Part 1

Q1)

Theoritical

## Step 1: Find the Transfer Function

As before, we can use the formula for the transfer function:

$$H(s) = C(sI - A)^{-1}B + D$$

Where s is the complex frequency variable, and I is the identity matrix.

#### Code

```
%------Q1------
% Define the open-loop transfer function G(s)
num_G = 1;
den_G = [1 1 0];  % s(s+1) = s^2 + s
G_S = tf(num_G, den_G)

% Define the feedback transfer function H(s)
num_H = [1];
den_H = [1];  % Unity Feedback
H_S = tf(num_H, den_H)
```

#### Output:

Continuous-time transfer function.

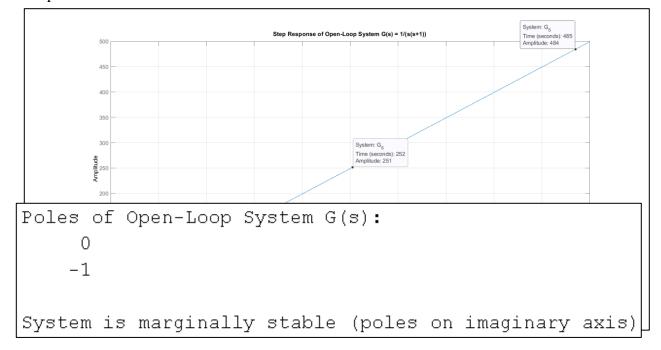
1

Static gain.

#### Q2) the step() command to plot the output of G(S)

Code: We made a function that plots step time response and checks stability

```
%-----Q2----- Step Response of G(s) (Open-Loop)
% Plot step response of G(s)
draw step(G S, 'Open-Loop System G(s)');
function draw step(sys, sys name)
% Create figure
    figure;
    % Plot step response
    step(sys);
    title(['Step Response of ', sys name]);
   grid on;
    % Display poles
    poles = pole(sys);
    disp(['Poles of ', sys_name, ':']);
    disp(poles);
    % Check stability
    if all(real(poles) < 0)</pre>
        disp('System is stable (all poles in LHP)');
    elseif any(real(poles) > 0)
        disp('System is unstable (at least one pole in RHP)');
    else
        disp('System is marginally stable (poles on imaginary axis)');
    end
end
```



```
%-----Q3------ Closed-Loop Analysis
disp('Closed-Loop TF using feedback():');
T_feedback = feedback(G_S, H_S)

disp('Closed-Loop TF using manual formula (G/(1+GH)):');
T_manual = (1 / (1 + G_S * H_S)) * G_S; % Equivalent to T(s) = G/(1+GH)
T_manual = minreal(T_manual) % Cancel common terms
```

```
Closed-Loop TF using feedback():
T feedback =
       1
  s^2 + s + 1
Continuous-time transfer function.
Closed-Loop TF using manual formula (G/(1+GH)):
T manual =
       1
  s^2 + s + 1
Continuous-time transfer function.
```

Q4)

## Code:

```
%------Q4------ Step Response of T(s) (Closed-Loop)
% Plot step response of T(s)
draw_step(T_feedback, 'Closed-Loop System T(s)');
```

### Output:

	Before $G_c(s)$	with $G_c(s)$	
$\left  e_{s.s} \right _{due\ to\ dist.}$	%	zero	
ζ	0.4	0.69	
$\omega_n$	14.8	58	
$M_p$	25%	5%	
$t_{\scriptscriptstyle S}$	0.67	0.1	

### Ouput:

System: Closed-Loop System T(s)

Poles: -0.5-0.86603i -0.5+0.86603i

Stability: stable (all poles in LHP)

Over shoot MP: 16.2929% at t = 3.592 sec

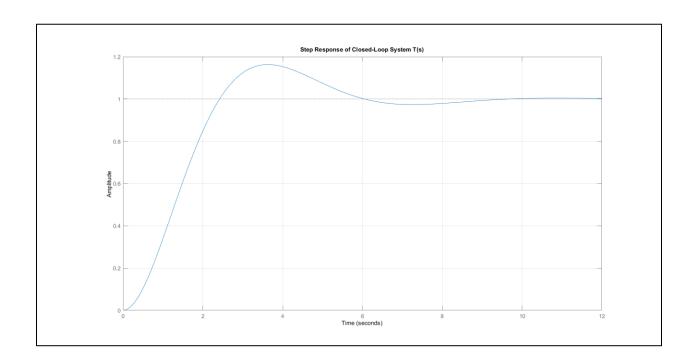
Damping ratio ( $\zeta$ ): 0.500

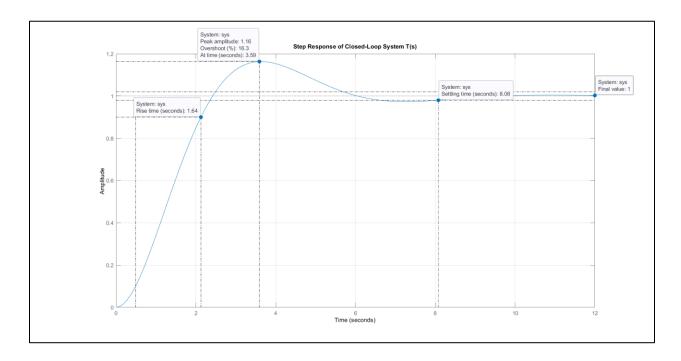
Natural frequency (on): 1.000 rad/s

Settling time (2%): 8.1051 sec

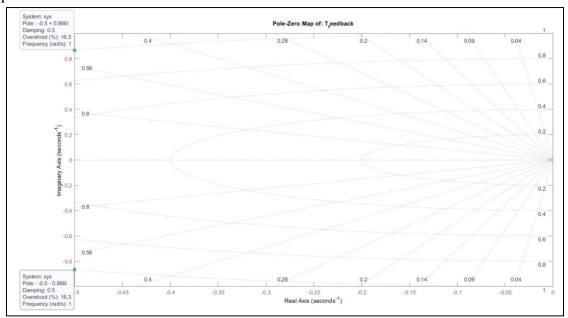
Rise time (10-90%): 1.6579 sec

Steady-state value: 1.0014





```
function [poles] = draw poles(sys)
   % Create figure
   figure;
    % Plot pole-zero map
   pzmap(sys);
   title(['Pole-Zero Map of: ' inputname(1)]);
   grid on;
   % Get poles
   poles = pole(sys);
   % Display poles
   disp(['Poles of ' inputname(1) ':']);
   disp(poles);
    % Damping characteristics (for complex poles)
   if ~isreal(poles)
        [wn, zeta] = damp(sys);
        fprintf('Damping ratio (?): %.3f\n', zeta(1));
        fprintf('Natural frequency (?n): %.3f rad/s\n', wn(1));
   end
end
```



Poles of T\_feedback:

-0.5000 + 0.8660i

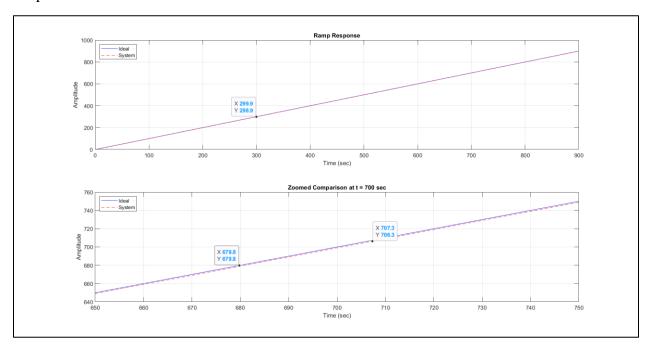
-0.5000 - 0.8660i

Damping ratio ( $\zeta$ ): 0.500

Natural frequency (wn): 1.000 rad/s

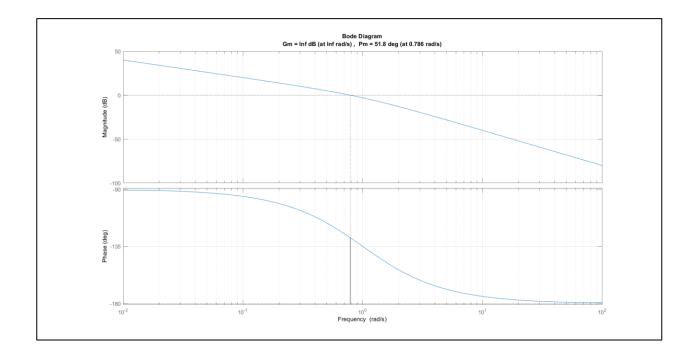
Q6,Q7 is done

```
function [ess, t_out, y_out] = draw_ramp(sys, t_end, zoom_time)
    % Set defaults if not provided
    if nargin < 2</pre>
        t_end = 100;
    end
   if nargin < 3</pre>
        zoom time = 700;
    end
    % Create time vector
    t = 0:0.1:t end;
    %getting the ramp
    ramp = tf(1,[1 0]);
    % Get response data
    [y_sys, t_sys] = step(sys.*ramp, t);
    [y_ideal, t_ideal] = step(ramp, t);
    % Create figure with three subplots
    figure;
    % Subplot 1: Ideal ramp input
    subplot(2,1,1);
    plot(t ideal, y ideal, 'b');
   hold on;
   plot(t sys, y sys, 'r--');
   title('Ramp Response');
   xlabel('Time (sec)');
   ylabel('Amplitude');
    legend('Ideal', 'System', 'Location', 'northwest');
    grid on;
    hold off;
    % Subplot 2: Zoomed comparison
    subplot(2,1,2);
   plot(t_ideal, y_ideal, 'b');
   hold on;
   plot(t_sys, y_sys, 'r--');
    xlim([zoom time-50 zoom time+50]);
    title(['Zoomed Comparison at t = ', num2str(zoom time), ' sec']);
   xlabel('Time (sec)');
    ylabel('Amplitude');
    legend('Ideal', 'System', 'Location', 'northwest');
    grid on;
    hold off;
end
```



Steady-state error (ess): 1

```
function [Gm, Pm, Wgc, Wpc] = draw_Bode_Plot(sys)
% BODE PLOT Analyzes system stability margins and compares margin()
     Bode Plot(sys)
용
응
    Input:
          sys - Transfer function (tf object or state-space model)
90
    Outputs:
         Gm - Gain margin (dB)
용
          Pm - Phase margin (degrees)
응
응
          Wgc - Gain crossover frequency (rad/sec)
응
          Wpc - Phase crossover frequency (rad/sec)
     % Create margin plot
     figure;
     margin(sys);
     grid on;
     % Get stability margins
     [Gm, Pm, Wgc, Wpc] = margin(sys);
     % Display results
     disp(['=== Stability Margins for ' inputname(1) ' ===']);
disp(['Gain Margin: ', num2str(Gm), ' dB at ', num2str(Wgc), ' rad/s']);
disp(['Phase Margin: ', num2str(Pm), '° at ', num2str(Wpc), ' rad/s']);
end
```



=== Stability Margins for ===

Gain Margin: Inf dB at Inf rad/s

Phase Margin:  $51.8273^{\circ}$  at 0.78615 rad/s

```
Part2
```

Q2)

Code:

Code

```
% Q3: State transition matrix calculation
% Compute ?(s) = [sI - A]^-1
Phi_s = inv(s*eye(n) - A);

% Compute ?(t) by inverse Laplace transform
syms t
Phi_t = ilaplace(Phi_s);

% Verify ?(0) = I
Phi_0 = subs(Phi_t, t, 0);

% Display results
disp('State transition matrix in s-domain (?(s)):');
pretty(Phi_s)

disp('State transition matrix in time domain (?(t)):');
pretty(Phi_t)

disp('Verification of ?(0) = I:');
disp(Phi_0);
```

State transition matrix in s-domain ( $\Phi(s)$ ): s + 5 1 | s + 5 s + 6 s + 5 s + 6 |6 s | 2 | 2 | State transition matrix in time domain  $(\Phi(t))$ :  $/ \exp(-2 t) 3 - \exp(-3 t) 2$ ,  $\exp(-2 t) - \exp(-3 t)$  $\ensuremath{\mbox{\sc exp(-3 t) 6 - exp(-2 t) 6, exp(-3 t) 3 - exp(-2 t) 2}/$ Verification of  $\Phi(0) = I$ : [1, 0][0, 1]

```
% Q4: Verify that ??(t) = A?(t)
Phi_dot = diff(Phi_t, t); % Take time derivative of ?(t)
A_Phi = A*Phi_t; % Multiply A with ?(t)

disp('Time derivative of state transition matrix (??(t)):');
pretty(Phi_dot)

disp('A*?(t):');
pretty(A_Phi)

disp('Verification successful: ??(t) = A?(t)');
```

```
Time derivative of state transition matrix (\Phi(t)):

/ \exp(-3 t) 6 - \exp(-2 t) 6, \exp(-3 t) 3 - \exp(-2 t) 2 \

| \exp(-2 t) 12 - \exp(-3 t) 18, \exp(-2 t) 4 - \exp(-3 t) 9 /

A*\Phi(t):

/ \exp(-3 t) 6 - \exp(-2 t) 6, \exp(-3 t) 3 - \exp(-2 t) 2 \

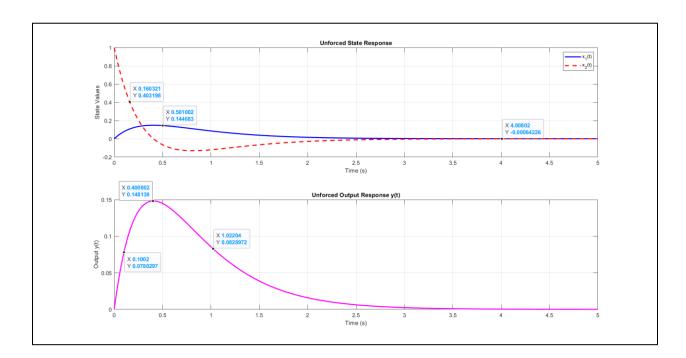
| \exp(-3 t) 12 - \exp(-3 t) 18, \exp(-2 t) 4 - \exp(-3 t) 9 /

Verification successful: \Phi(t) = A\Phi(t)
```

```
% Q5 Check Controllability and Observability
% Check Controllability
Co = ctrb(A, B); % Controllability matrix
rank Co = rank(Co);
disp('Controllability Matrix:');
disp(Co);
disp(['Rank of Controllability Matrix: ', num2str(rank Co)]);
if rank_Co == n
    disp('System is Controllable (as expected)');
else
    disp('System is Not Controllable (unexpected for this system)');
end
% Check Observability
Ob = obsv(A, C); % Observability matrix
rank Ob = rank(Ob);
disp('Observability Matrix:');
disp(Ob);
disp(['Rank of Observability Matrix: ', num2str(rank Ob)]);
if rank Ob == n
    disp('System is Observable (as expected)');
else
    disp('System is Not Observable (unexpected for this system)');
end
```

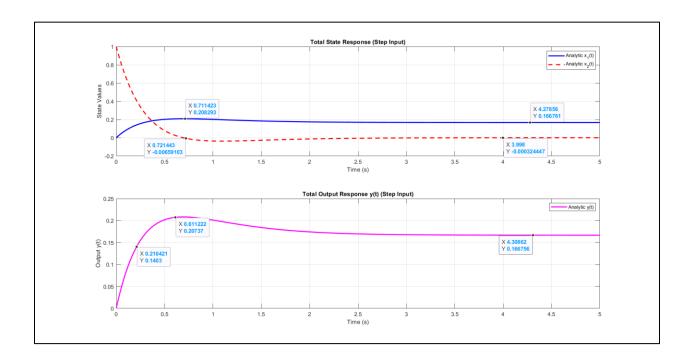
Controllability Matrix:			
0 1			
1 -5			
Rank of Controllability Matrix: 2			
System is Controllable (as expected)			
Observability Matrix:			
1 0			
0 1			
Rank of Observability Matrix: 2			
System is Observable (as expected)			

```
% Q6: Unforced (Homogeneous) Response
disp('=== Unforced Response Analysis ===');
% Compute state solution x(t) = ?(t)*x0
x t = Phi t * x0;
disp('Unforced state solution x(t):');
pretty(x t)
% Compute output solution y(t) = C*x(t) + D*u(t)
% Since u(t)=0 for unforced response:
y t = C*x t + D*0;
disp('Unforced output response y(t):');
pretty(y_t)
% Plot the results
t vals = linspace(0, 5, 500); % Time vector from 0 to 5 seconds
% Convert symbolic expressions to numeric functions
x1 func = matlabFunction(x t(1));
x2 func = matlabFunction(x_t^2(2));
y_func = matlabFunction(y_t);
% Evaluate solutions
x1_vals = arrayfun(x1_func, t_vals);
x2_vals = arrayfun(x2_func, t_vals);
y vals = arrayfun(y func, t vals);
% Plot state responses
figure;
subplot(2,1,1);
plot(t vals, x1 vals, 'b', 'LineWidth', 2);
hold on;
plot(t vals, x2 vals, 'r--', 'LineWidth', 2);
title('Unforced State Response');
xlabel('Time (s)');
ylabel('State Values');
legend('x 1(t)', 'x 2(t)');
grid on;
% Plot output response
subplot(2,1,2);
plot(t_vals, y_vals, 'm', 'LineWidth', 2);
title('Unforced Output Response y(t)');
xlabel('Time (s)');
ylabel('Output y(t)');
grid on;
% Compare with MATLAB's built-in initial() function
[\sim, t \text{ num}, x \text{ num}] = initial(sys, x0, t vals(end));
y_num = x_num*C'; % Equivalent to C*x since D=0
% Display symbolic solutions
disp(' ');
disp('Analytic Solutions:');
disp('x1(t) = '); pretty(x_t(1))
disp('x2(t) = '); pretty(x_t(2))
disp('y(t) = '); pretty(y t)
```



```
=== Unforced Response Analysis ===
Unforced state solution x(t):
/ \exp(-2 t) - \exp(-3 t)
\ensuremath{\mbox{exp(-3 t) 3 - exp(-2 t) 2}}
Unforced output response y(t):
\exp(-2 t) - \exp(-3 t)
Analytic Solutions:
x1(t) =
\exp(-2 t) - \exp(-3 t)
x2(t) =
\exp(-3 t) 3 - \exp(-2 t) 2
y(t) =
\exp(-2 t) - \exp(-3 t)
```

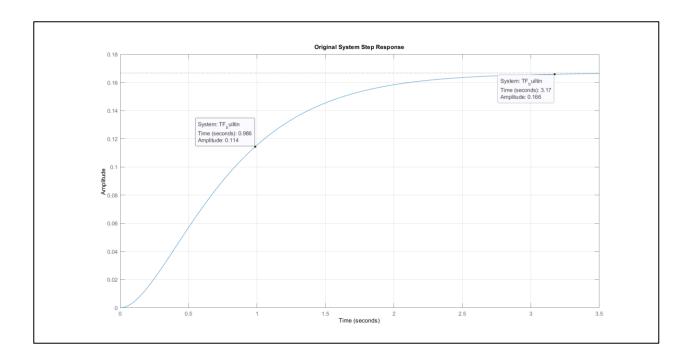
```
% Q7: Forced Response Analysis (Unit Step Input)
disp('=== Forced Response Analysis ===');
% Using Frequency Domain Approach
U s = 1/s; % Laplace transform of unit step
U t =ilaplace(U s);
% Compute forced component in frequency domain
X_forced_s = Phi_s * B * U_s;
% Convert to time domain
x forced t = ilaplace(X forced s);
% Total solution (homogeneous + forced)
x_t = x_t + x_f = x_t
% Output solution
y total t = C*x total t + D*U t; % D*u(t) where u(t)=1 for t>0
disp('Forced state solution (from step input):');
pretty(x_forced_t)
disp('Total state solution (unforced + forced):');
pretty(x_total_t)
% Direct evaluation using subs()
x1_vals = double(subs(x_total_t(1), t, t_vals));
x2_vals = double(subs(x_total_t(2), t, t_vals));
y_vals = double(subs(y_total_t, t, t_vals));
% Plot results
figure;
% State responses
subplot(2,1,1);
plot(t vals, x1 vals, 'b', 'LineWidth', 2);
hold on;
plot(t vals, x2 vals, 'r--', 'LineWidth', 2);
title('Total State Response (Step Input)');
xlabel('Time (s)');
ylabel('State Values');
legend('Analytic x_1(t)', 'Analytic x_2(t)');
grid on;
% Output response
subplot(2,1,2);
plot(t_vals, y_vals, 'm', 'LineWidth', 2);
hold on;
title('Total Output Response y(t) (Step Input)');
xlabel('Time (s)');
ylabel('Output y(t)');
legend('Analytic y(t)');
grid on;
disp(' ');
disp('Steady-State Values:');
disp(['x1(?) = ' char(ss x1)]);
disp(['x2(?) = ' char(ss x2)]);
disp(['y(?) = ' char(ss y)]);
```

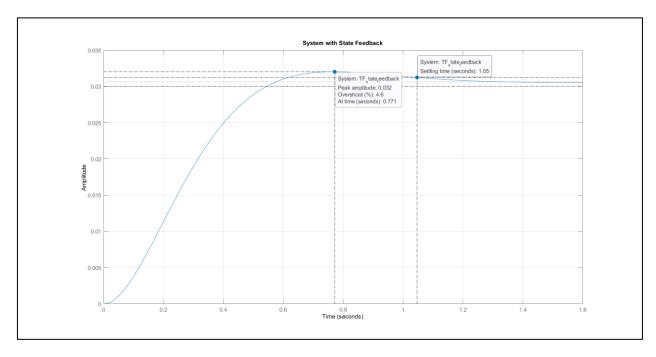


```
=== Forced Response Analysis ===
Forced state solution (from step input):
/\exp(-3 t) \exp(-2 t) 1
|-----+-|
| 3 2 6|
\setminus exp(-2 t) - exp(-3 t) /
Total state solution (unforced + forced):
/ \exp(-2 t) \exp(-3 t) 2 1
|-----+-|
| 2 3 6|
\langle \exp(-3 t) 2 - \exp(-2 t) \rangle
Steady-State Values:
x1(\infty) = 1/6
x2(\infty) = 0
```

 $y(\infty) = 1/6$ 

```
% Q8: State Feedback Design
disp('=== State Feedback Design ===');
% Original system step response
figure;
step(TF builtin);
title('Original System Step Response');
grid on;
% Design specifications
zeta_desired = 0.7; % Desired damping ratio
ts desired = 1;
                         % Desired settling time (sec)
% Hand analysis to determine desired poles
wn = 4/(zeta_desired*ts_desired); % Natural frequency from settling time
sigma = zeta desired*wn;
                                   % Real part of poles
                                 % Imaginary part
wd = wn*sqrt(1-zeta desired^2);
\mbox{\ensuremath{\upsigma}} Desired characteristic polynomial
desired poly = (s + sigma + 1i*wd)*(s + sigma - 1i*wd);
desired poly = expand(desired_poly);
% Convert to numerical polynomial
desired coeffs = sym2poly(desired poly);
% Hand calculation of K matrix
% Characteristic polynomial of A-BK: s^2 + (5+K2)s + (6+K1)
% Compare with desired polynomial: s^2 + 2*zeta*wn*s + wn^2
K1 = desired coeffs(3) - 6; % From constant term
K2 = desired_coeffs(2) - 5; % From s term
K = [K1 \ K2];
disp('Desired closed-loop poles:');
disp([-sigma+li*wd, -sigma-li*wd]);
disp('Feedback gain matarix K:');
disp(K);
% Verification
Ac = A - B*K;
[num_2, denum_2] = ss2tf(Ac,B,C,D);
TF state feedback = tf(num_2, denum_2);
% Step response analysis
figure;
step info = stepinfo(TF state feedback);
step (TF state feedback);
title('System with State Feedback');
grid on;
disp('Closed-loop system performance:');
disp(['Settling Time: ', num2str(step info.SettlingTime), ' sec']);
disp(['Overshoot: ', num2str(step info.Overshoot), '%']);
```





=== State Feedback Design ===

Desired closed-loop poles:

 $-4.0000 + 4.0808i \ -4.0000 - 4.0808i$ 

Feedback gain matrix K:

26.6531 3.0000

Closed-loop system performance:

Settling Time: 1.0463 sec

Overshoot: 4.5986%

#### **Appendix**

#### **Bode Plot Code:**

```
clc;
clear;
close all;
%----- Define G(s) and H(s)
% Define the open-loop transfer function G(s)
num G = 1;
den G = [1 \ 1 \ 0]; % s(s+1) = s^2 + s
% Define the feedback transfer function H(s)
num H = [1];
den H = [1]; % Unity Feedback
[G S, H S] = create system(num G, den G, num H, den H)
\mbox{\ensuremath{\$-----}}\mbox{\ensuremath{$Q$}}\mbox{\ensuremath{$------}}\mbox{\ensuremath{$Q$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(S)$}}\mbox{\ensuremath{$(
% Plot step response of G(s)
draw_step(G_S, 'Open-Loop System G(s)');
%-----Q3----- Closed-Loop Analysis
disp('Closed-Loop TF using feedback():');
T feedback = feedback(G S, H S)
disp('Closed-Loop TF using manual formula (G/(1+GH)):');
T manual = (1 / (1 + G S * H S)) * G S; % Equivalent to T(s) = G/(1+GH)
                                                                                            % Cancel common terms
T manual = minreal(T manual)
\mbox{\$-------Q4------} Step Response of T(s) (Closed-Loop)
% Plot step response of T(s)
draw step(T feedback, 'Closed-Loop System T(s)');
%-----Q5----- locations of the poles
draw poles(T feedback);
%----- Ramp Response
[ess, r_t_out, r_y_out] = draw ramp(T feedback, 700+200, 700);
%----- Frequency Response
[Gm, Pm, Wgc, Wpc] = draw Bode Plot(G S*H S);
%-----Functions-----
function [G S, H S] = create system(num G, den G, num H, den H)
% CREATE SYSTEM Creates open-loop and feedback transfer functions
        [G_S, H_S] = create_system(num_G, den_G, num_H, den_H)
응
용
       Inputs:
            num G - Numerator coefficients of G(s)
                den G - Denominator coefficients of G(s)
                num H - Numerator coefficients of H(s) (default: 1)
                den H - Denominator coefficients of H(s) (default: 1)
응
% Outputs:
             G S - Open-loop transfer function
                H S - Feedback transfer function
        % Set default unity feedback if not specified
        if nargin < 3</pre>
```

```
num H = 1;
        den H = 1;
    end
    % Create transfer functions
    G S = tf(num G, den G)
    H S = tf(num H, den H)
end
function [wn, zeta, response info] = draw step(sys, sys name)
% DRAW STEP Plots step response and returns key performance metrics
    [response info] = draw step(sys, sys name)
응
응
   Inputs:
       sys - Transfer function (tf object)
응
        sys name - Name of the system for title (string)
응
용
  Outputs:
용
       response info - Structure containing:
응
            .poles - System poles
응
            .stability - Stability classification
응
            .peak response - Peak response value and time
응
            .settling time - Time to settle within 2% of final value
응
            .rise time - 10-90% rise time
            .steady state - Final steady-state value
        Figure with step response
    % Create figure
    figure;
    % Get step response data
    [y, t] = step(sys);
    % Plot step response
    step(sys);
    title(['Step Response of ', sys name]);
    grid on;
    % Calculate response characteristics
    response info = struct();
    response info.poles = pole(sys);
    % Stability determination
    if all(real(response info.poles) < 0)</pre>
        response info.stability = 'stable (all poles in LHP)';
    elseif any(real(response info.poles) > 0)
        response info.stability = 'unstable (at least one pole in RHP)';
    else
        response_info.stability = 'marginally stable (poles on imaginary
axis)';
   end
    % Peak response (overshoot)
    [response_info.peak_response.value, peak_idx] = max(y);
    response_info.peak_response.time = t(peak_idx);
    % Steady-state value (last 10% of response)
    steady state val = mean(y(end-round(length(y)*0.1):end));
    response info.steady state = steady state val;
    % Settling time (within 2% of steady-state)
```

```
settled idx = find(abs(y - steady state val) > 0.02*steady state val, 1,
'last');
    if isempty(settled idx)
        response info.settling time = 0;
        response info.settling time = t(settled idx);
    end
    % Rise time (10% to 90% of steady-state)
    rise start = find(y \ge 0.1*steady state val, 1);
    rise end = find(y >= 0.9*steady state val, 1);
    if ~isempty(rise start) && ~isempty(rise end)
        response info.rise time = t(rise end) - t(rise start);
    else
        response info.rise time = NaN;
    end
    % Display results in command window
    disp(['System: ', sys_name]);
disp(['Poles: ', num2str(response_info.poles')]);
    disp(['Stability: ', response info.stability]);
    disp(['Over shoot MP: ', num2str(100*(response_info.peak_response.value-
1)), ...
          '% at t = ', num2str(response info.peak response.time), ' sec']);
    % Damping characteristics (for complex poles)
    if ~isreal(response info.poles)
        [wn, zeta] = damp(sys);
        fprintf('Damping ratio (?): %.3f\n', zeta(1));
        fprintf('Natural frequency (?n): %.3f rad/s\n', wn(1));
    end
    disp(['Settling time (2%): ', num2str(response info.settling time), '
sec']);
    disp(['Rise time (10-90%): ', num2str(response info.rise time), ' sec']);
    disp(['Steady-state value: ', num2str(response_info.steady_state)]);
end
function [poles] = draw poles(sys)
% DRAW POLES Plots pole-zero map and returns system poles
    [poles] = draw poles(sys)
응
응
   Input:
응
      sys - Transfer function (tf object) or state-space model
응
응
      poles - Array of system poles
응
응
  Displays:
응
    - Pole-zero plot
9
       - Pole locations in command window
       - Stability information
    % Create figure
    figure;
    % Plot pole-zero map
    pzmap(sys);
    title(['Pole-Zero Map of: ' inputname(1)]);
    grid on;
    % Get poles
```

```
poles = pole(sys);
    % Display poles
    disp(['Poles of ' inputname(1) ':']);
    disp(poles);
    % Damping characteristics (for complex poles)
    if ~isreal(poles)
        [wn, zeta] = damp(sys);
        fprintf('Damping ratio (?): %.3f\n', zeta(1));
        fprintf('Natural frequency (?n): %.3f rad/s\n', wn(1));
    end
end
function [ess, t out, y out] = draw ramp(sys, t end, zoom time)
% DRAW RAMP Plots ramp response in three subplots
    [ess, t_out, y_out] = draw_ramp(sys, t_end, zoom_time)
응
응
    Inputs:
응
      sys - Closed-loop transfer function (tf object)
응
       t end - End time for simulation (default: 100 sec)
응
       zoom time - Time to zoom in (default: 700 sec)
응
응
  Outputs:
응
      ess - Steady-state error
       t_out - Time vector
응
응
       y out - System response vector
용
응
  Generates figure with three subplots:
       1. Ideal ramp input
응
        2. System response
응
        3. Zoomed comparison at specified time
    % Set defaults if not provided
    if nargin < 2
        t end = 100;
    end
    if nargin < 3</pre>
        zoom time = 700;
    end
    % Create time vector
    t = 0:0.1:t end;
    %getting the ramp
    ramp = tf(1,[1 \ 0]);
    % Get response data
    [y sys, t sys] = step(sys.*ramp, t);
    [y ideal, t ideal] = step(ramp, t);
    % Create figure with three subplots
    figure;
    % Subplot 1: Ideal ramp input
    subplot(2,1,1);
    plot(t_ideal, y_ideal, 'b');
    hold on;
    plot(t_sys, y_sys, 'r--');
```

```
title('Ramp Response');
    xlabel('Time (sec)');
    ylabel('Amplitude');
    legend('Ideal', 'System', 'Location', 'northwest');
    grid on;
    hold off;
    % Subplot 2: Zoomed comparison
    subplot(2,1,2);
    plot(t ideal, y ideal, 'b');
    hold on;
    plot(t sys, y sys, 'r--');
    xlim([zoom time-50 zoom time+50]);
    title(['Zoomed Comparison at t = ', num2str(zoom time), ' sec']);
    xlabel('Time (sec)');
    ylabel('Amplitude');
    legend('Ideal', 'System', 'Location', 'northwest');
    grid on;
    hold off;
    % Calculate steady-state error (use last 10% of simulation)
    final idx = round(0.9*length(t sys)):length(t sys);
    ess = mean(y ideal(final_idx) - y_sys(final_idx));
    % Display results
    disp(['Steady-state error (ess): ', num2str(ess)]);
    % Return output data if requested
    if nargout > 1
        t out = t sys;
        y_out = y_sys;
    end
end
function [Gm, Pm, Wgc, Wpc] = draw_Bode_Plot(sys)
% BODE PLOT Analyzes system stability margins and compares margin()
   Bode Plot(sys)
용
응
   Input:
용
    sys - Transfer function (tf object or state-space model)
응
   Outputs:
       Gm - Gain margin (dB)
응
       Pm - Phase margin (degrees)
응
       Wgc - Gain crossover frequency (rad/sec)
        Wpc - Phase crossover frequency (rad/sec)
    % Create margin plot
    figure;
    margin(sys);
    grid on;
    % Get stability margins
    [Gm, Pm, Wgc, Wpc] = margin(sys);
    % Display results
    disp(['=== Stability Margins for ' inputname(1) ' ===']);
    disp(['Gain Margin: ', num2str(Gm), ' dB at ', num2str(Wgc), ' rad/s']);
    disp(['Phase Margin: ', num2str(Pm), '° at ', num2str(Wpc), ' rad/s']);
```

#### State Space Code::

```
clc
clear all
close all
% Given system matrices
A = [0 1; -6 -5];
B = [0; 1];
C = [1 \ 0];
D = [0];
n = 2;
                    % System order
sys = ss(A,B,C,D); % State Space model
                   % Initial condition
x0 = [0; 1];
% Q2: Transfer function conversion
[num, den] = ss2tf(A,B,C,D);
syms s
TF Manual = C*inv(s*eye(n)-A)*B + D
TF builtin = tf(num, den)
% Q3: State transition matrix calculation
% Compute ?(s) = [sI - A]^{-1}
Phi s = inv(s*eye(n) - A);
% Compute ?(t) by inverse Laplace transform
syms t
Phi t = ilaplace(Phi s);
% Verify ?(0) = I
Phi 0 = subs(Phi t, t, 0);
% Display results
disp('State transition matrix in s-domain (?(s)):');
pretty(Phi s)
disp('State transition matrix in time domain (?(t)):');
pretty(Phi t)
disp('Verification of ?(0) = I:');
disp(Phi 0);
% Q4: Verify that ??(t) = A?(t)
Phi dot = diff(Phi t, t); % Take time derivative of ?(t)
                         % Multiply A with ?(t)
A Phi = A*Phi t;
disp('Time derivative of state transition matrix (??(t)):');
pretty(Phi dot)
disp('A*?(t):');
pretty(A Phi)
disp('Verification successful: ??(t) = A?(t)');
% Q5 Check Controllability and Observability
% Check Controllability
Co = ctrb(A, B); % Controllability matrix
rank Co = rank(Co);
```

```
disp('Controllability Matrix:');
disp(Co);
disp(['Rank of Controllability Matrix: ', num2str(rank Co)]);
if rank Co == n
    disp('System is Controllable (as expected)');
    disp('System is Not Controllable (unexpected for this system)');
end
% Check Observability
Ob = obsv(A, C); % Observability matrix
rank Ob = rank(Ob);
disp('Observability Matrix:');
disp(Ob);
disp(['Rank of Observability Matrix: ', num2str(rank Ob)]);
if rank Ob == n
    disp('System is Observable (as expected)');
else
    disp('System is Not Observable (unexpected for this system)');
end
% Q6: Unforced (Homogeneous) Response
disp('=== Unforced Response Analysis ===');
% Compute state solution x(t) = ?(t) *x0
x t = Phi t * x0;
disp('Unforced state solution x(t):');
pretty(x t)
% Compute output solution y(t) = C*x(t) + D*u(t)
% Since u(t)=0 for unforced response:
y_t = C*x_t + D*0;
disp('Unforced output response y(t):');
pretty(y_t)
% Plot the results
t vals = linspace(0, 5, 500); % Time vector from 0 to 5 seconds
% Convert symbolic expressions to numeric functions
x1 \text{ func} = \text{matlabFunction}(x t(1));
x2 func = matlabFunction(x t(2));
y func = matlabFunction(y t);
% Evaluate solutions
x1 vals = arrayfun(x1 func, t vals);
x2 \text{ vals} = \operatorname{arrayfun}(x2 \text{ func, t vals});
y vals = arrayfun(y func, t vals);
% Plot state responses
figure;
subplot(2,1,1);
plot(t_vals, x1_vals, 'b', 'LineWidth', 2);
hold on;
plot(t vals, x2 vals, 'r--', 'LineWidth', 2);
title('Unforced State Response');
xlabel('Time (s)');
ylabel('State Values');
```

```
legend('x_1(t)', 'x_2(t)');
grid on;
% Plot output response
subplot(2,1,2);
plot(t vals, y vals, 'm', 'LineWidth', 2);
title('Unforced Output Response y(t)');
xlabel('Time (s)');
ylabel('Output y(t)');
grid on;
% Compare with MATLAB's built-in initial() function
[\sim, t \text{ num}, x \text{ num}] = initial(sys, x0, t vals(end));
y num = x num*C'; % Equivalent to C*x since D=0
% Display symbolic solutions
disp(' ');
disp('Analytic Solutions:');
disp('x1(t) = '); pretty(x t(1))
disp('x2(t) = '); pretty(x_t(2))
disp('y(t) = '); pretty(y_t)
% Q7: Forced Response Analysis (Unit Step Input)
disp('=== Forced Response Analysis ===');
% Using Frequency Domain Approach
U s = 1/s; % Laplace transform of unit step
U t =ilaplace(U_s);
% Compute forced component in frequency domain
X forced s = Phi s * B * U s;
% Convert to time domain
x forced t = ilaplace(X forced s);
% Total solution (homogeneous + forced)
x total t = x t + x forced t;
% Output solution
y total t = C*x total t + D*U t; % D*u(t) where u(t)=1 for t>0
disp('Forced state solution (from step input):');
pretty(x forced t)
disp('Total state solution (unforced + forced):');
pretty(x total t)
% Direct evaluation using subs()
x1 \text{ vals} = \text{double(subs(x total t(1), t, t vals));}
x2 \text{ vals} = \text{double(subs(x total t(2), t, t vals));}
y vals = double(subs(y total t, t, t vals));
% Plot results
figure;
% State responses
subplot(2,1,1);
plot(t vals, x1 vals, 'b', 'LineWidth', 2);
hold on;
plot(t vals, x2 vals, 'r--', 'LineWidth', 2);
title('Total State Response (Step Input)');
```

```
xlabel('Time (s)');
ylabel('State Values');
legend('Analytic x 1(t)', 'Analytic x 2(t)');
grid on;
% Output response
subplot(2,1,2);
plot(t vals, y vals, 'm', 'LineWidth', 2);
hold on;
title('Total Output Response y(t) (Step Input)');
xlabel('Time (s)');
ylabel('Output y(t)');
legend('Analytic y(t)');
grid on;
% Display final steady-state values
ss x1 = limit(x total t(1), t, inf);
ss x2 = limit(x total t(2), t, inf);
ss_y = limit(y_total_t, t, inf);
disp(' ');
disp('Steady-State Values:');
disp(['x1(?) = ' char(ss x1)]);
disp(['x2(?) = ' char(ss x2)]);
disp(['y(?) = ' char(ss y)]);
% Q8: State Feedback Design
disp('=== State Feedback Design ===');
% Original system step response
figure;
step(TF builtin);
title('Original System Step Response');
grid on;
% Design specifications
zeta_desired = 0.7; % Desired damping ratio
ts desired = 1;
                       % Desired settling time (sec)
% Hand analysis to determine desired poles
wn = 4/(zeta desired*ts desired); % Natural frequency from settling time
                             % Real part of poles
sigma = zeta desired*wn;
wd = wn*sqrt(1-zeta desired^2); % Imaginary part
% Desired characteristic polynomial
desired_poly = (s + sigma + 1i*wd)*(s + sigma - 1i*wd);
desired poly = expand(desired poly);
% Convert to numerical polynomial
desired coeffs = sym2poly(desired poly);
% Hand calculation of K matrix
% Characteristic polynomial of A-BK: s^2 + (5+K2)s + (6+K1)
% Compare with desired polynomial: s^2 + 2*zeta*wn*s + wn^2
K1 = desired coeffs(3) - 6; % From constant term
K2 = desired coeffs(2) - 5; % From s term
K = [K1 \ K2];
disp('Desired closed-loop poles:');
```

```
disp([-sigma+li*wd, -sigma-li*wd]);
disp('Feedback gain matrix K:');
disp(K);
% Verification
Ac = A - B*K;
[num_2, denum_2] = ss2tf(Ac,B,C,D);
TF_state_feedback = tf(num_2, denum_2);
% Step response analysis
figure;
step_info = stepinfo(TF_state_feedback);
step(TF_state_feedback);
title('System with State Feedback');
grid on;
disp('Closed-loop system performance:');
disp(['Settling Time: ', num2str(step_info.SettlingTime), ' sec']);
disp(['Overshoot: ', num2str(step_info.Overshoot), '%']);
```