

# ASEN 3113: Heat Conduction Prelab

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## 1 Question 1

Three assumptions made for the derivation were:

- 1) The rod is assumed to only have an axial dimension, which would introduce some error with our predicted rate of heat loss.
- 2) Entire cold end of the rod is at constant temperature  $T_0$ .
- 3) Constant initial temperature of the rod

## 2 Question 2

	Aluminum 7075-T651	Stainless Steel T-303 annealed	brass C360
$\rho(\frac{kg}{m^3})$	2,810	8,000	8,490
$k(W/m-K)$	130	16.2	115
$c_p(\frac{J}{kg \cdot K})$	960	500	380
$\alpha(\frac{m^2}{s})$	$4.819 * 10^{-5}$	$4.05 * 10^{-6}$	$3.565 * 10^{-5}$
Source	www.matweb.com	asm.matweb.com	www.matweb.com

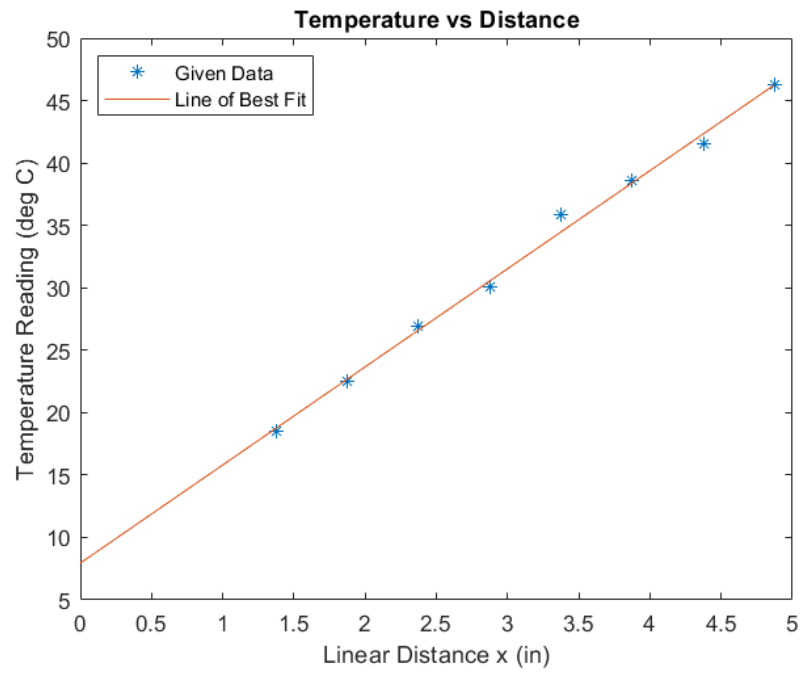
## 3 Question 3

Using the given data

$$T_0 = 7.949^\circ\text{C}$$

$$H = 7.861$$

on the next page is a graph which compares the temperature readings with the calculated best fit line.



## 4 Question 4

Derived 5equation:

$$b_n = \frac{-8HL(-1)^n}{(2n\pi - \pi)^2}$$

The below pages show the derivation.

$$b_n = -\frac{2H}{L} \int_0^L x \sin(\lambda_n x) dx$$

integration by parts:

$$\int u dv = uv - \int v du$$

$$u = x, \quad dv = \sin(\lambda_n x) dx$$

$$du = dx, \quad v = -\frac{\cos(\lambda_n x)}{\lambda_n}$$

$$\begin{aligned} \int x \sin(\lambda_n x) dx &= -\frac{x \cos(\lambda_n x)}{\lambda_n} - \int -\frac{\cos(\lambda_n x)}{\lambda_n} dx \\ &= -\frac{x \cos(\lambda_n x)}{\lambda_n} + \int \frac{\cos(\lambda_n x)}{\lambda_n} dx \end{aligned}$$

$$\text{let } u = \lambda_n x, \text{ so that } dx = \frac{1}{\lambda_n} du$$

$$\text{then: } \int \frac{\cos(u)}{\lambda_n^2} du = \frac{1}{\lambda_n^2} \int \cos(u) du = \frac{\sin(u)}{\lambda_n^2}$$

$$\text{then } u = \lambda_n x \text{ so}$$

$$\int \frac{\cos(\lambda_n x)}{\lambda_n^2} dx = \frac{\sin(\lambda_n x)}{\lambda_n^2}$$

$$\therefore \int_0^L x \sin(\lambda_n x) dx = \left[ -\frac{x \cos(\lambda_n x)}{\lambda_n} + \frac{\sin(\lambda_n x)}{\lambda_n^2} \right]_0^L$$

$$\text{then: } \int_0^L x \sin(\lambda_n x) dx = \frac{\sin(\lambda_n L)}{\lambda_n^2} - \frac{L \cos(\lambda_n L)}{\lambda_n}$$

$$\lambda_n = \frac{(2n-1)\pi}{2L}$$

$$\sin(\lambda_n L) = \sin\left[\frac{(2n-1)\pi}{2L} \cdot L\right] = \sin\left(\pi n - \frac{\pi}{2}\right)$$

$$\cos(\lambda_n L) = \cos\left[\frac{(2n-1)\pi}{2L} \cdot L\right] = \cos\left(\pi n - \frac{\pi}{2}\right)$$

Using the following identity:  $\sin(A-B) = -\cos(A)\sin(B) + \cos(B)\sin(A)$   
 then  $\sin(\pi n - \pi/2) = -\cos(\pi n)\sin(\pi/2) + \cos(\pi/2)\sin(\pi n)$

$$\cos(\pi/2) = 0$$

$$\sin(\pi/2) = 1$$

$$\sin(\pi n - \pi/2) = -\cos(\pi n)$$

for  $n = 1, 2, 3, 4, \dots$   $-\cos(\pi n)$  will alternate between 1 and -1  
 $\therefore$  we can represent it as  $(-1)^n$

using the following identity:  $\cos(A-B) = \cos(A)\cos(B) + \sin(A)\sin(B)$

$$\text{then } \cos(\pi n - \pi/2) = \cos(\pi n)\cos(\pi/2) + \sin(\pi n)\sin(\pi/2)$$

$$\therefore \cos(\pi n - \pi/2) = \sin(\pi n)$$

$$\therefore \cos(\pi n - \pi/2) = \sin(\pi n)$$

$$\text{for } n = 1, 2, 3, 4, \dots \quad \sin(\pi n) = 0$$

$$\text{Then } b_n = \frac{-2H}{L} \left[ (-1)^n \right]$$

$$\text{Then } b_n = \frac{-2H}{L} \left[ \frac{(-1)^n}{\pi_n^2} \right]$$

$$\pi_n^2 = \frac{((2n-1)\pi)^2}{(2L)^2}$$

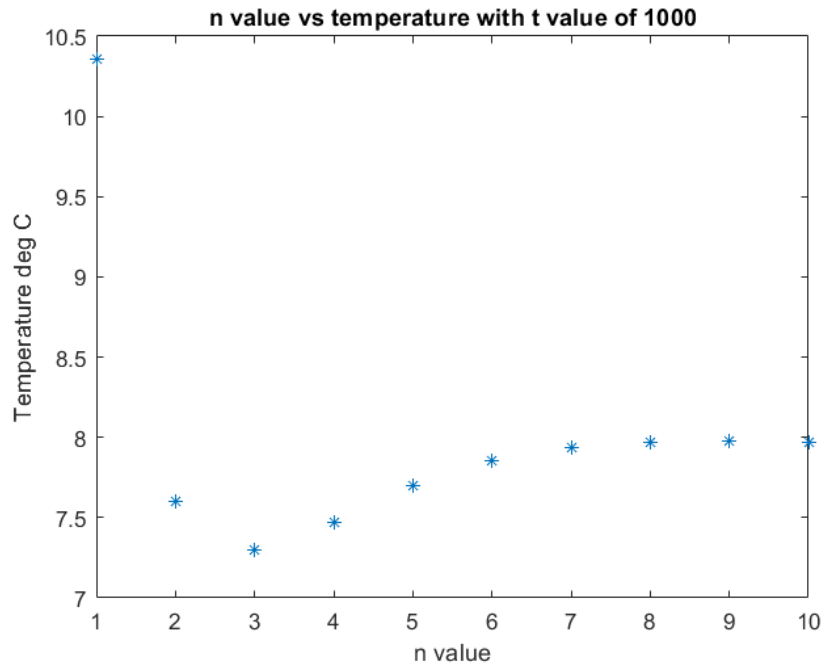
$$= \frac{((2n-1)\pi)^2}{4L^2}$$

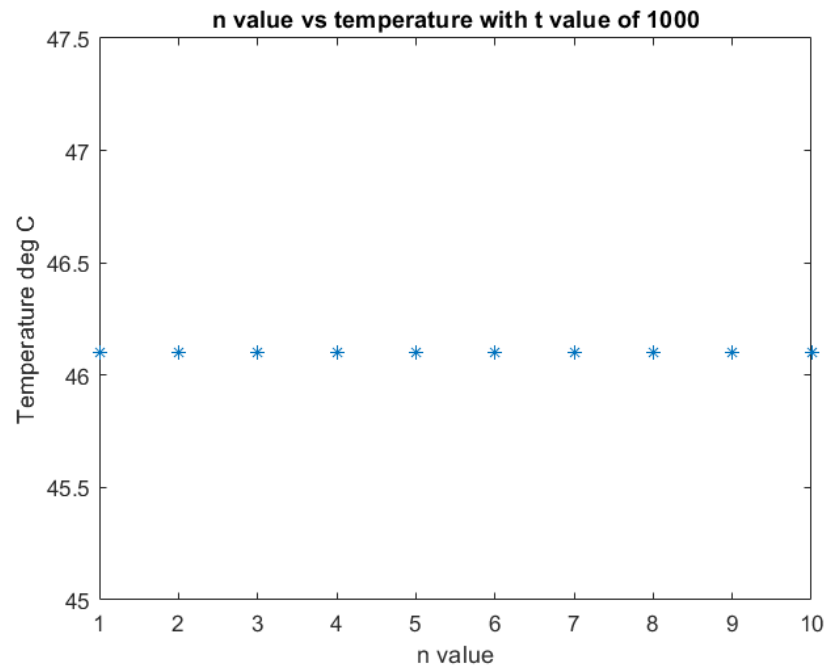
$$b_n = \frac{-2H}{L} \left[ (-1)^n \times \frac{4L^2}{(2n\pi - \pi)^2} \right]$$

$$b_n = \frac{-8HL(-1)^n}{(2\pi n - \pi)^2}$$

## 5 Question 5

Below are the graphs representing the value of the temperature reading at the last thermocouple with changing values of  $n$  and  $t$ . The higher the  $t$  value the less terms are needed to converge because the pipe would be closer to a steady state.





## 6 Question 6

The overall shape of the transient model becomes more linear as the thermal diffusivity decreases in value. In addition, the higher the thermal diffusivity the sooner the rod approaches its steady state. This is shown in the second graph on the next page.

