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# Qspice - Bode Frequency Response Analysis (.bode)

KS Kelvin Kelvin Leung

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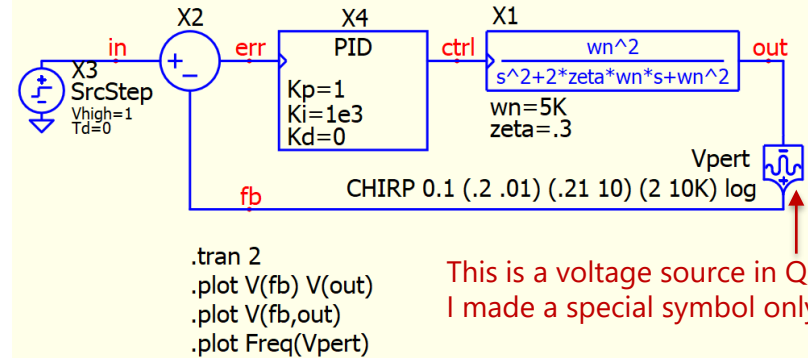
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# Concept of Frequency Response Analysis (FRA)

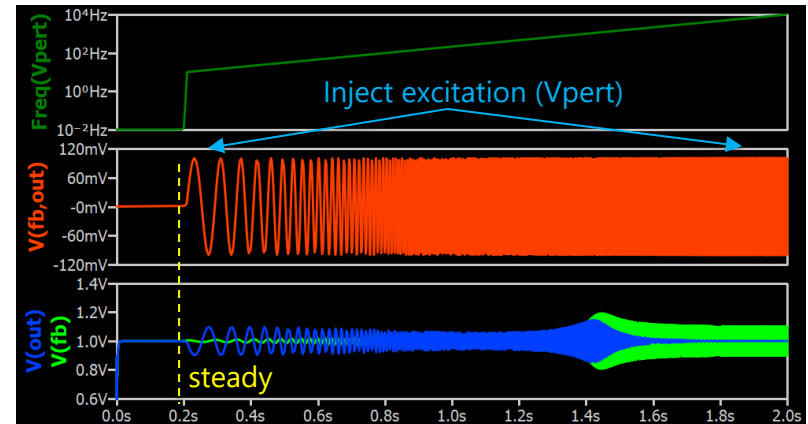
## Qspice : Bode - Sine Wave Excitation.qsch

- Frequency Response Analysis (FRA)
  - This is an example of frequency response analysis (FRA) in close-loop system with perturbing source inject into feedback path
  - Perturbing source signal is injected after the system has settled to a steady state
    - This perturbing source can be a sine wave or square wave (step response) in Qspice
    - This excitation can assist in calculating the transfer function between any two nodes affected by this excitation
  - Qspice FRA also requires the user to determine important system parameters like Tsettle, start and stop frequencies, perturbing amplitude and type, to simulate a time domain waveform for calculating transfer function of specified nodes

Example of Sine Wave Excitation / Perturbing Source into close-loop system



This is a voltage source in Qspice  
I made a special symbol only



# Qspice - Bode Frequency Response Analysis (.bode)

- Frequency Response Analysis (.bode)

- Help in Qspice : HELP > Simulator > Command Reference > Frequency Response Analysis (.bode)
- A perturbing voltage source can be inserted in the input (open loop) or feedback path (close loop)
- Both terminals of this perturbing voltage source must not be grounded

- Syntax:**

**.bode <SOURCE> <TSETTLE> [<FSTART> [<FSTOP> [<AMP>]]] [SQUARE=<value>] [DEBUG]**

- .bode is time domain analysis with perturbing voltage source <SOURCE> generates signal from frequency <FSTART> to <FSTOP> with fixed or variable [.options Bodeampfreq / BodeLoPow / BodeHiPow] amplitude <AMP>. It only collect time domain data after circuit settle to steady state <TSETTLE>
- Simulator performs frequency/phase analysis/deconvolution between output node [.options BODEOUT] and input node [.options BODEIN], and store results into *OpenLoopGain* or *TransferFunction*

## Syntax

Name	Description	Default
SOURCE <sup>2</sup>	Name of the perturbing voltage source inserted in the loop	No default but a value is required
TSETTLE <sup>3</sup>	Time required for the circuit to settle to steady state	No default but a value is required
FSTART <sup>4</sup>	Lowest frequency to analyze	1kHz
FSTOP	Highest frequency to analyze	1000 × FSTART
AMP <sup>5</sup>	Minimum amplitude of perturbing source	2mV <sup>6</sup>
SQUARE <sup>7</sup>	Minimum amplitude of perturbing source	0
DEBUG	Keep the time domain waveform data	not set

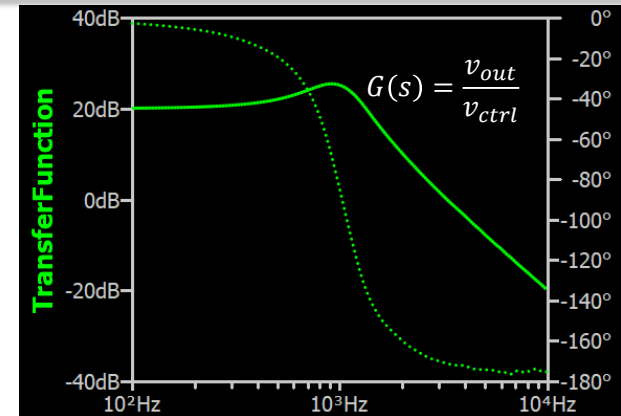
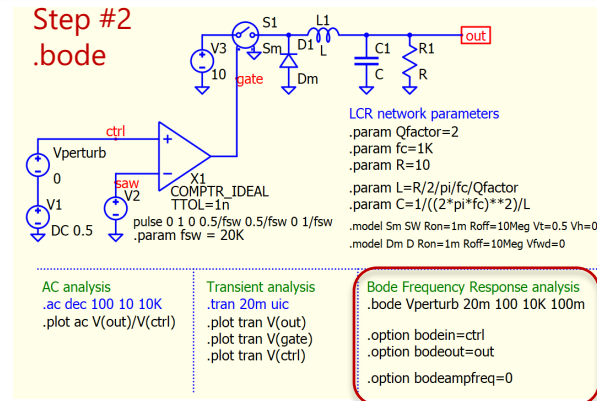
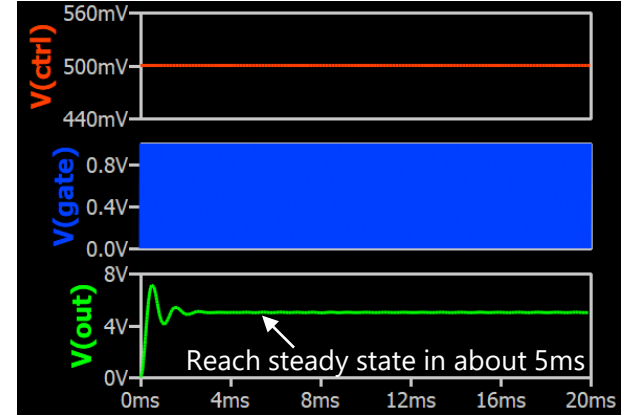
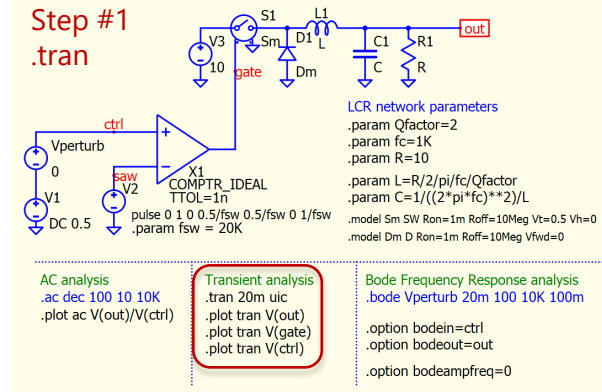
## .option

Name	Description	Default
BODEAMPFREQ	Frequency with the minimum perturbation amplitude. Set to 0. for constant amplitude.	(not set)
BODEHIPOW	Controls perturbation amplitude for above BODEAMPFREQ by pow (freq/BODEAMPFREQ, BODEHIPOW)	1.
BODEINPUT <sup>1</sup>	Override input node for transfer function computation(AKA BODEIN)	auto
BODELOPOW	Controls perturbation amplitude for below BODEAMPFREQ by pow (freq/BODEAMPFREQ, BODELOPOW)	1.
BODEPERIODS	Maximum number of periods to include in deconvolution	20
BODEREF	Reference node to use for Frequency Response Analysis	Node 0 (global ground)
BODEOUTPUT <sup>1</sup>	Override output node for transfer function computation(AKA BODEOUT)	auto
BODETOL	A Frequency Response Analysis relative tolerance	10.

# Basic Workflow of using .bode

## Qspice : Bode - Buck - transfer function (sine).qsch

- Identify <Tsettle> with .tran
  - [1] Use .tran to identify settling time for system to reach steady state
- Setup .bode with
  - [2] Add perturbing source to a suitable position
    - both terminals must not be grounded
  - [3] Set <Tsettle> larger than steady state time found in [1]
  - [4] User determine <Fstart> and <Fstop>
    - Within 3 decade and prevent <Fstart> from very low frequency to reduce simulation time
  - [5] Determine Transfer Function by specifying
    - .option bodein=<input node>
    - .option bodeout=<output node>
    - $TransferFunction = \frac{bodeout}{bodein}$
  - [6] Determine perturbing amplitude
    - <amp> set to a proper value
    - .option bodeampfreq=0** can force a constant perturbing amplitude (recommend to use this as initial run)

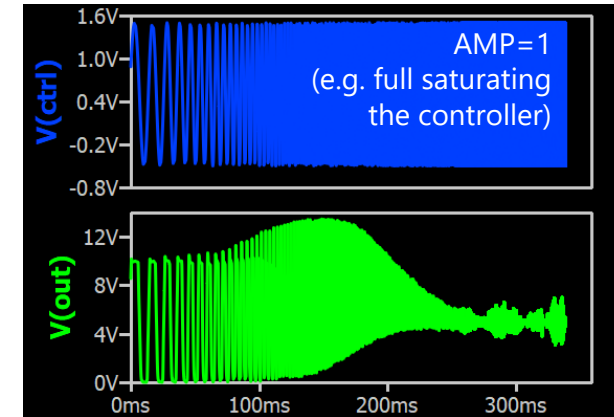
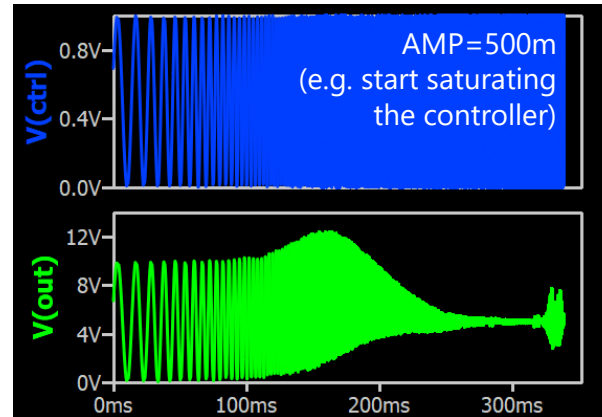
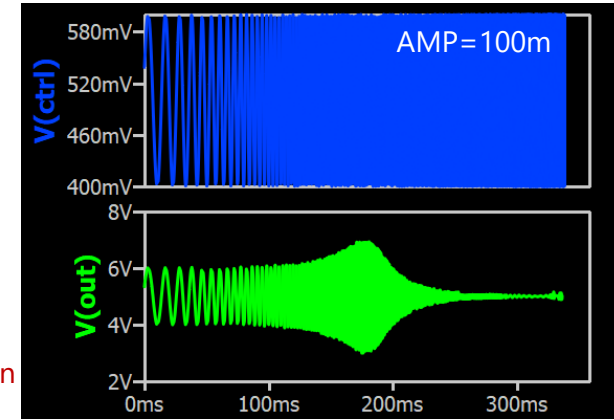
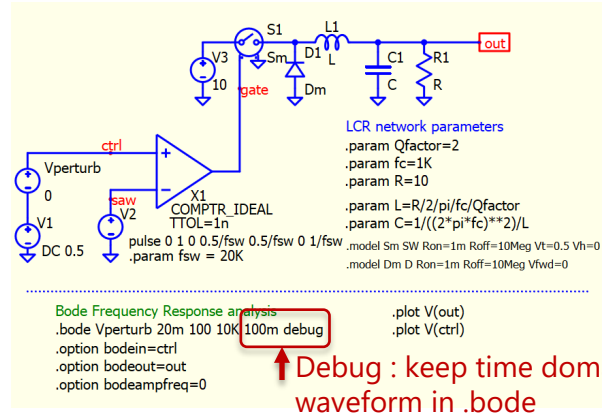


# Basic Workflow of using .bode – Determine AMP with Debug

Qspice : Bode - Buck - transfer function (sine-debug).qsch

- AMP and Debug

- It is necessary to determine amplitude profile that does not saturate the controller but can excite to a useful level for gain/phase calculation
- DEBUG** in .bode directive keep time domain waveform for users to observe how to adjust the amplitude (AMP)
- Users may need to adjust Bodeampfreq / BodeLoPow / BodeHiPow in .option to optimize amplitude at different frequencies to achieve the best signal resolution



# Basic Workflow of using .bode (Sine Wave Excitation)

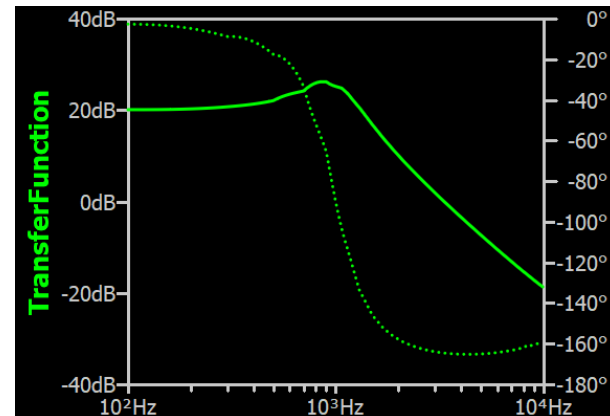
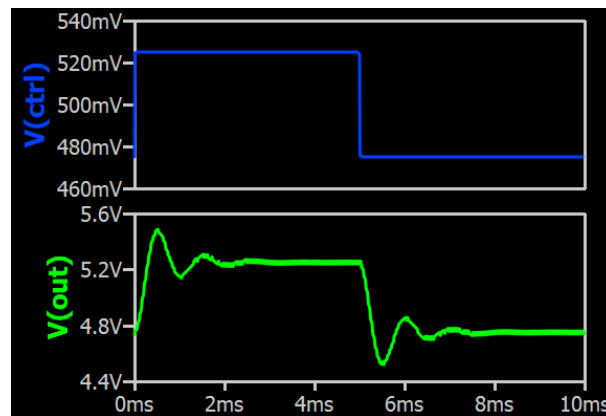
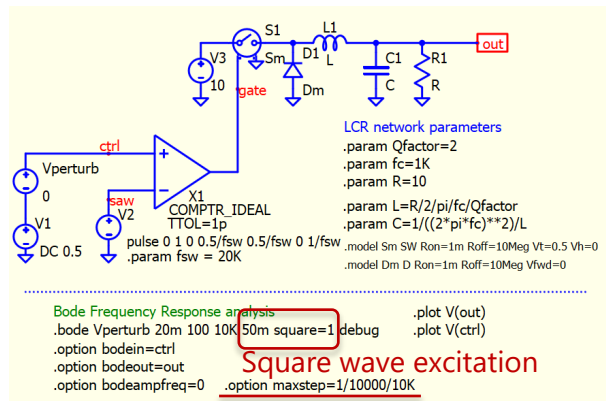
- .bode simulation process with sine wave excitation
  - .tran simulation with CHIRP as perturbing source
    - Time to achieve steady state : *<TSETTLE>*
    - Perturbing source name : *<SOURCE>*
    - Perturbing source frequency range : *<FSTART>* and *<FEND>*
    - Perturbing source amplitude
      - *.option BODEAMPFREQ*: to determine *<AMP>* min amplitude frequency (!=0) or constant amplitude (=0)
      - *.option BodeLoPow* and *.option BodeHiPow*: to determine amplitude vs frequency profile
    - Relative tolerance : *.option BODETOL*
      - A lower value results in a longer perturbing source .tran duration, providing higher resolution across frequencies (beneficial for high Q response)
  - Deconvoluting time domain data with 9 threads
    - INPUT and OUTPUT nodes : *.option BODEIN* and *.option BODEOUT*
      - **TransferFunction** =  $\frac{bodeout}{bodein}$
    - OUTPUT nodes reference : *.option BODEREF* (default = Node 0 = GND)
    - Maximum deconvolution periods : *.option BODEPERIODS*
  - Applying aperture diffraction corrections

# Excitation : Square Wave Excitation

## Qspice : Bode - Buck - transfer function (square-debug).qsch

- Square

- If Square is set to a positive number, a method based on square wave excitation is used
- A pulse source is used for excitation with peak-to-peak = AMP
- .option maxstep can be used to increase time step resolution, and therefore, to increase transfer function resolution
- Simulation time when using Square wave excitation is much faster than when using Sine wave excitation



# Basic Workflow of using .bode (Square Wave Excitation)

- .bode simulation process with square wave excitation
  - .tran simulation with PULSE as perturbing source
    - Time to achieve steady state : *<TSETTLE>*
    - Perturbing source name : *<SOURCE>*
    - Perturbing source frequency range : *<FSTART>* and *<FEND>*
    - Perturbing source amplitude (pulse peak-to-peak) : *<AMP>*
  - System identification from time domain data
    - INPUT and OUTPUT nodes : *.option BODEIN* and *.option BODEOUT*
      - **TransferFunction** =  $\frac{\text{bodeout}}{\text{bodein}}$
    - OUTPUT nodes reference : *.option BODEREF* (default = Node 0 = GND)
  - Improve resolution of system transfer function calculation
    - Limit and reduce maxstep : *.option maxstep*
      - Higher timestep resolution in time domain waveform can improve resolution of system transfer function
  - .option **NOT USED** in square wave excitation
    - *BodeAmpFreq, BodeLoPow, BodeHiPow, BodeTol, BodePeriods*



Study of syntax and  
.option parameters in  
.bode

# .bode Syntax and .Option

## syntax

Name	Description	Default
SOURCE <sup>2</sup>	Name of the perturbing voltage source inserted in the loop	No default but a value is required
TSETTLE <sup>3</sup>	Time required for the circuit to settle to steady state	No default but a value is required
FSTART <sup>4</sup>	Lowest frequency to analyze	1kHz
FSTOP	Highest frequency to analyze	1000 × FSTART
AMP <sup>5</sup>	Minimum amplitude of perturbing source	2mV <sup>6</sup>
SQUARE <sup>7</sup>	Minimum amplitude of perturbing source	0
DEBUG	Keep the time domain waveform data	not set

## .option

Name	Description	Default
BODEAMPFREQ	Frequency with the minimum perturbation amplitude. Set to 0. for constant amplitude.	(not set)
BODEHIPOW	Controls perturbation amplitude for above BODEAMPFREQ by pow (freq/BODEAMPFREQ, BODEHIPOW)	1.
BODEINPUT <sup>1</sup>	Override input node for transfer function computation(AKA BODEIN)	auto
BODELOPOW	Controls perturbation amplitude for below BODEAMPFREQ by pow (freq/BODEAMPFREQ, BODELOPOW)	1.
BODEPERIODS	Maximum number of periods to include in deconvolution	20
BODEREF	Reference node to use for Frequency Response Analysis	Node 0 (global ground)
BODEOUTPUT <sup>1</sup>	Override output node for transfer function computation(AKA BODEOUT)	auto
BODETOL	A Frequency Response Analysis relative tolerance	10.

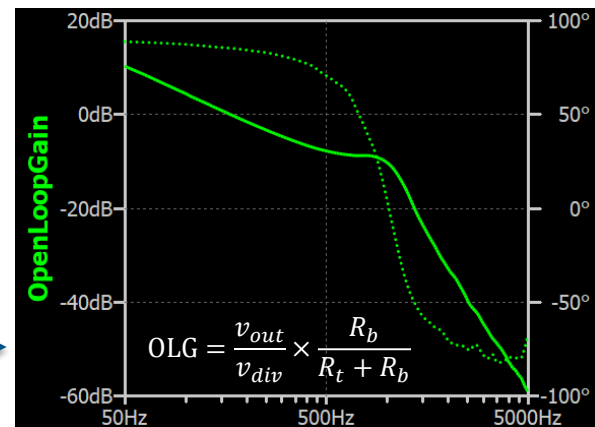
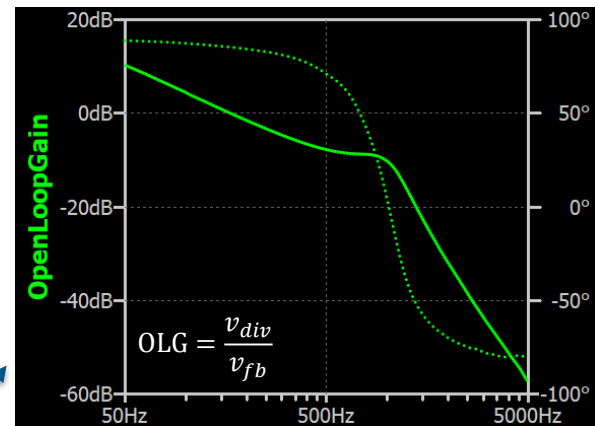
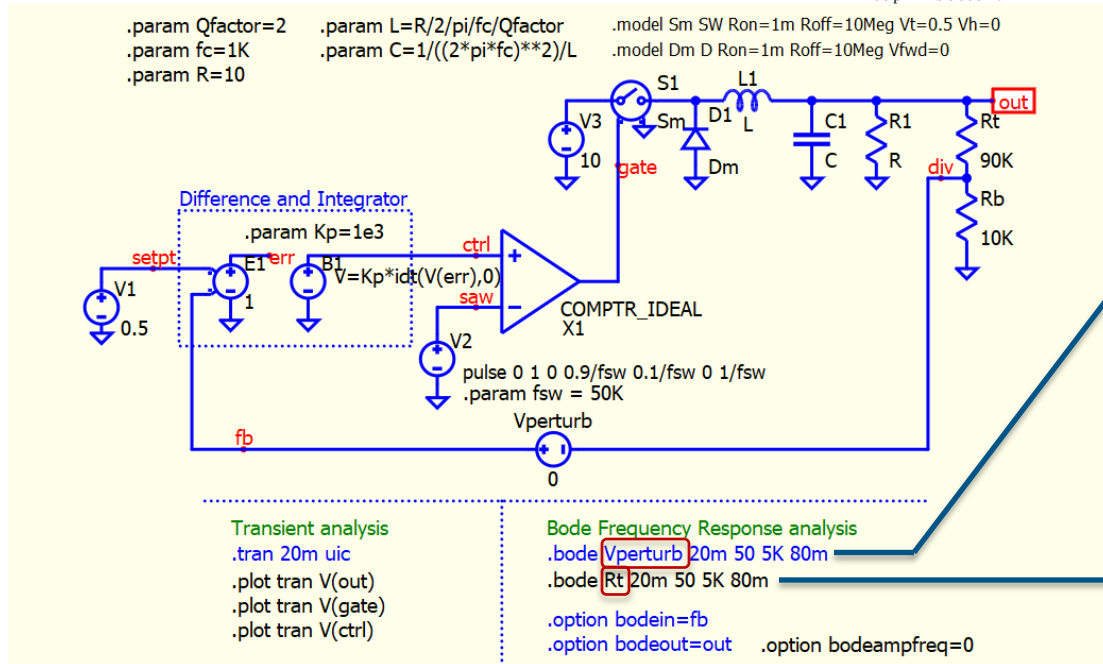
### Hint

- Normally not need to change BodeTol (except for high Q frequency response) and BodePeriods
- First run set BodeAmpFreq=0 for constant amplitude perturbation
- Fstart and Fstop within 3 decade, and Fstart doesn't set at very low frequency
- To improve overall profile, may require varying perturbation amplitude, which requires use of Bodeampfreq / Bodehipow / Bodelipow for amplitude user defined amplitude profile.

# Syntax <SOURCE>

## Qspice : bode - Source.qsch

- <Source> can be voltage source or top resistor
  - If bodein and bodeout are not defined in .option
  - <Source> as voltage source :  $OpenLoopGain = \frac{-ve\ terminal\ node}{+ve\ terminal\ node}$
  - <Source> as top resistor :  $OpenLoopGain = \frac{resistor\ net\ 1\ node}{resistor\ net\ 2\ node} \times \frac{R_{top}}{R_{top} + R_{bottom}}$



# Syntax <AMP> and .option Bodeampfreq / BodeLoPow / BodeHiPow

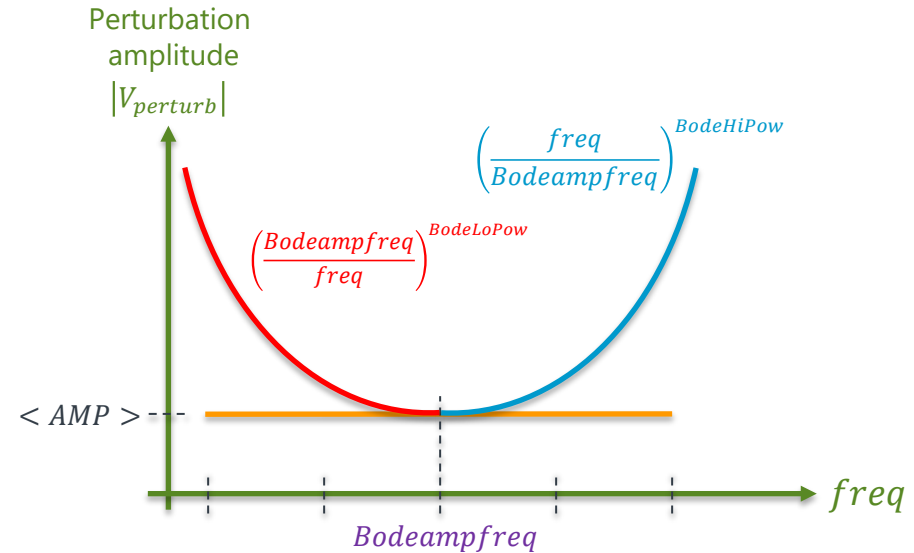
- Perturbing Source Signal Amplitude
  - In close-loop perturbing, it requires flexibility to change its amplitude across test frequency to boost signal in high attenuation region or prevent controller saturation

- .option Bodeampfreq

- If **.option Bodeampfreq=0**
  - $|V_{perturb}|$  for all frequency is unchanged = <AMP>
- If .option Bodeampfreq is not defined
  - Default  $\text{BodeAmpFreq} = 10^{\frac{\log_{10}(F_{stop}) + \log_{10}(F_{start})}{2}}$
- If .option Bodeampfreq=<value>
  - $\text{BodeAmpFreq} = \langle f_{\text{bodeampfreq}} \rangle$

- .option BodeLoPow and BodeHiPow (Default as 1)

- Assume  $freq$  is between <Fstart> and <Fstop>
- If  $freq < \text{Bodeampfreq}$  :  $|V_{perturb}| = \langle AMP \rangle \left( \frac{\text{Bodeampfreq}}{freq} \right)^{\text{BodeLoPow}}$
- If  $freq \geq \text{Bodeampfreq}$  :  $|V_{perturb}| = \langle AMP \rangle \left( \frac{freq}{\text{Bodeampfreq}} \right)^{\text{BodeHiPow}}$



# Syntax <AMP> and .option Bodeampfreq / BodeLoPow / BodeHiPow

## Qspice : bode - bodehipow bodelopow formula.qsch

- BodeLoPow / BodeHiPow
  - Formula is implemented in this schematic to demonstrate amplitude profile by changing BodeLoPow and BodeHiPow
  - \*\* In default, BodeLoPow=BodeHiPow=1
  - .option Bodeampfreq=0 force to constant amplitude

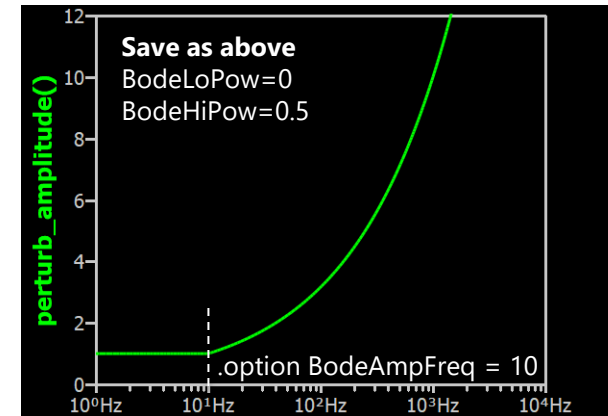
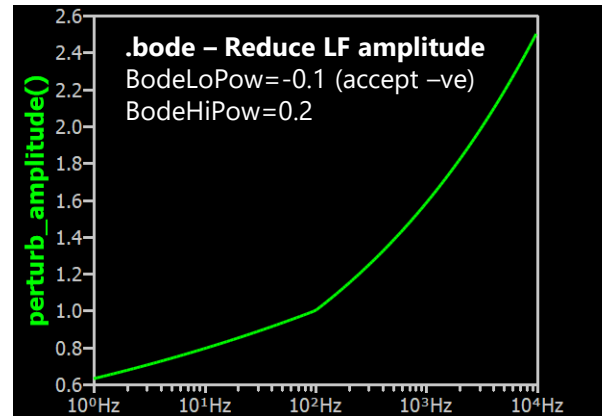
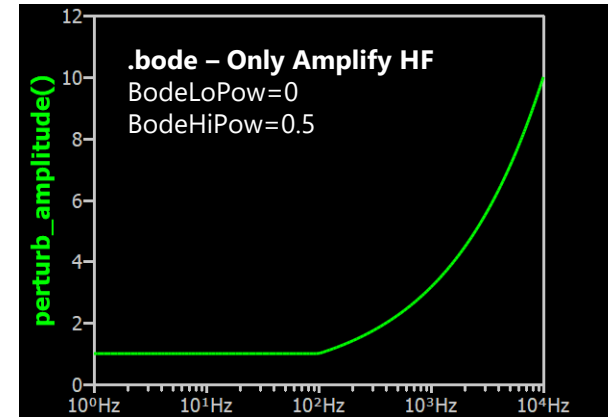
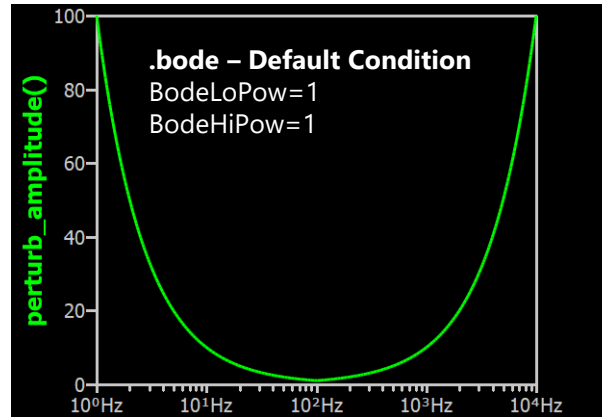
### .bode and .option parameters

```
.param Amp = 1 ; [AMP] in .bode
.param Fstart = 1 ; [Fstart] in .bode
.param Fstop = 1e4 ; [Fstop] in .bode
.param BodeAmpFreq = pow(10,(log10(Fstop)+log10(Fstart))/2) ; default
.param BodeAmpFreq = 20 ; manual define BodeAmpFreq in .option
```

```
.param BodeLoPow = 1
.param BodeHiPow = 1
```

### Calculate Amplitude vs Frequency Profile

```
.ac dec 100 Fstart Fstop
.func perturb_amplitude() AMP*if(Freq/BodeAmpFreq<1,
+pow(BodeAmpFreq/Freq, BodeLoPow),
+pow(Freq/BodeAmpFreq, BodeHiPow))
.plot perturb_amplitude()
```



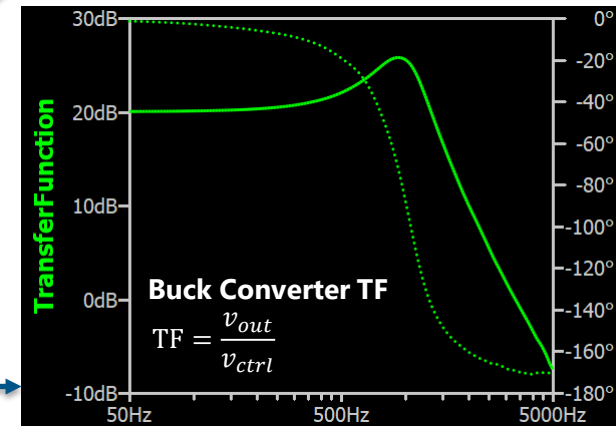
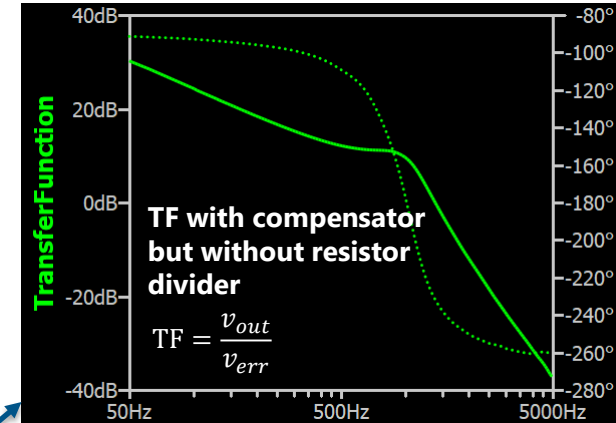
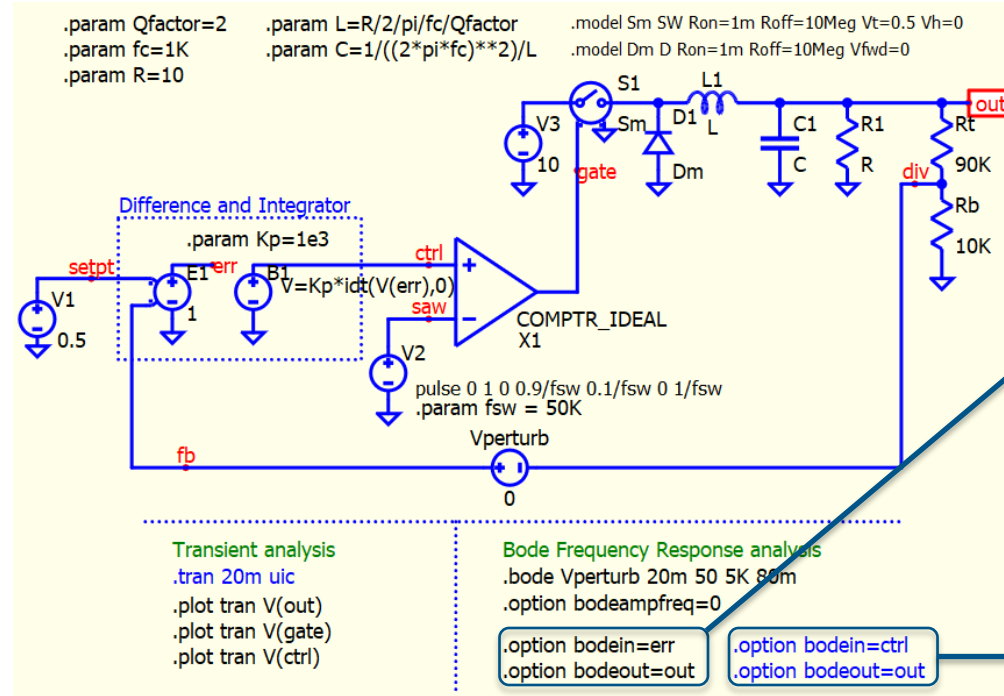
# .option Bodein and Bodeout

Qspice : bode - bodein bodeout.qsch

## • Bodein and Bodeout

- User can define voltage note name for bodein/bodeout params, result is store as TransferFunction

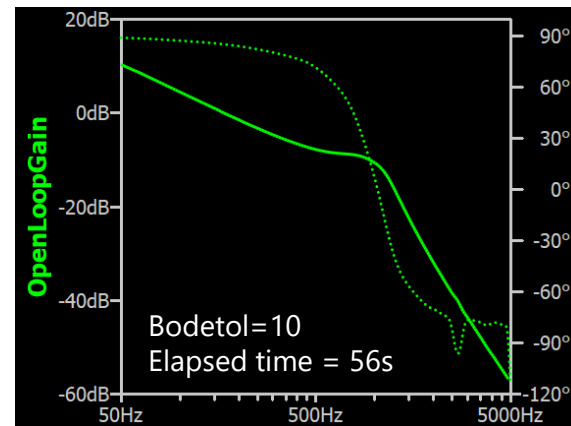
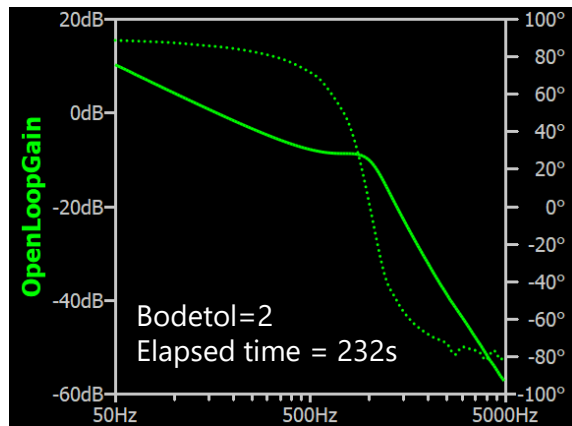
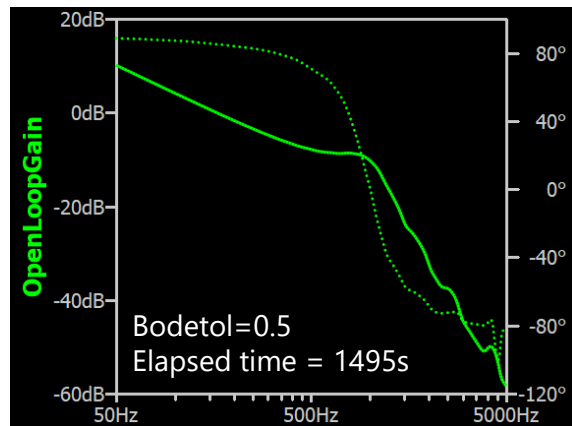
$$\text{TransferFunction} = \frac{\text{bodeout}}{\text{bodein}}$$



# .option BodeTol

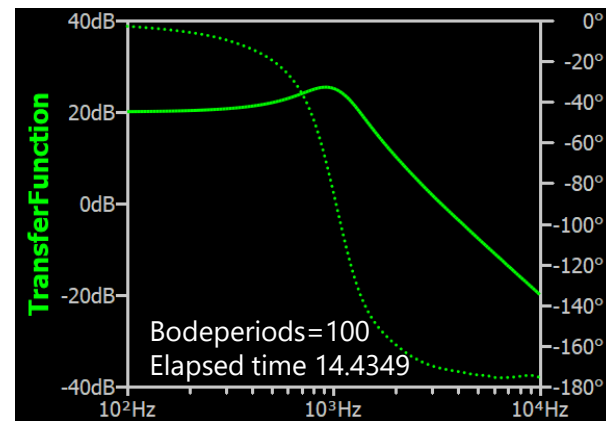
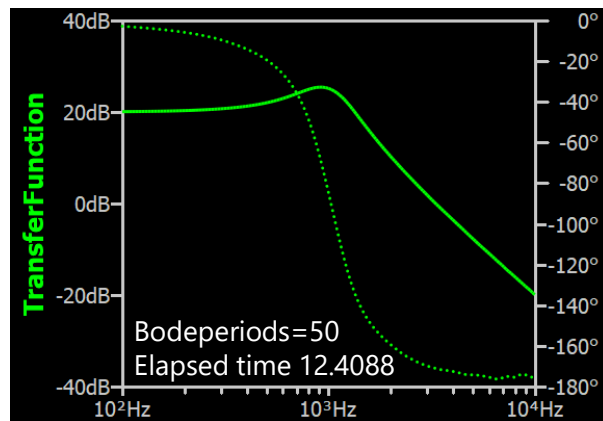
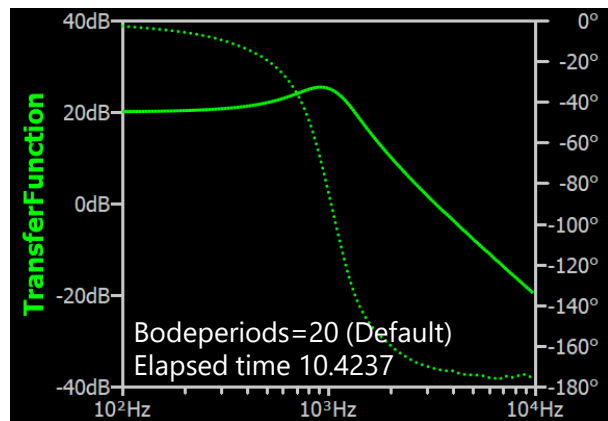
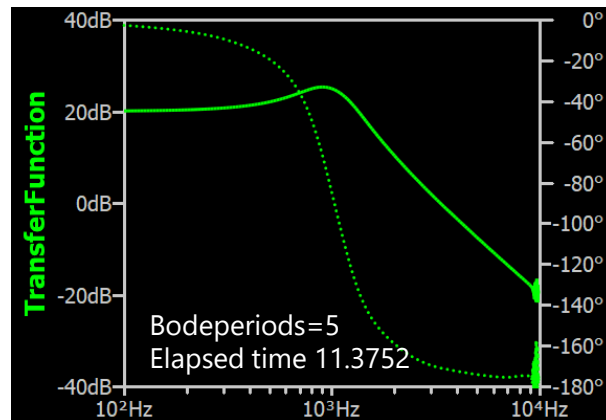
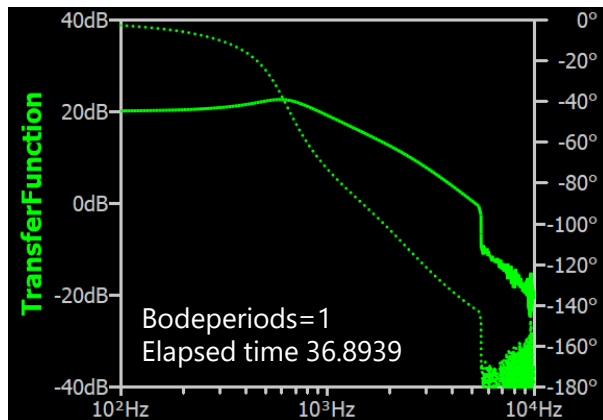
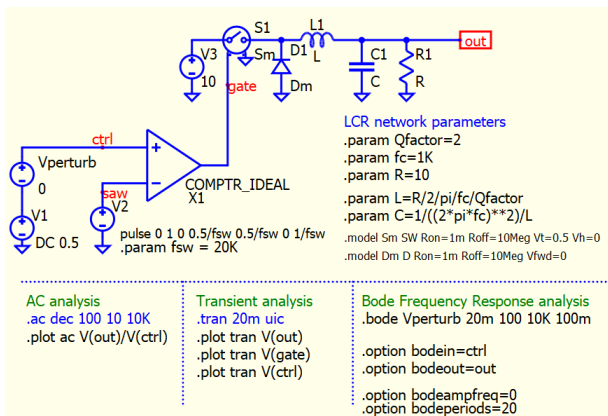
Qspice : bode - bodeTol.qsch

- BodeTol : A frequency response analysis relative tolerance
  - Default BodeTol=10
  - Acceptable value from 0.1 to 15
- BodeTol affects duration of time domain simulation during .bode
  - lower value = longer .tran duration = increase of simulation time
- Reduce this value to sharpen the gain profile for a high Q transfer function
- Reduce BodeTol may improve simulation results, but this is not guarantee if decrease too much!



# .option Bodeperiods

Qspice : bode - Buck - open loop - bodeperiods.qsch



\*\* I cannot identify its exact function, but setting in default can give a reasonable result



Explain .ac and .bode  
relationship

# Basic of Frequency Response Analysis

## Qspice : Bode - LCR - open loop.qsch

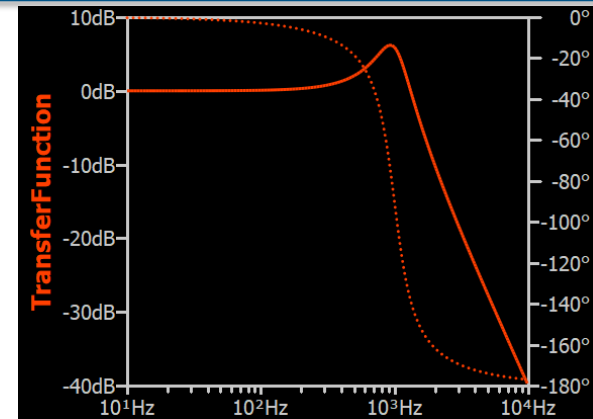
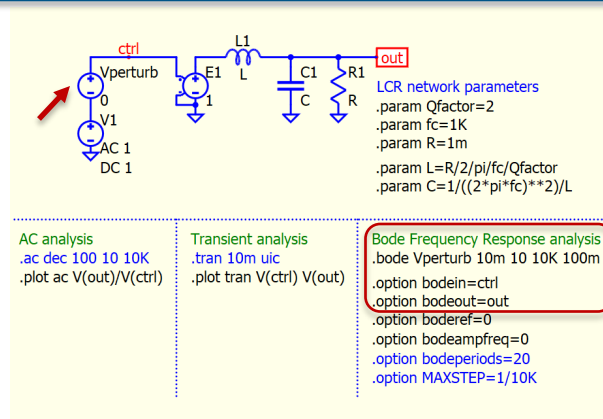
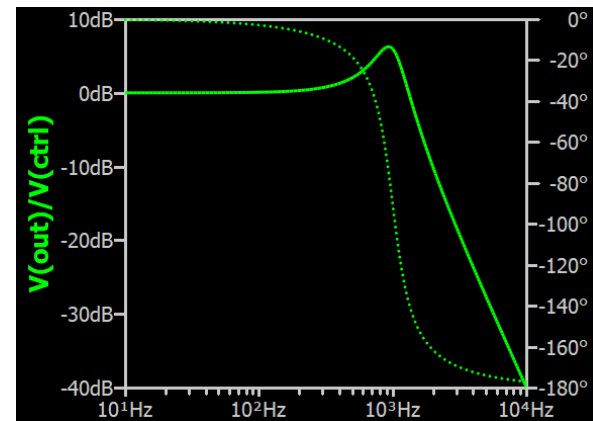
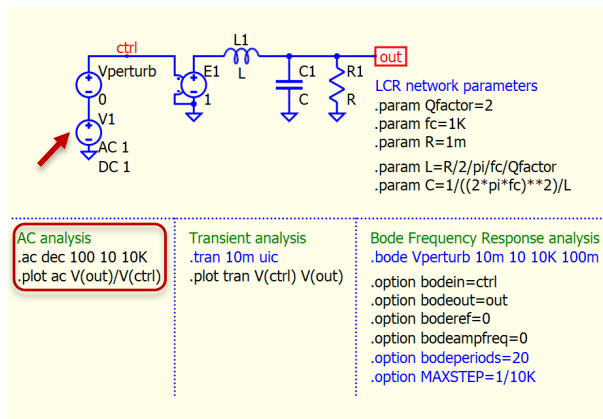
### Basic Theory

- Frequency response analysis is to insert a perturbing source into system, and measuring gain/phase between two voltage nodes
- .ac and .bode can achieve same result for linear circuit
- In .ac example, V1 has AC 1 as perturbation source, and

$$G(s) = \frac{v_{out}}{v_{ctrl}}$$

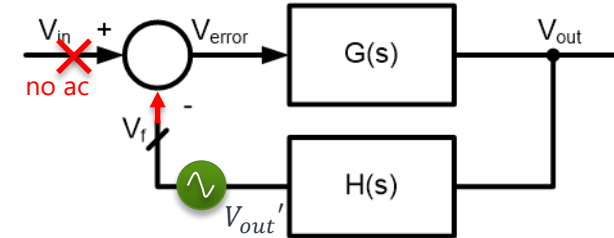
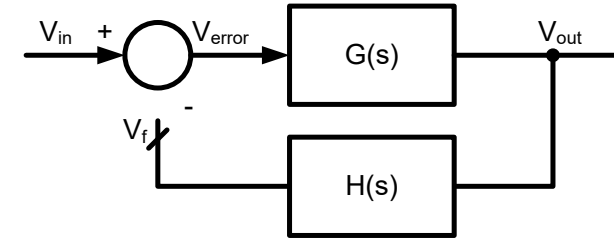
- In .bode example, Vperturb is inserted with a setting that voltage equals 100mV from 10Hz to 10kHz

$$G(s) = \frac{\text{bodeout}}{\text{bodein}} = \frac{v_{out}}{v_{ctrl}}$$



# Open Loop Transfer Function in Close Loop System : Theory

- For close-loop system, perturbing source is added in feedback path to measure its open loop transfer function without breaking the close-loop operation
- Definition of Open Loop Transfer Function
  - It is defined as cutting the feedback path as
  - $GH(s) = G(s)H(s) = G_c(s)G_{plant}(s)H(s)$
- When  $V_f$  is break from the loop and AC test signal is from  $V_{in}$ 
  - $GH(s) = \frac{\text{output of } H(s)}{\text{input of } G(s)} = \frac{\tilde{v}_f}{\tilde{v}_{in}} = \frac{\tilde{v}_f}{\tilde{v}_{error}}$
- If  $V_{in}$  is DC only and inject an AC to feedback path as test signal
  - $\tilde{v}_{error} = -\tilde{v}_f$
  - $GH(s) = \frac{\text{output of } H(s)}{\text{input of } G(s)} = \frac{\tilde{v}_{out}'}{\tilde{v}_{error}} = -\frac{\tilde{v}_{out}'}{\tilde{v}_f}$
  - If  $H(s) = 1$ ,  $V_{out} = V_{out}'$ 
    - $GH(s) = G_c(s)G_{plant}(s) = \frac{\tilde{v}_{out}}{\tilde{v}_{error}} = -\frac{\tilde{v}_{out}}{\tilde{v}_f}$



# Open Loop Transfer Function in Close Loop System

Qspice : Bode - LCR - open loop.qsch

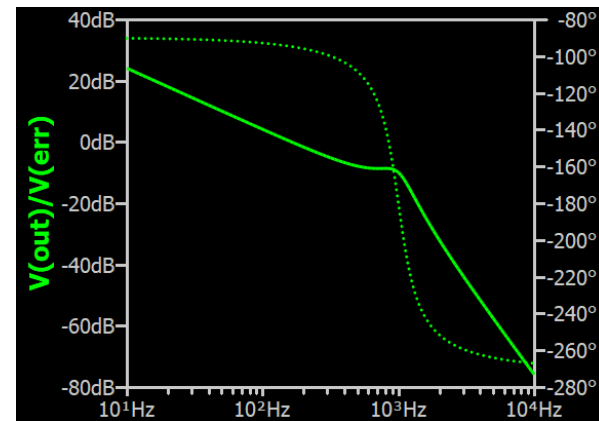
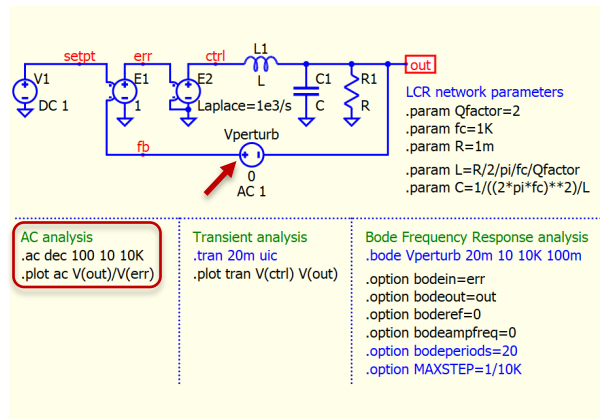
- Open Loop Transfer Function in Close Loop System

- Perturbing source is inserted into feedback path

- Open Loop Transfer Function

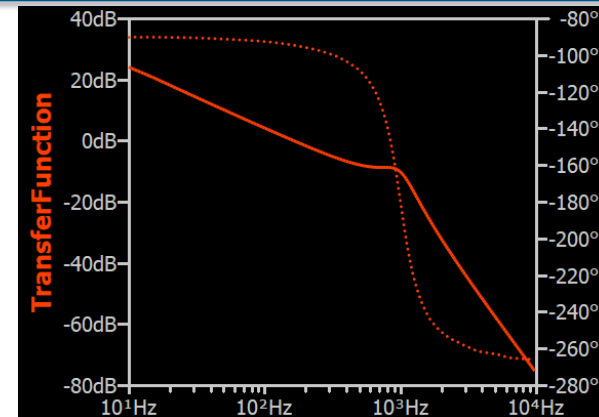
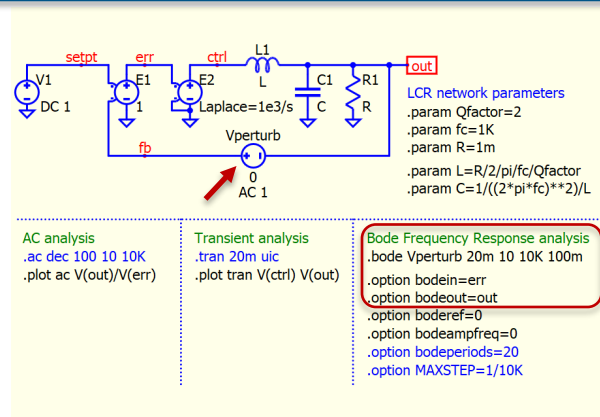
$$GH(s) = -\frac{v_{out}}{v_f} = \frac{v_{out}}{v_{err}}$$

- This is a linear system example, with E1 as difference and E2 as compensator (integrator), both .ac and .bode can be used in analyzing linear system



- Different of .ac and .bode

- .ac only computes frequency response for non-switching circuit which can linearized
- .bode extract frequency domain response from time domain analysis (.tran), to computes frequency response from switching circuit



## Appendix

### Step-by-Step Example A Buck Converter

# Part 1 : Close Loop Code Plot Example

## Qspice : Buck CloseLoop with Vperturb (.tran).qsch

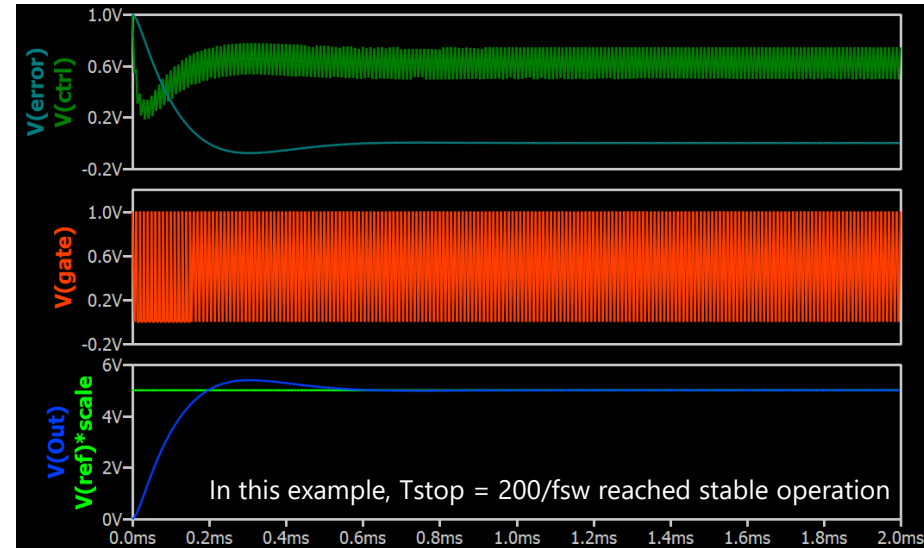
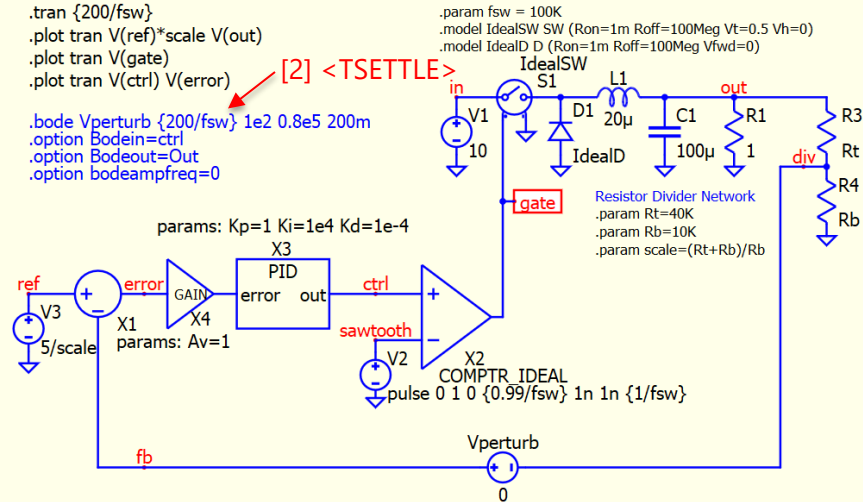
- Determine <Tsettle>
  - [1] Run .tran analysis to determine how long the circuit can settle to steady state
    - .bode can only perform for a stable system
  - [2] Time required to reach stable operation is <TSETTLE> for .bode directive

### Close Loop Feedback for Buck Converter with Bode Plot Analysis

```
.tran {200/fsw}  
.plot tran V(ref)*scale V(out)  
.plot tran V(gate)  
.plot tran V(ctrl) V(error)
```

```
.bode Vperturb {200/fsw} 1e2 0.8e5 200m  
.option Bodein=ctrl  
.option Bodeout=Out  
.option bodeampfreq=0
```

params: Kp=1 Ki=1e4 Kd=1e-4



# Part 1 : Close Loop Bode Plot Example - <SOURCE> is voltage source

## Qspice : Buck CloseLoop with Vperturb (.bode).qsch

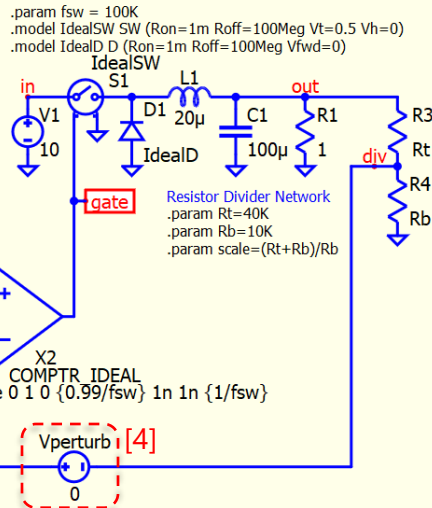
- .bode simulation with <SOURCE> is voltage source
  - [1] User determine <FSTART>, <FSTOP> and <AMP>, in this example, variable amplitude is used
  - [2] Perturbing source is added in series to feedback loop
    - If .option bodein and bodeout not specify
    - Bodeout is -ve terminal : transfer function numerator voltage node (e.g. div)
    - Bodein is +ve terminal : transfer function denominator voltage node (e.g. fb)
  - [3] Run simulation to get bode plot
    - If OpenLoopGain is not smooth, consider to adjust bodeLoPow and bodeHiPow for Amplitude <AMP> of perturbing source
    - If instability is observed at certain frequency, can use .option MAXSTEP to limit maximum time step in time domain analysis

### Close Loop Feedback for Buck Converter with Bode Plot Analysis

```
.tran {200/fsw}  
.plot tran V(ref)*scale V(out)  
.plot tran V(gate)  
.plot tran V(ctrl) V(error)
```

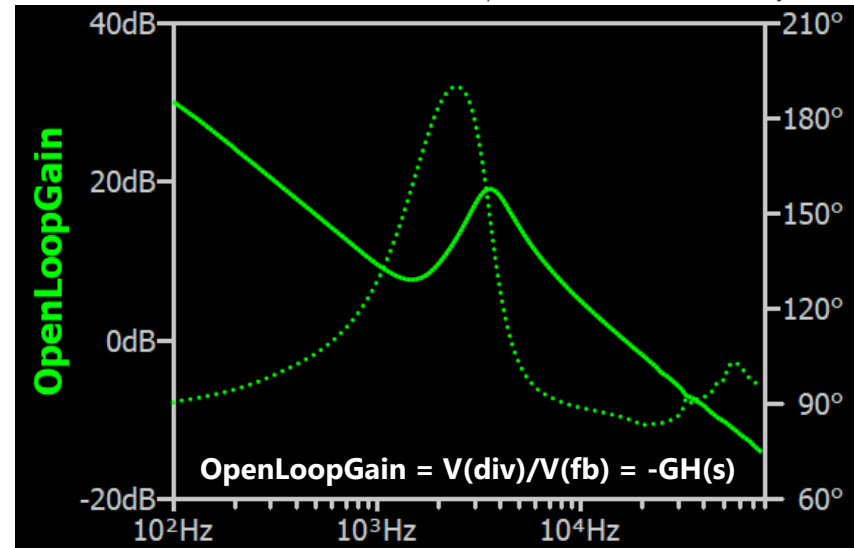
```
.bode Vperturb {200/fsw} 1e2 0.8e5 200m  
.option Bodein=ctrl  
.option Bodeout=Out  
.option bodeampfreq=0  
.option MAXSTEP=1/fsw/100  
.option bodeLoPow=0 bodeHiPow=-0.8
```

params: Kp=1 Ki=1e4 Kd=1e-4



Resistor Divider Network  
.param Rt=40K  
.param Rb=10K  
.param scale=(Rt+Rb)/Rb

X2 COMPTR IDEAL  
pulse 0 1 0 {0.99/fsw} 1n 1n {1/fsw}

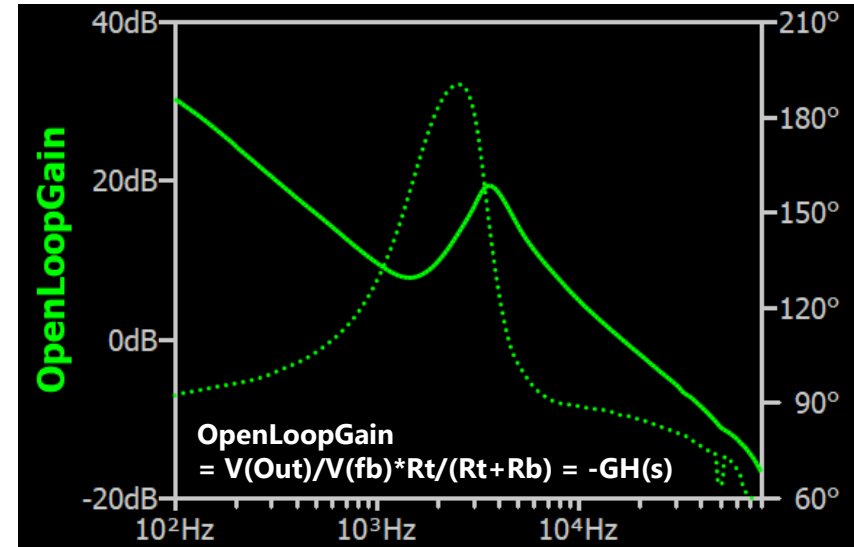
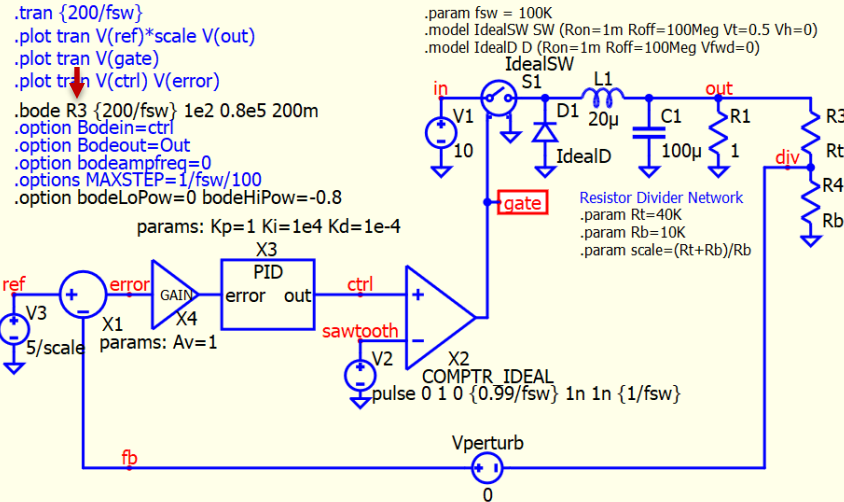


# Part 1 : Close Loop Bode Plot Example - <SOURCE> is Top Resistor

## Qspice : Buck CloseLoop with R3 (.bode).qsch

- .bode simulation with <SOURCE> is Top Resistor
  - [1] Alternatively, top resistor can be used as the perturbing source <SOURCE>
    - Resistor Pin 1 : transfer function numerator voltage node (e.g. out)
    - Resistor Pin 2 : transfer function denominator voltage node (e.g. div=fb)
  - [2] Run simulation to get bode plot

Close Loop Feedback for Buck Converter with Bode Plot Analysis



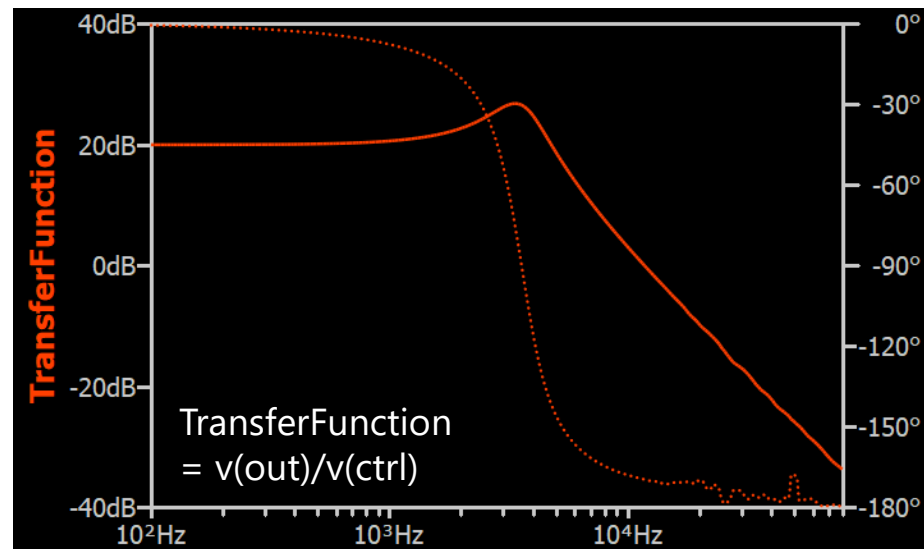
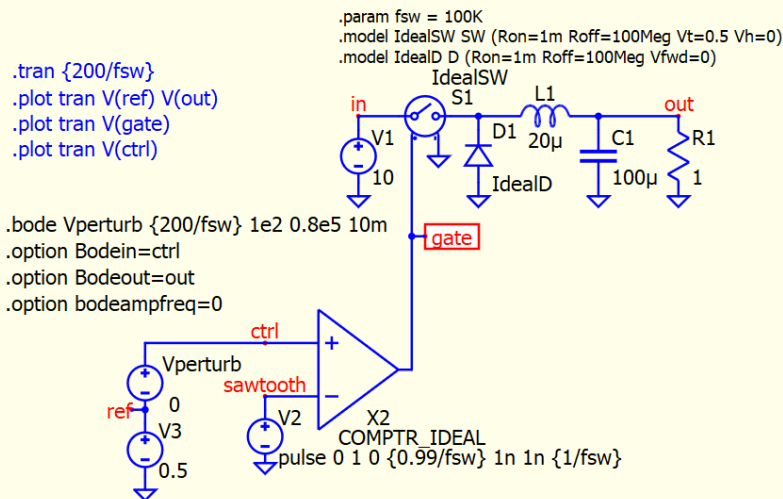


# Part 2 : Open Loop Bode Plot Example

## Qspice : Buck OpenLoop with Vperturb (.bode).qsch

- .bode for Open Loop
  - As numerator and denominator voltage node can be defined by in .option bodein / bodeout
  - [1] Arrange circuit into open loop operation, add perturbing source in series of reference/setpoint to input node (e.g. ctrl in this example)
  - [2] use .option to set input node with **.option Bodein** and output node with **.option Bodeout**
  - [3] Run simulation to get bode plot

### Open Loop Feedback for Buck Converter with Bode Plot Analysis



# Part 2 : Open Loop Bode Plot Example – C++ Comparator Block

## Qspice : Buck ConverterBodePlot - OpenLoop with Cpp.qsch

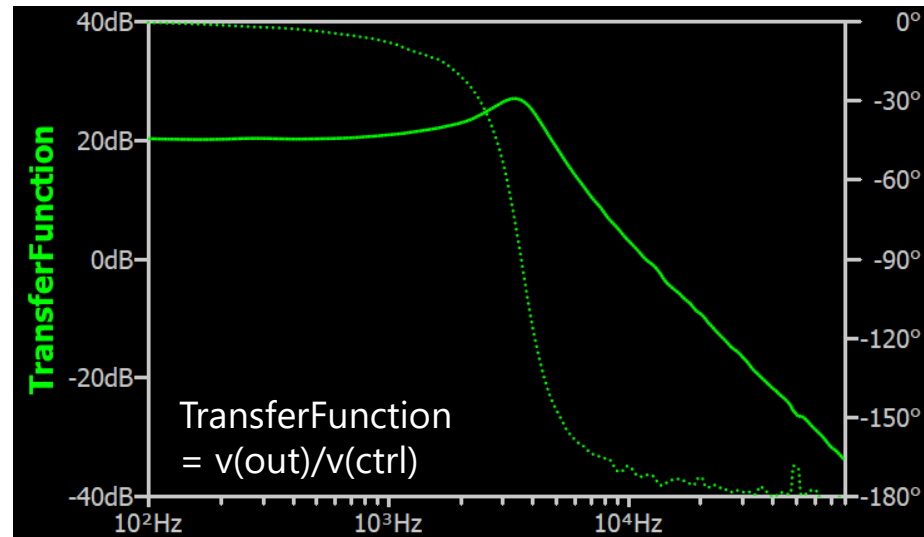
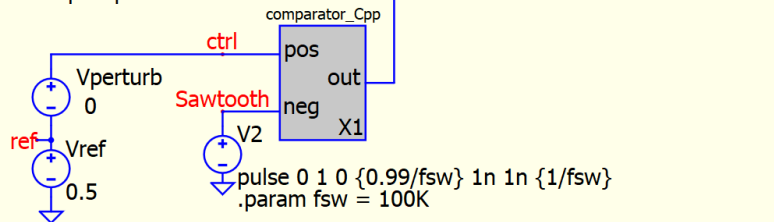
- .bode for Open Loop with a C++ Comparator Block
  - This is to demonstrate .bode can work with digital blockset

### Buck Converter Bode with Open Loop

```
.tran {200/fsw}  
.plot V(out)  
.plot V(gate)
```

```
.options MAXSTEP={1/fsw/50}
```

```
.bode Vperturb {200/fsw} 1e2 0.8e5 20m  
.options bodein=ctrl  
.options bodeout=out  
.options bodeampfreq=0
```



## Appendix B

### Qspice Demo :

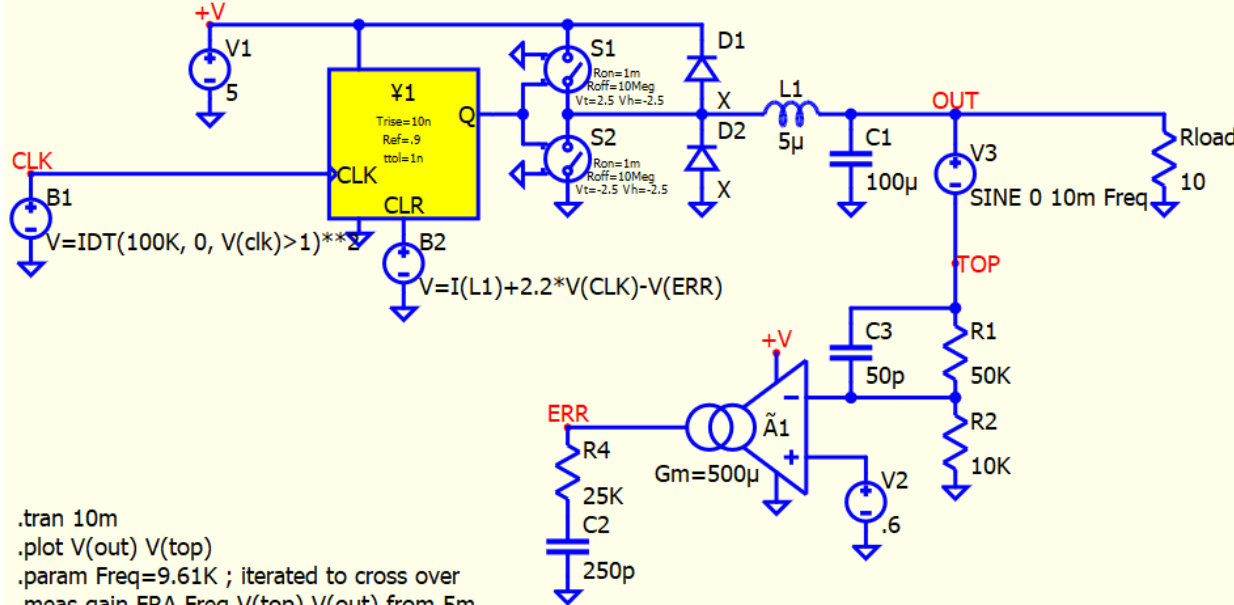
### FRA\_SMPS

Compare FRA and .bode

# Use Qspice Demo Circuit FRA\_SMPS.qsch to compare FRA and .bode

## Qspice : FRA\_SMPS (fra).qsch

Example of using the .meas FRA command. Probably the most accurate way of extracting the open loop voltage gain at a specific frequency.



```
.tran 10m
.plot V(out) V(top)
.param Freq=9.61K ; iterated to cross over
.meas gain FRA Freq V(top) V(out) from 5m
.step dec param Freq 1K 80K 50
```

[1] Modify FRA example with a .step for frequency sweep

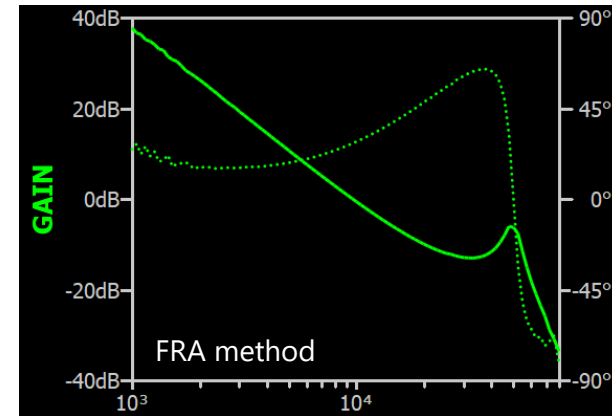
Output Window

.meas gain fra freq v(top) v(out) from 5m:			
37.7558dB	24.6736°		
36.5949dB	27.2906°		
36.2864dB	22.3482°		
35.1243dB	26.1136°		
34.7839dB	21.235°		

Simulation Post Process

Run Simulation  
Copy  
Select All  
Close Window  
Plot these Measurements

[2] In Post Process  
Right Click > Plot these Measurements  
This will generate below Bode Plot



Total elapsed time : 43.0839 seconds

## Use Qspice Demo Circuit FRA\_SMPS.qsch to compare FRA and .bode

