



# ECE497: Introduction to Mobile Robotics Lecture 2

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# Quote of the Week

*“In the fifties, it was predicted that in 5 years robots would be everywhere.*

*In the sixties, it was predicted that in 10 years robots would be everywhere.*

*In the seventies, it was predicted that in 20 years robots would be everywhere.*

*In the eighties, it was predicted that in 40 years robots would be everywhere...”*

Marvin Minsky



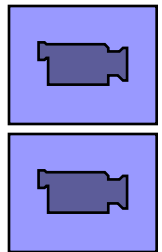
# Kinematics

## Chapter 3



# Mobile Robot Kinematics (3.1)

- Mobile Robot Kinematics is the dynamic model of how a mobile robot behaves
- Kinematics is a description of mechanical behavior of the robot for **design** and **control**
- Mobile Robot Kinematics is used for:
  - ☐ Position estimation
  - ☐ Motion estimation



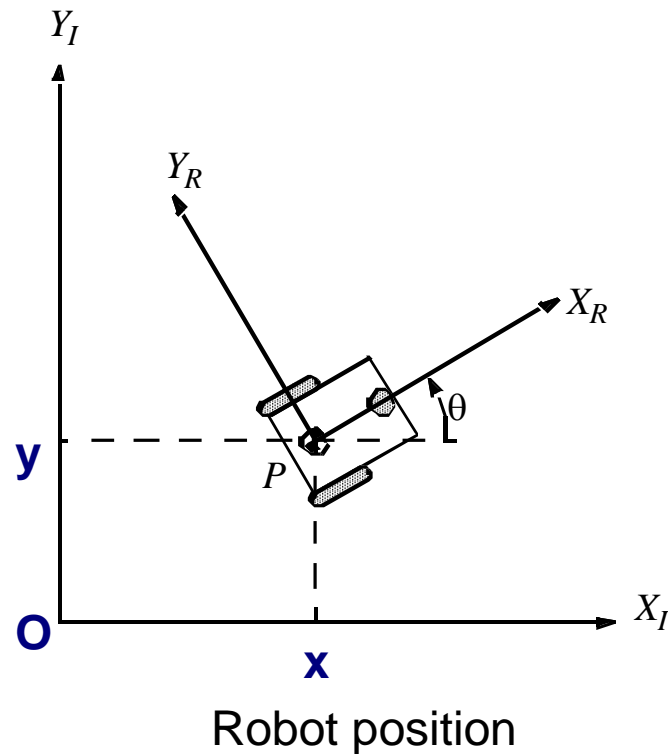


# Mobile Robot Kinematics, 2

- Robots move unbounded with respect to their environment
  - There is no direct way to measure robot position
  - Position must be integrated over time
  - The integration leads to inaccuracies in position and motion estimation
- Each wheel contributes to the robot's motion and imposes constraints on robot's motion
- All of the constraints must be expressed with respect to the reference frame



# Robot Reference Frame (3.2.1)



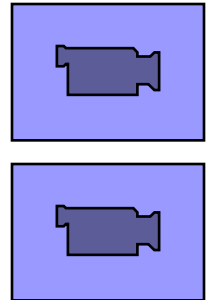
- The robot's reference frame is three dimensional including position on the plane and the orientation,  $\{X_R, Y_R, \theta\}$
- The axes  $\{X_I, Y_I\}$ , define inertial global reference frame with origin,  $O$
- The angular difference between the global and reference frames is  $\theta$
- Point  $P$  on the robot chassis in the global reference frame is specified by coordinates  $(x, y)$

$$\xi_I = \begin{bmatrix} x & y & \theta \end{bmatrix}^T$$



# Relative Positioning: Odometry and Kinematics

- Given wheel velocities at any given time, compute position/orientation for any future time
- Advantages
  - Self-contained
  - Can get positions anywhere along curved paths
  - Always provides an “estimate” of position
- Disadvantages
  - Requires accurate measurement of wheel velocities over time, including measuring acceleration and deceleration
  - Position error grows over time





# Orthogonal Rotation Matrix

The **orthogonal rotation matrix** is used to map motion in the global reference  $\{X_I, Y_I\}$  frame to motion in the robot's local reference frame  $\{X_R, Y_R\}$

$$R(\theta) = \begin{bmatrix} \cos \theta & \sin \theta & 0 \\ -\sin \theta & \cos \theta & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

The orthogonal rotation matrix is used to convert robot velocity in the global reference frame to components of motion along the robot's local axes  $\{X_R, Y_R\}$

$$\dot{\xi}_R = R(\theta)\dot{\xi}_I = R(\theta) \cdot \begin{bmatrix} \dot{x} & \dot{y} & \dot{\theta} \end{bmatrix}^T$$

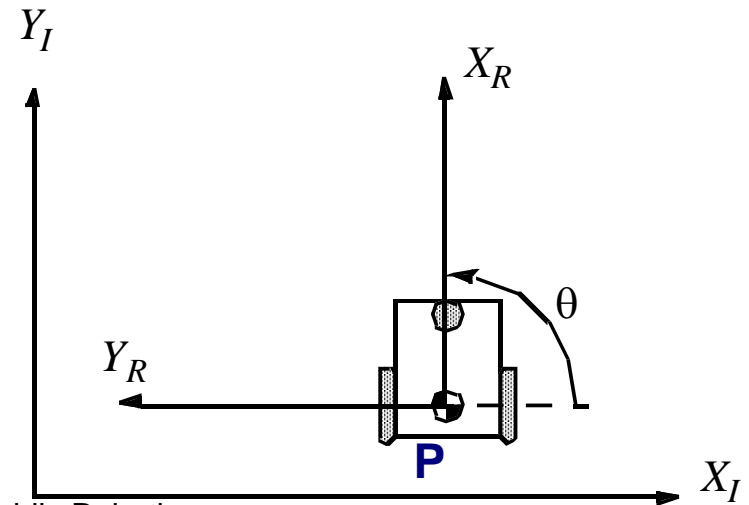




# Rotation Example

- Given some robot velocity  $(\dot{x}, \dot{y}, \dot{\theta})$  in the global reference frame
- Suppose that the robot is at P and  $\theta = \pi/2$  with respect to the global reference frame
- The motion along  $X_R$  and  $Y_R$  due to  $\theta$  is

$$\dot{\xi}_R = R\left(\frac{\pi}{2}\right)\dot{\xi}_I = \begin{bmatrix} 0 & 1 & 0 \\ -1 & 0 & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} \dot{x} \\ \dot{y} \\ \dot{\theta} \end{bmatrix} = \begin{bmatrix} \dot{y} \\ -\dot{x} \\ \dot{\theta} \end{bmatrix}$$





# Rotation Example 2

If a robot velocity has a velocity of  $(\dot{x}, \dot{y}, \dot{\theta})$  in the global reference frame and is positioned at P and  $\theta = \pi/3$  with respect to the global reference frame. What is the motion along  $X_R$  and  $Y_R$  due to  $\theta$  with respect to the robot reference?

$$\dot{\xi}_R = R\left(\frac{\pi}{3}\right)\dot{\xi}_I = \begin{bmatrix} \cos \pi/3 & \sin \pi/3 & 0 \\ -\sin \pi/3 & \cos \pi/3 & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} \dot{x} \\ \dot{y} \\ \dot{\theta} \end{bmatrix} = \begin{bmatrix} 0.5\dot{x} + 0.866\dot{y} \\ -0.866\dot{x} + 0.5\dot{y} \\ \dot{\theta} \end{bmatrix}$$

This robot will rotate with the same speed with respect to the robot reference frame as the global reference frame. However the linear velocity along the robot's x-axis and y-axis are a combination of the velocities with respect to the global reference frame.



# Rotation Example 2 (cont.)

What if the robot velocity is (2 cm/s, 3 cm/s, 5 rad/s) with respect to the global reference frame, what is the velocity with respect to the robot's local reference frame?

$$\dot{\xi}_R = R\left(\frac{\pi}{3}\right)\dot{\xi}_I = \begin{bmatrix} \cos \pi/3 & \sin \pi/3 & 0 \\ -\sin \pi/3 & \cos \pi/3 & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 2 \\ 3 \\ 5 \end{bmatrix} = \begin{bmatrix} 3.5981 \\ -0.23205 \\ 5 \end{bmatrix}$$

What if the robot velocity is (2 cm/s, 3 cm/s, 5 rad/s) with respect to the robot's local reference frame, what is the robot's velocity with respect to the global reference frame?

$$\dot{\xi}_I = R\left(\frac{\pi}{3}\right)^{-1} \dot{\xi}_R = \begin{bmatrix} \cos \pi/3 & -\sin \pi/3 & 0 \\ \sin \pi/3 & \cos \pi/3 & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 2 \\ 3 \\ 5 \end{bmatrix} = \begin{bmatrix} -1.5981 \\ 3.2321 \\ 5 \end{bmatrix}$$

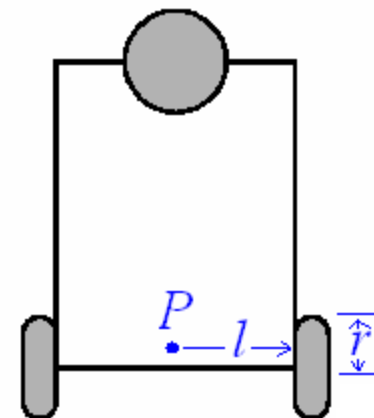


# Forward Kinematics Model

## Differential Drive Robot (3.2.2)

- *Forward Kinematics* provides an estimate of the robot's position given its geometry and speed of its wheels
- It requires accurate measurement of the wheel velocities over time
- However, position error (accumulation error) grows with time
- A differential drive robot with wheels that have speeds of  $\dot{\phi}_1$  and  $\dot{\phi}_2$  has the following forward kinematic model

$$\dot{\xi}_I = \begin{bmatrix} \dot{x} \\ \dot{y} \\ \dot{\theta} \end{bmatrix} = f(l, r, \theta, \dot{\phi}_1, \dot{\phi}_2)$$





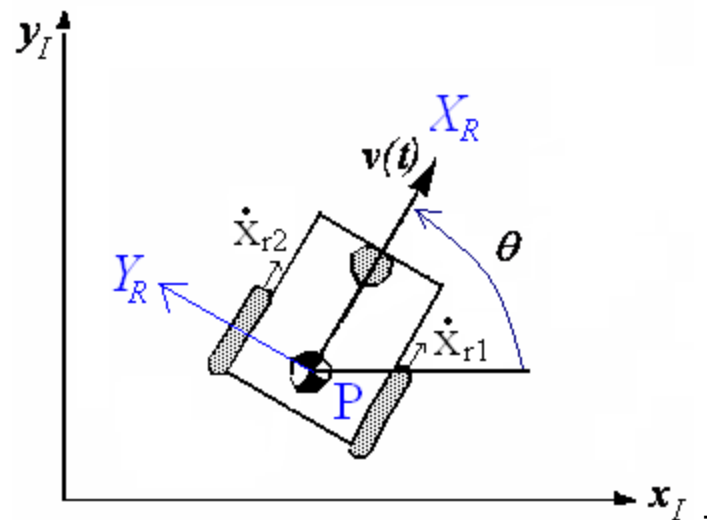
# Forward Kinematics Model

## Differential Drive Robot (3.2.2)

- To compute the robot's motion in the global reference frame from the local reference frame use  $\dot{\xi}_I = R(\theta)^{-1} \dot{\xi}_R$
- To find the linear velocity in the direction of  $+X_R$ , each wheel contributes one half of the total speed.

$$\dot{x}_{r1} = (1/2)r\dot{\phi}_1 \quad \dot{x}_{r2} = (1/2)r\dot{\phi}_2$$

- Since the wheels cannot compute sideways motion,  $Y_R$  is zero



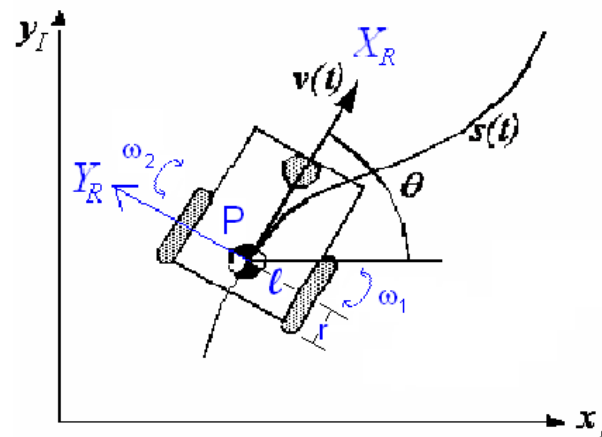


# Forward Kinematics, cont.

The angular velocity about  $\theta$  is calculated from the contribution from the two wheels. The right wheel,  $\omega_1$  contributes counterclockwise rotation about point P and the left wheel  $\omega_2$  contributes clockwise rotation about point P both with a radius of  $2l$

$$\omega_1 = \frac{r\dot{\phi}_1}{2l} \quad \omega_2 = -\frac{r\dot{\phi}_2}{2l}$$

$$\dot{\xi}_I = R(\theta)^{-1} \dot{\xi}_R = R(\theta)^{-1} \begin{bmatrix} \dot{x}_r \\ \dot{y}_r \\ \dot{\theta}_r \end{bmatrix} = R(\theta)^{-1} \begin{bmatrix} \dot{x}_{r1} + \dot{x}_{r2} \\ 0 \\ \omega_1 + \omega_2 \end{bmatrix} = \begin{bmatrix} \cos \theta & -\sin \theta & 0 \\ \sin \theta & \cos \theta & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} \frac{r\dot{\phi}_1}{2} + \frac{r\dot{\phi}_2}{2} \\ 0 \\ \frac{r\dot{\phi}_1}{2l} - \frac{r\dot{\phi}_2}{2l} \end{bmatrix}$$





# Forward Kinematics Example

A robot is positioned at a  $60^\circ$  angle with respect to the global reference frame and has wheels with a radius of 1 cm. These wheels are 2 cm from the center of the chassis. If the speeds of wheels 1 and 2, are 4 cm/s and 2 cm/s, respectively. What is the robot velocity with respect to the global reference frame?

$$\theta = \pi / 3$$

$$r = 1$$

$$l = 2$$

$$\dot{\phi}_1 = 4$$

$$\dot{\phi}_2 = 2$$

$$\dot{x}_{r1} = \frac{r\dot{\phi}_1}{2}$$

$$\dot{x}_{r2} = \frac{r\dot{\phi}_2}{2}$$

$$\omega_1 = \frac{r\dot{\phi}_1}{2l}$$

$$\omega_2 = -\frac{r\dot{\phi}_2}{2l}$$

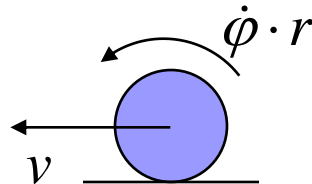
$$\dot{\xi}_I = R(\theta)^{-1} \begin{bmatrix} \dot{x}_{r1} + \dot{x}_{r2} \\ 0 \\ \omega_1 + \omega_2 \end{bmatrix} = \begin{bmatrix} \cos \pi/3 & -\sin \pi/3 & 0 \\ \sin \pi/3 & \cos \pi/3 & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 3.0 \\ 0 \\ 0.5 \end{bmatrix} = \begin{bmatrix} 1.5 \\ 2.5981 \\ 0.5 \end{bmatrix}$$

This robot will move instantaneously along the global reference frame x-axis with a speed of 1.5 cm/s and along the y-axis at 2.5981 cm/s while rotating with a speed of 0.5 radians/second.



# Wheel Kinematic Constraints (3.2.3)

- To create a kinematic model express constraints on the motions of individual wheels
- These motions are combined to compute motion for the whole robot
- Assumptions:
  - The wheel plane must remain vertical at all times
  - There is one single point of contact between the wheel and ground
  - There is no sliding at the single point of contact
  - Movement on a horizontal plane
  - Wheels not deformable
  - Pure rolling ( $v = 0$  at contact point)
  - No slipping, skidding or sliding
  - No friction for rotation around contact point
  - Steering axes orthogonal to the surface
  - Wheels connected by rigid frame (chassis)
- Constraints
  - The wheel must roll when motion takes place in the opposite direction
  - The wheel must not slide orthogonal to the wheel plane



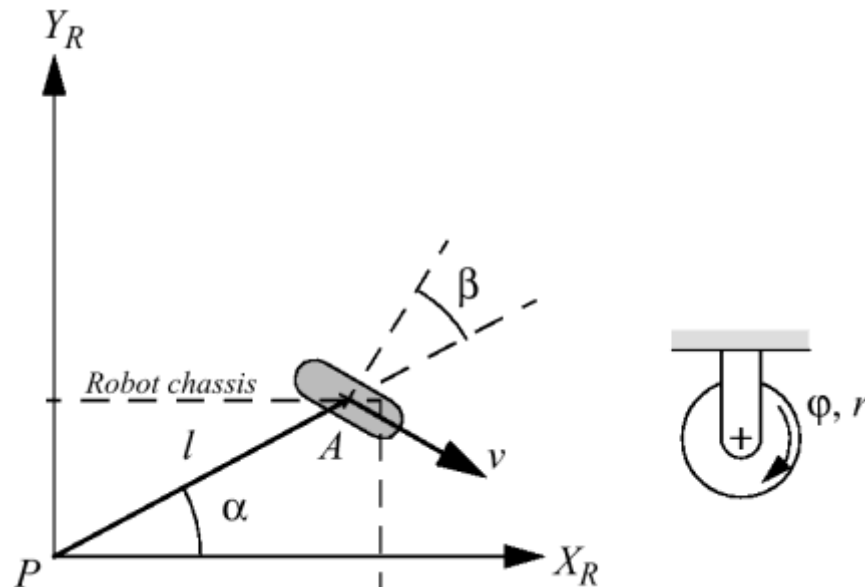
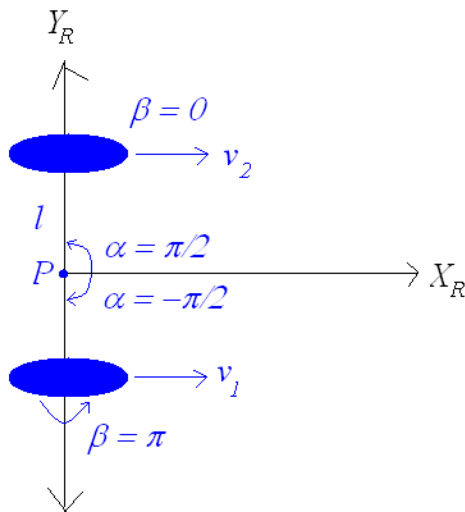




# Wheel Kinematic Constraints:

## Fixed Standard Wheel (3.2.3.1)

The *differential drive fixed standard wheel robot* in the text with right wheel 1 ( $\alpha = -\pi/2$ ,  $\beta = \pi$ ) and left wheel 2 ( $\alpha = \pi/2$ ,  $\beta = 0$ ) has the closest configuration to the tracked mobile robot used in this course and will be the one used for the kinematic analysis.





# Fixed Standard Wheel (3.2.3.1)

There are 2 wheel kinematic constraints:

- Rolling – the wheel must roll when motion takes place in the appropriate direction

$$[\sin(\alpha + \beta) \quad -\cos(\alpha + \beta) \quad (-l)\cos \beta]R(\theta)\dot{\xi}_1 - r\dot{\phi} = 0$$

- Sliding – there should be no lateral slippage (i.e. the wheel must not slide orthogonal to the wheel plane)

$$[\cos(\alpha + \beta) \quad \sin(\alpha + \beta) \quad l \sin \beta]R(\theta)\dot{\xi}_1 = 0$$



# Fixed Standard Wheel (3.2.4 – 3.2.5)

- Rolling constraint:  $J_1(\beta_s)R(\theta)\dot{\xi}_1 - J_2\dot{\phi} = 0$ 
  - $J_1$  is the matrix for projections for all wheels to their motions along their individual wheel planes
  - $J_2$  is an  $N \times N$  matrix whose entries are radii  $r$  of all wheels
- Sliding constraint:  $C_1(\beta_s)R(\theta)\dot{\xi}_1 = 0$ 
  - $C_1$  is the matrix for projections for all wheels to their components of motion orthogonal to their wheel planes
- For the differential-drive robot, the rolling and sliding constraints are

$$\begin{bmatrix} J_1(\beta_s) \\ C_1(\beta_s) \end{bmatrix} R(\theta) \dot{\xi}_1 = \begin{bmatrix} J_2 \dot{\phi} \\ 0 \end{bmatrix} \qquad \begin{bmatrix} \begin{bmatrix} 1 & 0 & l \\ 1 & 0 & -l \\ 0 & 1 & 0 \end{bmatrix} \\ \end{bmatrix} R(\theta) \dot{\xi}_1 = \begin{bmatrix} J_2 \dot{\phi} \\ 0 \end{bmatrix}$$

$$\dot{\xi}_1 = R(\theta)^{-1} \begin{bmatrix} 0.5 & 0.5 & 0 \\ 0 & 0 & 1 \\ 1/2l & -1/2l & 0 \end{bmatrix} \begin{bmatrix} J_2 \dot{\phi} \\ 0 \end{bmatrix}$$



# Differential drive robot example (3.2.5.1)

A differential drive robot is positioned at a  $60^\circ$  angle with respect to the global reference frame and has wheels with a radius of 1 cm that are 2 cm from the center of the chassis. If the speeds of wheels 1 and 2, are 4 cm/s and 2 cm/s, respectively. What is the robot velocity with respect to the global reference frame?

( $r = 1$  cm,  $l = 2$  cm,  $\theta = \pi/3$ ,  $v_1 = 4$  cm/s,  $v_2 = 2$  cm/s)

In summary, given a robot's kinematic constraints and wheel motion it is possible to find the motion with respect to the global reference frame. This robot will move instantaneously along the global reference frame x-axis with a speed of 1.5 cm/s and along the y-axis at 2.5981 cm/s while rotating with a speed of 0.5 radians/second (**same as previous example**)

$$\begin{bmatrix} J_1(\beta_s) \\ C_1(\beta_s) \end{bmatrix} R(\theta) \dot{\xi}_I = \begin{bmatrix} J_2 \dot{\phi} \\ 0 \end{bmatrix}$$

$$\begin{bmatrix} 1 & 0 & l \\ 1 & 0 & -l \\ 0 & 1 & 0 \end{bmatrix} R(\theta) \dot{\xi}_I = \begin{bmatrix} r \dot{\phi}_1 \\ r \dot{\phi}_2 \\ 0 \end{bmatrix}$$

$$\begin{bmatrix} 1 & 0 & 2 \\ 1 & 0 & -2 \\ 0 & 1 & 0 \end{bmatrix} R\left(\frac{\pi}{3}\right) \dot{\xi}_I = \begin{bmatrix} 4 \\ 2 \\ 0 \end{bmatrix}$$

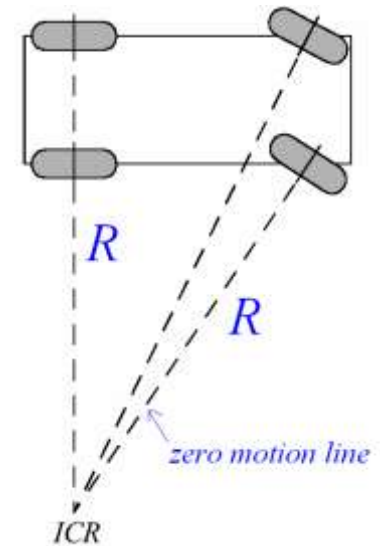
$$\dot{\xi}_I = R\left(\frac{\pi}{3}\right)^{-1} \begin{bmatrix} 0.5 & 0.5 & 0 \\ 0 & 0 & 1 \\ 0.25 & -0.25 & 0 \end{bmatrix} \begin{bmatrix} 4 \\ 2 \\ 0 \end{bmatrix}$$

$$\dot{\xi}_I = \begin{bmatrix} 1.5 \\ 2.5981 \\ 0.5 \end{bmatrix}$$



# Degree of Mobility (3.3.1)

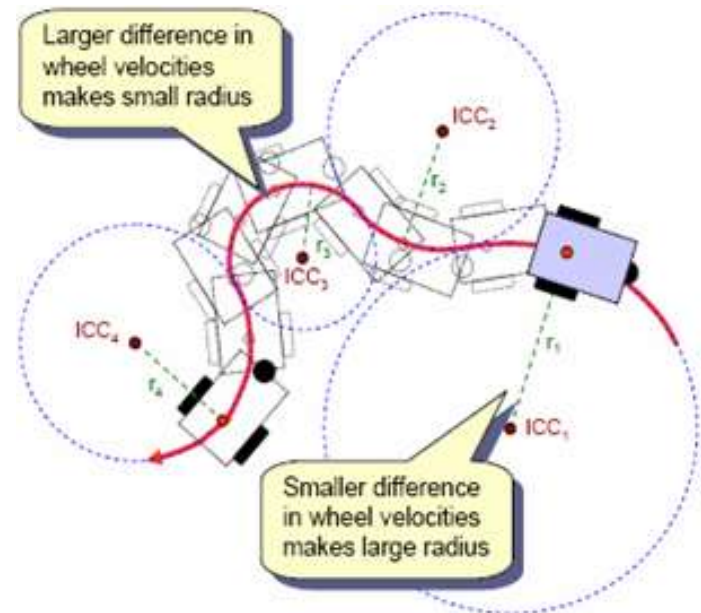
- The ***degree of mobility*** quantifies the degrees of controllable freedom of a mobile robot based on changes to wheel velocity
- The kinematic constraints of a robot with respect to the degree of mobility can be demonstrated geometrically by using the ***instantaneous center of rotation (ICR)***





# Instantaneous Center of Rotation (ICR)

- The **ICR** has a *zero motion line* drawn through the horizontal axis perpendicular to the wheel plane
- The wheel moves along a radius  $R$  with center on the zero motion line, the center of the circle is the **ICR**
- **ICR** is the point around which each wheel of the robot makes a circular course
- The **ICR** changes over time as a function of the individual wheel velocities

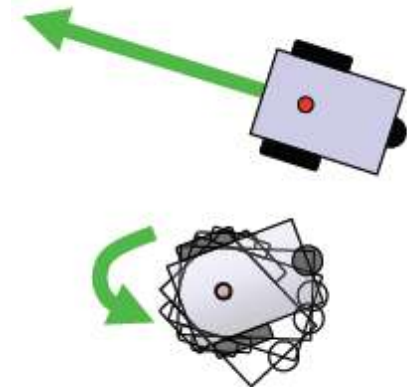


<http://www.scs.carleton.ca/~lanthier/teaching/COMP4900A/Notes/5%20-%20PositionEstimation.pdf>



# Instantaneous Center of Rotation (ICR)

- When  $R$  is infinity, wheel velocities are equivalent and the robot moves in a straight line
- When  $R$  is zero, wheel velocities are the negatives of each other and the robot spins in place
- All other cases,  $R$  is finite and non-zero and the robot follows a curved trajectory about a point which is a distance  $R$  from the robot's center
- Note that differential drive robot's are very sensitive to the velocity differences between the two wheels...making it hard to move in a perfectly straight line

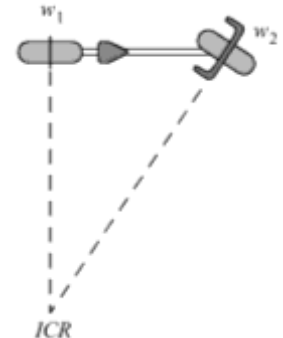


<http://www.scs.carleton.ca/~lanthier/teaching/COMP4900A/Notes/5%20-%20PositionEstimation.pdf>



# Degree of Mobility (3.3.1)

- *Robot mobility* is the ability of a robot chassis to directly move in the environment
- The *degree of mobility* quantifies the degrees of controllable freedom based on changes to wheel velocity
- *Robot mobility* is a function of the number of constraints on the robot's motion, not the number of wheels
  - A bicycle has 2 independent kinematic constraints
    - each wheel contributes a constraint, or a zero motion line
  - A differential drive robot has one independent kinematic constraint (see Figures 3.12, 3.13)
    - ICR lies along a line, 2<sup>nd</sup> wheel imposes no additional kinematic constraint
- So the bicycle has 2 independent kinematic constraints while the differential drive robot has only one
- Robot chassis kinematics is a function of the set of *independent* constraints on the standard wheels
- The *rank* of the matrix of all of the sliding constraints imposed by wheels of the mobile robot is the number of independent constraints







# Mobile Robot Maneuverability: (3.3.1)

## Degree of Mobility

- Robot chassis kinematics is a function of the set of *independent constraints*, or the rank of the sliding constraints
  - the greater the rank of  $C_1(\beta_s)$ , the more constrained the mobility
- In the differential drive robot, the matrix has 2 constraints but a rank of one

$$(l_1 = l_2, \alpha_1 + \pi = \alpha_2, \beta_1 - \pi = \beta_2)$$

$$C_1(\beta_s) = C_{1f} = \begin{bmatrix} \cos(\alpha_1 + \beta_1) & \sin(\alpha_1 + \beta_1) & l \sin(\beta_1) \\ \cos(\alpha_1 + \beta_1) & \sin(\alpha_1 + \beta_1) & l \sin(\beta_1 - \pi) \end{bmatrix}$$



# Mobile Robot Maneuverability: (3.3.1)

## Degree of Mobility

- no standard wheels means the  $\text{rank}[C_1(\beta_s)] = 0$
- all directions constrained means the  $\text{rank}[C_1(\beta_s)] = 3$
- therefore, the robot's ***degree of mobility*** is

$$\delta_m = \dim N[C_1(\beta_s)] = 3 - \text{rank}[C_1(\beta_s)], \text{ where } 0 \leq \text{rank}[C_1(\beta_s)] \leq 3$$

- this dimensionality of the nullspace (***dimN***) of the matrix ( $C_1(\beta_s)$ ) is a measure of the ***number of degrees of freedom*** of the robot chassis that can be manipulated through changes in wheel velocity



# Mobile Robot Maneuverability: (3.3.1)

## Differential Drive Chassis

- Two fixed standard wheels
  - wheels on same axle
  - the 2nd wheel adds no independent kinematic constraints
  - $\text{rank}[C_1(\beta_s)] = 1$  and  $\delta_m = 2$
- A differential drive robot can control both the rate of its change in orientation and its forward/reverse speed *by manipulating wheel velocities*
- The ICR lies on the infinite line extending from the wheels horizontal axis



# Mobile Robot Maneuverability: (3.3.2)

## Degree of Steerability

- The **degree of steerability**,  $\delta_s$ , of a mobile robot is defined by the number of independently controllable steering parameters,  $\delta_s = \text{rank}[C_{1s}(\beta_s)]$ 
  - An increase in the rank of  $C_1(\beta_s)$  implies more kinematic constraints and less mobility
  - Conversely, an increase in the rank of  $C_{1s}(\beta_s)$  implies more degrees of steering freedom and greater eventual maneuverability
  - Since  $C_1(\beta_s)$  includes  $C_{1s}(\beta_s)$ , a steered standard wheel can increase steerability and decrease mobility
  - The particular orientation of a steered standard wheel at any instant imposes a kinematic constraint
  - However, the ability to change that orientation can lead to an additional degree of maneuverability
- Range of  $\delta_s$ :  $0 \leq \delta_s \leq 2$ 
  - No steerable standard wheels means  $\delta_s = 0$
  - No fixed standard wheels,  $\delta_s = 2$

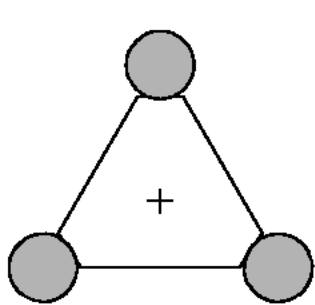


# Degree of Maneuverability (3.3.3)

- The robot's *overall degrees of freedom (DOF)* or *degree of maneuverability* is defined in terms of mobility and steerability:

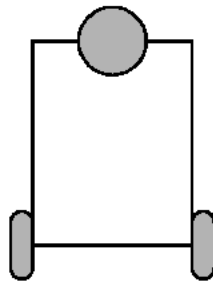
$$\delta_M = \delta_m + \delta_s$$

- Includes degrees of freedom that a robot manipulates through wheel velocity and degrees of freedom that it indirectly manipulates through steering configuration and moving
- Two robots with same  $\delta_M$  are not necessarily equal (i.e. tricycle and differential drive robot)
- For any robot with  $\delta_M = 2$ , the ICR is always constrained to *lie on a line*
- For any robot with  $\delta_M = 3$ , the ICR is not constrained and can *be set to any point on the plane*



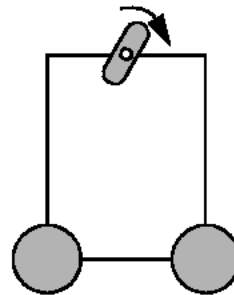
*Omnidirectional*

$$\begin{aligned}\delta_M &= 3 \\ \delta_m &= 3 \\ \delta_s &= 0\end{aligned}$$



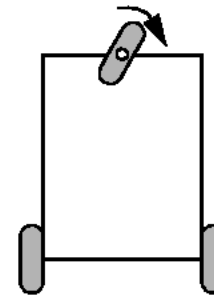
*Differential*

$$\begin{aligned}\delta_M &= 2 \\ \delta_m &= 2 \\ \delta_s &= 0\end{aligned}$$



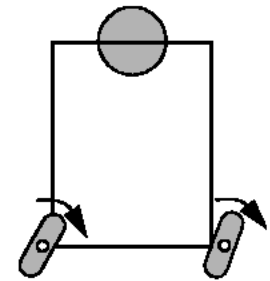
*Omni-Steer*

$$\begin{aligned}\delta_M &= 3 \\ \delta_m &= 2 \\ \delta_s &= 1\end{aligned}$$



*Tricycle*

$$\begin{aligned}\delta_M &= 2 \\ \delta_m &= 1 \\ \delta_s &= 1\end{aligned}$$



*Two-Steer*

$$\begin{aligned}\delta_M &= 3 \\ \delta_m &= 1 \\ \delta_s &= 2\end{aligned}$$



# Mobile Robot Workspace (3.4)

- Robot maneuverability is equivalent to its control degrees of freedom
- A robot's space of possible configurations in an environment is the *workspace* and it can exceed the number of control degrees of freedom,  $\delta_M$ .
- The workspace *degrees of freedom (DOF)* governs the robot's ability to achieve various poses
- The number of dimensions in the velocity space of a robot is called the *differential degrees of freedom (DDOF)*
- The *DDOF* governs a robot's ability to achieve various paths
- The *DDOF* is always equal to the degree of mobility,  $\delta_m$ ,  
$$(DDOF \leq \delta_M \leq DOF)$$
- The objective of a *kinematic controller* is to follow a trajectory described by its position and/or velocity profiles as function of time.
- Motion control is not straight forward because mobile robots are non-holonomic systems (may require the derivative of a position variable).
- It is only through non-holonomic constraints (imposed by fixed or steerable wheels) that a robot can achieve a workspace with degrees of freedom exceeding its differential degrees of freedom  $DOF > DDOF$



## Path and trajectory considerations (3.4.3)

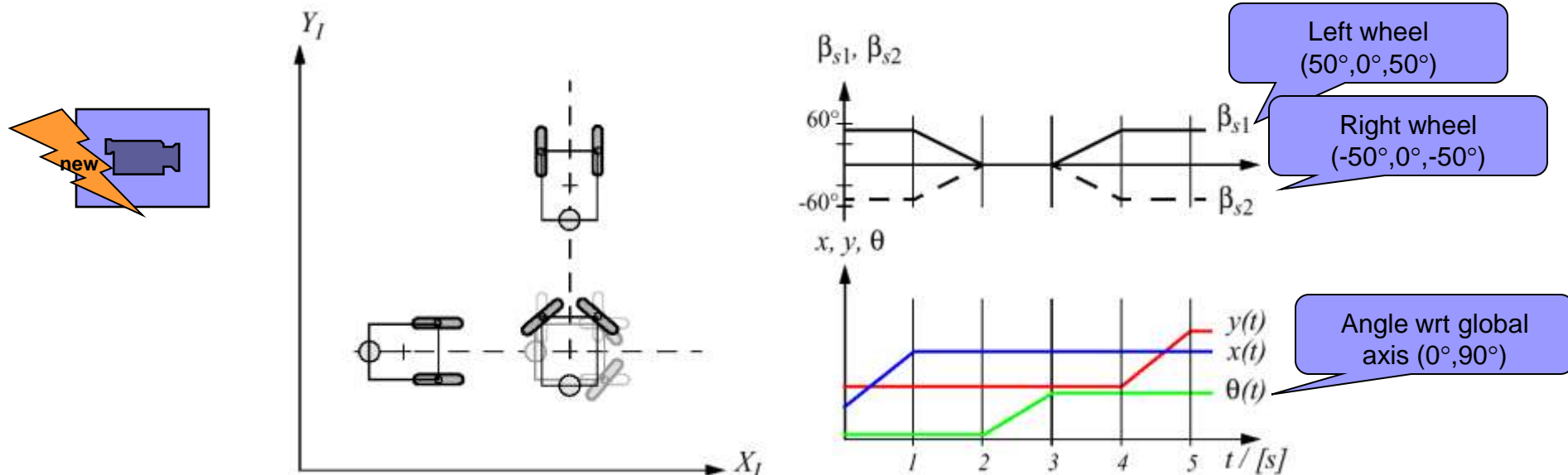
- There is a difference between DOF granted by steering versus direction control of wheel velocity
- The difference is in the context of *trajectories* rather than paths
- A trajectory is like a path but it has the additional dimension of *time*
- *Motion control (kinematic control)* is not straight forward because mobile robots are non-holonomic systems.



# Path and trajectory considerations

## Two-steer robot (3.4.3)

A robot has a goal trajectory in which the robot moves along axis  $X_I$  at a constant speed of 1 m/s for 1 second. Wheels adjust for 1 second. The robot then turns counterclockwise at 90 degrees in 1 second. Wheels adjust for 1 second. Finally, the robot then moves parallel to axis  $Y_I$  for 1 final second.



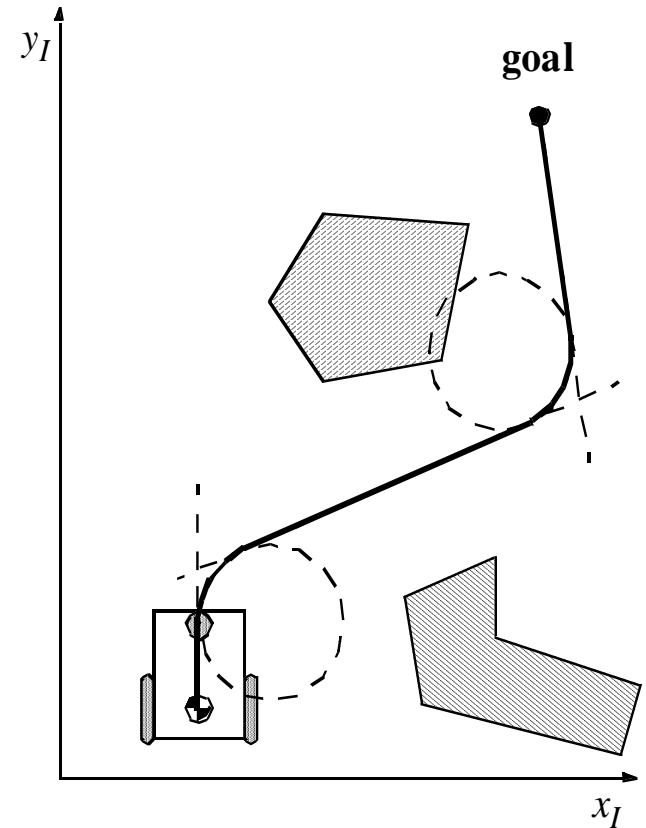




# Motion Control:

## Open Loop Control (3.6.1)

- The objective of a kinematic controller is to follow a trajectory described by its position and/or velocity profiles as a function of time.
- One method is to divide the trajectory (path) into motion segments of clearly defined shape:
  - straight lines and segments of a circle.  
(open loop control)
- control problem:
  - pre-compute a smooth trajectory based on line and circle segments





# Motion Control:

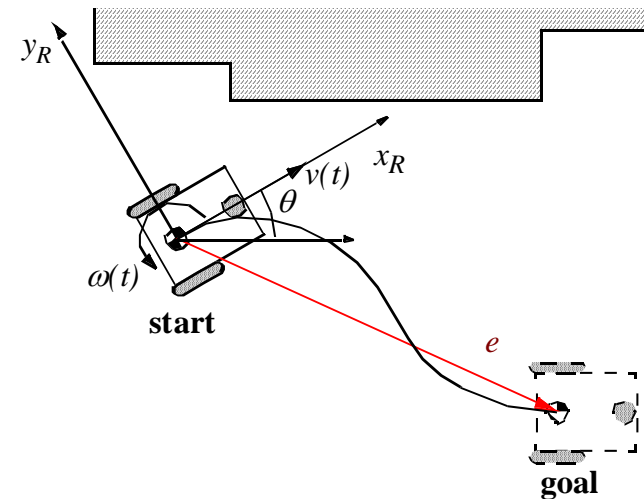
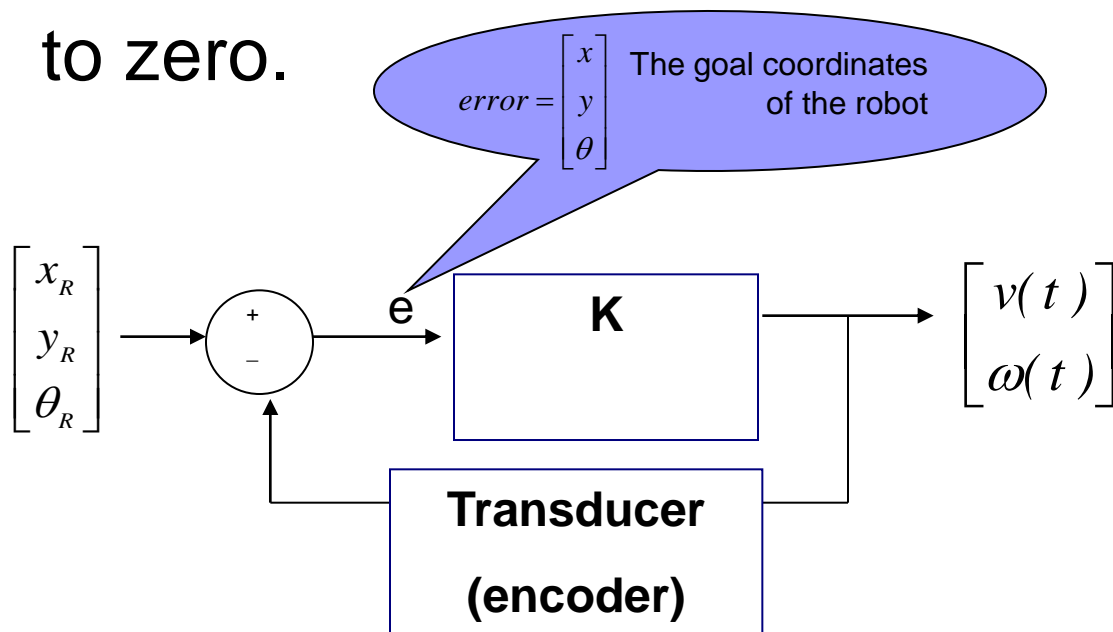
## Open Loop Control (3.6.1)

- Disadvantages:
  - It is not easy to pre-compute a feasible trajectory
  - There are limitations and constraints on the robots velocities and accelerations
  - The robot does not adapt or correct the trajectory if dynamic changes in the environment occur.
  - The resulting trajectories are usually not smooth
  - There are discontinuities in the robot's acceleration
- A more appropriate approach in motion control is to use a real-state feedback controller



# Feedback Control Example (3.6.2.1)

Given a robot with an arbitrary position and orientation and a predefined goal position and orientation. Design a control matrix for a real-state feedback controller to drive the pose error to zero.





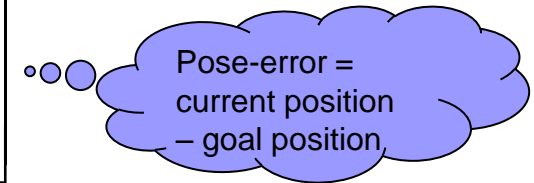
# Motion Control:

## Feedback Control, Problem Statement (3.6.2.1)

- The task of the controller is to find a control matrix  $K$ , if exists with  $k_{ij}=k(t,e)$
- such that the control signals,  $v(t)$  and  $\omega(t)$

$$K = \begin{bmatrix} k_{11} & k_{12} & k_{13} \\ k_{21} & k_{22} & k_{23} \end{bmatrix}$$

$$\begin{bmatrix} v(t) \\ \omega(t) \end{bmatrix} = K \cdot e = K \cdot \begin{bmatrix} x \\ y \\ \theta \end{bmatrix}^R$$



- drive the position error  $e$  to zero:  $\lim_{t \rightarrow \infty} e(t) = 0$



# Kinematic Model (cartesian) (3.6.2)

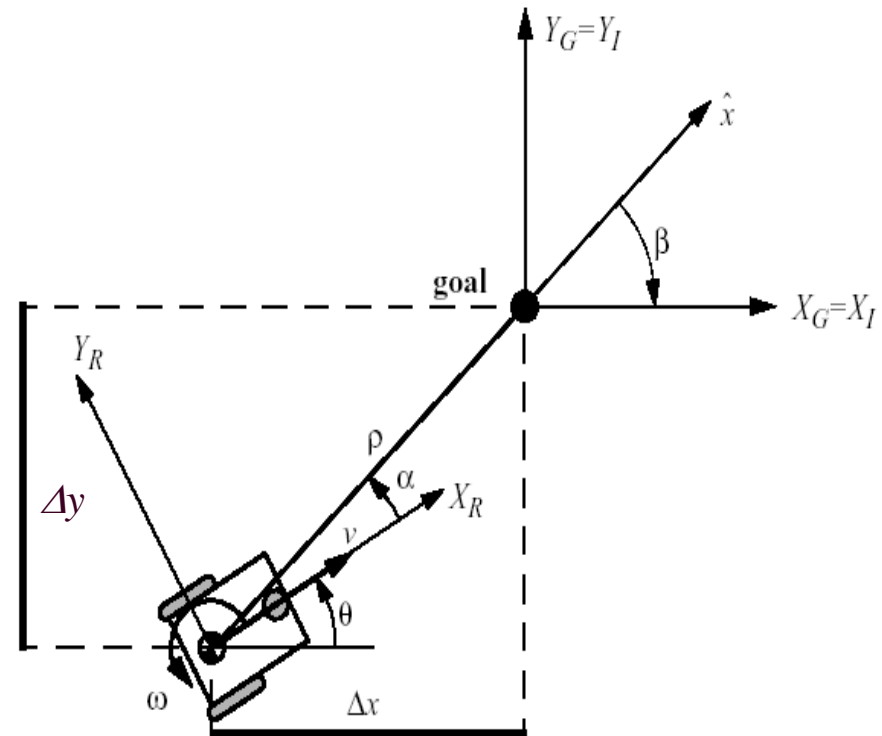
Assume that the goal of the robot is the origin of the global inertial frame. The *kinematics* for the differential drive mobile robot with respect to the global reference frame are:

$${}^I \begin{bmatrix} \dot{x} \\ \dot{y} \\ \dot{\theta} \end{bmatrix} = \begin{bmatrix} \cos \theta & 0 \\ \sin \theta & 0 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} v \\ \omega \end{bmatrix}$$

$$\rho = \sqrt{\Delta x^2 + \Delta y^2}$$

$$\alpha = -\theta + \text{atan2}(\Delta y, \Delta x)$$

$$\beta = -\theta - \alpha$$





# Kinematic Model (polar coordinates) (3.6.2)

**Robot is facing  
the goal point**

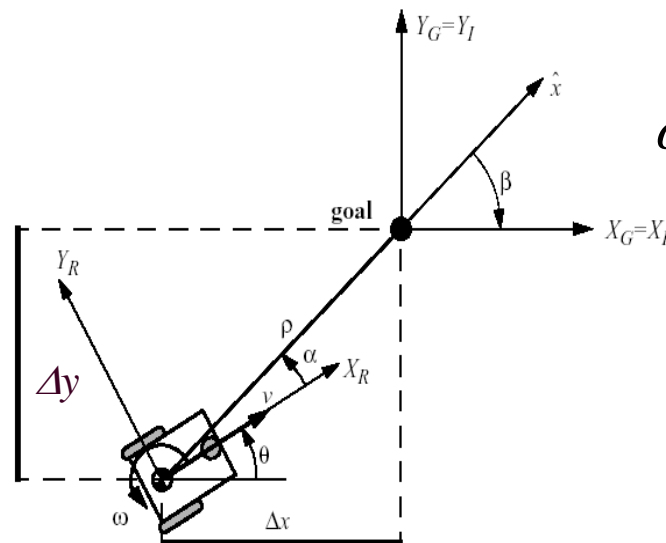
$$\begin{bmatrix} \dot{\rho} \\ \dot{\alpha} \\ \dot{\beta} \end{bmatrix} = \begin{bmatrix} \cos \alpha & 0 \\ -\frac{\sin \alpha}{\rho} & 1 \\ \frac{\sin \alpha}{\rho} & 0 \end{bmatrix} \begin{bmatrix} v \\ \omega \end{bmatrix}$$

$$\alpha \in (-\pi/2, \pi/2]$$

**Robot's back is to  
the goal point**

$$\begin{bmatrix} \dot{\rho} \\ \dot{\alpha} \\ \dot{\beta} \end{bmatrix} = \begin{bmatrix} -\cos \alpha & 0 \\ \frac{\sin \alpha}{\rho} & -1 \\ -\frac{\sin \alpha}{\rho} & 0 \end{bmatrix} \begin{bmatrix} v \\ \omega \end{bmatrix}$$

$$\alpha \in (\pi/2, \pi] \cup (-\pi, -\pi/2]$$





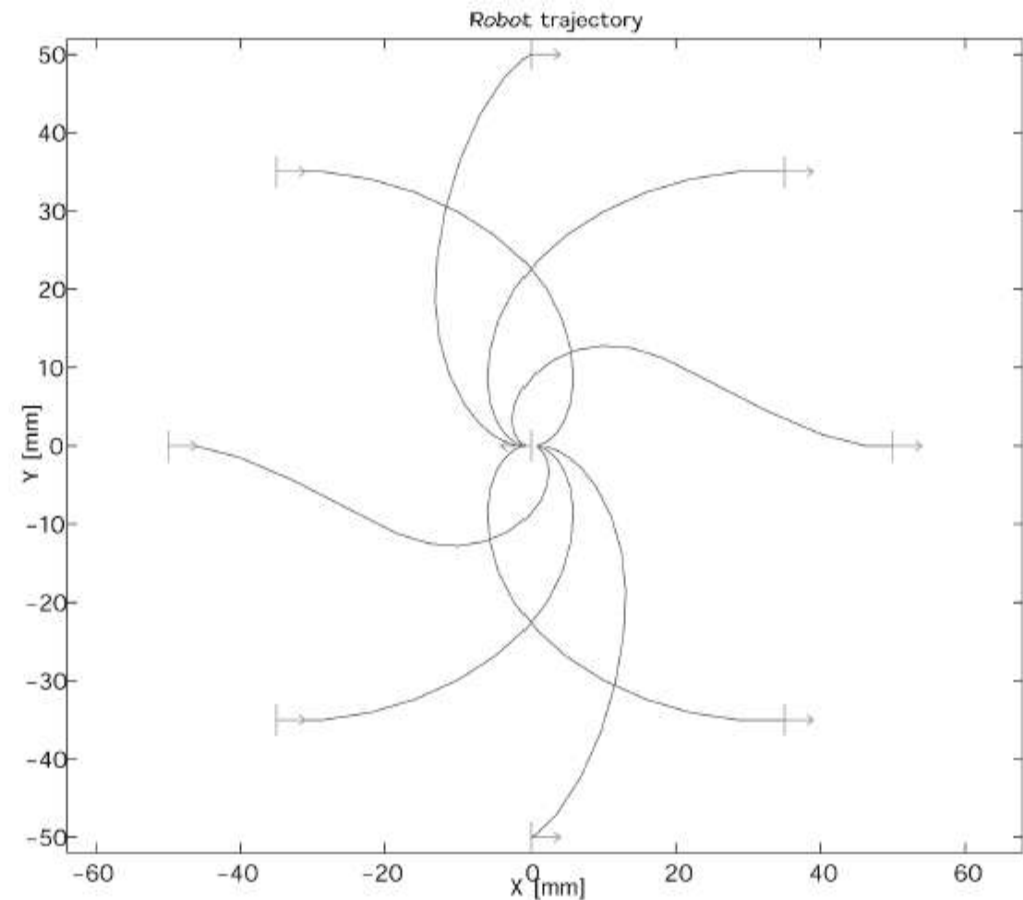
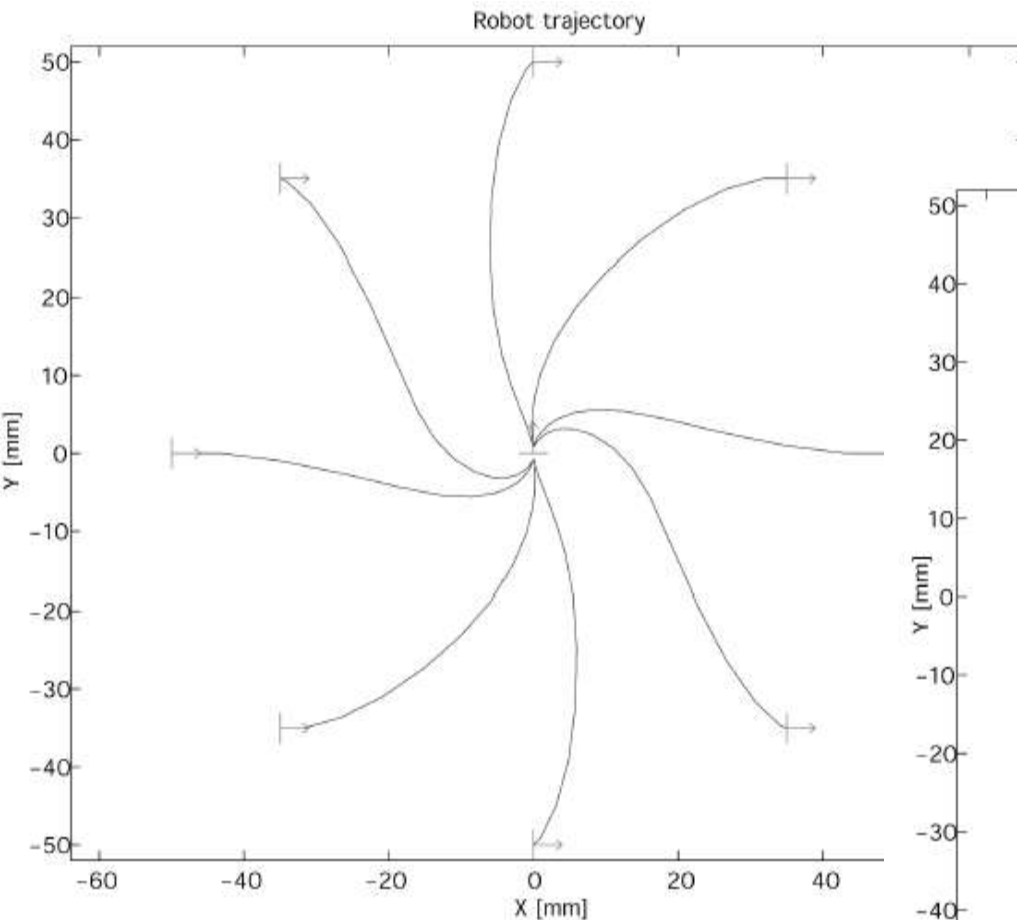
# The Control Law (3.6.2.4)

- The controls signals  $v$  and  $\omega$  must be designed to drive the robot from  $(\rho_o, \alpha_o, \beta_o)$  to the goal position
- Consider the control law,  $v = k_\rho \rho$  and  $\omega = k_\alpha \alpha + k_\beta \beta$
- The closed loop system description becomes,

$$\begin{bmatrix} \dot{\rho} \\ \dot{\alpha} \\ \dot{\beta} \end{bmatrix} = \begin{bmatrix} -k_\rho \rho \cos \alpha \\ k_\rho \sin \alpha - k_\alpha \alpha - k_\beta \beta \\ -k_\rho \sin \alpha \end{bmatrix}$$



# Kinematic Position Control: Resulting Path (3.6.2.4)







# Forward Kinematics

Assume that at each instance of time, the robot is following the **ICR** with radius  $R$  at angular rate  $\omega$ ,

$$\omega = \frac{(v_1 - v_2)}{2l} \quad R = \frac{V}{\omega} = \frac{l(v_1 + v_2)}{(v_1 - v_2)} \quad \bullet \quad \bullet \quad \bullet$$

$$s = r\theta$$
$$v = r\omega$$

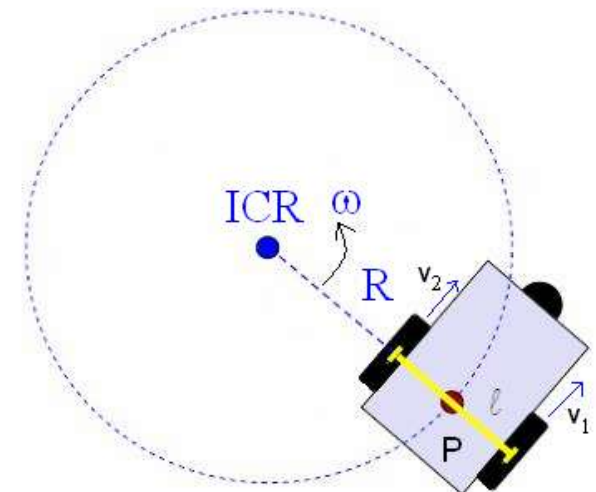
$V$  = robot forward velocity

$v_1$  – right wheel velocity

$v_2$  – left wheel velocity

$\omega$  - robot angular velocity

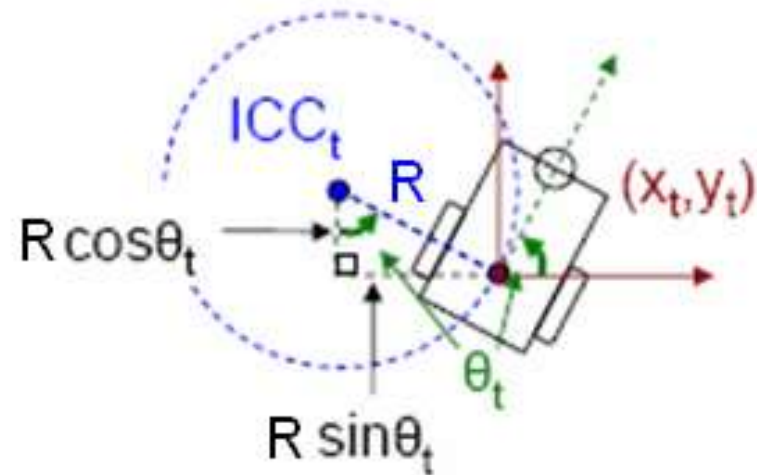
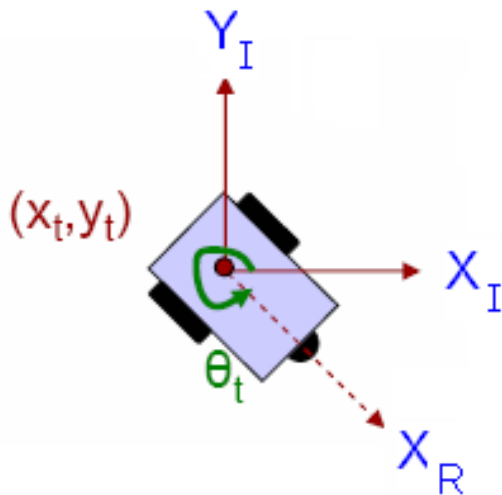
$l$  – distance from robot center to wheel





# Forward Kinematics

- Given some control parameters (e.g. wheel velocities) determine the poses of the robot
- The position can be determined recursively as a function of the velocity and position,  $p(t + \Delta) = F(v_1, v_2) p(t)$
- To solve determine the ICR(t) =  $(ICR_x, ICR_y) = (x_t - R \sin \theta_t, y_t + R \cos \theta_t)$





# Forward Kinematics: instantaneous pose

- At time  $t + \Delta$ , the robot pose with respect to the ICR is

$$p(t + \Delta) = R(\omega\Delta)^{-1} p(t) + ICR(t)$$

$$p(t + \Delta) = \begin{bmatrix} x(t + \Delta) \\ y(t + \Delta) \\ \theta(t + \Delta) \end{bmatrix} = \begin{bmatrix} \cos(\omega\Delta) & -\sin(\omega\Delta) & 0 \\ \sin(\omega\Delta) & \cos(\omega\Delta) & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} R \sin \theta_t \\ -R \cos \theta_t \\ \theta_t \end{bmatrix} + \begin{bmatrix} ICR_x \\ ICR_y \\ \omega\Delta \end{bmatrix}$$

- Since  $ICR(t) = (x(t) - R \sin \theta, y(t) + R \cos \theta)$

$$p(t + \Delta) = \begin{bmatrix} R \cos(\omega\Delta) \sin \theta_t + R \sin(\omega\Delta) \cos \theta_t + (x_t - R \sin \theta_t) \\ R \sin(\omega\Delta) \sin \theta_t - R \cos(\omega\Delta) \cos \theta_t + (y_t + R \cos \theta_t) \\ \theta_t + \omega\Delta \end{bmatrix}$$



# Forward Kinematics: linear displacement

- When  $v_1 = v_2 = v_t$ ,  $R = \infty$ , the robot moves in a straight line so ignore the *ICR* and use the following equations:
- $x(t + \Delta) = x_t + v_t \Delta \cos \theta_t$
- $y(t + \Delta) = y_t + v_t \Delta \sin \theta_t$
- $\theta(t + \Delta) = \theta_t$



# Forward Kinematics Example

## linear displacement

- A differential steering robot with  $\ell = 5.3 \text{ cm}$  starts at  $(x_o, y_o) = (20 \text{ cm}, 20 \text{ cm})$ ,  $\theta = 0^\circ$ ,  $t = 0$  seconds
- The robot moves both wheels at  $2 \text{ cm/sec}$  and moves for  $10$  seconds
- Where is the robot at  $t = 10 \text{ seconds}$ ?

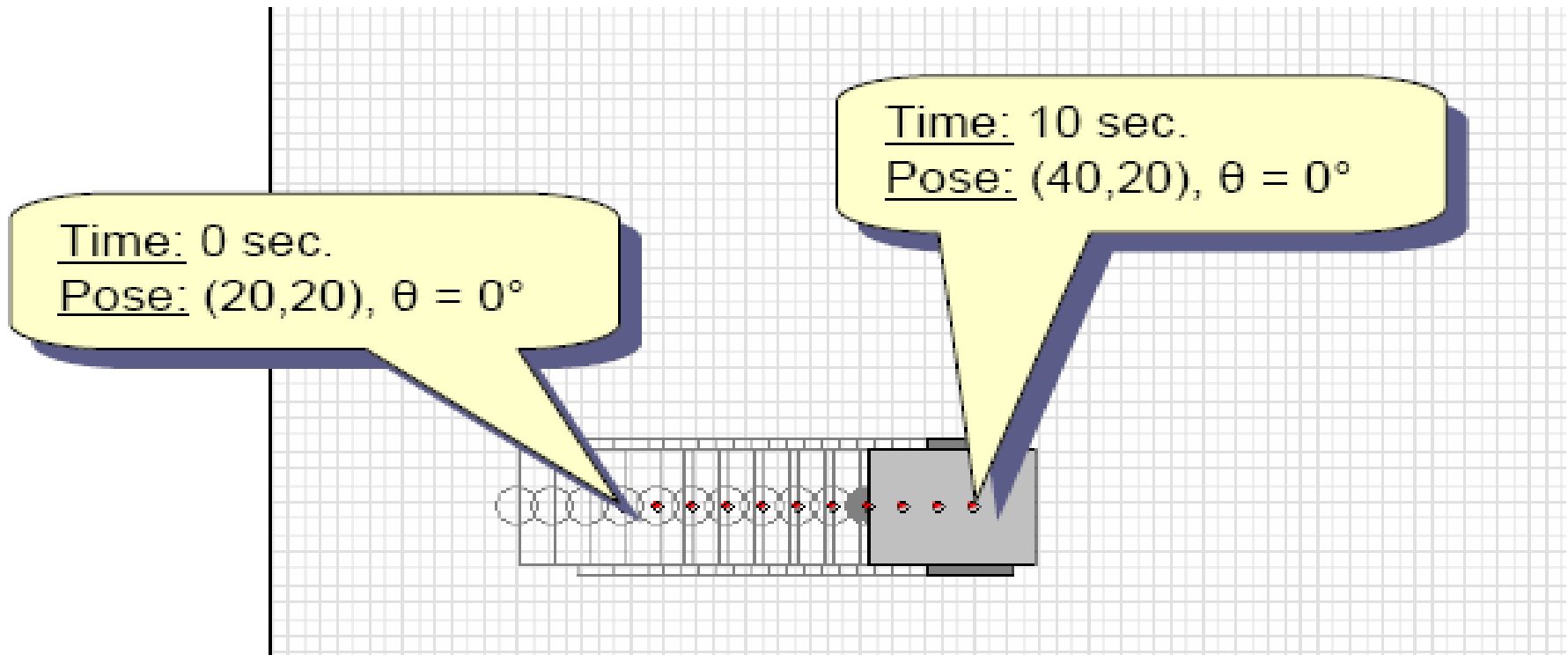
$$x(t + \Delta) = x_t + v_t \Delta \cos \theta_t \rightarrow x(10) = x(0) + v(0) \cdot (10) \cdot \cos(0^\circ) = 40 \text{ cm}$$

$$y(t + \Delta) = y_t + v_t \Delta \sin \theta_t \rightarrow y(10) = y(0) + v(0) \cdot (10) \cdot \sin(0^\circ) = 20 \text{ cm}$$

$$\theta(t + \Delta) = \theta_t \rightarrow \theta(10) = \theta(0) = 0^\circ$$



# Forward Kinematics Example: linear displacement



<http://www.scs.carleton.ca/~lanthier/teaching/COMP4900A/Notes/5%20-%20PositionEstimation.pdf>



# Forward Kinematics Example: counterclockwise turn

- Now the robot sets the right wheel to  $3 \text{ cm/s}$  and the left wheel to  $2 \text{ cm/s}$  and moves for  $10 \text{ more seconds}$
- Where is the robot at  $t = 20 \text{ seconds}$ ,  $\Delta = 10 \text{ seconds}$ ?

$$R = l(v_1 + v_2)/(v_1 - v_2) = (5.3)(3+2)/(3-2) = 26.5 \text{ cm}$$

$$\omega = (v_1 - v_2)/2l = 0.094 \text{ rad/s}$$

$$x(t + \Delta) = R \cos(\omega \Delta) \sin(\theta_t) + R \sin(\omega \Delta) \cos(\theta_t) + x_t - R \sin(\theta_t) \rightarrow$$

$$x(20) = (26.5)(0.587)(0) + 26.5(0.810)(1) + 40 - 26.5(0) = \mathbf{61.465 \text{ cm}}$$

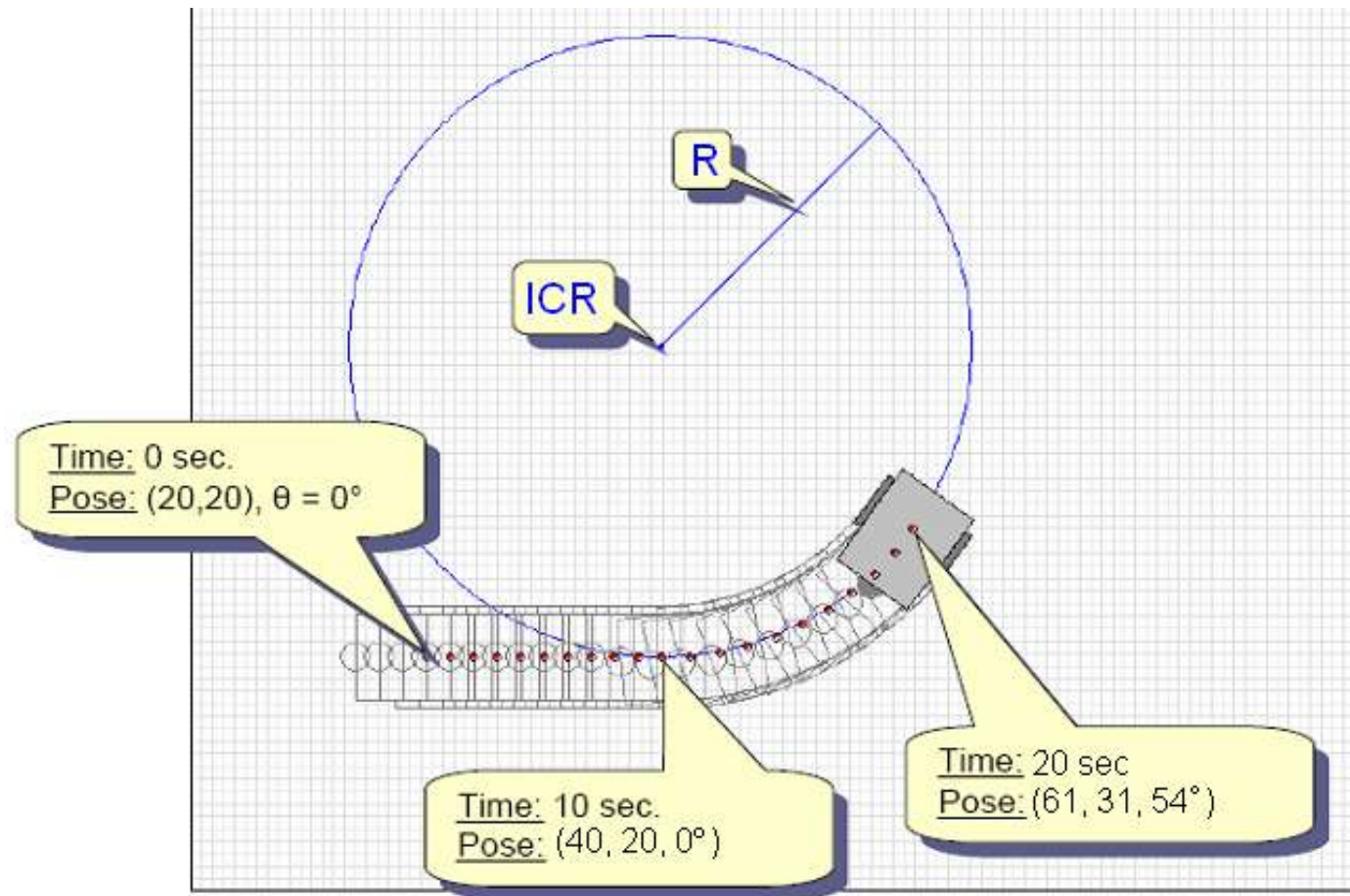
$$y(t + \Delta) = R \sin(\omega \Delta) \sin(\theta_t) - R \cos(\omega \Delta) \cos(\theta_t) + y_t + R \cos(\theta_t) \rightarrow$$

$$y(20) = (26.5)(0.810)(0) - 26.5(1)(0.587) + 20 + 26.5(1) = \mathbf{30.95 \text{ cm}}$$

$$\theta(t + \Delta) = \theta_t + \omega \Delta \rightarrow \theta(20) = \theta(10) + \omega(10) = 0^\circ + (0.09433 \text{ rad/s})(10 \text{ sec}) = \mathbf{54^\circ}$$



# Forward Kinematics: counterclockwise turn



<http://www.scs.carleton.ca/~lanthier/teaching/COMP4900A/Notes/5%20-%20PositionEstimation.pdf>  
ECE 497: Introduction to Mobile Robotics -

Locomotion & Kinematics





# Forward Kinematics: counterclockwise spin

- Now set the robots right wheel to **2 cm/s** and the left wheel to **-2 cm/s** for **5 seconds**
- Where is the robot at **t = 25 s**,  **$\Delta = 5$  seconds**?

$$\omega = (v_1 - v_2)/2l = (2 - -2\text{cm/s})/10.6 \text{ cm} = 0.37736 \text{ rad/s}$$

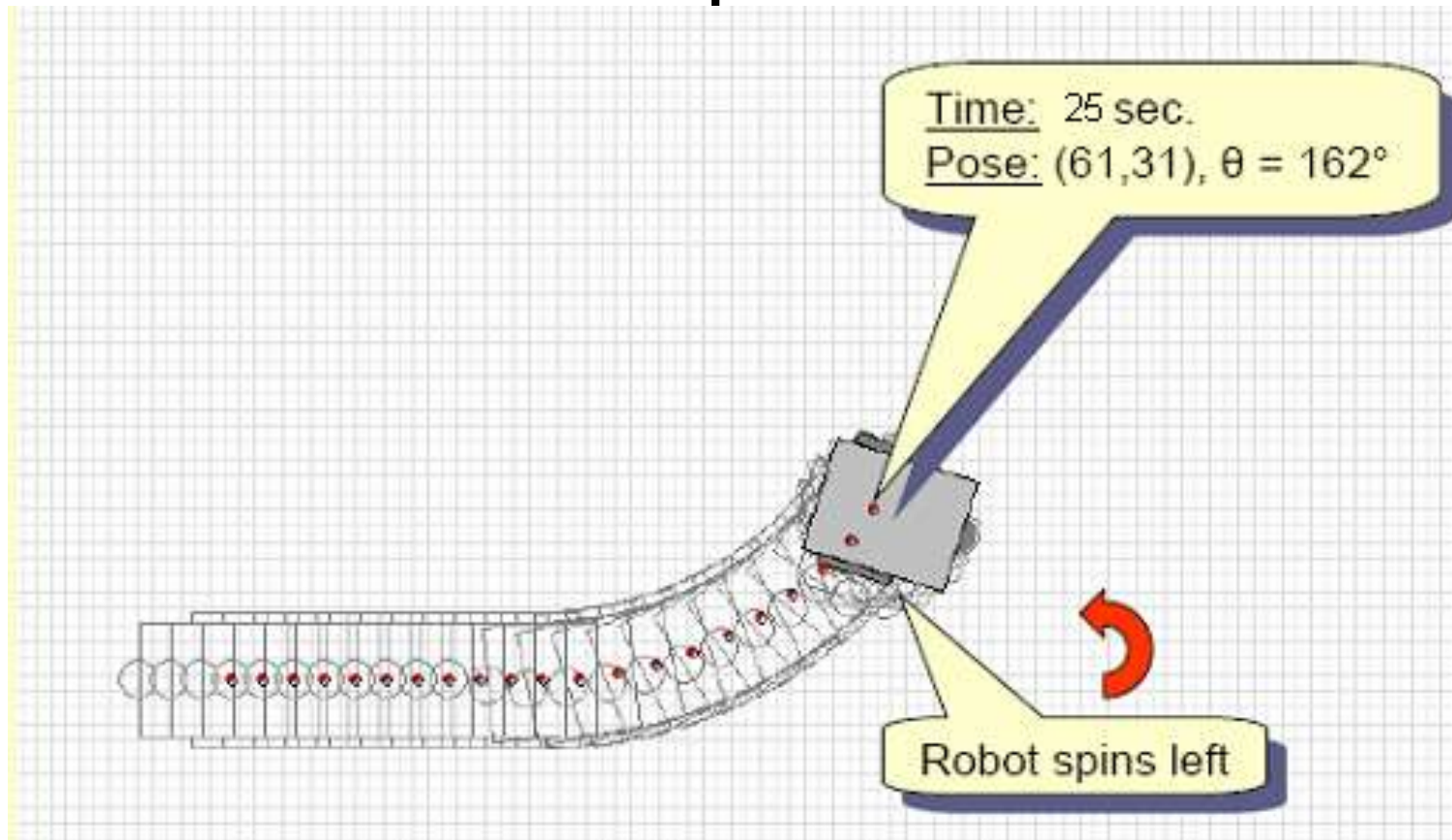
$$x(25) = \mathbf{61.465 \text{ cm}}$$

$$y(25) = \mathbf{30.95 \text{ cm}}$$

$$\theta(25) = \theta(20) + \omega\Delta = 54^\circ + (0.377\text{rad/s})(5\text{s}) = \mathbf{162^\circ}$$



# Forward Kinematics: counterclockwise spin



<http://www.scs.carleton.ca/~lanthier/teaching/COMP4900A/Notes/5%20-%20PositionEstimation.pdf>



# Forward Kinematics: clockwise turn

- Now set the robot's right wheel to **3 cm/s** and the left wheel to **3.5 cm/sec** for **15 seconds**
- Where is the robot at **t = 40 seconds**,  $\Delta = 15$  seconds?

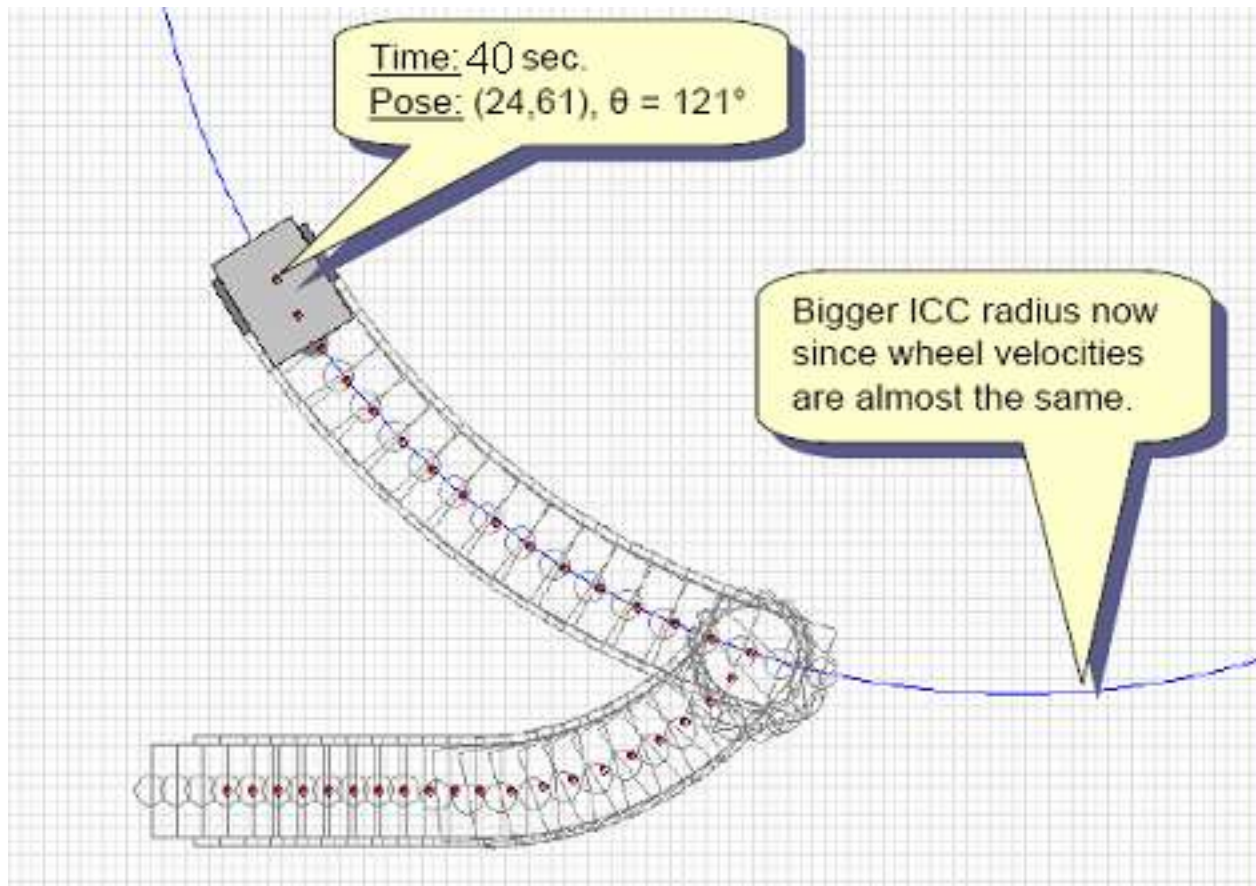
$$x(40) = 23.52 \text{ cm}$$

$$y(40) = 60.55 \text{ cm}$$

$$\theta(40) = \theta(25) + \omega\Delta = 162^\circ - (0.047 \text{ rad/s})(15 \text{ sec}) = 121^\circ$$



# Forward Kinematics: clockwise turn





# Forward Kinematics: clockwise spin

- Finally, the robot sets the right wheel to  $0 \text{ cm/s}$  and the left wheel to  $3 \text{ cm/s}$  for  $10 \text{ s}$ .
- Where is the robot at  $t = 50 \text{ s}$ ,  $\Delta = 10 \text{ s}$ ?

$$R = (5.3)(3 + 0)/(0 - 3) = -5.3 \text{ cm}$$

$$\omega = (0 - 3)/10.6 = -0.28202 \text{ rad/s}$$

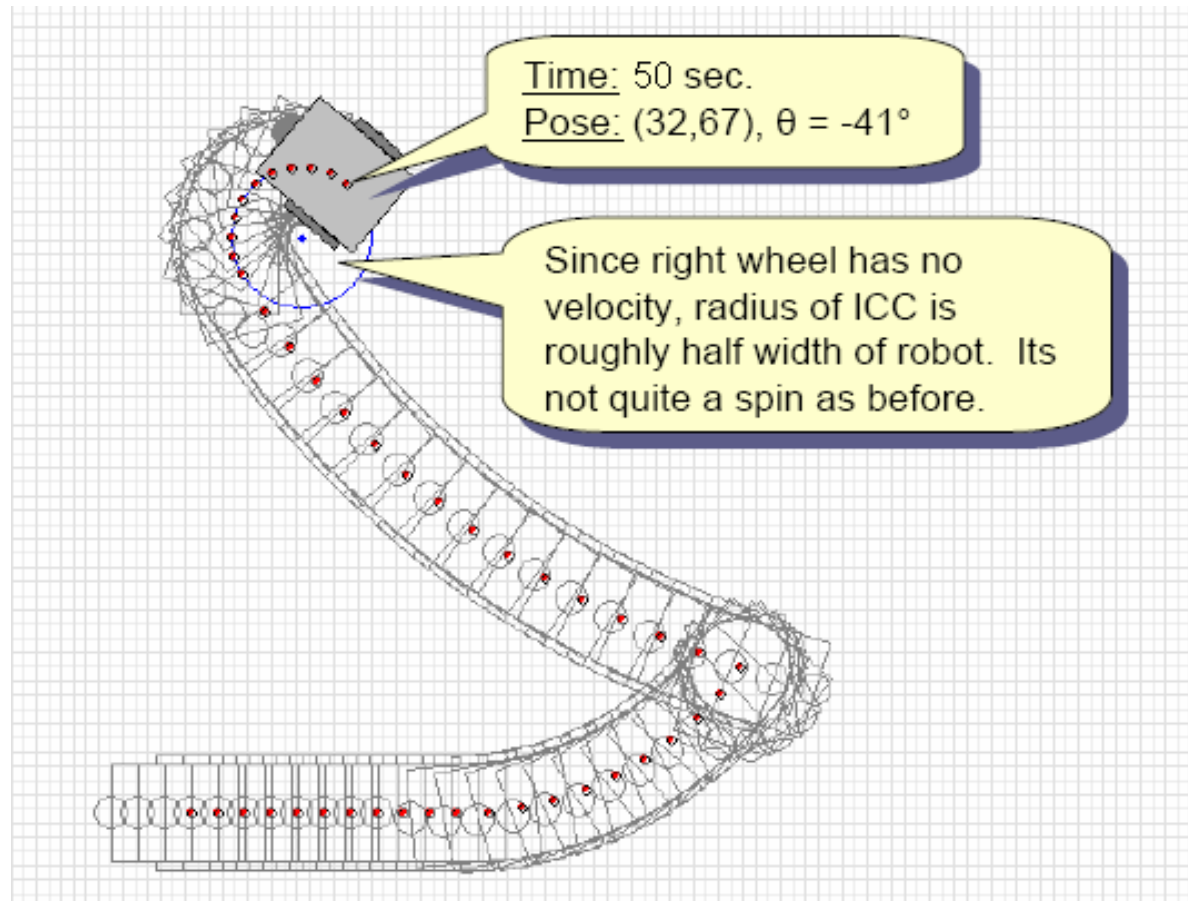
$$x(50) = \mathbf{31.5 \text{ cm}}$$

$$y(50) = \mathbf{67.47 \text{ cm}}$$

$$\theta(50) = \theta(40) + \omega\Delta = 121^\circ - (0.283 \text{ rad/s})(10 \text{ sec}) = \mathbf{-41^\circ}$$



# Forward Kinematics - Example

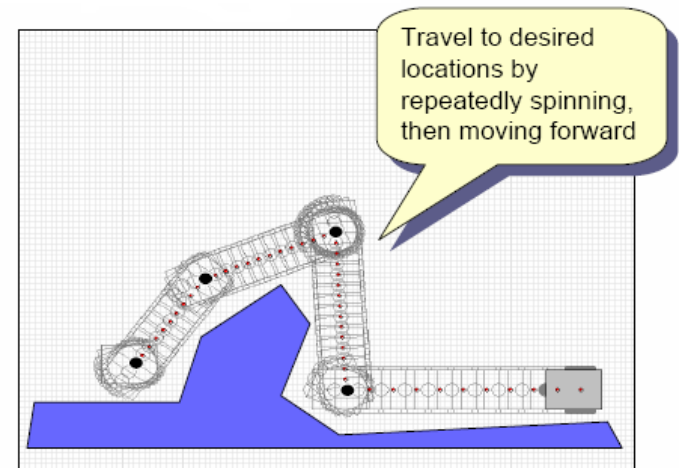


<http://www.scs.carleton.ca/~lanthier/teaching/COMP4900A/Notes/5%20-%20PositionEstimation.pdf>



# Inverse Kinematics

- *Inverse Kinematics* is determining the control parameters (wheel velocities) that will make the robot move to a new pose from its current pose
- This is a very difficult problem
  - Too many unknowns, not enough equations and multiple solutions
- The easy solution is to
  - Spin the robot to the desired angle
  - Move forward to the desired location



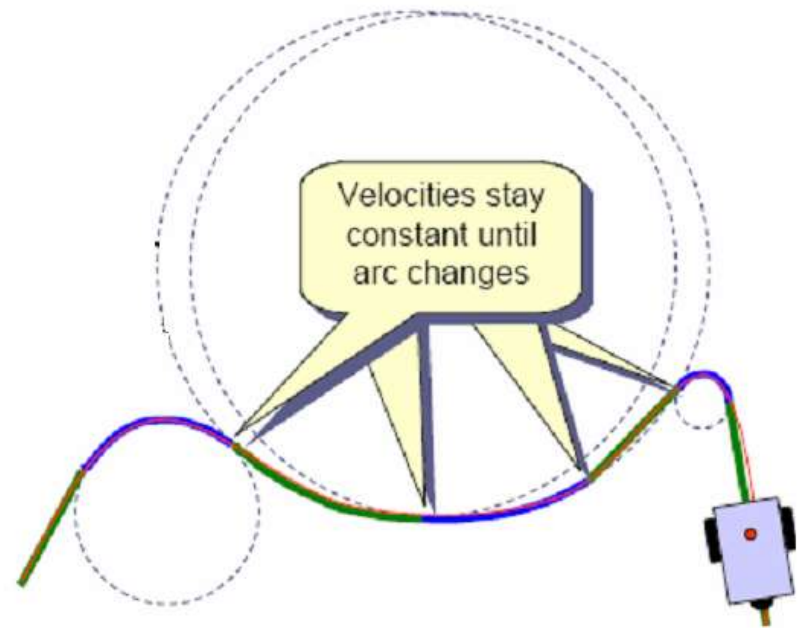
<http://www.scs.carleton.ca/~lanthier/teaching/COMP4900A/Notes/5%20-%20PositionEstimation.pdf>





# Inverse Kinematics

- Approximate a desired path with arcs based upon computing ICR values
- Result is a set of straight-line paths and ICR arc portions
- Either set the robot drive time and compute velocities for each portion of the path
- Or set velocities and compute drive time for each portion of the path







# Inverse Kinematics: spin time and velocities

- The length of time to spin the wheels is determined by the velocity
  - $\theta(t + \Delta) = \theta_t - \omega\Delta \rightarrow \Delta = (\theta(t + \Delta) - \theta(t)) / \omega$
  - Since  $\omega = (v_1 - v_2) / (2l)$  and  $v_1 = -v_2$
  - $\Delta = l (\theta(t + \Delta) - \theta(t)) / v_1$
- Alternately, set the spin time and calculate the wheel velocities
  - $v_1 = l (\theta(t + \Delta) - \theta(t)) / \Delta$



# Inverse Kinematics: forward time

- The length of time to move forward is determined by the velocity ( $v_t = v_1 = v_2$ )
- Since  $x(t + \Delta) = x_t + v_t \Delta \cos(\theta_t)$  and  $y(t + \Delta) = y_t + v_t \Delta \sin(\theta_t)$ 
  - if  $x(t + \Delta) \neq x_t$ 
    - $\Delta = (x(t + \Delta) - x_t) / (v_t \cos(\theta_t))$ , or
  - if  $x(t + \Delta) = x_t$ 
    - $\Delta = (y(t + \Delta) - y_t) / (v_t \sin(\theta_t))$



# Inverse Kinematics: forward velocities

- Conversely, the wheel velocities,  $v_t = v_1 = v_2$ , can be determined by setting the forward move time
- Since  $x(t + \Delta) = x_t + v_t \Delta \cos(\theta_t)$  and  $y(t + \Delta) = y_t + v_t \Delta \sin(\theta_t)$ 
  - if  $x(t + \Delta) \neq x_t$ 
    - $v_t = (y(t + \Delta) - y_t) / (\Delta \cos(\theta(t)))$
  - if  $x(t + \Delta) = x(t)$ 
    - $v_t = (y(t + \Delta) - y_t) / (\Delta \sin(\theta(t)))$

