-\frac{F_{hX}}{m_X} = -\dot{v}_x = -\ddot{X} = b_1 \frac{\dot{X}}{\sqrt{\Delta}} + b_2 \frac{\dot{\Delta}\dot{X}}{\Delta^{7/2}} + b_3 \frac{\dot{\Delta}\dot{\Theta}}{\Delta^{7/2}} + b_4 \frac{\ddot{\Theta}}{\Delta^{5/2}} + b_5 \frac{\ddot{X}}{\Delta^{5/2}} + b_6 \tag{Yilin.36}$$

$$\begin{aligned}
F_{1hX} &= -m_X \left( b_1 \frac{\dot{X}}{\sqrt{\Delta}} + b_2 \frac{\dot{\Delta}\dot{X}}{\Delta^{7/2}} + b_3 \frac{\dot{\Delta}\dot{\Theta}}{\Delta^{7/2}} + b_6 \right) \\
F_{2hXZ} &= 0 \quad F_{2hXX} = -\frac{m_X b_5}{\Delta^{5/2}} \quad F_{2hX\Theta} = -\frac{m_X b_4}{\Delta^{5/2}}
\end{aligned} \tag{Yilin.37}$$

and

$$-\frac{F_{h\Theta}}{m_\Theta} = -\dot{v}_\theta = -\ddot{\Theta} = c_1 \frac{\dot{\Theta}}{\sqrt{\Delta}} + c_2 \frac{\dot{\Delta}\dot{\Theta}}{\Delta^{7/2}} + c_3 \frac{\dot{\Delta}\dot{X}}{\Delta^{7/2}} + c_4 \frac{\ddot{X}}{\Delta^{5/2}} + c_5 \frac{\ddot{\Theta}}{\Delta^{5/2}} + c_6 \tag{Yilin.38}$$

$$\begin{aligned}
F_{1h\Theta} &= -m_\Theta \left( c_1 \frac{\dot{\Theta}}{\sqrt{\Delta}} + c_2 \frac{\dot{\Delta}\dot{\Theta}}{\Delta^{7/2}} + c_3 \frac{\dot{\Delta}\dot{X}}{\Delta^{7/2}} + c_6 \right) \\
F_{2h\Theta Z} &= 0 \quad F_{2h\Theta X} = -\frac{m_\Theta c_4}{\Delta^{5/2}} \quad F_{2h\Theta\Theta} = -\frac{m_\Theta c_5}{\Delta^{5/2}}
\end{aligned} \tag{Yilin.39}$$

We pose that  $M_{\alpha\beta} = \delta_{\alpha\beta}m_\alpha - F_{2h\alpha\beta}(\mathbf{x})$ , hence ( $m_X = m, m_\Theta = mr^2/2$ )

$$\begin{aligned}
M_{ZZ} &= m_Z + \frac{m_Z a_5}{\Delta^{5/2}} \\
M_{XX} &= m_X + \frac{m_X b_5}{\Delta^{5/2}} \quad M_{X\Theta} = \frac{m_X b_4}{\Delta^{5/2}} \\
M_{\Theta X} &= \frac{m_\Theta c_4}{\Delta^{5/2}} \quad M_{\Theta\Theta} = m_\Theta + \frac{m_\Theta c_5}{\Delta^{5/2}}
\end{aligned} \tag{Yilin.40}$$

We know that  $a_5 = -\frac{15\kappa\xi}{8}$ ,  $b_4 = \frac{\kappa\xi\epsilon}{12}$ ,  $b_5 = -\frac{\kappa\xi\epsilon}{12}$ ,  $c_4 = \frac{\kappa\xi\epsilon}{6}$ ,  $c_5 = -\frac{\kappa\xi\epsilon}{6}$ , so

$$M = \begin{pmatrix} m_Z - \frac{15\kappa\xi m_Z}{8\Delta^{5/2}} & 0 & 0 \\ 0 & m_X - \frac{\kappa\xi\epsilon m_X}{12\Delta^{5/2}} & \frac{\kappa\xi\epsilon m_X}{12\Delta^{5/2}} \\ 0 & \frac{\kappa\xi\epsilon m_\Theta}{6\Delta^{5/2}} & m_\Theta - \frac{\kappa\xi\epsilon m_\Theta}{6\Delta^{5/2}} \end{pmatrix} \tag{Yilin.41}$$

and its inverse matrix

$$M^{-1} = \begin{pmatrix} \frac{1}{m_Z - \frac{15\kappa\xi m_Z}{8\Delta^{5/2}}} & 0 & 0 \\ 0 & \frac{12\Delta^{5/2} - 2\kappa\xi\epsilon}{12\Delta^{5/2}m_X - 3\kappa\xi\epsilon m_X} & \frac{\kappa\xi\epsilon}{3m_\Theta(\kappa\xi\epsilon - 4\Delta^{5/2})} \\ 0 & \frac{2\kappa\xi\epsilon}{3m_X(\kappa\xi\epsilon - 4\Delta^{5/2})} & \frac{12\Delta^{5/2} - \kappa\xi\epsilon}{12\Delta^{5/2}m_\Theta - 3\kappa\xi\epsilon m_\Theta} \end{pmatrix} \tag{Yilin.42}$$

with the approximation expressed by the series of  $\kappa$ :

$$M_{app}^{-1} \approx \begin{pmatrix} \frac{1}{m_Z} + \frac{15\kappa\xi}{8\Delta^{5/2}m_Z} + \frac{225\kappa^2\xi^2}{64\Delta^5m_Z} & 0 & 0 \\ 0 & \frac{1}{m_X} + \frac{\kappa\xi\epsilon}{12\Delta^{5/2}m_X} + \frac{\kappa^2\xi^2\epsilon^2}{48\Delta^5m_X} & -\frac{\kappa(\xi\epsilon)}{12(\Delta^{5/2}m_\Theta)} - \frac{\kappa^2(\xi^2\epsilon^2)}{48(\Delta^5m_\Theta)} \\ 0 & -\frac{\kappa(\xi\epsilon)}{6(\Delta^{5/2}m_X)} - \frac{\kappa^2(\xi^2\epsilon^2)}{24(\Delta^5m_X)} & \frac{1}{m_\Theta} + \frac{\kappa\xi\epsilon}{6\Delta^{5/2}m_\Theta} + \frac{\kappa^2\xi^2\epsilon^2}{24\Delta^5m_\Theta} \end{pmatrix} \tag{Yilin.43}$$

Only taking the first-order correction, we could verify

$$M \cdot M_{app}^{-1} = \begin{pmatrix} 1 - \frac{225\kappa^2\xi^2}{64\Delta^5} & 0 & 0 \\ 0 & 1 - \frac{\kappa^2\xi^2\epsilon^2}{48\Delta^5} & \frac{\kappa^2\xi^2\epsilon^2m_X}{48\Delta^5m_\Theta} \\ 0 & \frac{\kappa^2\xi^2\epsilon^2m_\Theta}{24\Delta^5m_X} & 1 - \frac{\kappa^2\xi^2\epsilon^2}{24\Delta^5} \end{pmatrix} \approx \begin{pmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{pmatrix}$$

### 3 Numerical Practice

#### 3.1 JPCB2014: Discrete-Time Langevin Integration

*J. Phys. Chem. B, 2014, 118, 6466-6474, one article about Discrete-Time Langevin Integration.*

*For multiple dimensions, see its Support Information:*

[https://pubs.acs.org/doi/suppl/10.1021/jp411770f/suppl\\_file/jp411770f\\_si\\_001.pdf](https://pubs.acs.org/doi/suppl/10.1021/jp411770f/suppl_file/jp411770f_si_001.pdf)

Consider a Langevin equation

$$dv = \frac{f(t)}{m}dt - \gamma v dt + \sqrt{\frac{2\gamma}{\beta m}}dW(t)$$

we have

- Ornstein-Uhlenbeck operator for stochastic thermalization:  $\mathcal{L}_o = -\gamma \frac{\partial}{\partial v}v - \frac{\gamma}{\beta m} \frac{\partial^2}{\partial x^2}$
- Deterministic Newtonian evolutions:  $\mathcal{L}_v = \frac{f}{m}$ ,  $\mathcal{L}_r = v \frac{\partial}{\partial r}$
- Hamiltonian:  $\exp(\mathcal{L}_h \Delta t) \mathcal{H}(n) = \mathcal{H}(n+1)$

where  $n$  is the time step index and  $t = n\Delta t$ .

For this operator splitting, a single update step that advances the simulation clock by  $\Delta t$  is given explicitly by

$$\begin{aligned} \mathbf{v}\left(n + \frac{1}{4}\right) &= \sqrt{a} \cdot \mathbf{v}(n) + \left[\frac{1}{\beta}(\mathbf{1} - \mathbf{a}) \cdot \mathbf{m}^{-1}\right]^{1/2} \cdot \mathbf{N}^+(n) \\ \mathbf{v}\left(n + \frac{1}{2}\right) &= \mathbf{v}\left(n + \frac{1}{4}\right) + \frac{\Delta t}{2} \mathbf{b} \cdot \mathbf{m}^{-1} \cdot \mathbf{f}(n) \\ \mathbf{r}\left(n + \frac{1}{2}\right) &= \mathbf{r}(n) + \frac{\Delta t}{2} \mathbf{b} \cdot \mathbf{v}\left(n + \frac{1}{2}\right) \\ \mathcal{H}(n) &\rightarrow \mathcal{H}(n+1) \\ \mathbf{r}(n+1) &= \mathbf{r}\left(n + \frac{1}{2}\right) + \frac{\Delta t}{2} \mathbf{b} \cdot \mathbf{v}\left(n + \frac{1}{2}\right) \\ \mathbf{v}\left(n + \frac{3}{4}\right) &= \mathbf{v}\left(n + \frac{1}{2}\right) + \frac{\Delta t}{2} \mathbf{b} \cdot \mathbf{m}^{-1} \cdot \mathbf{f}(n+1) \\ \mathbf{v}(n+1) &= \sqrt{a} \cdot \mathbf{v}\left(n + \frac{3}{4}\right) + \left[\frac{1}{\beta}(\mathbf{1} - \mathbf{a}) \cdot \mathbf{m}^{-1}\right]^{1/2} \cdot \mathbf{N}^-(n+1) \end{aligned}$$

where  $a_{ij} = \delta_{ij} \exp(-\gamma_i \Delta t)$ ,  $\mathcal{N}^\pm$  are independent normally distributed random variables with zero mean and unit variance,  $b_{ij} = \delta_{ij} \sqrt{\frac{2}{\gamma_i \Delta t} \tanh \frac{\gamma_i \Delta t}{2}}$



### 3.2 Update $\gamma_{\text{eff}}$

We have obtained the  $\gamma$  matrix in the subsection 2.2, without mass vector. Here we update the effective matrix  $\gamma_{\text{eff}}$  with  $M^{-1}$ , starting from

$$\begin{aligned} m_\alpha \cdot \dot{v}_\alpha &= F_\alpha(t) - m_\alpha \cdot \gamma_{\alpha\beta} v_\beta = [F_{1\alpha}(\mathbf{x}) + F_{2\alpha\beta}(\mathbf{x}) \dot{v}_\beta] - m_\alpha \cdot \gamma_{\alpha\beta} v_\beta \\ m_\alpha \cdot \dot{v}_\alpha - F_{2\alpha\beta}(\mathbf{x}) \dot{v}_\beta &= (m_\alpha \cdot \delta_{\alpha\beta} - F_{2\alpha\beta}(\mathbf{x})) \dot{v}_\beta = F_{1\alpha}(\mathbf{x}) - m_\alpha \cdot \gamma_{\alpha\beta} v_\beta \\ \dot{v}_\beta &= (m_\alpha \cdot \delta_{\alpha\beta} - F_{2\alpha\beta}(\mathbf{x}))^{-1} (F_{1\alpha}(\mathbf{x}) - m_\alpha \cdot \gamma_{\alpha\beta} v_\beta) = M_{\alpha\beta}^{-1} (F_{1\alpha}(\mathbf{x}) - m_\alpha \cdot \gamma_{\alpha\beta} v_\beta) \end{aligned}$$

Note that the  $\gamma$  matrix above only contains terms about first derivatives

$$\begin{aligned} \gamma_{Z\beta} v_\beta &= a_1 \frac{\dot{\Delta}}{\Delta^{3/2}} + a_2 \frac{\dot{\Delta}^2}{\Delta^{9/2}} + a_3 \frac{\dot{\Theta}^2}{\Delta^{7/2}} + a_3 \frac{\dot{X}^2}{\Delta^{7/2}} + a_4 \frac{\dot{\Theta}\dot{X}}{\Delta^{7/2}} \\ \gamma_{X\beta} v_\beta &= b_1 \frac{\dot{X}}{\sqrt{\Delta}} + b_2 \frac{\dot{\Delta}\dot{X}}{\Delta^{7/2}} + b_3 \frac{\dot{\Delta}\dot{\Theta}}{\Delta^{7/2}} \\ \gamma_{\Theta\beta} v_\beta &= c_1 \frac{\dot{\Theta}}{\sqrt{\Delta}} + c_2 \frac{\dot{\Delta}\dot{\Theta}}{\Delta^{7/2}} + c_3 \frac{\dot{\Delta}\dot{X}}{\Delta^{7/2}} \end{aligned}$$

To avoid the possible confusion, we write  $\gamma^*$  below. Consider  $dv = \frac{f(t)}{m} dt - \gamma v dt + \sqrt{\frac{2\gamma}{\beta m}} dW$ , we have  $\gamma_{\text{eff}}$  :

$$\gamma_{\text{eff}} = M_{\alpha\beta}^{-1} \cdot \begin{pmatrix} m_Z & 0 & 0 \\ 0 & m_X & 0 \\ 0 & 0 & m_\Theta \end{pmatrix} \cdot \gamma_{\alpha\beta}^* \quad (\text{Yilin.44})$$

Surprisingly, we recover almost the same  $\gamma_{\alpha\beta}$  shown previously

$$\begin{aligned} \gamma_{\text{eff},zz} &= \frac{\xi}{\Delta^{3/2}} + \kappa \left( \frac{15\xi^2}{8\Delta^4} + \frac{21\xi v_z}{4\Delta^{9/2}} \right) + O(\kappa^2) \\ \gamma_{\text{eff},xx} &= \frac{2\xi\epsilon}{3\sqrt{\Delta}} + \frac{\kappa\xi \left( 4\sqrt{\Delta}\xi\epsilon^2 + 18v_z + 57\epsilon v_\theta \right)}{72\Delta^{7/2}} + O(\kappa^2) \\ \gamma_{\text{eff},\theta\theta} &= \frac{4\xi\epsilon}{3\sqrt{\Delta}} + \frac{\kappa\xi \left( 8\sqrt{\Delta}\xi\epsilon^2 + 57\epsilon v_z + 9v_z \right)}{36\Delta^{7/2}} + O(\kappa^2) \\ \gamma_{\text{eff},zx} &= \frac{\kappa\xi \left( (\epsilon + 3)v_\theta - 3v_X \right)}{12\Delta^{7/2}} + O(\kappa^2) \\ \gamma_{\text{eff},z\theta} &= -\frac{\kappa \left( \xi(3v_\theta + (\epsilon - 3)v_X) \right)}{12\Delta^{7/2}} + O(\kappa^2) \\ \gamma_{\text{eff},x\theta} &= -\frac{\kappa \left( \xi \left( 16\Delta^3\xi\epsilon^2 + 36\Delta^{5/2}(\epsilon + 1)v_z \right) \right)}{144\Delta^6} + O(\kappa^2) \end{aligned}$$

### 3.3 Possible modification

Here we consider the following approaches for the sake of better numerical practices

- Solve Langevin equation numerically or solve Fokker-Planck equation directly;
- Add second derivatives or not; ( $b_4 = b_5 = c_4 = c_5 = 0$ )
- Ignore rotation and fix  $\Theta = 0$
- Modify Gaussian random force with "Heaviside" function or not; to avoid sudden collapse  $z < 0$
- How to determine the initial  $z$  value near the equilibrium position;
- Add Coulomb interaction or not; ( $\frac{Q^2}{4\pi\epsilon z} \exp(-\lambda_D/z)$ )
- Diagonalize M matrix or not? physical meaning?
- Consider  $\kappa$  correction to which order?