

Stability Improvements at FLUTE (Verbesserung der Stabilität von FLUTE)

Master thesis
of

Marvin-Dennis Noll

at the Institute for Beam Physics and Technology

Reviewer:	Prof. Dr.-Ing. John Jelonnek (IHM)
Second Reviewer:	Prof. Dr. Anke-Susanne Müller (IBPT)
Advisor:	Dr. Nigel Smale (IBPT)

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Prof. Dr.-Ing. John Jelonnek (IHM)

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1. Interfacing FLUTE

This chapter covers methods on interfacing the FLUTE accelerator, that is how to read diagnostic measurements into the control system from FLUTE and how to influence the electron acceleration appropriately to achieve stabilization.

In this chapter *input* and *output* refer to the view from the control system.

1.1 Inputs

FLUTE uses the *Experimental Physics and Industrial Control System (EPICS)*[1] for control of various parts of the accelerator, to send real time data to be archived and to build user interfaces via *Control System Studio (CSS)*[2], a JAVA based integrated development environment (IDE).

EPICS offers client/server and publish/subscribe paradigms to access data in so called process variables (PV) through channels. Modules are usually written in the C programming language. To ease the access to EPICS channels in programs written with the Python language, the package *PyEpics*[3] can be used. Since all data of interest as input for the control system can be extracted through an EPICS channel, the next section deals with using PyEpics to obtain the data.

1.1.1 Accessing EPICS channels in Python with PyEpics

Before usage PyEpics needs to be installed, e.g. with `pip3 install pyepics` from the *PyPi* repository. If the computer running the Python code can reach the EPICS CA repeater on the machine network, the connection is established automatically in the background. To get a channel value asynchronously, i.e. at an arbitrary time, the function `caget(pvname)` can be used with the name of the desired process value, see ??.

Listing 1.1: Using `caget()` to get the value of an EPICS process value

```
1 from epics import caget
2 print(f"Cavity RF power: {caget('F:RF:LLRF:01:GunCav1:Power:Out')}")
```

Another way is to setup a channel object and create a subscription with an user defined callback function that is executed each time the process variable changes. This implements synchronous access to the PV and can be compared to an interrupt rather than polling the variable as in Listing 1.1.

For a non trivial example see Listing 1.2. In this program, the time differences between new values and their statistics are printed to the console.

Listing 1.2: Using a user defined callback function to access an EPICS process value

```
1 from epics import ca
2 import time
3 import numpy as np
4
```

```

5 dts=np.array([])
6 lastCalled=time.time()
7
8 def call(pvname, value, **kwargs):
9     global lastCalled, dts
10    now=time.time()
11    dt=now-lastCalled
12    lastCalled=now
13    dts=np.append(dts, dt)
14
15 chid=ca.create_channel("F:RF:LLRF:01:GunCav1:Power:Out")
16 - , - , eventID=ca.create_subscription(chid, callback=call, use_time=True)
17
18 while(True):
19     time.sleep(2)
20     print(f"N:{len(dts)},mean:{np.mean(dts)},min:{np.min(dts)},max:{np.max(dts)},std:{np.std(dts)}")

```

1.1.2 Properties of the Available Process Variables

In this section some process variables that may be used as inputs for the control system are analyzed. These are:

- **F:RF:LLRF:01:GunCav1:Power:Out Value:** The RF power measured immediately before the cavity
- **F:AX:DAQDT:01:1:Wave:05:Sample Value:** The charge measured with a Faraday cup (RadiaBeam Technologies FARC-04 [4]) and amplified with a charge sensitive amplifier (PCB 421A25 [5])
- **F:INJ-1:Gun:01:Temperature:Body Value:** The body temperature of the cavity

In Figure 1.1 all three are plotted for a duration of 15 min without any interference to the system and the system being in steady state operation.

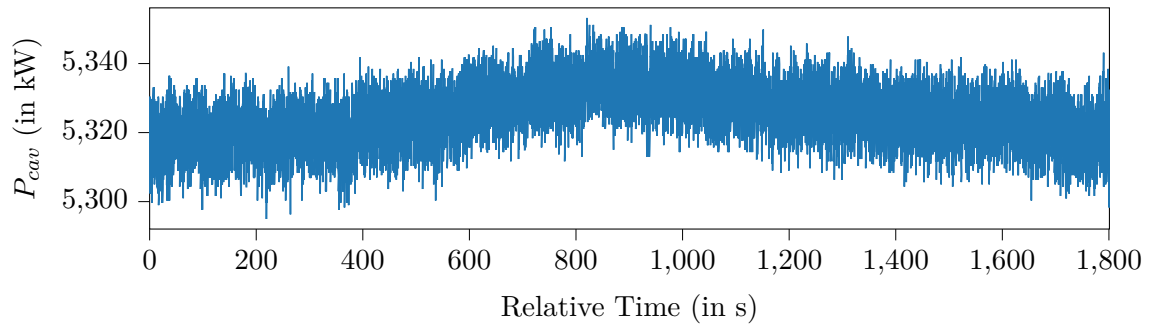
In addition the sample times of the process variables is examined if the method with a custom callback is used (see Listing 1.2) or the data is extracted from the archive. The differences in the sample times are calculated according to

$$\Delta = t_{n+1} - t_n. \quad (1.1)$$

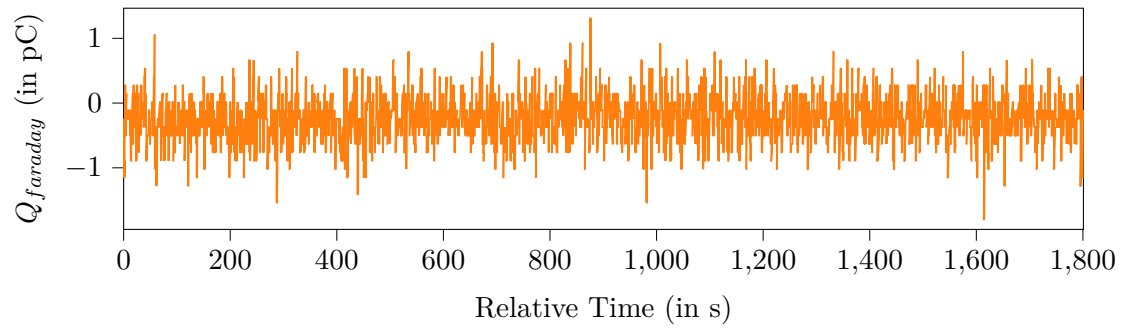
Then a histogram with the relative frequency on the y axis is used as an estimator for the probability density function of the sample time intervals (see Figure 1.2). The histogram shows that the time series resulting from recording process variables out of the EPICS system are highly unevenly spaced. Thus the data needs to be converted to posses evenly spaced sample times to use common signal processing methods like the DFT or digital LTI filters. For offline analysis of prerecorded data, it can easily be resampled to a fixed time grid. But for online operation of a filter or a whole control system it is not possible to use an arbitrary resample method because they are often non causal or introduce significant group delay when made causal. Instead calling `caget()` with a (software-) timer can be used to get evenly spaced samples online.

Table 1.1: Comparing quantization steps

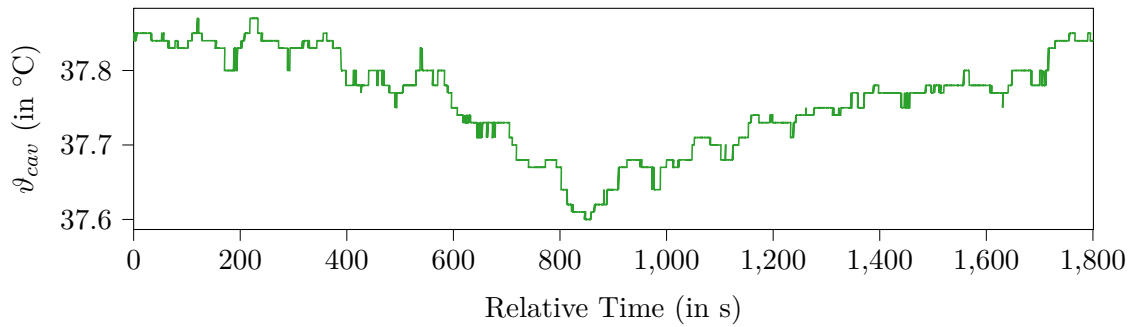
PV	N_{unique}	q_{avg}	q_{norm}
F:RF:LLRF:01:GunCav1:Power:Out Value	84	0.6935	0.011 904
F:AX:DAQDT:01:1:Wave:05:Sample Value	22	0.015	0.045 45
F:INJ-1:Gun:01:Temperature:Body Value	18	0.1294	0.055 55



(a) Cavity RF power F:RF:LLRF:01:GunCav1:Power:Out Value



(b) Faraday cup charge F:AX:DAQDT:01:1:Wave:05:Sample Value



(c) Cavity body temperature F:INJ-1:Gun:01:Temperature:Body Value

Figure 1.1: Comparing the quantization noise of three process variables

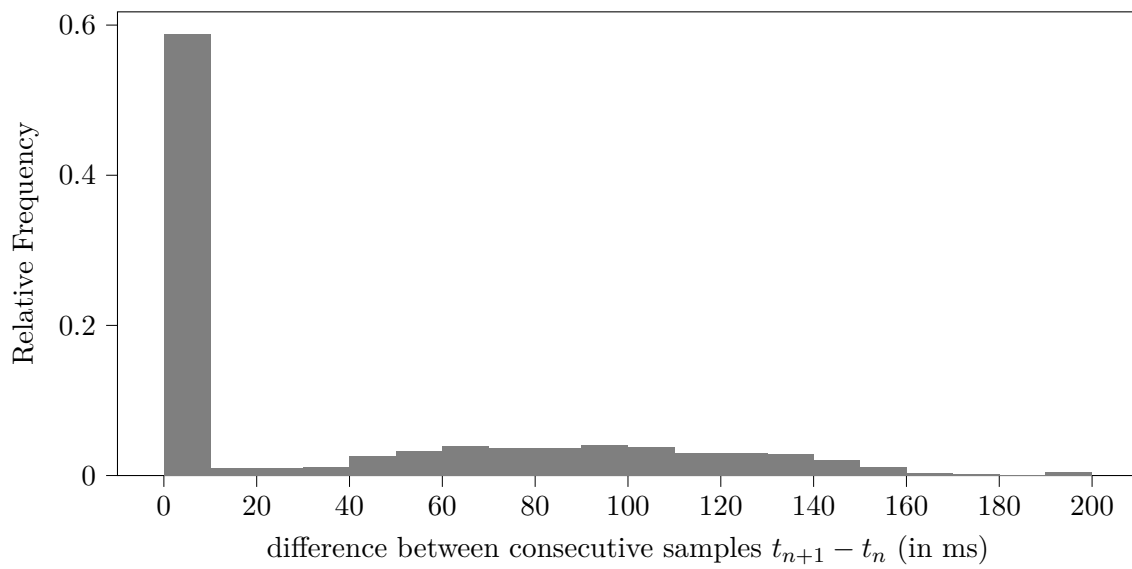


Figure 1.2: Histogram of the sample time intervals Δ of the plots in Figure 1.1

1.2 Output: Controllable RF Attenuator

The output signal computed by the control systems has to have a way of influencing the RF power send to the cavity. This could be done over an EPICS channel (e.g. with the PyEpics function `caput()` to set the value of a process variable via a channel access). However to make it possible to move the control system from a general purpose personal computer to a dedicated digital signal processor, FPGA or similar in the future, using a physical device in the signal path is preferred.

1.2.1 Defining Requirements

Table 1.2: Requirements for the controllable RF attenuator

Requirement	Value/Range
minimum attenuation	
maximum attenuation	
attenuation resolution	
setup time	
operating temperature range	
supply voltage	
control voltage	

1.2.2 Evaluation of the ZX73-2500-S+ Controllable RF Attenuator

The *ZX73-2500-S+* is a voltage controllable RF attenuator with coaxial SMA connectors by the company Mini-Circuits. As there is no alternative model from Mini-Circuits and devices from other manufactures are offered with similar specifications, only the ZX73-2500-S+ is evaluated in detail in this section.

The ZX73-2500-S+ attenuator consists of a brass housing/shielding containing the Mini-Circuits RVA-2500+, a variable SMD attenuator in the DV874 case form factor. The RF input and output are connected with female SMA screw connectors. The power supply and control voltage are connected with solder pins. In order to use shielded cables and a reliable connection, for all measurements SMA connectors are soldered to the supply and control pins. According to equivalent circuit in the data sheet[6] it can be assumed it is based on the common quad- π pin diode design[7].

The attenuation versus frequency measurements from the manufactures data sheet are redone to both get a first impression of the device and verify it is generally operational and also as a sanity check for the used laboratory test equipment. Because the signal used by the FLUTE RF system is a 3 GHz single harmonic, the frequency measurement range is augmented over the maximum of 2.5 GHz in the data sheet to 4 GHz. Between the measurement of each network analyzer trace, the control voltage $V_{control}$ of the attenuator is set to 0 V, 2 V, 4 V, 6 V or 12 V. The result is shown in Figure 1.3¹. When comparing the measured plots to the plots in the data sheet, there are obvious discrepancies. For $V_{control} = 0$ V the attenuator is very susceptible to noise on the control input, which could explain the differences for this curve. In the case of 2 V and 4 V, the almost constant offset scales with a similar logarithmic fashion as the attenuation does, which suggests device tolerances causing the deviations.

From this quick examination it is not possible to predict how the attenuator behaves for small changes in $V_{control}$ and how changes in the environment, such as the body temperature or the supply voltage, cause unwanted variations in the attenuation.

For this reason, the ZX73-2500-S+ is examined in greater detail with different measurement setups in the next sections.

¹A through calibration of the network analyzer reduces the influence of the cables and connectors on the measurement. Change in attenuation due to play in the connectors and slight bend changes in the cables exceed the trace noise (0.004 dBrms) and cause an uncertainty of about 0.5 dB

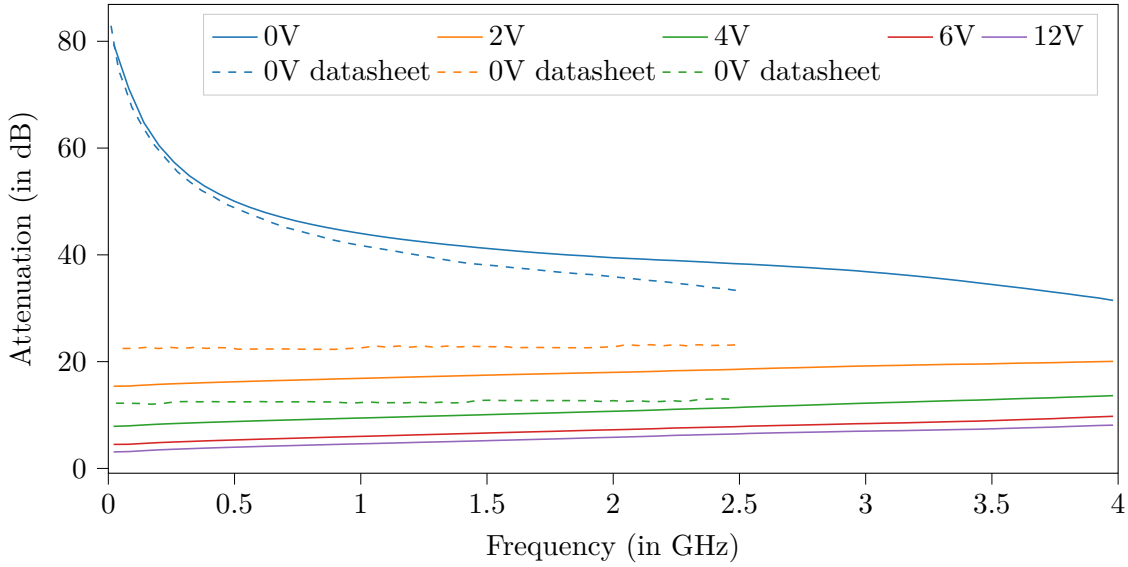


Figure 1.3: Attenuation vs. frequency over DC control voltage; measured with network analyzer (see A.6.1, parameters: $\#AVG$: 16, $IF-BW$: 10 kHz); plotted in dashed lines are the measurements from the data sheet (see [6, p. 2])

1.2.2.1 Common Measurement Setup

For the following measurements a common setup is used to ease the recording of data and the sequential control for parameter studies. The needed tasks are:

- Supply the attenuator with the supply voltage V_+
- Supply the attenuator with the adjustable control voltage $V_{control}$
- Supply the RF input power
- Measure the RF output power
- Record all data as time series to a computers storage device

To achieve this, the setup in Figure 1.4 is used. The supply and control voltage are generated by a Keysight 34972A with a 34907A module (see subsubsection A.2.1). To get a more accurate measurement of the actual voltages, two digital multimeters (Models 34470A and 34411A, see subsubsection A.1.2) are connected directly at the $V_{control}$ and V_+ pins. The RF signal is generated by a Rhode und Schwarz SMC 100A signal generator. With the HP E4419B and its two inputs and a power splitter, it is possible to directly get the attenuation of the ZX73-2500-S+. The body temperature of the device is monitored with a PT100 temperature sensor connected to the 34972A.

Each of the lab devices used is compatible with VXI11, which is a widely adopted standard that is used to send ASCII SCPI commands over an ethernet network (called LXI) or GPIB [8]. This enables remote and programatically control of the devices over the network. With the library *python-vxi11*, it is now possible to write a custom script, that sets the measurement devices to known initial conditions, drives the inputs of the attenuator and records the generated data. The whole setup of the hardware in ?? and the Python software, a measurement frequency of about 0.5 Hz to 1 Hz can be achieved, which is enough because most measurements taken are of a static nature and in the case of the temperature influence measurement, the thermal time constant is in the order of a few seconds. The limiting device is the HP E4419B which takes the longest to perform one measurement. Without it, measurement frequencies of over 4 Hz are possible.

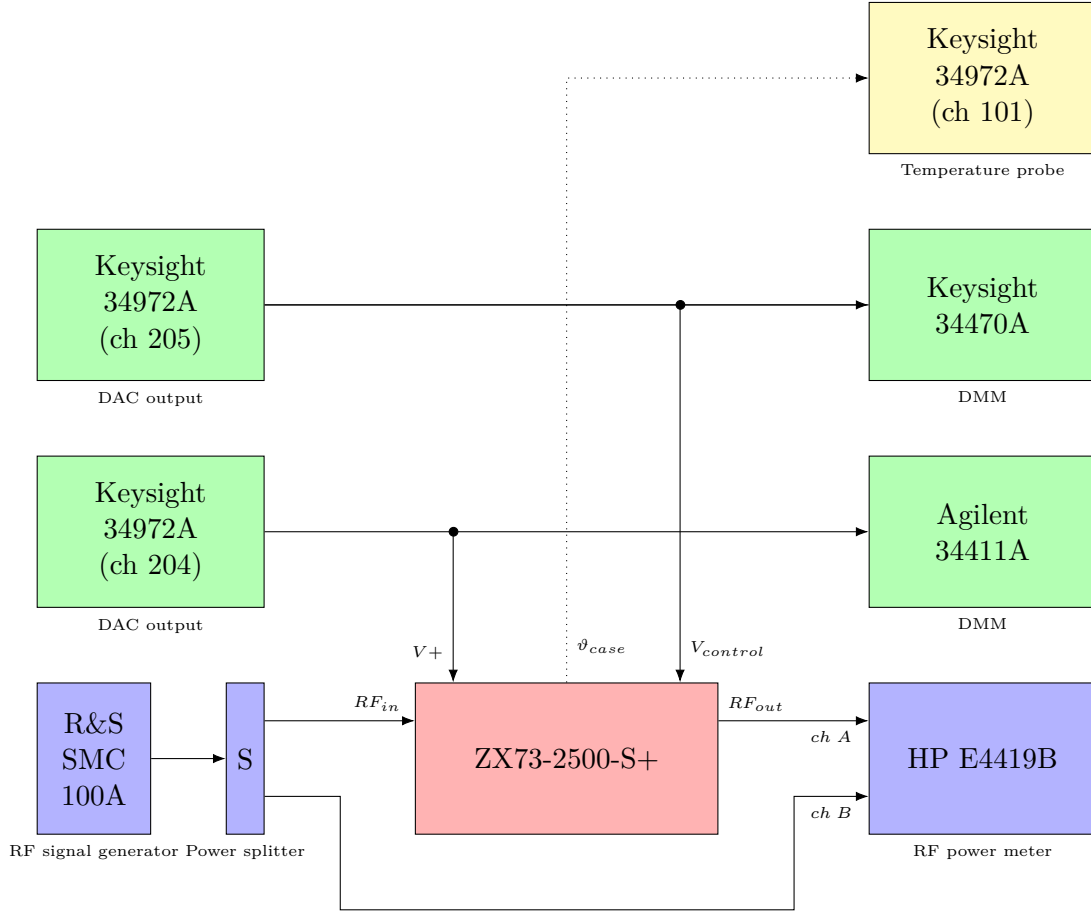


Figure 1.4: Measurement setup: DUT(red), RF generator/power splitter/meter(blue), DC sources/meters(green), temperature probe(yellow)

All measurements are performed in the “RF lab” in building 348 (KARA hall on KIT Campus North) which is air conditioned to about $(20 \pm 2)^\circ\text{C}$.

1.2.2.2 Relation between Control Voltage and Attenuation

The measured spectra in Figure 1.3 already suggest that there is a non linear relationship between the control voltage $V_{control}$ and the attenuation A of the attenuator:

$$A = A(V_{control}, f) \neq const. \cdot V_{control} \cdot A(f). \quad (1.2)$$

This also means the sensitivity

$$S(V_{control}, f) = \frac{dA(V_{control}, f)}{dV_{control}} \quad (1.3)$$

(for a fixed frequency) is not constant. In other words, for a desired relative change in attenuation, the needed adjustment in $V_{control}$ depends on the chosen operating point $A_0 := A(V_{control,0}, f_0)$.

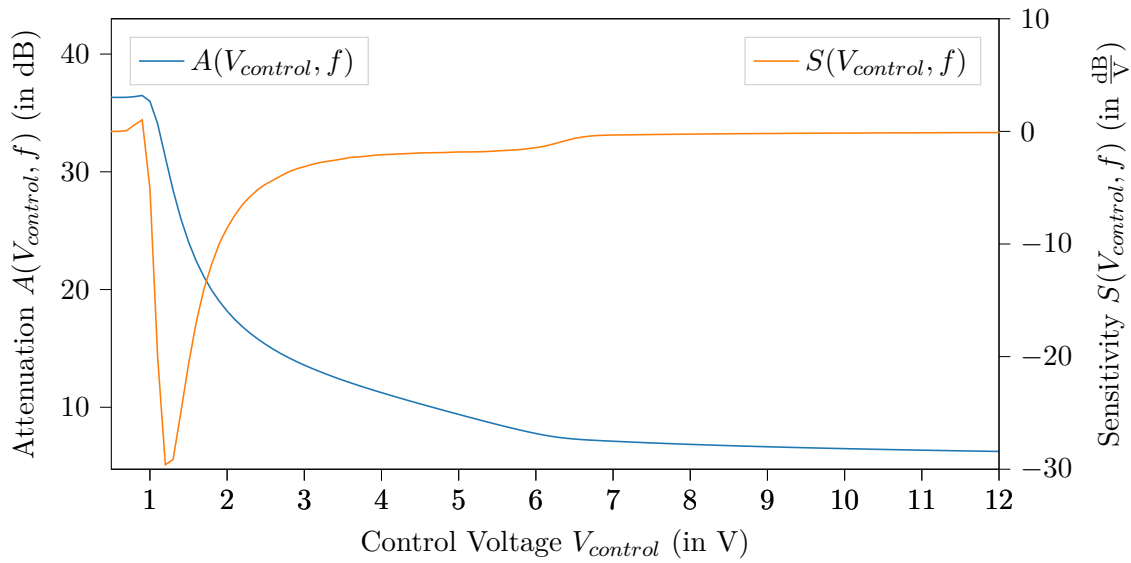


Figure 1.5

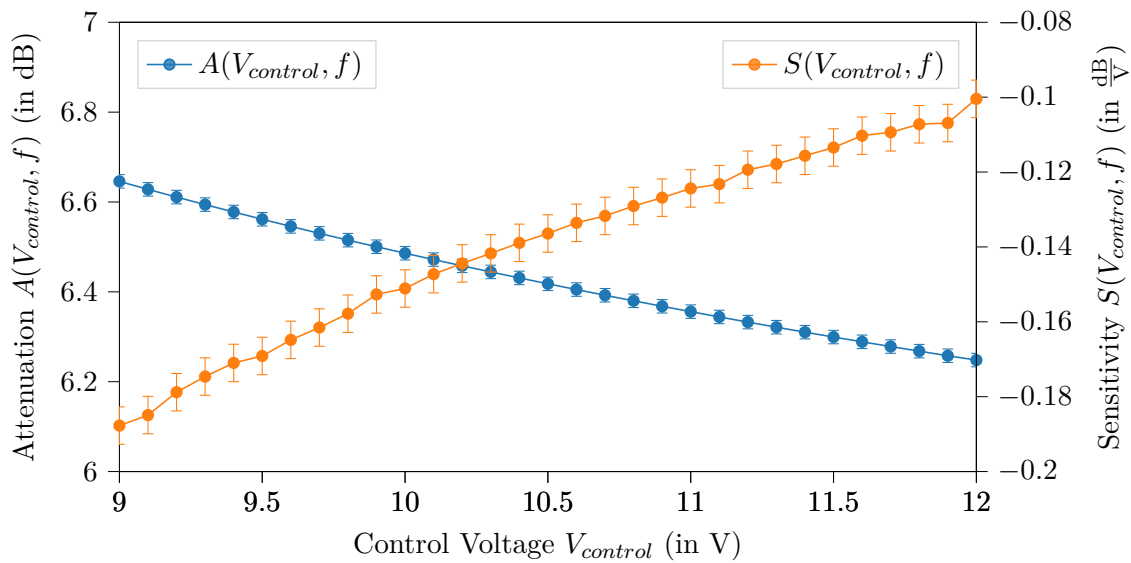


Figure 1.6

1.2.2.3 Influence of Supply Voltage Noise on Attenuation

1.2.2.4 Influence of Body Temperature Variations on Attenuation

1.2.2.5 Influence of Small Changes in RF Frequency on Attenuation

1.2.2.6 Final Test of the Attenuator in the FLUTE LLRF Cabinet

1.2.3 Conclusion

Appendix

A Lab Test and Measurement Equipment

A.1 Benchtop multimeters

A.1.1 Agilent 34411A

Table A.3: Agilent 34411A specifications

Specification	Value
	DC volt
Digits	6 1/2
Measurement method	cont integrating multi-slope IV A/D converter
Accuracy (10 V range, 24 hours)	0.0015 % + 0.0004 % (% of reading + % of range)
Bandwidth	15 kHz (typ.)

Table A.4: Agilent 34411A some SCPI commands

Description	Example command	Example return
Read current measurement	READ?	+2.84829881E+00 (2.848 V)

A.1.2 Keysight 34470A

Table A.5: Keysight 34470A specifications

Specification	Value
	DC volt
Digits	7 1/2
Measurement method	cont integrating multi-slope IV A/D converter
Accuracy (10 V range, 24 hours)	0.0008 % + 0.0002 % (% of reading + % of range)
Bandwidth (10 V range)	15 kHz (typ.)

Table A.6: Keysight 34470A some SCPI commands

Description	Example command	Example return
Read current measurement	READ?	+9.99710196E+00 (9.997 V)

A.2 Data Acquisition/Switch Unit

A.2.1 Keysight 34972A

Table A.7: Keysight 34972A specifications

Specification	Value
	34907A (Multifunction module)
DAC range	± 12 V
DAC resolution	16 bit ($24\text{ V}/2^{16} = 366.21\text{ }\mu\text{V}$ per bit)
DAC maximum current	10 mA
	34901A (20 channel multiplexer)

Table A.8: Keysight 34972A some SCPI commands

Description	Example command	Example return
Read current measurement	READ?	+2.00200000E+01 (20.02 °C)
Set DAC voltage of ch 204 to 3.1 V	SOUR:VOLT 3.1, (@204)	

A.3 Oscilloscopes

A.3.1 Tektronix MSO64

Table A.9: Tektronix MSO64 specifications

Specification	Value
Bandwidth	6 GHz
Sample rate	25 GS/s
ADC resolution	12 bit
DC gain accuracy (@ 50 Ω , >2 mV/div)	± 2 %

Table A.10: Tektronix MSO64 some SCPI commands

Description	Example command	Example return
Read mean of measurement 1 (current acq.)	MEASUREMENT:MEAS1:RESULTS:CURR:MEAN?	3.0685821787408

A.4 RF signal generator

A.4.1 Rohde and Schwarz SMC100A

Table A.11: Rohde and Schwarz SMC100A specifications

Specification	Value
Frequency range	9 kHz to 3.2 GHz
Maximum power level	17 dBm
SSB phase noise (@ 1 GHz, $f_o = 20$ kHz, $BW = 1$ Hz)	-111 dBc
Level error	<0.9 dB

Table A.12: Rohde and Schwarz SMC100A some SCPI commands

Description	Example command	Example return
Set RF power level to 10.5 dBm	SOUR:POW 10.5	
Set RF frequency to 3.1 GHz	SOUR:FREQ:FIX 3.1e9	
Enable the RF output	OUTP on	

A.5 RF power meter

A.5.1 HP E4419B

Table A.13: HP E4419B specifications

Specification	Value
Digits	4
Accuracy (abs. without power sensor)	± 0.02 dB
Power probe: E4412A	
Frequency range	10 MHz to 18 GHz
Power range	-70 dBm to 20 dBm

Table A.14: HP E4419B some SCPI commands

Description	Example command	Example return
Measure power on input 1	MEAS1?	+2.89435802E+000 (2.894 dBm)

A.6 Vector Network Analyzer

A.6.1 Agilent E5071C

Table A.15: Agilent E5071C specifications

Specification	Value
Frequency range	9 kHz to 8.5 GHz

A.7 Phase noise analyzer

A.7.1 Holzworth HA7062C

Table A.16: Holzworth HA7062C specifications

Specification	Value
DUT input frequency	10 MHz to 6 GHz
Measurement bandwidth	0.1 Hz to 40 MHz offsets

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