Routine Core Analysis Well: <u>Poseidon - 2</u> Offshore Western Australia

Prepared for ConocoPhillips Exploration Australia Pty. Ltd.

October 2010

File: PRP-09079

Rock Properties Core Laboratories Perth Australia

11th October 2010

ConocoPhillips Exploration Australia Pty. Ltd.

Level 3 53 Ord Street PERTH WA 6005

Attention: Rob Rutherford

Subject : Routine Core Analysis

Well : Poseidon - 2 File : PRP-09079

Dear Rob,

Presented herein is the final report of a routine core analysis study conducted on a core from the above well that arrived at our laboratory in December 2009.

We appreciate the opportunity to present this service to ConocoPhillips Exploration Australia Pty. Ltd. Please contact us should you require any further information or assistance.

Yours sincerely,

Core Laboratories Australia Pty Ltd

James Brown Senior Core Analyst

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INTRODUCTION

Cores 1 to 3 arrived at Core Laboratories on the 8th December 2009.

Services performed and presented in the report include:

- Surface spectral core gamma
- CT scanning
- Profile permeametry on slabbed core
- Core photography on slabbed core ultra violet and white light (prints and CD-Rom)
- Permeability, porosity (at ambient and overburden) and grain density measurements on plugs
- Residual fluid saturations by Dean Stark

The reported data for the above services are presented digitally on a CD-Rom, with the exception of the core photographs and CT-Scans which are presented under separate covers.

SUMMARY

A total of 237 horizontal and 8 vertical plugs were cut from the core. Porosity, permeability and grain density measurements were made on 201 horizontal and all vertical samples at net confining stresses of 400psi, 800psi and 5600psi. Residual fluid saturations were determined on 31 samples.

	<u>Minimum</u>	<u>Maximum</u>	<u>Average</u>
Net Confining Pressure of 400psig. SS Permeability, Hg Bulk Volume Porosity Cool Solvent, Humidity Dried			
Porosity (%) Permeability, Kair, (md) (Horizontal) Permeability, Kair, (md) (Vertical) Grain Density (g/cc)	0.1 <0.001 0.002 2.616	12.9 0.940 0.055 3.489	3.2 0.080 0.014 2.724
Net Confining Pressure of 400psig.			
Warm Solvent, Convection Oven Dried			
Porosity (%) Permeability, Kair, (md) (Horizontal) Permeability, Kair, (md) (Vertical) Grain Density (g/cc) Residual Brine Saturation, Sw. (%)	0.2 0.003 0.009 2.638 26.9	12.8 1.50 0.067 3.514 85.6	4.0 0.074 0.026 2.734 57.4
Net Confining Pressure of 5600psig. CMS-300 Porosity (%) Permeability, Kair, (md) (Horizontal) Permeability, Kinf, (md) (Horizontal)	0.3 <0.001 <0.001	12.2 0.275 0.171	4.8 0.026 0.024

Note: Permeability from fractured samples is not included in the above table.

LABORATORY PROCEDURES

Initial Inventory:

The cores arrived on the 8th December 2009 resinated in aluminium inner core barrels, each approximately 4.5m in length. From the markings on the core barrels and the accompanying manifest, an inventory of the core was made and can be found in the back of this report.

Core Preparation:

After the core inventory, the 4.5m lengths of core were cut down into one metre lengths (and sealed) for ease of handling and processing. A surface spectral core gamma was run down the core, prior to being CT scanned. Core 2 was not scanned as it was fast tracked for routine core analysis. After reviewing the CT-Scans, seven full diameter sections were chosen and preserved for later analysis.

The aluminium inner core barrel was then milled from the core (Dean-Stark samples were taken at this point). Next plug samples (both horizontal and vertical plugs) were taken; this was followed by Scal samples. After all the samples were taken the cores were slabbed in half and the core surfaces cleaned. One half of the core underwent ultra violet photography prior to the profile permeability being determined down the core (cores 1 and 2 only). After profile permeability was run, the cores were photographed under white light. The other half section of core was described.

Surface Core Gamma:

The spectral core gamma was calibrated using known standards prior to the core being run. The total core gamma trace is plotted on the integrated core log.

CT Scanning:

The one metre lengths of core were CT scanned, to identify bedding dip, fractures, lithology and rubble sections so that the cores could be orientated for plugging and slabbing. Core 2 was not CT scanned as the routine core analysis was fast tracked.

Sample Preparation:

Six sets of samples were taken.

- Set 1 31 horizontal samples taken for residual fluid saturations (identified as _DS)
- Set 2 170 horizontal routine core analysis samples taken from cores 2 and 3 with no identifier
- Set 3 8 vertical samples taken from the cores (identified as _V)
- Set 4 11 horizontal samples taken from the cores for later analysis (identified as samples S1_)
- Set 5 25 horizontal samples taken from the cores for later analysis (identified as samples S2_)
- Set 6 7 full diameter samples taken from the cores (identified as GM_)
- Set 7 19 samples for petrology from core 1(identified as _TS)

Set 1 Samples were 1.5" diameter plugs cut and trimmed with mineral oil. These then underwent Dean-Stark analysis. After completion of Dean-Stark analysis, the samples were warm solvent cleaned with toluene and methanol, to remove any residual hydrocarbons and salts, prior to

WELL

convection oven drying. Porosity, permeability and grain density were measured on the cleaned and dried samples. Off-cuts from the trimmed plugs were placed into labelled snap-lock plastic bags.

Set 2 Samples were 1.0" diameter plugs cut and trimmed with 2% potassium chloride brine. These were cool solvent cleaned with toluene and methanol, to remove any residual hydrocarbons and salts. Complete salt removal was indicated by the methanol, in which the samples were immersed, producing a negative reaction to silver nitrate, prior to being controlled humidity oven dried (at 60°C and 40% relative humidity). Off-cuts from the trimmed plugs were placed into labelled snaplock plastic bags. The samples were allowed to cool down to room temperature in the snap-lock plastic bags prior to porosity, permeability and grain density being determined.

The samples were then re-cleaned with warm solvents, toluene followed by methanol to remove any residual hydrocarbons and salts. Complete salt removal was indicated by the methanol, in which the samples were immersed, producing a negative reaction to silver nitrate, prior to being dried in a convection oven at 105°C. The samples were cooled down to room temperature in an evacuated desiccator prior to re-determining porosity, permeability and grain density. To ensure complete drying at both drying stages (humidity and convection drying), the samples were weighted at regular intervals to a constant weight (+/- 0.01g).

Set 3 Samples were prepared in the same manner as Set 2 samples.

Sets 4 and 5 Samples were 1.5" diameter plugs cut and trimmed using a 2% potassium chloride brine. The plugs were wrapped in Saran wrap, aluminium foil and placed into snap-lock plastic bags, then stored in a cooler unit for later analysis.

Set 6 Samples were full diameter samples taken at the requested depths, preserved and stored for later analysis.

Set 7 Samples were petrology samples taken where indicated from core 1 and placed into labelled snap-lock plastic bags.

Core Slabbing:

The cores were slabbed in half using brine as the blade lubricant except for the preserved full diameter sections. After slabbing, the cut faces of the core sections were cleaned prior to having profile permeability measured, being photographed and described.

Profile Permeametry:

Profile permeametry was conducted on the cut face of the one half core section using the PDPK[™]300 profile permeameter. Measurements were made approximately every ten centimetres; a total of 568 point measurements were made. Core 1 profile permeability was not determined.

Core Photography:

Prior to profile permeametry, the one-half section of the core was photographed under ultra violet light. White light photography was done after the profile permeability using a digital camera. The large format images of the core were annotated with the ambient (400psig (convection oven dried)) routine core

analysis data. A set of A4 prints and a CD-ROM containing the images was forwarded under a separate cover.

Grain Volume and Grain Density:

The weight, diameter and length of all routine core analysis plug samples were measured before they were processed through the Ultrapore[™] porosimeter to determine grain volume. As a standard quality control measure, a calibration check plug was run with every batch of samples. Grain density data is calculated from grain volume and sample weight data.

Permeability and Porosity:

Permeability was determined using an Ultra-Perm[™] 500 at a confining stress of 400psi. Permeability is calculated using the Darcy equation below for all samples both after cool solvent/humidity drying and warm solvent/convection drying.

Kair =
$$2000P_1\mu Q_1L/(P_1^2 - P_2^2)A$$

Where:

Kair = Permeability (md)

 μ = Viscosity (Centipoise)

 Q_1 = Flow rate (cc/sec) at upstream pressure

L = Sample length (cm)

A = Sample cross-sectional area (cm²)

P₁ = Upstream pressure (atmospheres)

P₂ = Downstream pressure (atmospheres)

Porosity was calculated using the grain and bulk (mercury bulk volume) volumes as follows:

 $\phi = ((Vb-Vg)/Vb)*100$ Where : ϕ = Porosity, fraction

Vg = Grain volume, cm³ Vb = Bulk volume, cm³

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A sub selection of the above samples underwent porosity and permeability measurements using the CMS- 300^{TM} at confining pressures of 800psi and 5600psi. Klinkenberg permeability (K_{inf}) and Forchheimer Factor Beta values are obtained directly from the CMS-300, since it operates by unsteady-state principles. Porosity data was obtained by combining pore volumes from the CMS-300 data with grain volumes from the Ultrapore porosimeter.

POROSITY, PERMEABILITY and GRAIN DENSITY

		Cool	Solvent and H	umidity Dried		Warm Solvent and Connvection Oven			CMS 300					CMS 300				
SAMPLE	SAMPLE	CONFINING S	TRESS 400psi	Hg	GRAIN	CONFINING	STRESS 400psi	Hg	GRAIN	CONFIN	ING STRE	ESS 800psi.		CONFIN	IING STRESS	5 5600psi.		COMMENTS
NUMBER	DEPTH	Steady - State F	•				PERMEABILITY	_			ABILITY	POROSITY	PERME	ABILITY	POROSITY	<u> </u>	b(N2)	1
		Kinf	Kair	POROSITY		Kinf	Kair	POROSITY		Kinf	Kair		Kinf	Kair				
	(m)	(md)	(md)	(%)	(g/cc)	(md)	(md)	(%)	(g/cc)	(md)	(md)	(%)	(md)	(md)	(%)	(ft-1)	(psi)	
Core 2																		1
1	5061.30		0.024	3.9	2.677		0.023	4.6	2.684									
2	5061.60		0.002	3.2	2.728		0.020	3.9	2.739									
3	5061.90		0.034	2.1	2.713		0.015	2.8	2.725	0.002	0.005	3.0	< 0.001	0.001	2.3	1.53E+17	232.56	
4	5062.20		0.016	1.6	2.660		0.021	2.6	2.675	0.002	0.000	0.0	10.00.	0.00.				
5	5062.49		0.020	3.1	2.707		0.034	3.4	2.712									
6	5062.79		0.037	4.0	2.697		0.026	4.4	2.703	0.030	0.054	4.6	0.001	0.002	4.3	1.84E+16	176 68	
7	5063.40		0.030	4.4	2.693		0.030	4.5	2.696	0.000	0.001	1.0	0.001	0.002	1.0	1.012110	170.00	
8	5063.70		0.055	5.0	2.675		0.073	5.2	2.680									
9	5063.76		0.056	5.0	2.684		0.041	5.3	2.689	0.016	0.022	5.6	0.001	0.002	5.0	1.18E+16	166 01	
10	5064.30		0.034	4.8	2.678		0.036	5.4	2.687	0.010	0.022	5.0	0.001	0.002	3.0	1.102+10	100.31	
11	5064.60		0.034	4.0 6.5	2.702		0.036	5. 4 6.6	2.709									
	5064.60		0.045		2.680		0.020		2.682	0.015	0.021	6.9	0.001	0.004	6.3	3.86E+15	11111	
12	5064.91		0.045	6.2 6.3	2.706		0.043	6.7	2.710	0.015	0.021	0.9	0.001	0.004	0.3	3.00⊑+13	144.44	
13								6.6										
14	5065.80		0.046	5.1	2.686		0.046	5.7	2.697	0.000	0.000	0.4	0.004	0.004	0.0	0.045.40	040.50	
15	5066.10		0.017	1.8	2.709		0.019	2.9	2.725	0.003	0.008	3.1	<0.001	0.001	2.2	9.81E+16	219.50	
16	5066.40		0.036	3.1	2.694		0.033	3.4	2.697									
17	5066.70		0.040	3.4	2.672		0.043	3.7	2.675	0.040	0.047	- 4	0.004		4.0	4 005 40	405.05	
18	5066.97		0.033	4.6	2.685		0.042	5.2	2.700	0.013	0.017	5.4	0.001	0.002	4.8	1.08E+16	165.05	
19	5067.30		0.082	5.6	2.670		0.135	6.2	2.677									
20	5067.61		0.020	3.4	2.733		0.029	4.3	2.746									
21	5067.90		0.027	3.7	2.687		0.032	3.6	2.692	0.006	0.014	4.4	0.001	0.002	3.7	1.32E+16	169.35	
22	5068.21		0.040	4.0	2.676		0.042	4.4	2.688									
23	5068.51		0.035	3.2	2.667		0.055	3.4	2.671									
24	5068.81		0.015	1.8	2.654		-	2.6	2.672	-	-	-	-	-	-	-	-	Fractured
25	5069.13		0.019	3.1	2.692		0.026	3.9	2.703									
26	5069.43		0.033	3.4	2.645		0.028	3.6	2.664									
27	5069.71		0.013	3.1	2.693		0.021	3.5	2.697	0.007	0.010	3.8	<0.001	0.001	3.0	4.65E+16	199.33	
28	5069.97		0.022	3.7	2.693		0.031	4.1	2.700									
29	5070.30		0.028	3.5	2.663		0.037	4.1	2.670									
30	5070.61		0.194	3.3	2.728		0.020	3.7	2.737	0.003	0.006	4.2	< 0.001	0.001	3.3	8.05E+16	214.07	
31	5070.91		0.019	2.9	2.723		0.026	3.7	2.733									
32	5071.24		0.029	2.1	2.682		0.030	3.7	2.695									
33	5071.50		0.014	2.5	2.734		0.021	3.1	2.744	0.003	0.006	3.2	< 0.001	0.001	2.6	1.01E+17	220.44	
34	5071.81		0.025	2.6	2.706		0.036	2.7	2.713									
35	5072.11		0.017	2.2	2.758		0.025	3.1	2.769									
36	5072.41		0.021	3.3	2.755		0.019	4.2	2.774	0.003	0.007	4.7	< 0.001	0.001	3.6	7.12E+16	210.73	
37	5072.72		0.021	4.3	2.679		0.033	4.6	2.685						- -			
38	5073.31		0.028	4.2	2.673		0.031	5.0	2.688									
39	5073.61		0.041	3.8	2.679		0.035	3.7	2.685	0.006	0.013	4.6	< 0.001	0.002	3.8	1.99E+16	178.56	
40	5073.90		0.021	3.7	2.736		0.026	4.0	2.745	3.000	3.010		.5.501	3.002	0.0	552.110	0.00	
41	5074.20		0.020	3.1	2.690		0.020	3.5	2.697									
42	5074.50		0.023	1.8	2.705		0.028	2.6	2.719	0.005	0.011	3.5	<0.001	0.001	2.5	2.74E+16	186 16	
43	5074.30		0.008	1.9	2.789		0.028	2.4	2.719	0.000	5.011	0.0	~0.00 i	0.001	2.0	2.7 72 710	100.10	
43 44	5075.10		0.022	2.7	2.769		0.013	2. 4 5.8	2.799									
	5075. 4 0 5075.70		0.022							0.006	0.013	3.8	<0.001	0.001	2.9	4.02E+16	105 70	
45 46				2.6	2.684		0.036	3.4	2.696	0.006	0.013	3.0	<0.001	0.001	2.9	4.020+10	130.70	
46 47	5075.97 5076.31		0.017	2.7	2.732		0.030	3.2	2.738									
47	5076.31		0.019	3.2	2.689		0.029	3.8	2.699									
48	5076.60		0.025	3.2	2.697		0.030	3.7	2.706	-	-	-	-	-	-	-	-	
49	5076.91		0.024	2.1	2.678		0.032	3.1	2.693									
50	5077.21		0.007	2.2	2.842		0.012	3.0	2.861									
51	5077.51		0.012	2.0	2.918		0.013	2.3	2.927	0.011	0.022	2.7	<0.001	< 0.001	1.1	-	-	

POROSITY, PERMEABILITY and GRAIN DENSITY

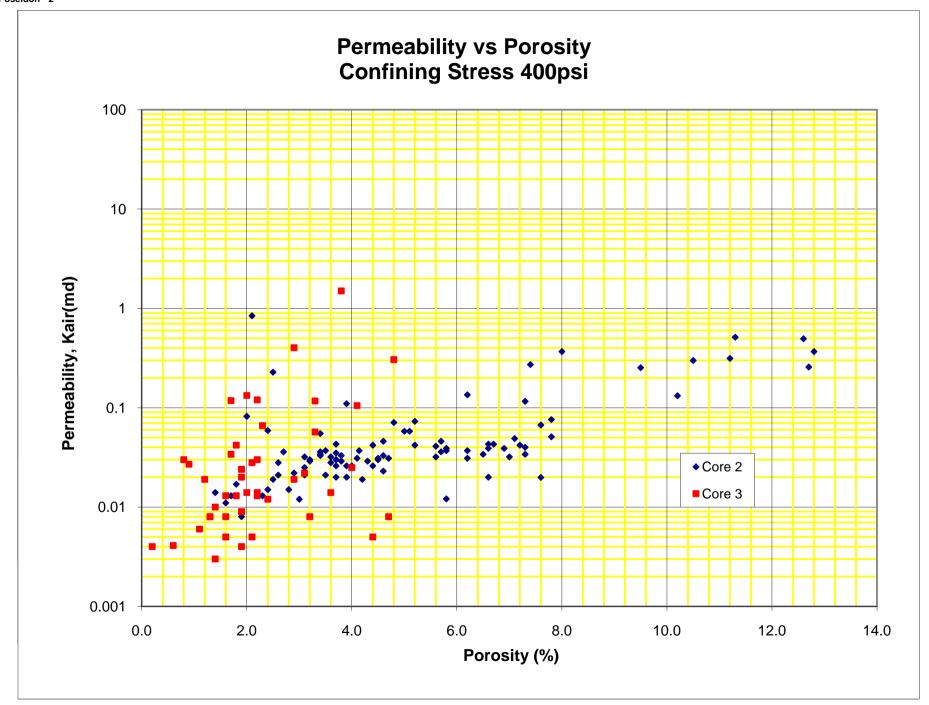
		Cool Solve	ent and Hur	nidity Dried		Warm	Solvent and Cor	nvection Ove	n		CMS 30	0			CMS 300			
SAMPLE	SAMPLE	CONFINING STRES	S 400psi	Hg	GRAIN	CONFINING S	TRESS 400psi	Hg	GRAIN	CONFIN	IING STRE	SS 800psi.		CONFINI	ING STRESS	5 5600psi.		COMMENTS
NUMBER	DEPTH	Steady - State PERM	•	-			PERMEABILITY				ABILITY	POROSITY	PERME	ABILITY	POROSITY	1 -	b(N2)	
		Kinf	Kair	POROSITY		Kinf	Kair	POROSITY		Kinf	Kair		Kinf	Kair				
	(m)	(md)	(md)	(%)	(g/cc)	(md)	(md)	(%)	(g/cc)	(md)	(md)	(%)	(md)	(md)	(%)	(ft-1)	(psi)	
52	5077.81		0.004	1.0	2.738		0.011	1.6	2.748		•	•		•	1	•	I.	
53	5078.11		0.014	1.4	2.726		0.017	1.8	2.733									
54	5078.43		0.072	4.9	2.704		0.071	4.8	2.706	0.018	0.024	5.3	0.001	0.002	4.5	1.26E+16	168.34	
55	5078.73		0.033	6.0	2.693		0.037	6.2	2.698									
56 57	5079.03		0.032	6.2	2.707		0.039	6.6	2.715	0.000	0.040	F 7	0.004	0.000	5 4	4.705.40	475.54	
57 50	5079.31		0.038	5.3	2.719		0.037	5.8	2.725	0.006	0.013	5.7	0.001	0.002	5.1	1.73E+16	1/5.51	
58 59	5079.61 5080.20		0.026 0.037	2.7 6.5	2.680 2.671		0.022 0.039	2.9 6.9	2.683 2.673									
60	5080.20		0.037	5.7	2.719		0.039	6.2	2.724	0.005	0.011	6.5	0.001	0.002	5.8	1.67E+16	174 75	
61	5080.81		0.026	6.0	2.733		0.034	6.5	2.742	0.000	0.011	0.0	0.001	0.002	0.0	1.07 = 1.10	174.70	
62	5081.11		0.028	6.4	2.684		0.032	7.0	2.690									
63	5081.42		0.035	6.9	2.694		0.034	7.3	2.703	0.013	0.017	7.6	0.001	0.003	7.0	4.65E+15	148.05	
64	5082.10		0.035	7.2	2.703		0.040	7.3	2.706									
65	5082.41		0.033	7.2	2.713		0.020	7.6	2.718									
66	5082.74		0.048	8.0	2.732		0.051	7.8	2.734	0.019	0.024	8.4	0.002	0.005	7.4	2.47E+15	136.42	
67	5083.04		0.031	5.4	2.726		0.039	5.8	2.727									
68	5083.58		0.019	1.4	2.668		0.059	2.4	2.699									
69	5083.89		0.082	7.6	2.657		0.076	7.8	2.664	0.028	0.037	8.2	0.004	0.009	7.4	5.62E+14	112.64	
70	5084.19		0.058	7.4	2.725		0.067	7.6	2.730									
71	5084.48		0.281	7.1	2.717		0.272	7.4	2.723	0.007	0.000	7.0	0.000	0.000	7.0	0.005.44	400.00	
72 72	5084.80		0.078	7.8	2.667		0.070	8.0	2.674	0.027	0.036	7.8	0.003	0.008	7.2	9.36E+14	120.28	
73 74	5085.10 5085.41		0.042 0.052	6.8 6.9	2.718 2.638		0.042 0.049	7.0 7.1	2.722 2.737									
7 4 75	5085.71		0.032	1.2	2.703		0.049	1.4	2.737									
76	5086.01		0.019	10.2	2.659		0.132	10.2	2.662	0.060	0.081	10.5	0.032	0.041	9.9	1.62E+13	20.05	
77	5086.61		0.304	12.8	2.763		0.257	12.7	2.762	0.163	0.281	12.8	0.083	0.108	12.1	2.58E+12		
78	5086.91		0.370	12.9	2.762		0.368	12.8	2.759	0.197	0.302	12.9	0.111	0.187	12.2	3.73E+12		
79	5087.19		0.498	12.4	2.728		0.495	12.6	2.731	0.299	0.434	12.9	0.171	0.275	12.1	6.17E+11		
80	5087.49		0.274	9.5	2.721		0.253	9.5	2.719	0.140	0.242	9.8	0.070	0.092	9.1	1.01E+12		
81	5087.80		0.477	10.7	2.693		0.513	11.3	2.691									
82	5088.11		0.318	10.6	2.678		0.299	10.5	2.674	0.179	0.261	10.5	0.076	0.099	9.7	3.75E+12		
83	5088.40		0.311	11.1	2.727		0.314	11.2	2.725	0.185	0.279	11.4	0.090	0.119	10.7	3.01E+12	22.18	
84	5088.70		0.016	3.0	2.696		0.033	3.8	2.705									
85	5088.98		0.078	4.0	2.680		0.031	4.7	2.685									
86	5089.60		0.032	3.1	2.692		0.029	3.2	2.693	0.004	0.009	3.8	0.001	0.003	3.1	7.58E+16	157.59	
87	5089.91		0.071	7.3	2.755		0.116	7.3	2.756									
88	5090.51		0.004	5.1	2.788		0.032	5.6	2.795	0.014	0.010	F. 6	0.001	0.002	F 2	6 205 . 15	152.05	
89 90	5090.81 5091.09		0.047 0.053	5.1 4.9	2.652 2.653		0.058 0.058	5.1 5.0	2.659 2.654	0.014	0.019	5.6	0.001	0.003	5.2	6.28E+15	155.65	
91	5091.09		0.039	4.9	2.654		0.046	4.6	2.660									
92	5091.85		0.039	1.5	2.651		0.048	2.5	2.657	0.013	0.020	2.9	0.001	0.002	1.9	1.51E+16	172 18	
93	5092.15		0.116	0.6	2.704		0.843	2.1	2.728	0.010	0.020	2.0	0.001	0.002	1.0			
94	5092.45		0.422	0.5	2.659		-	-	-									Fractured
95	5092.79		-	-	2.686		-	-	-	-	-	-	-	-	-	-	-	Badly fractured
96	5093.08	<	<0.001	1.6	2.682		-	2.1	2.686									Fractured
97	5093.53		0.019	1.2	2.652		0.013	1.7	2.653									
98	5093.84		0.053	1.3	2.647		0.082	2.0	2.654									
99	5094.17		0.056	3.5	2.657		0.110	3.9	2.660									
100	5094.44		<0.001	4.8	2.666		-	4.7	2.665									Fractured
101	5095.03		0.210	2.5	2.655		0.228	2.5	2.655									
102	5095.38		-	0.6	2.684		-	-	-									Fractured
103	5095.82	<	<0.001	2.0	2.636		-	2.7	2.638									Fractured
RP-09079							CORELARO	RATORIES AUSTRALIA	0040									Pad

POROSITY, PERMEABILITY and GRAIN DENSITY

		Coo	Solvent and Hu	umidity Dried		Warm	Solvent and Cor	nnvection Ove	n		CMS 30	00			CMS 300			
SAMPLE	SAMPLE	CONFINING S	TRESS 400psi	Hg	GRAIN	CONFINING S	STRESS 400psi	Hg	GRAIN	CONFIN	IING STRE	ESS 800psi.		CONFIN	ING STRESS	5600psi.		COMMENTS
NUMBER	DEPTH	Steady - State	PERMEABILITY	1 - 1	DENSITY	Steady - State	PERMEABILITY	_	DENSITY	PERME	ABILITY	POROSITY	PERME	ABILITY	POROSITY	BETA	b(N2)	1
		Kinf	Kair	POROSITY		Kinf	Kair	POROSITY		Kinf	Kair		Kinf	Kair				
	(m)	(md)	(md)	(%)	(g/cc)	(md)	(md)	(%)	(g/cc)	(md)	(md)	(%)	(md)	(md)	(%)	(ft-1)	(psi)	
104	5096.08		0.013	1.8	2.919		0.008	1.9	2.922									
Core 3																		
105	5097.53		0.012	2.3	2.725		0.012	2.4	2.730	0.003	0.006	2.6	< 0.001	< 0.001	-	-	-	
106	5098.18		0.075	1.9	2.712		0.120	2.2	2.718									
107	5098.48		0.041	0.3	2.645		0.133	2.0	2.670									
108	5098.81		0.010	3.0	3.064		0.008	3.2	3.071	0.001	0.002	4.5	< 0.001	< 0.001	-	-	-	
109	5099.11		0.003	3.9	2.907		0.005	4.4	2.920									
110	5099.54		0.029	3.8	2.803		0.025	4.0	2.804									
111	5099.87		0.042	1.2	2.662		0.028	2.1	2.675	0.005	0.012	2.9	< 0.001	< 0.001	-	-	-	
112	5100.30		0.305	4.8	2.714		0.305	4.8	2.718									
113	5100.61		0.098	3.7	2.645		0.105	4.1	2.648									
114	5101.30		0.099	0.4	2.693		0.042	1.8	2.714	0.035	0.041	2.8	<0.001	<0.001	-	-	-	
115	5101.61		0.015	0.3	2.668		0.024	1.9	2.692									
116	5101.89		-	0.7	2.859		-	-	-									Fractured
117	5102.49		-	1.0	2.732		-	2.2	2.748	-	-	-	-	-	-	-	-	Fractured
118	5102.78		-	1.0	2.641		-	-	-									Fractured
119	5103.09		-	0.6	2.619		-	-	-									Fractured
120	5103.38		0.940	1.0	2.620		-	-	-	-	-	-	-	-	-	-	-	Fractured
121	5104.30		0.135	2.9	2.648		0.117	3.3	2.651									
122	5104.61		0.004	1.9	2.943		0.014	2.2	2.947									
123	5104.90		0.008	3.5	3.042		0.008	4.7	3.054	0.001	0.003	4.5	<0.001	<0.001	-	-	-	
124	5105.21		0.011	2.1	3.151		0.019	2.9	3.159									
125	5105.49		0.014	0.9	2.648		0.010	1.4	2.654									
126	5105.85		0.019	0.6	2.660		0.030	2.2	2.679	0.006	0.012	2.4	<0.001	<0.001	-	-	-	
127	5106.25		0.036	1.2	2.649		0.034	1.7	2.657									
128	5106.50		0.007	0.3	2.644		0.004	0.6	2.652									
129	5107.09		0.014	0.8	2.657		0.008	1.3	2.666									
130	5107.50		0.007	0.8	2.674		0.006	1.1	2.694	0.001	0.003	1.7	<0.001	0.001	0.7	2.68E+17	249.36	
131	5107.83		0.199	0.6	2.643		0.402	2.9	2.684									
132	5108.15		1.78	0.9	2.742		-	2.4	2.763									Fractured
133	5108.71		0.006	0.1	2.635		0.008	1.6	2.655	0.001	0.002	3.0	<0.001	<0.001	-	-	-	
134	5109.06		-	0.8	2.717		-	-	-									Fractured
135	5109.35		0.373	0.6	2.639		-	-	-									Fractured
136	5109.76		5.000	0.9	2.654		-	2.1	2.673									Fractured
137	5110.22		0.016	0.3	3.489		0.019	1.2	3.514									Fractured
138	5110.57		0.019	1.2	3.225		-	-	-	0.000	0.000	0.5	0.001	0.004	4.0	4 075 45		Fractured
139	5110.97		0.012	1.1	2.664		0.013	1.8	2.673	0.002	0.006	2.5	<0.001	0.001	1.6	1.27E+17	227.03	
140	5111.21		0.001	0.2	3.029		0.004	1.9	3.067									For at 11 1
141	5111.63		0.636	4.2	2.636		-	-	-									Fractured
142	5111.95		0.401	0.3	2.619		-	2.6	2.643									Fractured
143	5112.22		0.792	0.6	2.810		- 0.024	2.2	2.834	0.000	0.044	0.0	0.004	0.000	4 5	0.445 : 40	100.04	Fractured
144	5112.51		0.041	1.4	2.677		0.024	1.9	2.702	0.006	0.014	2.6	0.001	0.002	1.5	2.14E+16	180.21	
145	5112.80 5112.05		0.002	0.7	3.073		0.022	3.1	3.121									
146 147	5113.05 5113.53		0.018	0.1	2.616		0.014	2.6	2.684	0.077	0.400	2.4	0.004	0.000	4.0	7 005 .45	150 47	
147	5113.52		<0.001	0.4	2.842		0.057	3.3	2.900	0.077	0.123	3.4	0.001	0.003	1.8	7.83E+15	158.17	Fronture d
148	5114.13		-	0.8	2.790		-	-	- 2.752									Fractured
149	5114.47		0.006	0.5	2.734		0.003	1.4	2.752									
150	5114.73		0.007	0.9	2.874		0.005	1.6	2.885									Frank
151	5115.03		-	0.5	2.720		-	-	-	0.000	0.007	4.4	0.004	0.000	0.0	0.045 40	404.04	Fractured
152	5115.41		0.016	3.5	2.682		0.014	3.6	2.681	0.003	0.007	4.1	0.001	0.002	3.2	2.31E+16	181.84	
153	5115.77		0.013	2.0	2.678		0.013	2.2	2.680									
154	5116.34		0.010	1.2	2.668		0.009	1.9	2.677									

POROSITY, PERMEABILITY and GRAIN DENSITY

		Cool	Solvent and Hu	ımidity Dried		Warm	Solvent and Cor	nvection Ove	n		CMS 30	0			CMS 300			
SAMPLE	SAMPLE	CONFINING S	TRESS 400psi	Hg	GRAIN	CONFINING S	STRESS 400psi	Hg	GRAIN	CONFIN	ING STRE	SS 800psi.		CONFINI	NG STRESS	5600psi.		COMMENTS
NUMBER	DEPTH	Steady - State I	PERMEABILITY	Bulk Volume	DENSITY	Steady - State	PERMEABILITY	Bulk Volume	DENSITY	PERME	ABILITY	POROSITY	PERME	ABILITY	POROSITY	BETA	b(N2)	
		Kinf	Kair	POROSITY		Kinf	Kair	POROSITY		Kinf	Kair		Kinf	Kair				
	(m)	(md)	(md)	(%)	(g/cc)	(md)	(md)	(%)	(g/cc)	(md)	(md)	(%)	(md)	(md)	(%)	(ft-1)	(psi)	
155	5116.61		0.018	1.2	2.656		0.020	1.9	2.671	0.004	0.009	2.1	<0.001	0.001	1.5	2.80E+16	186.59	
156	5116.94		0.002	0.6	2.690		0.005	2.1	2.707	< 0.001	<0.001	-	-	-	-	-	-	
157	5117.24		0.069	0.1	2.665		0.013	1.6	2.677									
158	5117.55		0.058	0.9	2.675		0.027	0.9	2.676	0.017	0.024	1.5	0.004	0.009	0.9	6.19E+14	113.70	
159	5117.92		-	-	2.724		-	-	-									Badly fractured
160	5118.29		0.043	0.3	2.654		0.066	2.3	2.678									
161	5118.57		-	3.3	2.869		-	-	-									Fractured
162	5118.88		0.592	0.2	2.727		1.50	3.8	2.791									Fractured
163	5119.30		-	1.5	2.868		-	-	-									Fractured
164	5119.55		-	-	2.673		-	-	-									Badly fractured
165	5119.91		-	0.6	2.752		-	-	-									Fractured
166	5120.08		0.012	0.6	2.740		0.030	8.0	2.743	0.001	0.003	0.9	<0.01	<0.001	-	-	-	
167	5120.52		0.009	1.1	2.677		0.009	1.9	2.683									
168	5121.21		0.007	0.9	2.653		0.008	1.3	2.660									
169	5121.58		0.004	0.2	2.907		0.004	0.2	2.900	<0.001	<0.001	-	-	-	-	-	-	
170	5121.82		0.083	1.5	2.675		0.118	1.7	2.679									Hairline fract
Vertical sam	nples																	
1V	5062.13		0.008	1.8	2.669		0.026	2.9	2.684									
2V	5067.22		0.022	4.5	2.692		0.033	5.2	2.701									
3V	5072.13		0.012	2.0	2.723		0.020	3.2	2.742									
4V	5077.42		0.005	2.2	2.937		0.009	2.7	2.953									
5V	5082.97		0.055	4.3	2.693		0.067	4.5	2.698									
6V	5097.83		0.007	3.8	3.000		0.012	4.4	3.010									
7V	5108.09		0.003	0.6	2.634		-	-	-									
8V	5114.65		0.002	0.9	2.723		0.016	1.8	2.739									



SAMPLE	DEPTH	PERME	ABILITY	COMMENTS	SAMPLE	DEPTH	PERME	ABILITY	COMMENTS
POINT	(m)	Ka	Kinf		POINT	(m)	Ka	Kinf	
		(md)	(md)				(md)	(md)	
		Core	2		47	5065.94	0.068	0.029	· L
1	5061.35	0.135	0.065		48	5066.05	0.043	0.016	
2	5061.45	0.168	0.087		49	5066.16	-	-	Poor seal
3	5061.55	0.215	0.116		50	5066.16	0.424	0.262	
4	5061.65	0.043	0.015		51	5066.25	0.106	0.050	
5	5061.75	0.053	0.020		52	5066.34	0.067	0.028	
6	5061.84	0.044	0.016		53	5066.43	0.149	0.076	
7	5061.95	0.144	0.072		54	5066.54	0.092	0.042	
8	5062.03	0.232	0.128		55	5066.62	0.049	0.019	
9	5062.12	0.298	0.172		56	5066.73	0.136	0.068	
10	5062.23	-	-	Poor seal	57	5066.83	0.126	0.062	
11	5062.22	-	-	Poor seal	58	5066.94	0.131	0.065	
12	5062.32	0.083	0.036		59	5067.05	0.061	0.024	
13	5062.42	0.193	0.102		60	5067.16	0.049	0.018	
14	5062.51	0.254	0.142		61	5067.25	0.102	0.047	
15	5062.62	0.104	0.048		62	5067.35	0.061	0.025	
16	5062.69	0.179	0.094		63	5067.43	0.010	0.002	
17	5062.81	0.090	0.040		64	5067.54	0.020	0.006	
18	5062.90	0.112	0.052		65	5067.70	0.059	0.024	
19	5063.10	0.142	0.070		66	5067.79	0.035	0.012	
20	5063.20	0.141	0.070		67	5067.87	0.027	0.008	
21	5063.30	0.102	0.048		68	5067.97	0.035	0.012	
22	5063.37	0.078	0.034		69	5068.05	0.065	0.027	
23	5063.50	0.277	0.159		70	5068.16	0.087	0.038	
24	5063.60	0.094	0.043		71 	5068.25	0.075	0.032	
25	5063.72	0.357	0.215		72	5068.34	0.074	0.031	
26	5063.80	0.087	0.039		73	5068.45	0.061	0.024	
27	5063.90	0.123	0.060		74 75	5068.54	0.094	0.043	
28	5064.03	0.183	0.097		75 70	5068.63	0.006	0.001	Б
29	5064.13	0.218	0.120		76	5068.75	-	-	Poor seal
30	5064.22	0.068	0.029		77	5068.79	0.016	0.004	
31	5064.33	0.121	0.059		78 70	5068.88	0.031	0.010	
32	5064.43	0.273	0.156		79	5068.95	0.104	0.048	
33	5064.55	0.081	0.036		80	5069.05	0.037	0.013	
34	5064.65 5064.74	0.056	0.022		81 92	5069.15	0.032	0.010	
35		0.098	0.045		82	5069.24	0.046	0.017	
36	5064.85	0.059	0.024		83	5069.35	0.042	0.015	
37	5064.95	0.235	0.131 0.109		84 95	5069.47 5069.55	0.089	0.039 0.033	
38 39	5065.06	0.202			85 86		0.078	0.033	
39 40	5065.18 5065.26	0.074 0.069	0.032 0.029		87	5069.65 5069.74	0.045 0.117	0.017	
41	5065.26	0.058	0.029		88	5069.74	0.117	0.036	
42	5065.43	0.036	0.023		89	5070.02	0.065	0.037	
42 43	5065.54	0.172	0.090		90	5070.02	0.045	0.017	
43 44	5065.65	0.057	0.039		90 91	5070.12	0.071	0.030	
44 45	5065.74	0.059	0.024		91 92	5070.24	0.065	0.026	
45 46	5065.74	0.090	0.040		92 93	5070.34	0.056	0.024	
40	5005.65	0.000	0.024		33	5070.43	0.050	0.022	

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SAMPLE	DEPTH	PERME	ABILITY	COMMENTS	SAMPLE	DEPTH	PERME	ABILITY	COMMENTS
POINT	(m)	Ka	Kinf		POINT	(m)	Ka	Kinf	
		(md)	(md)				(md)	(md)	
94	5070.54	-	_	Poor seal	141	5075.35	0.075	0.032	
95	5070.65	-	_	Poor seal	142	5075.45	0.163	0.083	
96	5070.77	-	_	Poor seal	143	5075.55	0.154	0.078	
97	5070.77	0.083	0.036		144	5075.67	0.255	0.143	
98	5070.87	0.047	0.017		145	5075.78	0.154	0.078	
99	5070.96	0.035	0.012		146	5075.86	0.152	0.077	
100	5071.05	0.111	0.052		147	5075.94	0.295	0.170	
101	5071.15	0.025	0.007		148	5076.02	0.261	0.147	
102	5071.27	0.033	0.011		149	5076.12	0.068	0.028	
103	5071.36	0.016	0.004		150	5076.20	0.028	0.009	
104	5071.41	0.121	0.058		151	5076.34	0.120	0.057	
105	5071.53	0.031	0.010		152	5076.44	0.194	0.103	
106	5071.66	0.019	0.005		153	5076.52	0.197	0.105	
107	5071.76	0.032	0.011		154	5076.64	0.106	0.049	
108	5071.86	0.014	0.003		155	5076.74	0.099	0.045	
109	5071.95	0.023	0.007		156	5076.84	0.052	0.020	
110	5072.03	0.069	0.029		157	5076.95	0.055	0.022	
111	5072.21	0.188	0.100		158	5077.05	0.086	0.038	
112	5072.30	0.071	0.030		159	5077.15	0.051	0.019	
113	5072.39	0.065	0.026		160	5077.27	0.066	0.027	
114	5072.48	0.044	0.016		161	5077.35	0.147	0.074	
115	5072.57	0.056	0.022		162	5077.53	0.049	0.018	
116	5072.75	0.096	0.043		163	5077.65	0.137	0.068	
117	5072.85	0.062	0.025		164	5077.74	0.091	0.041	
118	5072.95	0.073	0.031		165	5077.89	0.112	0.053	
119	5073.03	0.462	0.287		166	5078.05	0.065	0.027	
120	5073.15	0.097	0.044		167	5078.15	0.049	0.018	
121	5073.25	0.052	0.020		168	5078.24	0.187	0.098	
122	5073.35	0.065	0.026		169	5078.32	0.106	0.049	
123	5073.45	0.083	0.036		170	5078.40	0.272	0.154	
124	5073.56	0.151	0.076		171	5078.50	0.392	0.237	
125	5073.65	0.082	0.036		172	5078.61	0.134	0.065	
126	5073.75	0.071	0.030		173	5078.77	0.506	0.319	
127	5073.86	0.111	0.052		174	5078.85	0.178	0.093	
128	5073.95	0.060	0.024		175	5078.95	0.269	0.152	
129	5074.05	0.185	0.097		176	5079.06	0.331	0.194	
130	5074.12	0.075	0.032		177	5079.18	0.216	0.117	
131	5074.25	0.123	0.059		178	5079.28	0.248	0.138	
132	5074.35	0.208	0.112		179	5079.37	0.194	0.103	
133	5074.47	0.280	0.159		180	5079.46	0.415	0.253	
134	5074.56	0.089	0.039		181	5079.57	0.125	0.060	
135	5074.65	0.171	0.089		182	5079.69	0.110	0.051	
136	5074.72	0.199	0.106		183	5079.79	0.134	0.065	
137	5075.05	0.048	0.018		184	5079.79	0.204	0.109	
138	5075.15	0.068	0.028		185	5079.90	0.020	0.006	
139	5075.25	-	-	Poor seal	186	5079.98	0.234	0.129	
140	5075.26	0.082	0.036		187	5080.07	0.247	0.137	

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SAMPLE	DEPTH	PERME	ABILITY	COMMENTS	SAMPLE	DEPTH	PERME	ABILITY	COMMENTS
POINT	(m)	Ka	Kinf		POINT	(m)	Ka	Kinf	
		(md)	(md)				(md)	(md)	
188	5080.17	0.180	0.094	1	15	5084.44	0.494	0.313	Fast track
189	5080.28	0.094	0.042		16	5084.55	1.11	0.779	Fast track
190	5080.36	0.100	0.046		17	5084.59	0.370	0.223	Fast track
191	5080.47	0.195	0.104		18	5084.64	0.083	0.036	Fast track
192	5080.56	0.362	0.215		19	5084.68	0.150	0.076	Fast track
193	5080.67	0.201	0.108		20	5084.73	0.596	0.386	Fast track
194	5080.77	0.095	0.043		21	5084.78	0.500	0.317	Fast track
195	5080.86	0.085	0.037		22	5084.86	0.333	0.197	Fast track
196	5080.96	0.091	0.041		23	5084.91	0.558	0.358	Fast track
197	5081.04	0.139	0.069		24	5084.96	0.480	0.302	Fast track
198	5081.15	0.117	0.056		25	5085.01	0.175	0.092	Fast track
199	5081.25	0.259	0.145		26	5085.05	0.298	0.173	Fast track
200	5081.36	0.212	0.114		27	5085.14	1.01	0.703	Fast track
201	5081.45	0.221	0.120		28	5085.18	0.815	0.553	Fast track
202	5081.54	0.389	0.234		29	5085.23	0.321	0.189	Fast track
203	5081.65	0.087	0.038		30	5085.28	0.149	0.076	Fast track
204	5081.75	0.271	0.153		31	5085.37	0.853	0.579	Fast track
205	5081.85	0.298	0.171		32	5085.46	0.357	0.214	Fast track
206	5081.95	0.198	0.106		33	5085.56	0.033	0.011	Fast track
207	5082.05	0.278	0.158		34	5085.65	0.039	0.014	Fast track
208	5082.19	0.144	0.072		35	5085.79	0.185	0.098	Fast track
209	5082.30	0.173	0.090		36	5085.87	0.624	0.407	Fast track
210	5082.43	0.178	0.093		37	5085.98	0.702	0.466	Fast track
211	5082.49	0.108	0.050		38	5086.09	0.925	0.635	Fast track
212	5082.59	0.323	0.189		39	5086.20	0.850	0.577	Fast track
213	5082.68	0.093	0.042		40	5086.32	0.978	0.676	Fast track
214	5082.78	0.311	0.180		41	5086.40	1.03	0.716	Fast track
215	5082.90	0.114	0.054		42	5086.47	1.34	0.960	Fast track
216	5083.06	0.220	0.120		43	5086.52	0.700	0.465	Fast track
217	5083.17	0.103	0.048		44	5086.64	0.741	0.496	Fast track
218	5083.26	0.197	0.105		45	5086.72	1.15	0.810	Fast track
219	5083.37	0.034	0.011		46	5086.82	0.907	0.621	Fast track
220	5083.45	0.222	0.121		47	5086.93	1.03	0.718	Fast track
1	5083.64	0.069	0.028	Fast track	48	5087.01	1.32	0.945	Fast track
2	5083.79	0.890	0.609	Fast track	49	5087.12	0.827	0.559	Fast track
3	5083.82	1.02	0.708	Fast track	50	5087.23	1.05	0.734	Fast track
4	5083.93	0.300	0.175	Fast track	51	5087.31	1.05	0.733	Fast track
5	5083.97	1.02	0.712	Fast track	52	5087.40	1.48	1.060	Fast track
6	5084.02	0.903	0.618	Fast track	53	5087.44	1.12	0.784	Fast track
7	5084.06	-	-	Poor seal	54	5087.52	0.346	0.206	Fast track
8	5084.06	0.162	0.084	Fast track	55	5087.62	0.567	0.364	Fast track
9	5084.12	0.213	0.117	Fast track	56	5087.72	0.871	0.593	Fast track
10	5084.15	0.428	0.265	Fast track	57	5087.83	1.01	0.700	Fast track
11	5084.21	0.942	0.649	Fast track	58	5087.92	0.648	0.425	Fast track
12	5084.27	0.149	0.076	Fast track	59	5088.05	0.290	0.168	Fast track
13	5084.31	0.275	0.157	Fast track	60	5088.16	0.632	0.413	Fast track
14	5084.39	0.231	0.128	Fast track	61	5088.25	0.434	0.269	Fast track

SAMPLE	DEPTH	PERME	ABILITY	COMMENTS	SAMPLE	DEPTH	PERME	ABILITY	COMMENTS
POINT	(m)	Ka	Kinf		POINT	(m)	Ka	Kinf	
		(md)	(md)				(md)	(md)	
62	5088.32	0.720	0.480	Fast track	242	5093.03	0.141	0.070	
63	5088.44	0.734	0.490	Fast track	243	5093.18	0.092	0.041	
64	5088.52	0.114	0.054	Fast track	244	5093.28	0.051	0.020	
65	5088.68	0.820	0.554	Fast track	245	5093.39	-	-	Poor seal
66	5088.75	0.881	0.601	Fast track	246	5093.48	-	-	Poor seal
67	5088.85	1.30	0.927	Fast track	247	5093.57	0.039	0.014	
68	5089.03	1.09	0.761	Fast track	248	5093.64	0.063	0.026	
69	5089.14	1.45	1.05	Fast track	249	5093.78	0.059	0.024	
70	5089.23	0.448	0.279	Fast track	250	5093.91	0.049	0.019	
71	5089.32	0.110	0.052	Fast track	251	5093.98	0.113	0.054	
72	5089.42	0.261	0.148	Fast track	252	5094.05	0.175	0.092	
73	5089.52	0.089	0.040	Fast track	253	5094.12	0.180	0.094	
74	5089.66	0.433	0.268	Fast track	254	5094.22	0.077	0.033	
75	5089.75	0.130	0.064	Fast track	255	5094.33	0.107	0.050	
76	5089.85	0.225	0.124	Fast track	256	5094.41	-	-	Poor seal
77	5089.95	0.485	0.306	Fast track	257	5094.43	0.492	0.310	
78	5090.05	0.337	0.200	Fast track	258	5094.55	0.226	0.124	
79	5090.14	0.506	0.321	Fast track	259	5094.65	0.033	0.011	
80	5090.28	0.233	0.130	Fast track	260	5094.65	0.044	0.016	
81	5090.38	0.737	0.493	Fast track	261	5094.72	0.273	0.155	
82	5090.47	0.942	0.647	Fast track	262	5094.83	0.240	0.133	
83	5090.56	0.843	0.571	Fast track	263	5094.94	0.132	0.065	
84	5090.66	0.940	0.646	Fast track	264	5095.02	0.101	0.046	
85	5090.76	0.910	0.623	Fast track	265	5095.16	0.179	0.094	
86	5090.89	0.114	0.055	Fast track	266	5095.27	0.119	0.057	
87	5090.97	0.436	0.270	Fast track	267	5095.36	0.040	0.014	
221	5091.07	0.141	0.069		268	5095.45	0.089	0.040	
222	5091.17	0.123	0.060		269	5095.53	-	-	Poor seal
223	5091.24	0.071	0.030		270	5095.58	0.098	0.045	
224	5091.34	0.054	0.021		271	5095.90	0.157	0.080	
225	5091.42	0.143	0.072		272	5095.90	0.061	0.025	
226	5091.52	0.052	0.020		273	5096.00	0.007	0.001	
227	5091.64	0.046	0.017		274	5096.12	0.246	0.138	
228	5091.72	0.046	0.017		275	5096.23	0.047	0.018	
229	5091.80	0.136	0.068		276	5096.31	0.049	0.018	
230	5091.90	0.119	0.057		277	5096.40	0.056	0.022	
231	5092.02	0.100	0.046		278	5096.50	0.088	0.039	
232	5092.11	0.080	0.035		279	5096.59	0.061	0.024	
233	5092.22	0.401	0.245		280	5096.69	0.077	0.033	
234	5092.31	0.012	0.003		281	5096.79	0.061	0.024	
235	5092.39	-	-	Poor seal			Core		
236	5092.39	_	-	Poor seal	282	5097.56	0.077	0.033	
237	5092.52	0.121	0.058		283	5097.65	0.035	0.012	
238	5092.63	0.158	0.081		284	5097.75	0.048	0.018	
239	5092.73	0.872	0.593		285	5097.85	0.029	0.009	_
240	5092.84	0.223	0.122		286	5098.00	-	-	Poor seal
241	5092.93	0.124	0.060		287	5098.00	0.210	0.114	

SAMPLE	DEPTH	DEDME	ABILITY	COMMENTS	SAMPLE	DEPTH	DEDME	ABILITY	COMMENTS
POINT		Ka	Kinf	COMMENTS	POINT		Ka	Kinf	COMMENTS
POINT	(m)				POINT	(m)			
		(md)	(md)				(md)	(md)	
288	5098.10	0.146	0.073		335	5102.30	-	-	Poor seal
289	5098.17	0.600	0.388		336	5102.31	-	-	Poor seal
290	5098.25	0.076	0.032		337	5102.81	0.104	0.048	
291	5098.35	0.097	0.044		338	5102.93	0.091	0.041	
292	5098.43	0.116	0.055		339	5103.06	-	-	Poor seal
293	5098.53	0.044	0.016		340	5103.06	-	-	Poor seal
294	5098.63	0.043	0.016		341	5103.17	-	-	Poor seal
295	5098.72	0.721	0.479		342	5103.28	0.093	0.042	
296	5098.88	0.047	0.017		343	5103.34	0.212	0.115	
297	5098.98	0.108	0.051		344	5103.46	0.273	0.155	
298	5099.05	0.158	0.081		345	5103.78	0.115	0.055	
299	5099.15	0.333	0.196		346	5103.88	-	-	Poor seal
300	5099.30	0.188	0.099		347	5103.90	0.985	0.679	
301	5099.39	0.187	0.099		348	5104.04	0.029	0.009	
302	5099.49	0.275	0.157		349	5104.14	0.003	0.000	
303	5099.57	0.287	0.165		350	5104.23	0.071	0.029	
304	5099.67	0.154	0.078		351	5104.34	0.113	0.053	
305	5099.80	0.521	0.331		352	5104.44	0.016	0.004	
306	5099.89	0.306	0.177		353	5104.53	0.043	0.016	
307	5099.98	0.113	0.053		354	5104.64	0.088	0.039	
308	5100.03	0.138	0.068	Deersel	355	5104.72	0.048	0.018	
309	5100.13	-	-	Poor seal	356	5104.83	0.040	0.014	
310	5100.13	- 0.400	-	Poor seal	357	5104.93	0.004	0.001	
311	5100.21	0.138	0.069		358	5105.03	0.020	0.005	
312	5100.33	0.835	0.566		359	5105.15	0.037	0.013	
313 314	5100.41 5100.50	0.148 0.138	0.075 0.069		360 361	5105.24 5105.34	0.111 0.010	0.052 0.002	
314	5100.50	0.136			362	5105.34	0.010	0.002	
316	5100.56	0.422	0.259 0.242		362 363	5105.42	0.034	0.012	
	5100.08						-	-	Eracturo
317 318	5100.77	0.152 -	0.077 -	Poor sool	364 365	5105.61 5105.66	- 0.045	- 0.017	Fracture
319	5100.86	-	-	Poor seal Poor seal	366	5105.00	0.045	0.017	
320	5100.86	0.060	0.024	ruui seai	367	5105.73	0.045	0.033	
321	5101.17	3.46	2.69		368	5105.61	0.043	0.017	
322	5101.26	2.42	1.83		369	5105.93	0.023	0.007	
323	5101.20	0.065	0.026		370	5106.01	0.373	0.016	
324	5101.37	0.138	0.020		371	5106.12	0.573	0.353	
325	5101.56	0.138	0.068		371	5106.29	0.002	<0.001	
326	5101.66	-	-	Poor seal	372	5106.29	0.002	0.001	
327	5101.68	0.204	0.110	1 001 3041	374	5106.45	0.076	0.033	
328	5101.08	0.204	0.110		374	5106.43	0.076	0.066	
329	5101.70	0.132	0.043		376	5106.63	0.033	0.000	
330	5101.07	0.034	0.052		377	5106.03	0.003	<0.001	
331	5101.93	-	-	Poor seal	378	5106.72	-	-	Fracture
332	5102.03	0.090	0.041	. 55. 55ai	379	5106.85	_	-	Fracture
333	5102.04	0.129	0.063		380	5106.96	_	-	Fracture
334	5102.20	1.46	1.06		381	5107.01	0.021	0.006	. 1401470
00 -1	0102.20	1.70	1.00		301	0101.01	0.021	0.000	

0.4.455; =	DEET:	DED.:-	A DII 1777	001115	04555	DEDT:	DED.:-	ADII :=\;	001115155
SAMPLE	DEPTH		ABILITY	COMMENTS	SAMPLE	DEPTH		ABILITY	COMMENTS
POINT	(m)	Ka	Kinf		POINT	(m)	Ka	Kinf	
		(md)	(md)				(md)	(md)	
382	5107.12	0.023	0.007		429	5111.80	-	-	Poor seal
383	5107.29	0.027	0.008		430	5111.91	0.002	<0.001	
384	5107.37	0.001	< 0.001		431	5112.04	0.010	0.002	
385	5107.44	<0.001	<0.001		432	5112.15	0.404	0.242	
386	5107.54	0.034	0.011		433	5112.31	0.111	0.053	
387	5107.66	0.043	0.015		434	5112.38	0.213	0.116	
388	5107.75	0.027	0.008		435	5112.43	0.149	0.076	
389	5107.86	0.378	0.226		436	5112.55	0.015	0.004	
390	5107.96	0.039	0.014		437	5112.65	0.537	0.343	
391	5108.02	-	-	Poor seal	438	5112.75	0.015	0.004	
392	5108.06	0.019	0.005		439	5112.83	0.123	0.059	
393	5108.21	6.55	5.32	Poor seal	440	5113.02	0.046	0.017	
394	5108.21	5.58	4.48	Poor seal	441	5113.10	0.018	0.005	
395	5108.48	0.022	0.006		442	5113.20	0.135	0.067	
396	5108.63	-	-	Poor seal	443	5113.30	0.030	0.010	
397	5108.69	0.457	0.284		444	5113.39	0.039	0.013	
398	5108.77	0.019	0.005		445	5113.56	0.010	0.002	
399	5108.90	-	-	Poor seal	446	5113.66	0.086	0.038	
400	5108.96	-	-	Poor seal	447	5113.74	0.059	0.024	
401	5109.03	-	-	Poor seal	448	5113.86	0.035	0.012	
402	5109.12	-	-	Poor seal	449	5113.86	0.048	0.018	
403	5109.17	-	-	Poor seal	450	5113.94	0.003	<0.001	
404	5109.29	< 0.001	< 0.001		451	5114.04	0.010	0.002	
405	5109.43	0.001	< 0.001		452	5114.21	0.063	0.026	
406	5109.52	0.001	< 0.001		453	5114.30	0.014	0.003	
407	5109.61	0.005	0.001		454	5114.39	0.056	0.022	
408	5109.69	0.142	0.071		455	5114.54	0.153	0.077	
409	5109.80	0.001	< 0.001		456	5114.64	0.083	0.036	
410	5109.90	0.056	0.022		457	5114.76	-	-	Poor seal
411	5109.99	0.461	0.287		458	5114.80	0.027	0.008	
412	5110.03	0.042	0.015		459	5114.91	0.001	<0.001	
413	5110.13	-	-	Poor seal	460	5114.98	0.009	0.002	
414	5110.25	0.052	0.020		461	5115.06	0.088	0.039	
415	5110.34	0.021	0.006		462	5115.36	0.625	0.406	
416	5110.40	0.059	0.024		463	5115.46	0.080	0.035	
417	5110.50	0.046	0.017		464	5115.57	0.069	0.029	
418	5110.59	0.016	0.004		465	5115.66	0.106	0.050	
419	5110.72	0.001	< 0.001		466	5115.78	0.117	0.056	
420	5110.86	0.009	0.002		467	5115.87	0.246	0.137	
421	5110.99	-	-	Poor seal	468	5115.96	0.260	0.147	
422	5111.19	-	-	Poor seal	469	5116.03	0.025	0.008	
423	5111.34	0.013	0.003		470	5116.11	0.002	<0.001	
424	5111.36	-	-	Poor seal	471	5116.18	0.034	0.011	
425	5111.47	<0.001	< 0.001		472	5116.31	0.186	0.099	
426	5111.61	-	-	Poor seal	473	5116.43	0.144	0.072	
427	5111.71	0.010	0.002		474	5116.56	0.187	0.099	
428	5111.80	-	-	Poor seal	475	5116.65	0.021	0.006	

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SAMPLE	DEPTH	PERME	ABILITY	COMMENTS	SAMPLE	DEPTH	PERME	ABILITY	COMMENTS
POINT	(m)	Ka	Kinf		POINT	(m)	Ka	Kinf	
		(md)	(md)				(md)	(md)	
476	5116.75	0.018	0.005		523	5121.30	0.021	0.006	
477	5116.84	0.005	0.001		524	5121.42	0.031	0.010	
478	5116.95	0.019	0.005		525	5121.51	0.015	0.004	
479	5117.07	0.185	0.098		526	5121.62	0.192	0.102	
480	5117.13	0.115	0.055		527	5121.72	0.125	0.061	
481	5117.18	0.932	0.637		528	5121.80	0.025	0.007	
482	5117.30	0.135	0.067		529	5121.87	0.053	0.020	
483	5117.38	0.008	0.002		530	5122.02	0.098	0.044	
484	5117.50	0.005	0.001		531	5122.12	0.037	0.013	
485	5117.61	0.082	0.036		532	5122.21	0.051	0.019	
486	5117.73	0.002	0.000		533	5122.30	0.448	0.277	
487	5117.70	0.008	0.001		534	5122.40	0.042	0.015	
488	5117.89	0.065	0.001		535	5122.47	0.042	0.013	
489	5117.03	-	-	Poor seal	536	5122.54	0.013	0.003	
490	5118.05	0.029	0.009	1 001 3641	330	3122.04	0.013	0.003	
491	5118.14	0.023	0.003						
492	5118.21	0.090	0.043						
492	5118.33	0.10 4 -	0.09 <i>1</i> -	Poor seal					
493 494	5118.34	0.345	0.204	FUUI Seai					
49 4 495	5118.50	0.343	0.204						
495 496	5118.62	U.232 -	0.120	Poor cool					
490 497			0.006	Poor seal					
	5118.67	0.021							
498 400	5118.76	0.030	0.010	Door oool					
499 500	5118.86	0.026	- 0.012	Poor seal					
500 501	5118.97	0.036	0.012						
501	5119.13	0.931	0.631	Door oool					
502	5119.32	- 0.010	- 0.000	Poor seal					
503	5119.41		0.002						
504	5119.50	0.038	0.013						
505	5119.68	0.313	0.182						
506	5119.76	0.422	0.259						
507	5119.82	0.018	0.005						
508	5119.99	0.658	0.430						
509	5120.05	8.47	7.00						
510	5120.06	0.101	0.046						
511	5120.16	0.109	0.051						
512	5120.27	0.019	0.005						
513	5120.34	0.006	0.001						
514	5120.46	0.444	0.274	Danner I					
515	5120.54	-	-	Poor seal					
516	5120.54	-	-	Poor seal					
517	5120.73	0.074	0.031						
518	5120.82	0.105	0.049						
519	5120.93	-	-	Poor seal					
520	5121.01	0.128	0.062						
521	5121.11	0.043	0.015						
522	5121.20	0.101	0.046						

POROSITY, PERMEABILITY, GRAIN DENSITY and RESIDUAL FLUID SATURATIONS

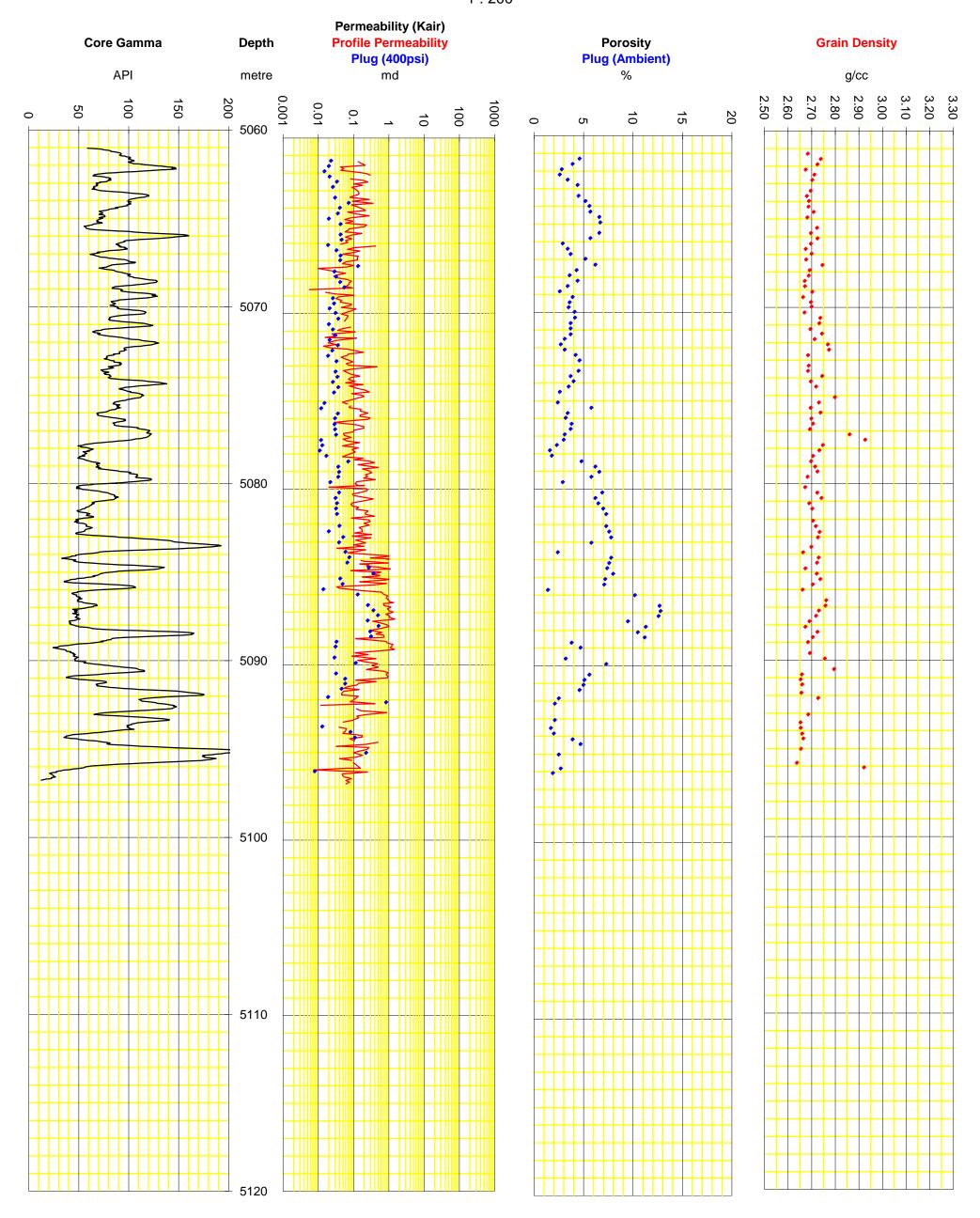
	Warm Solvent and Convection Oven Dried							
SAMPLE	SAMPLE	E CONFINING STRESS 400psi		Hg	GRAIN	Residual Fluid		COMMENTS
NUMBER	DEPTH			Bulk Volume	DENSITY	Satur		
		Kinf	Kair	POROSITY		Sw	So	
	(m)	(md)	(md)	(%)	(g/cc)	(%)	(%)	
100	5004.04		0.040	0.0	0.000	70.4	0.4	
1DS	5061.04		0.013	3.9	2.690	72.1	9.4	
2DS	5063.03		0.019	5.8	2.669	71.5	23.6	
3DS	5065.14		0.011	4.0	2.685	63.4	29.4	
4DS	5067.45		0.015	2.9	2.715	60.0	36.3	
5DS	5071.62		0.004	1.1	2.728	65.1	2.5	
6DS	5073.06		0.020	4.5	2.673	57.6	40.7	
7DS	5074.75		0.015	2.7	2.760	59.3	36.1	
8DS	5076.15		0.004	1.1	2.709	29.4	48.3	
9DS	5077.94		0.004	1.5	2.773	71.3	11.1	
10DS	5079.86		0.014	3.0	2.687	66.2	20.6	
11DS	5081.78		0.022	7.2	2.717	73.6	15.3	
12DS	5083.29		0.005	3.0	2.728	42.1	47.5	
13DS	5084.35		0.054	7.3	2.718	69.4	5.8	
14DS	5086.29		0.258	10.7	2.682	58.3	4.9	
15DS	5087.35		0.261	10.4	2.674	57.3	7.2	
16DS	5089.36		0.070	1.7	2.718	52.5	36.6	
17DS	5091.58		0.010	3.0	2.656	37.8	58.8	
18DS	5094.75		0.029	4.9	2.663	28.7	67.9	
19DS	5090.18		0.051	8.5	2.765	62.9	14.3	
20DS	5097.93		0.006	1.9	2.747	61.9	35.5	
21DS	5100.07		0.013	2.4	2.699	33.7	65.9	
22DS	5102.89		-	3.4	2.661	-	-	Fracture
23DS	5104.09		0.012	6.4	3.127	36.7	22.2	
24DS	5106.07		0.039	1.3	2.654	76.6	9.8	

POROSITY, PERMEABILITY, GRAIN DENSITY and RESIDUAL FLUID SATURATIONS

		Warm	Solvent and Conv					
SAMPLE	SAMPLE	CONFINING STRESS 400psi Steady - State PERMEABILITY		Hg GRAIN		Residual Fluid		COMMENTS
NUMBER	DEPTH			Bulk Volume	DENSITY	Saturations		
		Kinf	Kair	POROSITY		Sw	So	
	(m)	(md)	(md)	(%)	(g/cc)	(%)	(%)	
25DS	5109.55		3.51	2.0	2.775	85.6	2.1	Fracture
26DS	5111.75		2.32	1.8	2.616	-	-	Fracture
27DS	5113.86		0.007	1.4	2.694	47.3	48.9	
28DS	5115.92		-	3.2	2.748	79.5	17.3	Fracture
29DS	5118.05		-	4.3	2.963	26.9	49.8	Fracture
30DS	5120.97		0.020	2.4	2.678	50.8	47.0	
31DS	5114.87		0.008	2.4	2.682	66.1	21.4	



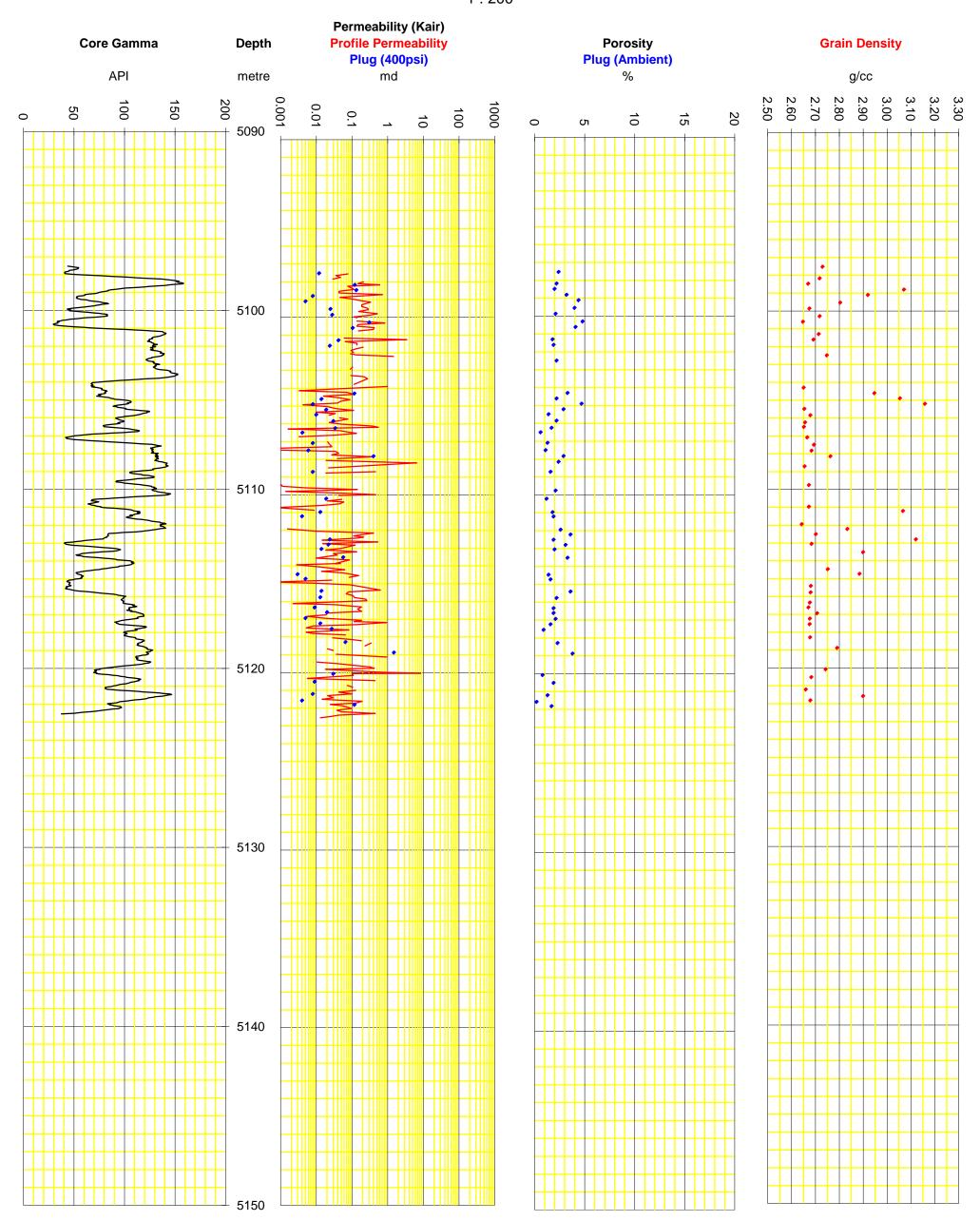
INTEGRATED CORELOG



: Poseidon - 2

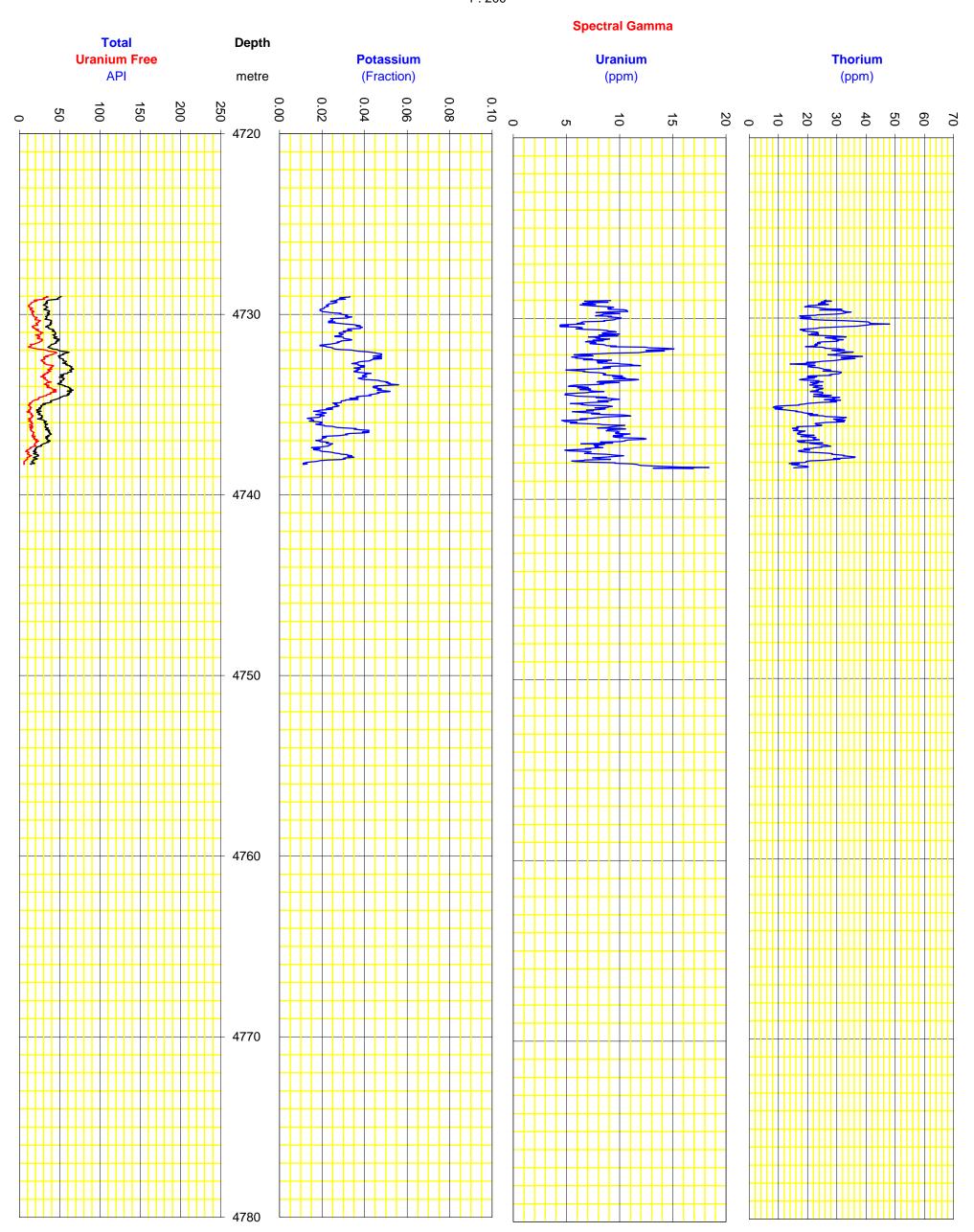


INTEGRATED CORELOG



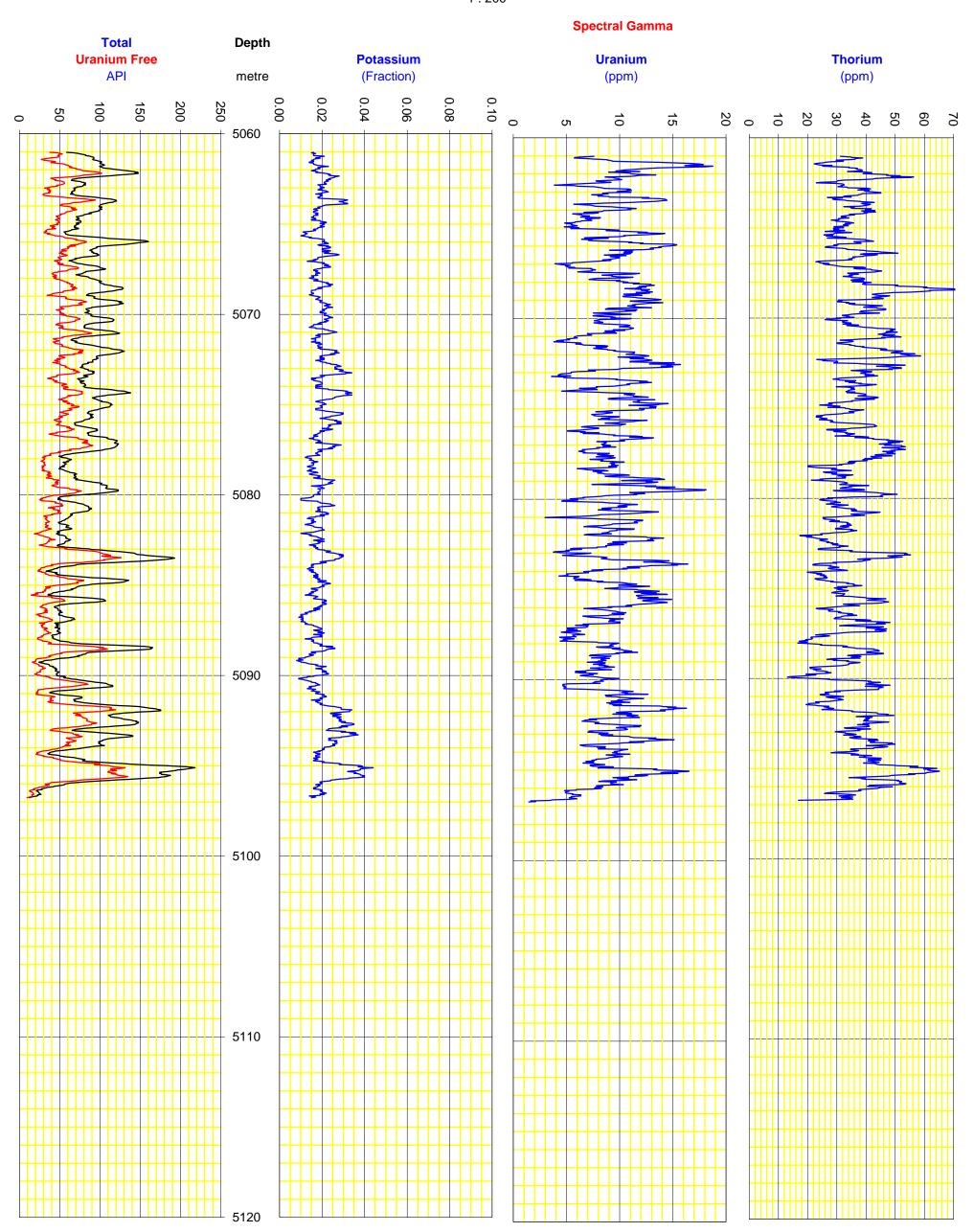


SPECTRAL CORE GAMMA



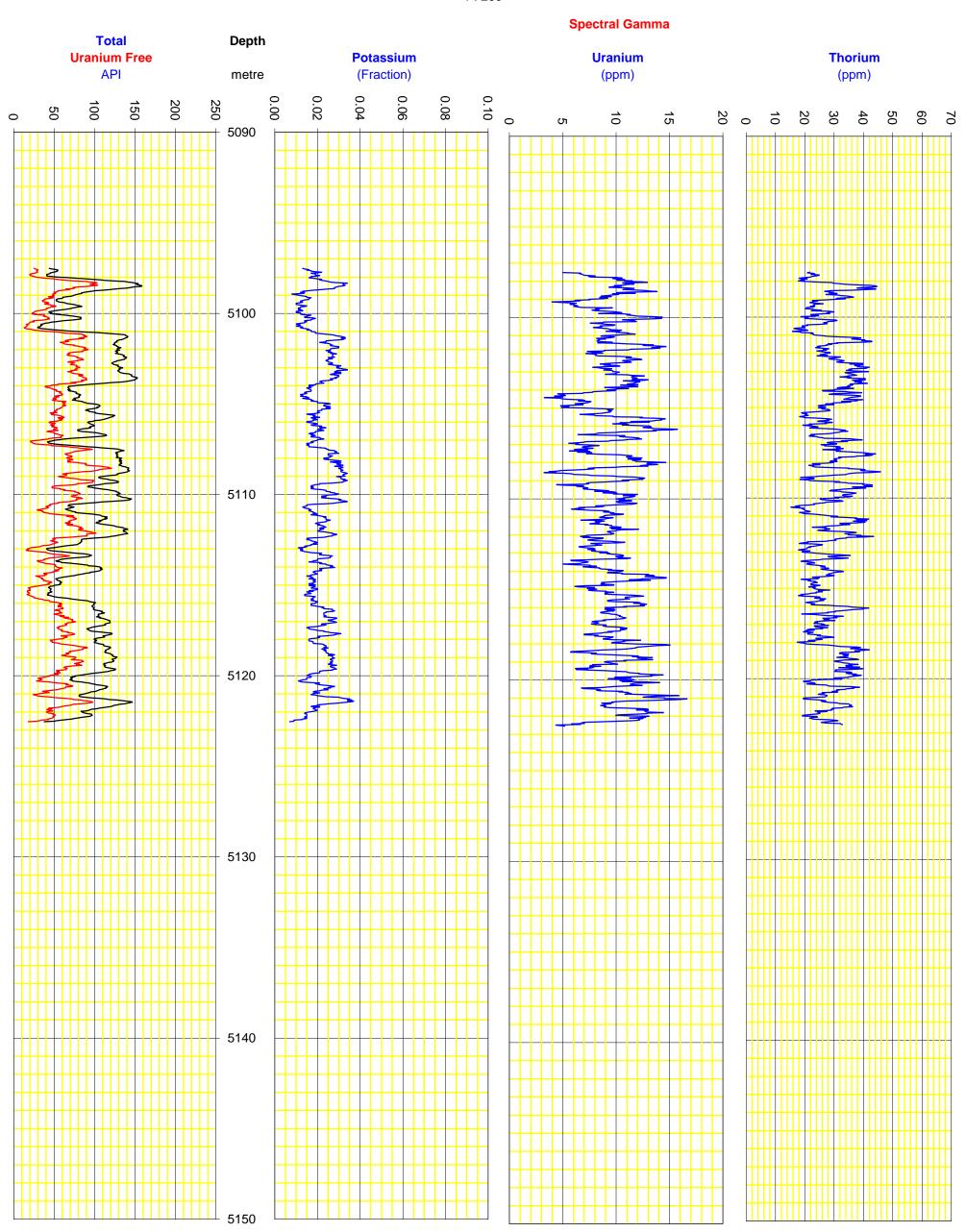


SPECTRAL CORE GAMMA





SPECTRAL CORE GAMMA



CORE INVENTORY

Barrel	Depth		Comments	Barrel	De	pth	Comments
	Тор	Bottom			Тор	Bottom	
	(m)	(m)			(m)	(m)	
		Coro 1					

Core 1

1 4729.00 4733.50 2 4733.50 4738.40

Laboratory Depths 4729.00-4738.40m

Core	2
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1	5061.00	5064.50
2	5064.50	5068.92
3	5068.92	5073.38
4	5073.38	5078.04
5	5078.04	5082.54
6	5082.54	5087.17
7	5087.17	5091.67
8	5091.67	5096.82

Laboratory Depths 5061.00-5096.82

Core 3

1	5097.50	5099.24	
2	5099.24	5103.50	
(C3-A)	5103.50	5103.74	Waxed sample
3	5103.74	5108.24	
(C3-B)	5108.24	5108.49	Waxed sample
4	5108.49	5113.25	
5	5113.25	5117.75	
6	5117.75	5122.64	

Laboratory Depths 5097.50-5122.60m

SAMPLE and PLUG INVENTORY

Sample	Depth	Comments	Sample	Depth	Comments	Sample	Depth	Comments
	(m)			(m)			(m)	
Core 1	,		17	5066.70		49	5076.91	
1 TS	4729.50		18	5066.97		50	5077.21	
2 TS	4730.20		V2	5067.22		V4	5077.42	
3 TS	4730.57		19	5067.30		51	5077.51	
4 TS	4731.20		4DS	5067.45		52	5077.81	
5 TS	4731.85		20	5067.61		S2-11	5077.87	
6 TS	4732.25		S2-5	5067.66		9DS	5077.94	
7 TS	4732.45		21	5067.90		53	5078.11	
8 TS	4733.15		22	5068.21		54	5078.43	
9 TS	4733.80		23	5068.51		S1-5	5078.49	
10 TS	4734.50		24	5068.81		S2-12	5078.68	
11 TS	4734.72		S2-6	5069.09		55	5078.73	
12 TS	4735.10		25	5069.13		56	5079.03	
13 TS	4735.80		26	5069.43		57	5079.31	
14 TS	4736.35		27	5069.71		58	5079.61	
15 TS	4736.90		S1-3	5069.93		S2-13	5079.65	
16 TS	4737.10		28	5069.97		10DS	5079.86	
17 TS	4737.50		29	5070.30		59	5080.20	
18 TS	4738.15		30	5070.61		S2-14	5080.24	
19 TS	4738.30		31	5070.91		60	5080.51	
Core 2			32	5071.24		61	5080.81	
1DS	5061.04		S2-7	5071.45		62	5081.11	
1	5061.30		33	5071.50		63	5081.42	
2	5061.60		5DS	5071.62		S2-15	5081.48	
S2-1	5061.88		34	5071.81		11DS	5081.78	
3	5061.90		S2-8	5072.07		64	5082.10	
V1	5062.13		35	5072.11		S1-6	5082.15	
4	5062.20		V3	5072.13		S2-16	5082.15	
5	5062.49		36	5072.41		65	5082.41	
S1-1	5062.58		37	5072.72		66	5082.74	
S2-2	5062.75		6DS	5073.06		V5	5082.97	
6	5062.79		38	5073.31		67	5083.04	
2DS	5063.03		39	5073.61		12DS	5083.29	
7	5063.40		40	5073.90		68	5083.58	
8	5063.70		S2-9	5074.15		69	5083.89	
9	5063.98		41	5074.20		70	5084.19	
S2-3	5064.25		42	5074.50		13DS	5084.35	
10	5064.30		7DS	5074.75		71	5084.48	
11	5064.60		43	5075.10		72	5084.80	
12	5064.91		44	5075.40		73	5085.10	
3DS	5065.14		45	5075.70		74	5085.41	
13	5065.50		S1-4	5075.75		75	5085.71	
14	5065.80		46	5075.97		S2-17	5085.76	
15	5066.10		8DS	5076.15		76	5086.01	
16	5066.40		47	5076.31		14DS	5086.29	
S1-2	5066.50		S2-10	5076.56		S2-18	5086.56	
S2-4	5066.65		48	5076.60		77	5086.61	
			-					

SAMPLE and PLUG INVENTORY

(m)	Sample	Depth	Comments	Sample	Depth	Comments	Sample	Depth	Comments
78 5086.91 110 5099.54 148 5114.13 79 5087.19 111 5099.87 149 5114.47 15DS 5087.35 21DS 5100.07 S1-11 5114.59 80 5087.49 112 5100.30 S2-23 5114.59 \$1-7 5087.76 113 5100.61 V8 5114.59 \$1-7 5087.80 114 5101.30 150 5114.73 \$2-19 5088.35 116 5101.89 151 5116.50 \$2-19 5088.35 116 5101.89 151 5116.81 \$4 5088.70 118 5102.78 153 5115.77 \$1-8 5088.98 119 5103.09 154 5116.34 \$16DS 5089.36 120 5103.38 S2-24 516.61 \$6 5089.60 23DS 5104.09 155 5116.61 \$7 5089.91 S2-22 5104.26 156 5116.94		(m)			(m)			(m)	
The color of the	78			110			148		
15DS 5087.35 21DS 5100.07 S1-11 5114.50 80 5087.49 112 5100.30 S2-23 5114.59 \$117 5087.76 113 5100.61 V8 5114.65 81 5087.80 114 5101.30 150 5114.73 82 5088.11 115 5101.61 31DS 5114.87 \$12-19 5088.35 116 5101.89 151 5115.03 83 5088.40 117 5102.49 152 5115.41 84 5088.93 22DS 5102.89 28DS 5115.92 85 5088.98 119 5103.09 154 5116.34 16DS 5089.36 120 5103.38 S2-24 516.40 86 5089.60 23DS 5104.09 155 5116.61 87 5089.91 S2-22 5104.26 156 5116.94 19DS 5090.18 121 5104.30 157 5117.24 \$2-20 5090.24 122 5104.61 158 5117.55 88 5090.81 124 5105.21 29DS 5118.05 90 5091.09 125 5105.49 160 5118.29 91 5091.38 126 5105.85 161 5118.57 17DS 5091.88 24DS 5106.07 162 5118.88 92 5091.85 127 5106.25 163 5119.30 93 5092.15 128 5107.09 165 5119.91 94 5092.45 129 5107.09 165 5119.91 95 5092.79 130 5107.50 166 5120.08 96 5093.08 131 5107.50 166 5120.08 97 5093.53 77 5108.05 300S 5120.97 98 5094.17 133 5108.71 168 5121.21 100 5094.44 134 5109.35 170 5121.82 101 5095.38 136 5109.76 103 5095.38 136 5109.76 103 5095.38 136 5109.76 104 5096.08 139 5110.97 Core 3 140 5111.75 5096.04 138 5110.57 5096.04 138 5110.97 5097.93 143 5110.97 5098.81 144 5112.51 107 5098.86 144 5112.51 107 5098.86 144 5112.51 107 5098.88 144 5112.51 107 5098.86 147 5113.52 511.05 5098.86 147 5113.52 511.05 5098.86 147 5113.52									
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101 5095.03 25DS 5109.55 102 5095.38 136 5109.76 103 5095.82 137 5110.22 S1-9 5096.04 138 5110.57 104 5096.08 139 5110.97 Core 3 140 5111.21 S2-21 5096.14 141 5111.63 105 5097.53 26DS 5111.75 V6 5097.83 142 5111.95 20DS 5097.93 143 5112.22 106 5098.18 144 5112.51 107 5098.48 145 5112.80 108 5098.81 146 5113.05 S1-10 5098.86 147 5113.52	100	5094.44		134	5109.06		169	5121.58	
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107 5098.48 145 5112.80 108 5098.81 146 5113.05 S1-10 5098.86 147 5113.52	20DS	5097.93		143	5112.22				
108 5098.81 146 5113.05 S1-10 5098.86 147 5113.52	106	5098.18		144	5112.51				
S1-10 5098.86 147 5113.52	107	5098.48		145	5112.80				
	108	5098.81		146	5113.05				
109 5099 11 27DS 5113 86	S1-10	5098.86		147	5113.52				
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