

$$\Psi_{y\hat{r}} = \hat{a}_r \cdot \hat{a}_y = \sin \theta \sin \phi$$

$$\Psi_{-\hat{x}\hat{r}} = \hat{a}_r \cdot (-i)\hat{a}_x = -\cos \theta \sin \phi$$

$$\Psi_{-\hat{y}\hat{r}} = \hat{a}_r \cdot (-i)\hat{a}_y = -\sin \theta \sin \phi$$

$$\Psi_{\hat{x}\hat{r}} = \hat{a}_r \cdot \hat{a}_x = \cos \theta \sin \phi$$

$$(a) s = \lambda/2 \rightarrow ks = \frac{2\pi}{\lambda} \cdot \frac{\lambda}{2} = \pi \quad kI = \frac{2\pi}{\lambda} \cdot \frac{\lambda}{4} = \pi/2$$

$$AF = -e^{j\pi \cos \theta \sin \phi} - e^{-j\pi \cos \theta \sin \phi} + e^{j\pi \sin \theta \sin \phi} + e^{-j\pi \sin \theta \sin \phi}$$

$$AF = -2 \cos(\pi \cos \theta \sin \phi) + 2 \cos(\pi \sin \theta \sin \phi)$$

$$E_{\text{dipole}}(\theta, \phi) = C [(\cos(\pi/2 \cos \theta) - \cos(\pi/2)) / \sin \theta]$$

$$E_t(\theta, \phi) = \frac{j\eta I_0 e^{jkr}}{2\pi r} \left(\frac{\cos(\pi/2 \cos \theta)}{\sin \theta} \right) (\cos(\pi \sin \theta \sin \phi) - \cos(\pi \cos \theta \sin \phi))$$

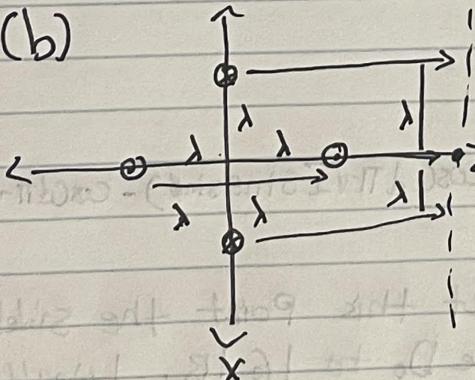
E-Plane: xz H-Plane: $xy \rightarrow$ E-Plane: $\phi=0, \theta=[0, \pi]$ H-Plane: $\theta=[0, 2\pi], \phi=90^\circ$

$$P_{\text{rad}} = \frac{1}{2} \rho R^2 \{E \times H^*\} \cdot \hat{a}_r f \sin \theta d\theta d\phi \approx 52.9565$$

$$U_{\text{max}} = \pi/2$$

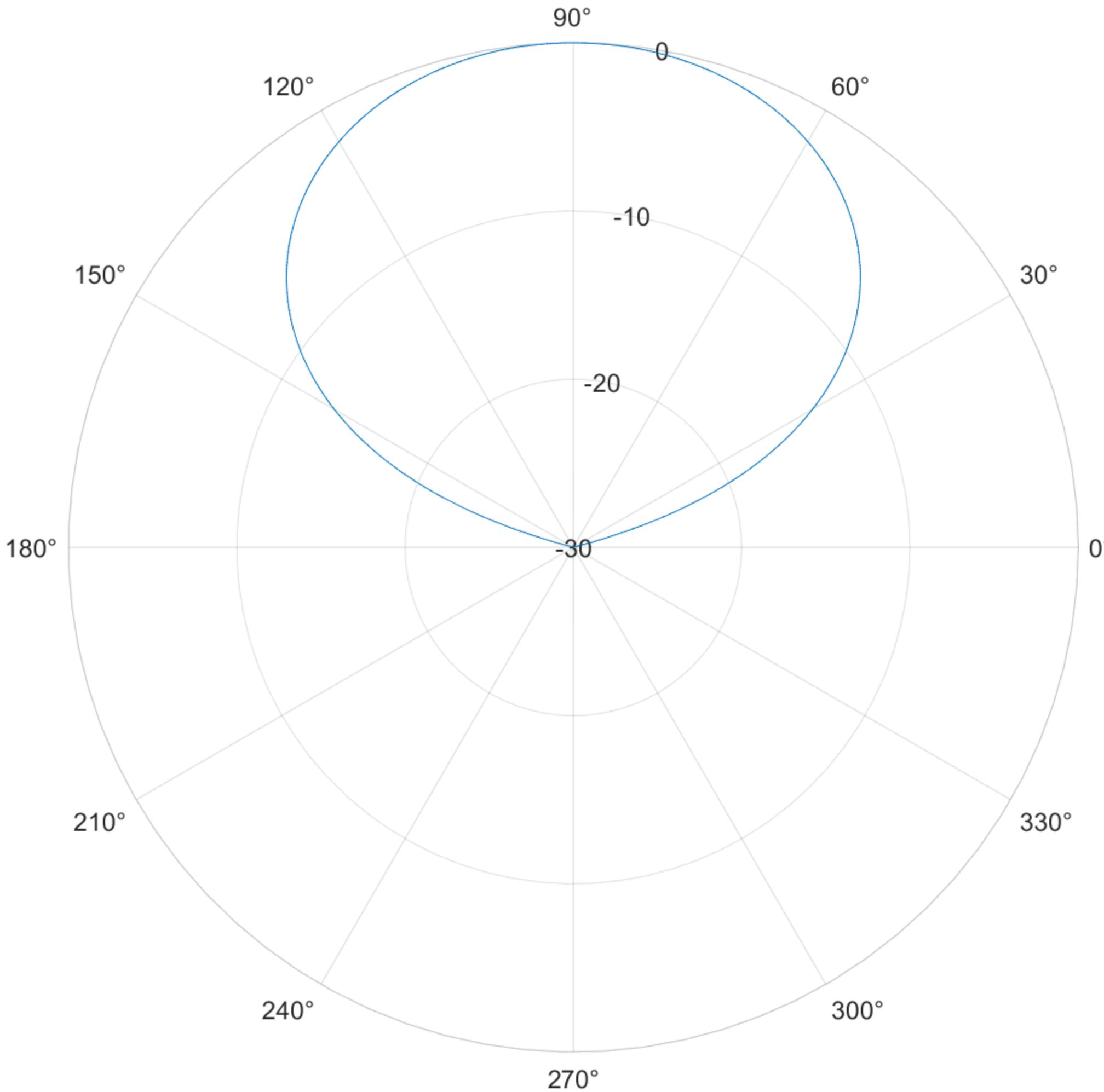
$$D_0 = \frac{4\pi U_{\text{max}}}{P_{\text{rad}}} \approx \frac{4\pi(\pi/2)}{52.9565} = 3.7967 \quad D_0(\text{dB}) = 5.79 \text{ dB}$$

(b)

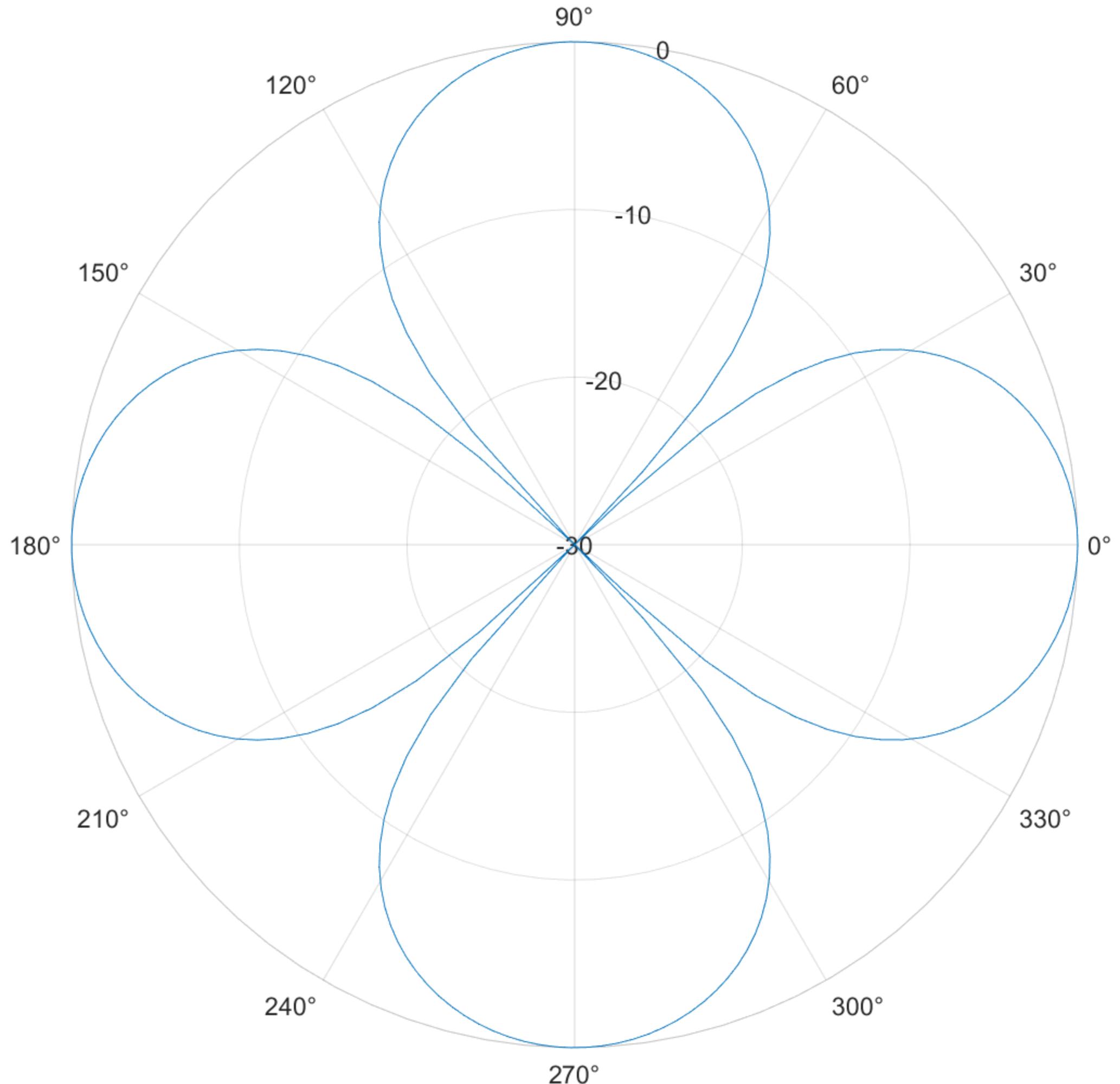


The array factor is equal 0 when $y=0$ therefore there is no radiation. This is because in the far field, the plane waves radiated by the source and the images have a path phase difference due to the spacing factor, s ($s=\lambda$), which results in a 360° phase shift for all 3 images when $y=0$ (or $x=0$). Since two of the images have opposing magnitude to the other two sources, they will destructively interfere at this point.

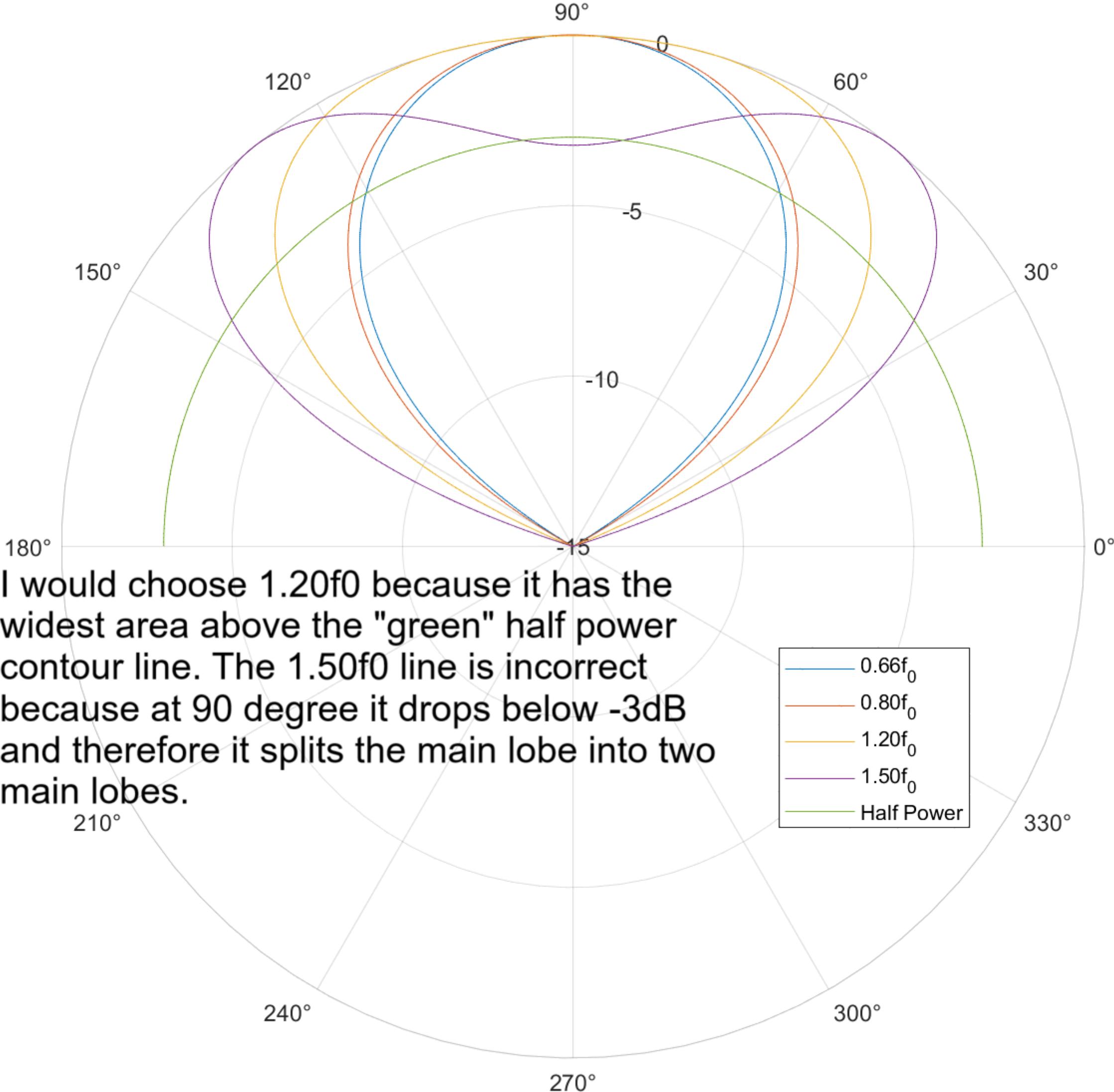
Question 1, Part A) E-Plane, phi=0, theta=[0, pi]



Question 1, Part A) H-Plane, phi=[0, 2pi] theta=pi/2



Varying Spacing Factor, s, Effect on Beamwidth; E-Plane(s), phi=0, theta=[0, pi]



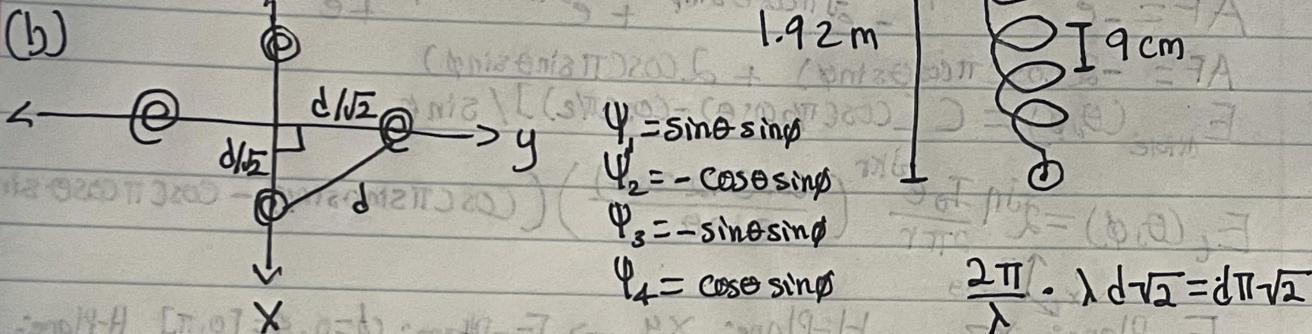
$$\textcircled{2} \quad \lambda_0 = \frac{3 \times 10^8}{800 \text{ MHz}} = 37.5 \text{ cm}$$

$$(a) \quad C = \lambda \quad d = 13.5 \quad S = C \tan(\alpha) = 9 \text{ cm} \quad N = 5$$

$$D_0 = 10 \log_{10} \left[15N \frac{C^2 S}{\lambda^3} \right] = 12.55 \text{ dB}$$

$$L_0 = N \sqrt{C^2 + S^2} = 1.92 \text{ m} \quad \text{HPBW} = \frac{52 \lambda^{3/2}}{C \sqrt{N} S} \quad 37.5 \text{ cm}$$

$$R_r = 140 \Omega$$



$$AF = 2 \left[\cos(d\pi\sqrt{2} \sin \theta \sin \phi) - \cos(d\pi\sqrt{2} \cos \theta \sin \phi) \right]$$

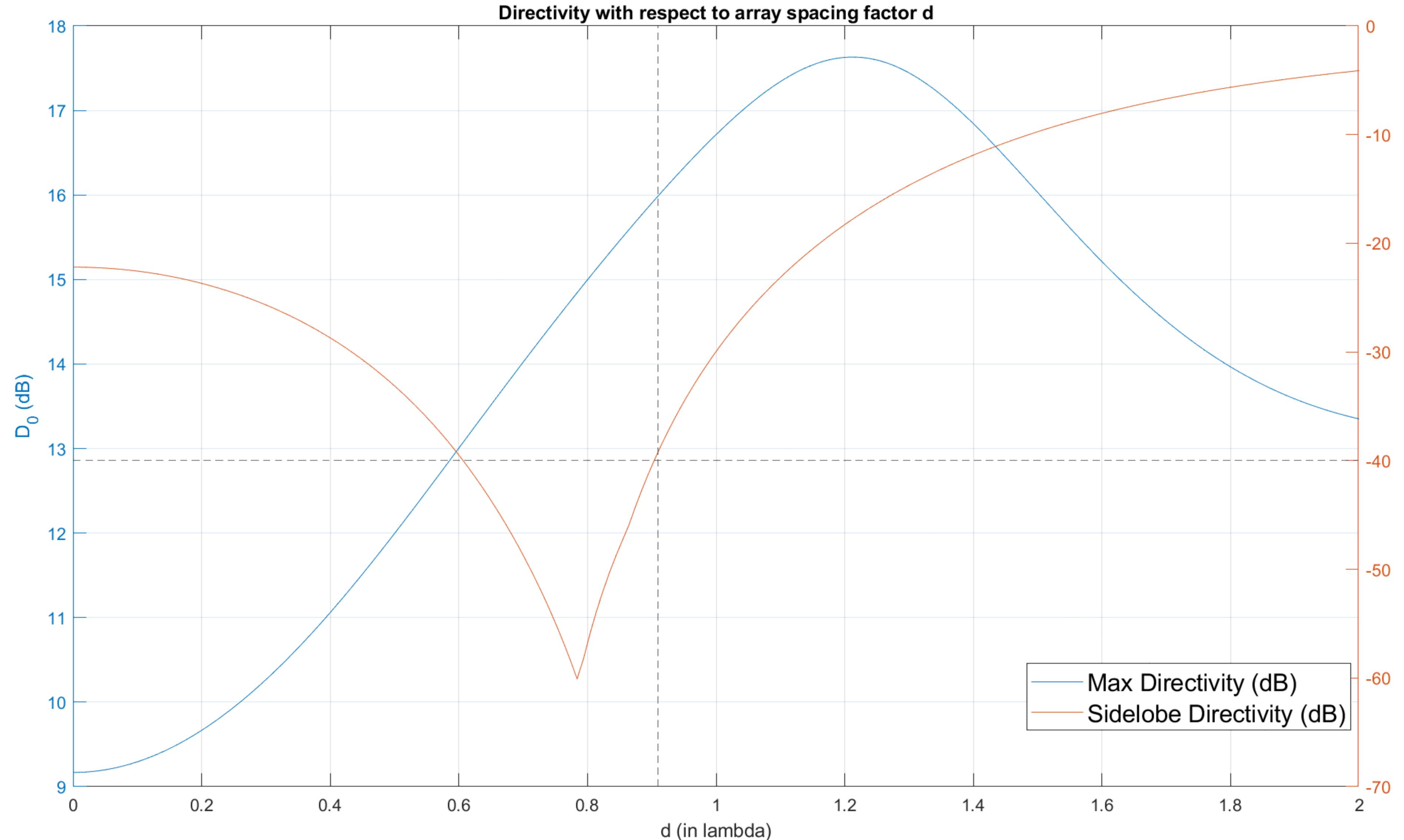
Element factor:

$$\Psi = k_0 (S \cos \theta - \frac{L_0}{\rho}) = 1.508 \cos(\theta) - 7.792$$

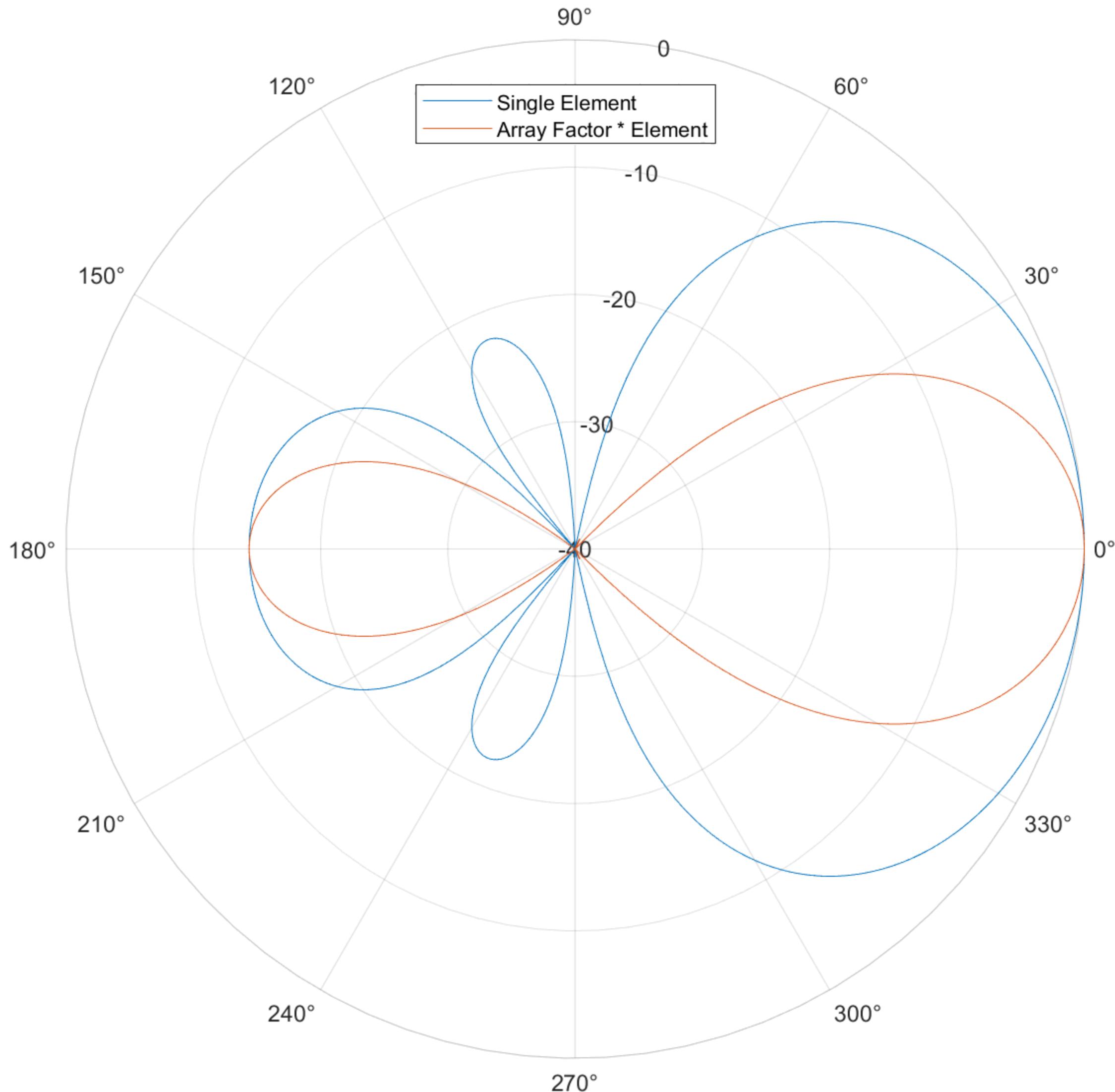
$$\rho = \frac{L_0 / \lambda_0}{S / \lambda_0 + 1} = 0.8293$$

$$E_t(\theta, \phi) = 2 \sin\left(\frac{\pi}{2N}\right) \cos \theta \frac{\sin(N/2)\Psi}{\sin(\Psi/2)} \left[\cos(d\pi\sqrt{2} \sin \theta \sin \phi) - \cos(d\pi\sqrt{2} \cos \theta \sin \phi) \right]$$

I would choose $d = 0.91\lambda$ because at this point the sidelobe level is -40 dB while increasing the D_0 to 16 dB . I would not choose $d = 1.2\lambda$ because it introduces grating lobes.



Radiation Pattern of Single Element vs Array System



(3)

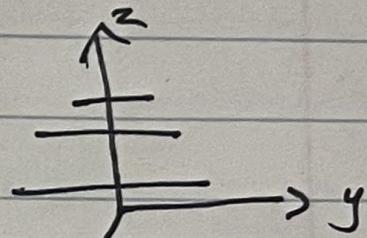
$$AF = 0.9e^{-j0.4\pi + \gamma} + 1 \text{ for } e^{j0.6\pi \cos\theta + \alpha} + 0.5e^{j\pi \cos\theta + \beta}$$

$$\alpha = -0.6\pi \quad \beta = -\pi \quad \gamma = 0.4\pi$$

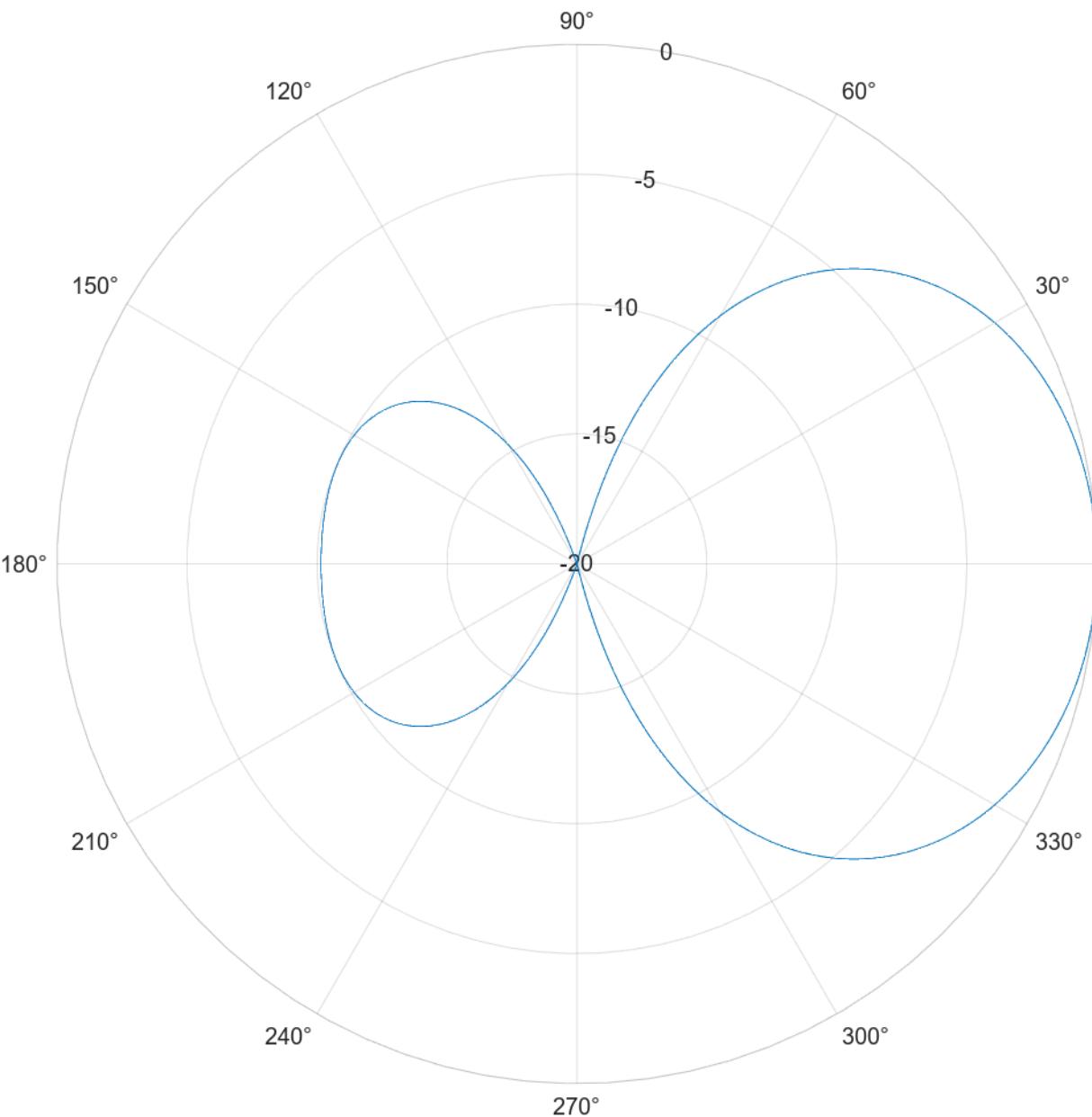
Element factor = $\cos\theta$

$$D_0 = 6.4 \Rightarrow D_0(\text{dB}) = 8.1 \text{ dB} \quad \text{Front-to-back ratio} = 10.4$$

E-Plane: xy Plane H-Plane: xz Plane



E Plane Radiation Pattern $D_0 = 6.42$ --- $D_0(\text{dB}) = 8.07$



H-Plane Radiation Pattern $D_0 = 6.42$ --- $D_0(\text{dB}) = 8.07$

