

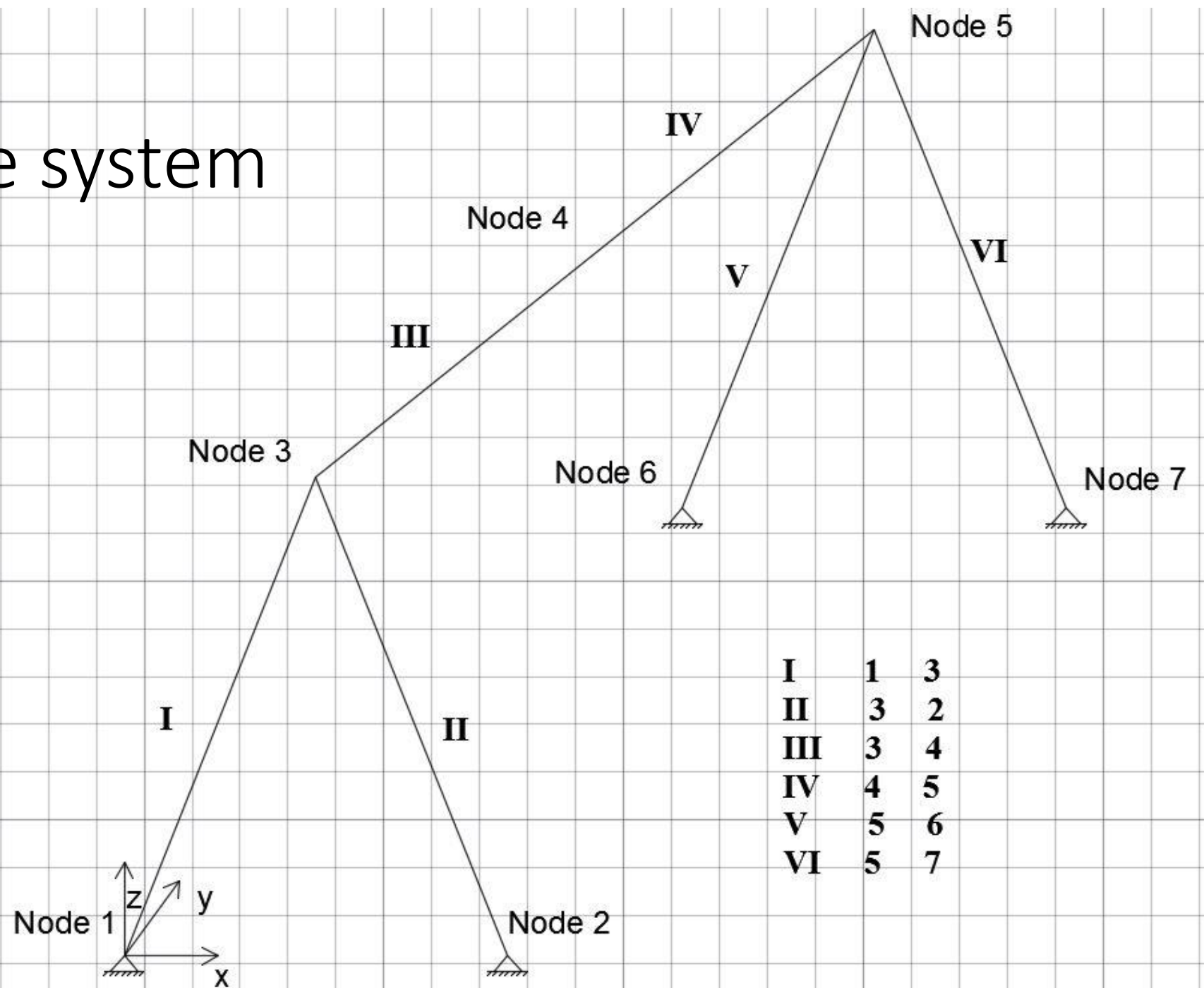
# Final Project

ECI211 Fall 2015

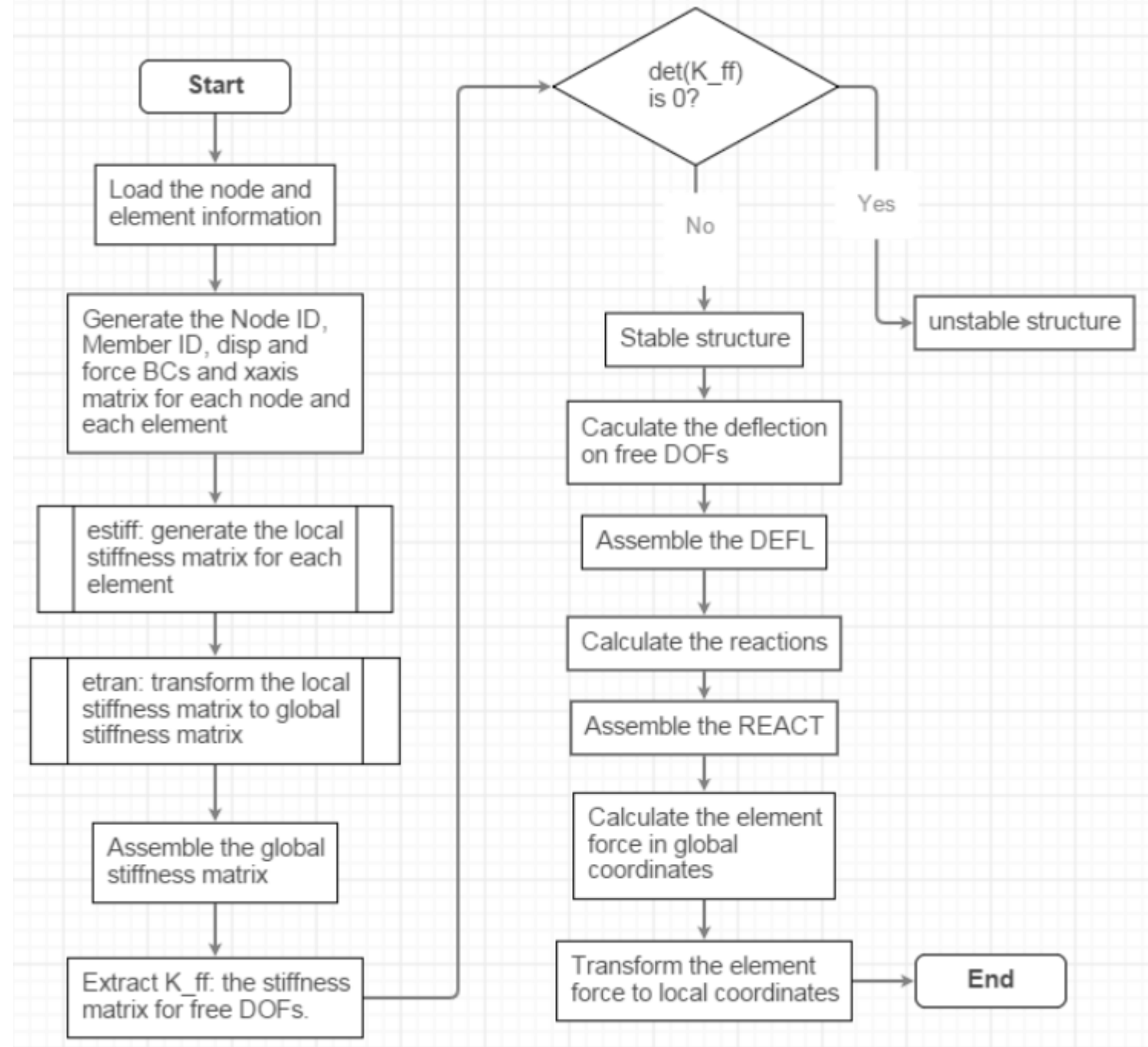
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My global  
coordinate system



# My flowchart



# Load the node and element information

- % load the input information.
- load nnodes.txt;
- load coord.txt;
- load concen.txt;
- load fixity.txt;
- load nele.txt;
- load ends.txt;
- load Area.txt;
- load lzz.txt;
- load lyy.txt;
- load J.txt;
- load E.txt;
- load v.txt;
- load beta\_ang.txt;

Generate the node id.

Each line represents the 6 DOFs for one node.

- `node_id=zeros(nnodes,6);`
- `for i=1:nnodes`
- `for j=1:6`
- `node_id(i,j)=(i-1)*6+j;`
- `end`
- `end`

1	2	3	4	5	6
7	8	9	10	11	12
13	14	15	16	17	18
19	20	21	22	23	24
25	26	27	28	29	30
31	32	33	34	35	36
37	38	39	40	41	42

# Generate the member id.

Each line represents the 12 DOFs for one element.

- `mem_id=zeros(nele,12);`
- `for i=1:nele`
- `mem_id(i,1:6)=node_id(ends(i,1),1:6);`
- `mem_id(i,7:12)=node_id(ends(i,2),1:6);`
- `end`

1	2	3	4	5	6	13	14	15	16	17	18
13	14	15	16	17	18	7	8	9	10	11	12
13	14	15	16	17	18	19	20	21	22	23	24
19	20	21	22	23	24	25	26	27	28	29	30
25	26	27	28	29	30	31	32	33	34	35	36
25	26	27	28	29	30	37	38	39	40	41	42

Generate the displacement boundary conditions.  
 Each line in fixity represents the disp BC on 6 DOFs of one node.  
0 represents that the DOF is fixed.  
NaN represents that the DOF is free.

- fixity\_tran=fixity';
- D=fixity\_tran(:);
- free\_dof=find(isnan(D));
- fixed\_dof=find(D==0);

0	0	0	NaN	NaN	NaN
0	0	0	NaN	NaN	NaN
NaN	NaN	NaN	NaN	NaN	NaN
NaN	NaN	NaN	NaN	NaN	NaN
NaN	NaN	NaN	NaN	NaN	NaN
0	0	0	NaN	NaN	NaN
0	0	0	NaN	NaN	NaN

1 2 3 7 8 9 31 32 33 37 38 39

4 5 6 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 34  
 35 36 40 41 42

Generate the force boundary conditions.

Each line in concen represents the force BC on 6 DOFs of one node.

0 represents that the DOF does not has external force.

The number represnts that the force values on the DOF.

- concen\_tran=concen';
- P\_total=concen\_tran(:);
- 
- P\_free=P\_total(free\_dof);

0	0	0	0	0	0
0	0	0	0	0	0
0	0	0	0	0	0
0	0	-4.5	0	0	0
0	0	0	0	0	0
0	0	0	0	0	0
0	0	0	0	0	0



Generate the xaxis.

xaxis will be used in the rotation matrix.

The rotation matrix is to transform the stiffness matrix from global to local coordinate system.

- for i=1:nele
- xaxis(i,:)=(coord(ends(i,2),:)-coord(ends(i,1),:));
- Length(i) = norm(xaxis(i,:));
- xaxisunit(i,:)=xaxis(i,:)/Length(i) ;
- end

0.3713	0	0.9284
0.3713	0	-0.9284
0.0000	1	0.0000
0.0000	1	0.0000
-0.3713	0	-0.9284
0.3713	0	-0.9284

# Generate the local stiffness matrix for each element.

- `k_stack_local=zeros(nele,12,12);`
- `gamma_stack_local=zeros(nele,12,12);`
- `for i=1:nele`
  - `k_stack_local(i,:,:) = estiff(Area(i),lzz(i),lyy(i),J(i),E(i),v(i),Length(i));`
  - `gamma_stack_local(i,:,:) = etran(beta_ang(i),xaxisunit(i,1:3));`
- `end`

# Transform the local stiffness matrix to global stiffness matrix.

- `k_stack_global=zeros(nele,12,12);`
- `for i=1:nele`
- `k_stack_global(i,:,:)=(squeeze(gamma_stack_local(i,:,:))' )...`
- `*squeeze(k_stack_local(i,:,:))...`
- `*squeeze(gamma_stack_local(i,:,:));`
- `end`

```
size(squeeze(k_stack_local(i,:,:)))  
12  12  
size(k_stack_local(i,:,:))  
1  12  12
```

# Assemble the global stiffness matrix together.

- `ndof=6*nnodes;`
- `k_total=zeros(ndof,ndof);`
- `for i=1:nele`
- `k_total(mem_id(i,1:6),mem_id(i,1:6))=k_total(mem_id(i,1:6),mem_id(i,1:6))+squeeze(k_stack_global(i,1:6,1:6));`
- `k_total(mem_id(i,1:6),mem_id(i,7:12))=k_total(mem_id(i,1:6),mem_id(i,7:12))+squeeze(k_stack_global(i,1:6,7:12));`
- `k_total(mem_id(i,7:12),mem_id(i,1:6))=k_total(mem_id(i,7:12),mem_id(i,1:6))+squeeze(k_stack_global(i,7:12,1:6));`
- `k_total(mem_id(i,7:12),mem_id(i,7:12))= k_total(mem_id(i,7:12),mem_id(i,7:12))+squeeze(k_stack_global(i,7:12,7:12));`
- `end`

$$\begin{array}{c}
 \mathbf{K}^{(1)} \qquad \qquad \mathbf{0} \\
 \left[ \begin{array}{cc|cc|cc}
 K_{11} & K_{12} & K_{13} & K_{14} & K_{15} & K_{16} \\
 K_{21} & K_{22} & K_{23} & K_{24} & K_{25} & K_{26} \\
 K_{31} & K_{32} & K_{33} & K_{34} & K_{35} & K_{36} \\
 K_{41} & K_{42} & K_{43} & K_{44} & K_{45} & K_{46} \\
 K_{51} & K_{52} & K_{53} & K_{54} & K_{55} & K_{56} \\
 K_{61} & K_{62} & K_{63} & K_{64} & K_{65} & K_{66}
 \end{array} \right]
 \begin{Bmatrix} d_1 \\ d_2 \\ d_3 \\ d_4 \\ d_5 \\ d_6 \end{Bmatrix} = \begin{Bmatrix} F_1 \\ F_2 \\ F_3 \\ F_4 \\ F_5 \\ F_6 \end{Bmatrix}
 \end{array}$$

$\mathbf{0} \qquad \qquad \mathbf{K}^{(2)}$

# Extract the $K_{ff}$ .

- $K_{ff} = k_{total}(free\_dof, free\_dof);$
- $K_{sf} = k_{total}(fixed\_dof, free\_dof);$

$C = \det(A)$  returns the determinant for  $A$ .  
If the structure is stable,  $\det(A)$  is positive.  
If the structure is unstable,  $\det(A)$  is near 0.

- `if abs(det(K_ff)) < (10^(-15))`
- `AFLAG=0;`
- `display('Unstable Structure.');`
- `display('Maybe you should fix more DOFs .');`
- `else`
- `AFLAG=1;`
- `display('The structure is stable.');`
- `end`

$C = \text{rcond}(A)$  returns the reciprocal condition number of  $A$ .  
If  $A$  is well conditioned,  $\text{rcond}(A)$  is near 1.0.  
If  $A$  is badly conditioned,  $\text{rcond}(A)$  is near 0.

- `if abs(rcond(K_ff)) < (10-15))`
- `BFLAG=0;`
- `display('The matrix is badly conditioned. ');`
- `display('The results may have a large error. ');`
- `display('Some element may have a way bigger stiffness than others.');`
- `display('Maybe you need to check the units of element properties.');`
- `else`
- `BFLAG=1;`
- `display('The matrix is well-conditioned.');`
- `end`

Put the deflection to its appropriate location.  
Include the fixed DOF.

- `defl=K_ff\P_fr`
- `defl_vector_total=zeros(ndof,1);`
- `defl_vector_total(free_dof)=defl;`



Each line in DEFL' represents the 6 DOFs at each node.

- `DEFL=reshape(defl_vector_total,6,nnodes);`
- `DEFL=DEFL';`
- `display(DEFL)`

# Generate the reaction.

- `react=K_sf*defl;`
- `react_vector_total=zeros(ndof,1);`
- `react_vector_total(fixed_dof)=react;`
- `REACT=reshape(react_vector_total,6,nnodes);`
- `REACT=REACT';`
- `display(REACT)`

# Calculate the element force.

## Transform the element from global to local coordinate system.

- `ELE_FOR=zeros(nele,12);`
- `for i=1:nele`
- `d_global_tmp=zeros(1,12);`
- `d_global_tmp(1:6)=DEFL(ends(i,1),1:6);`
- `d_global_tmp(7:12)=DEFL(ends(i,2),1:6);`
- `d_global_tmp=d_global_tmp';`
- `f_local_tmp=squeeze(k_stack_local(i,,:))*squeeze(gamma_stack_local(i,,:))*d_global_tmp;`
- `for j=1:12`
- `ELE_FOR(i,j)=f_local_tmp(j);`
- `end`
- `end`
- `display(ELE_FOR)`

# Results

- The structure is stable.
- The matrix is well-conditioned.

# Results

- DEFL =

	1	2	3	4	5	6
1	0	0	0	7.5737e-04	2.5418e-06	-0.0013
2	0	0	0	7.5737e-04	-2.5418e-06	0.0013
3	-9.3650e-18	0.0026	-0.0123	-0.0026	-2.8740e-21	-3.4050e-19
4	3.7910e-16	-5.3331e-12	-4.4649	-5.2095e-16	-1.3301e-21	9.6745e-21
5	-2.1273e-18	-0.0026	-0.0123	0.0026	-5.3117e-23	2.8733e-19
6	0	0	0	-7.5737e-04	2.5418e-06	0.0013
7	0	0	0	-7.5737e-04	-2.5418e-06	-0.0013
8						

# Results

- REACT =

	1	2	3	4	5	6
1	0.4498	0.2505	1.1250	0	0	0
2	-0.4498	0.2505	1.1250	0	0	0
3	0	0	0	0	0	0
4	0	0	0	0	0	0
5	0	0	0	0	0	0
6	0.4498	-0.2505	1.1250	0	0	0
7	-0.4498	-0.2505	1.1250	0	0	0

# Results

- ELE\_FOR =

	1	2	3	4	5	6	7	8	9	10	11	12
1	1.2116	0.2505	1.7670e-04	3.6971e-14	1.7152e-17	3.3173e-14	-1.2116	-0.2505	-1.7670e-04	-3.6971e-14	-0.4758	674.5522
2	1.2116	-0.2505	-1.7670e-04	-1.4211e-14	0.4758	-674.5522	-1.2116	0.2505	1.7670e-04	1.4211e-14	-1.1102e-16	2.8422e-14
3	0.5010	1.2575e-16	2.2500	-1.9951e-16	-1.2526e+03	3.5484e-14	-0.5010	-1.2575e-16	-2.2500	1.9951e-16	-2.1224e+03	1.5314e-13
4	0.5010	-1.4200e-16	-2.2500	-1.6503e-16	2.1224e+03	-1.5314e-13	-0.5010	1.4200e-16	2.2500	1.6503e-16	1.2526e+03	-5.9851e-14
5	1.2116	0.2505	1.7670e-04	0	-0.4758	674.5522	-1.2116	-0.2505	-1.7670e-04	0	3.3307e-16	-2.8422e-14
6	1.2116	0.2505	-1.7670e-04	-2.8422e-14	0.4758	674.5522	-1.2116	-0.2505	1.7670e-04	2.8422e-14	-8.8818e-16	-8.5265e-14

# Thanks!

- Questions?