

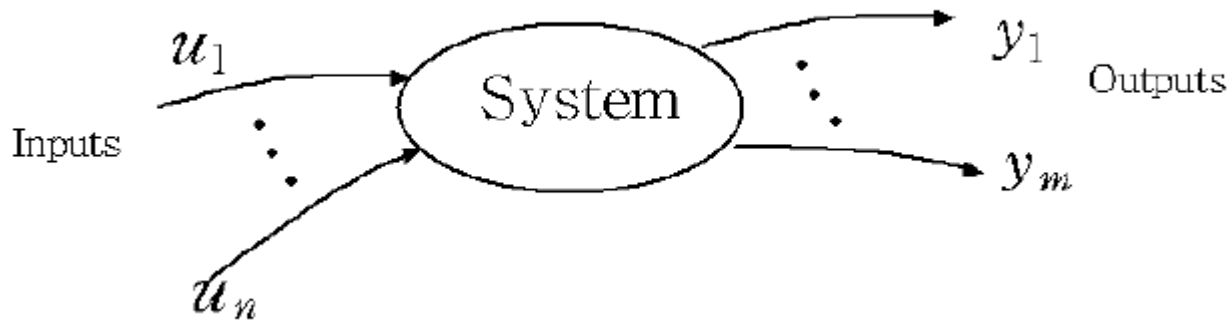
Mathematical Models of Systems

Contents

- Introduction
 - Differential equations of physical systems
 - Laplace transform
 - Models
 - Transfer function
 - State equation
-

System / Control / Design

- System : A combination of components acting together to perform a certain objective



- Control: Applying inputs to the system to correct or limit deviation of the output values from desired values
-

Introduction

- Mathematical models
 - To analyze relationship between the system variables and
 - To obtain a mathematical model
 - Differential equations
 - Systems under consideration are dynamic in nature
 - Laplace transform
 - can be utilized, if the differential equations can be linearized, to simplify the method of solution
 - The approach to dynamic system problems
 - Define the system and its components.
 - Formulate the mathematical model and list the assumptions.
 - Write the differential equations describing the model.
 - Solve the equations for the desired output variables.
 - Examine the solutions and the assumptions.
 - If necessary, reanalyze or redesign the system.
-

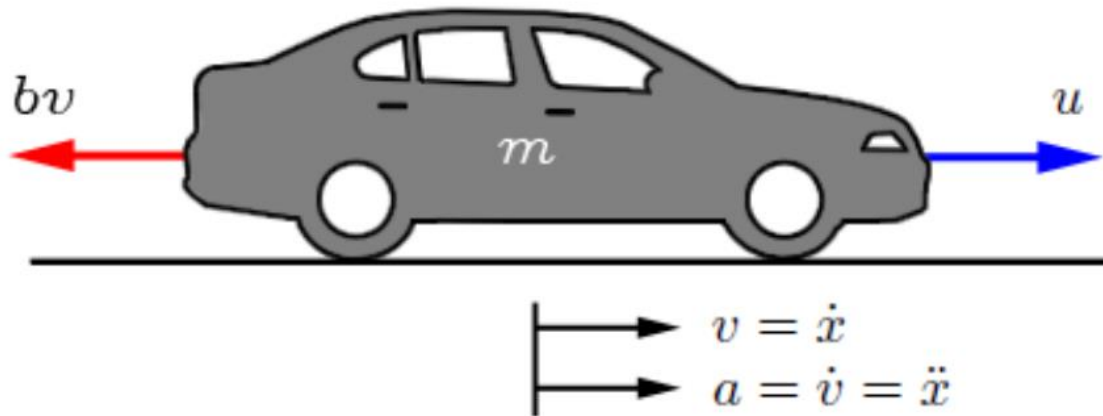
Differential equations of physical systems

- The differential equations describing the dynamic performance of a physical system are obtained by utilizing the physical laws of the process.
 - For mechanical systems : Newton's laws
 - For electrical systems : Kirchhoff's voltage/current laws
 - *Summary of describing differential equations for ideal elements*
 - Analogous variables and analogous systems
 - electrical, mechanical, thermal, and fluid systems
 - *Examples:*
 - Simple spring-mass-damper mechanical system
 - RLC circuit
-

Contents

- Introduction
 - **Differential equations of physical systems**
 - Laplace transform
 - Models
 - Transfer function
 - State equation
 - Block Diagram models
 - Signal flow Graph models
-

Exercise



$$m \frac{dv}{dt} + bv = u,$$
$$y = v$$

$$m = 1000, b = 50 \text{Ns/m}$$

Differential equations of physical systems

- First order differential equations solution (1)

$$\text{(Ex)} \quad \frac{dx(t)}{dt} + x(t) = 1$$

Multiplying e^t



$$\begin{aligned} \frac{d(f(t)g(t))}{dt} &= \frac{df(t)}{dt}g(t) + f(t)\frac{dg(t)}{dt} \\ \frac{de^{at}}{dt} &= ae^{at} \end{aligned}$$

$$e^t \frac{dx(t)}{dt} + e^t x(t) = \frac{d[e^t x(t)]}{dt} = e^t$$

$$\rightarrow \int_0^t \frac{d[e^\tau x(\tau)]}{d\tau} d\tau = e^t x(t) - x(0) = \int_0^t e^\tau d\tau$$

$$\rightarrow x(t) = e^{-t} x(0) + e^{-t} \int_0^t e^\tau d\tau = e^{-t} x(0) + 1 - e^{-t}$$

Differential equations of physical systems

- First order differential equations solution (2)

$$(\text{Ex}) \ y' + p(x)y = 0$$

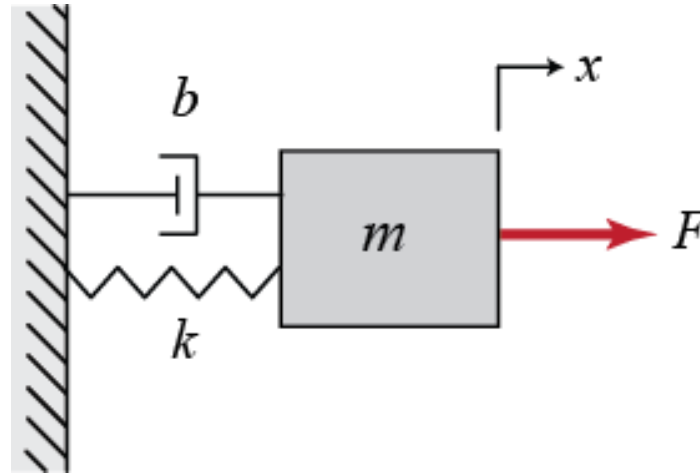
$$\frac{dy}{dx} = -p(x)y$$

$$\frac{dy}{y} = -p(x)dx$$

$$\ln|y| = -\int p(x)dx + c^*$$

$$y = ce^{-\int p(x)dx}$$

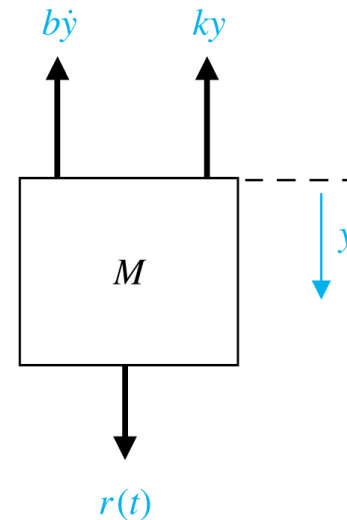
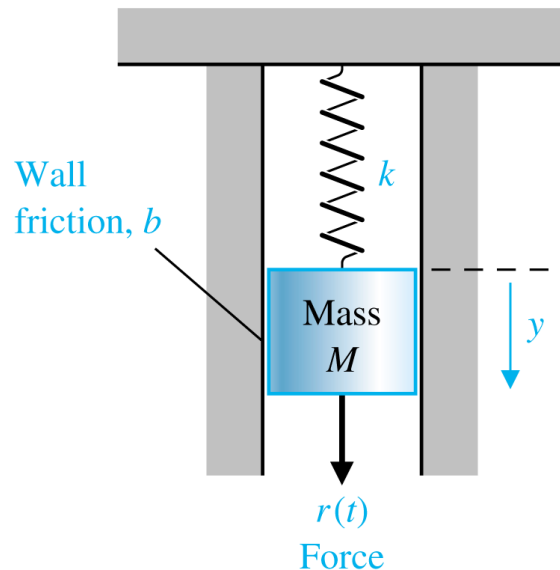
Mass spring damper system



$$\sum F = ma \Rightarrow F - kx - b\dot{x} = m\ddot{x}$$

Differential equations of physical systems

- Simple spring-mass-damper mechanical system



Force-displacement
(Newton's 2nd law)

$$M \frac{d^2 y(t)}{dt^2} + b \frac{dy(t)}{dt} + ky(t) = r(t)$$

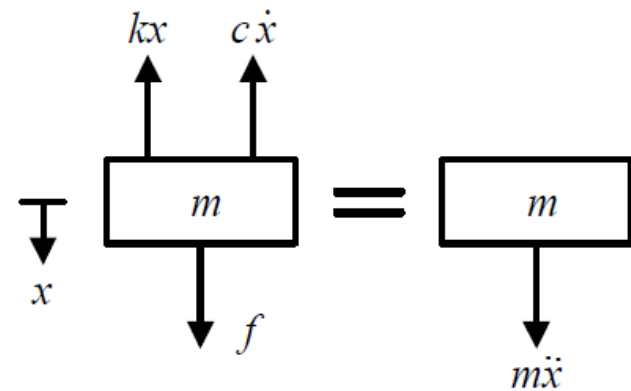
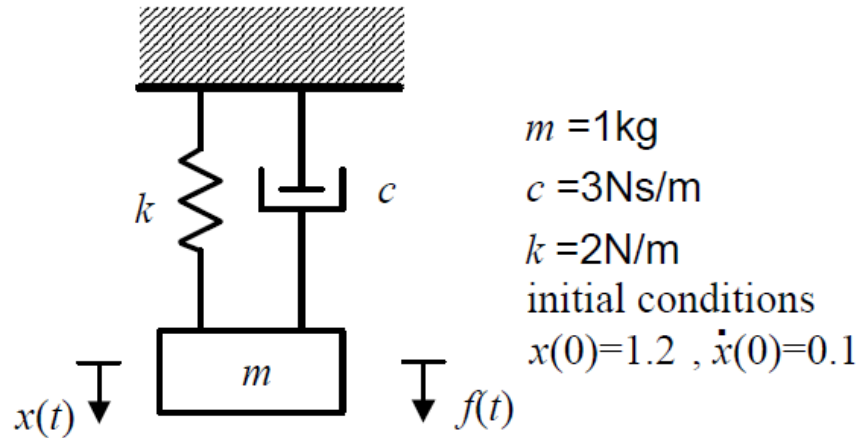
Force-velocity($v(t) = \frac{dy(t)}{dt}$)

$$M \frac{dv(t)}{dt} + bv(t) + k \int_0^t v(t) = r(t)$$

The solution :
(underdamped)

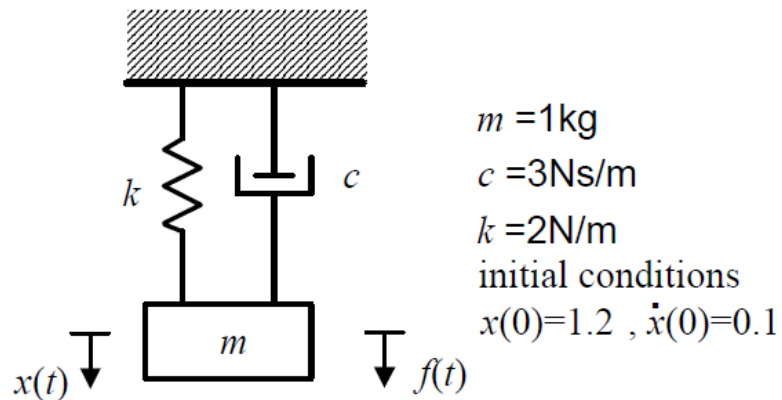
$$y(t) = K_1 e^{-\alpha_1 t} \sin(\beta_1 t + \theta_1)$$

Differential equations of physical systems



$$m\ddot{x} + c\dot{x} + kx = f(t) = 5u(t)$$

Differential equations of physical systems



$$ms^2x(s) + csx(s) + kx(s) = 5u(s)$$

$$s^2x(s) + 3sx(s) + 2x(s) = 5u(s)$$

$$y(s) = x(s)$$

$$\frac{y(s)}{u(s)} = \frac{5}{s^2 + 3s + 2}$$

Differential equations of physical systems

- *RLC circuit*

Kirchhof's current law

$$\frac{v(t)}{R} + C \frac{dv(t)}{dt} + \frac{1}{L} \int_0^t v(t) = r(t)$$

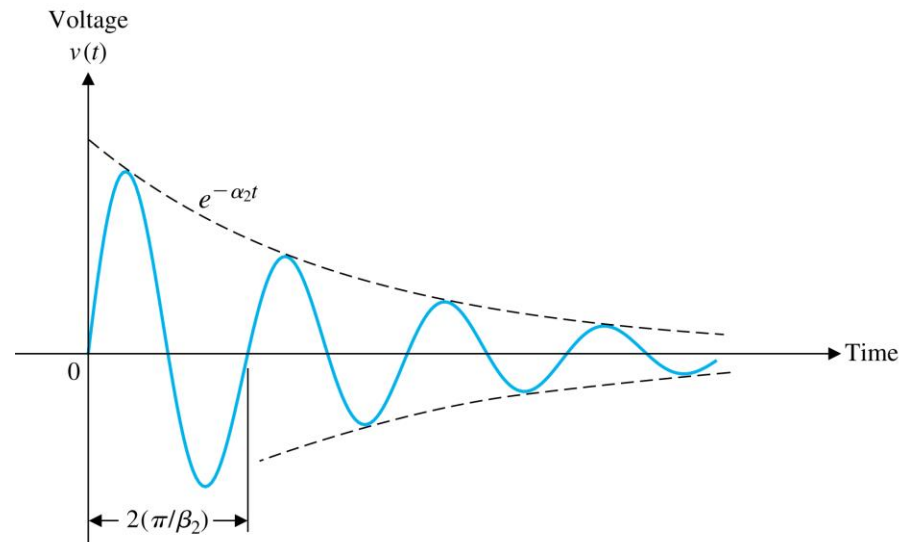
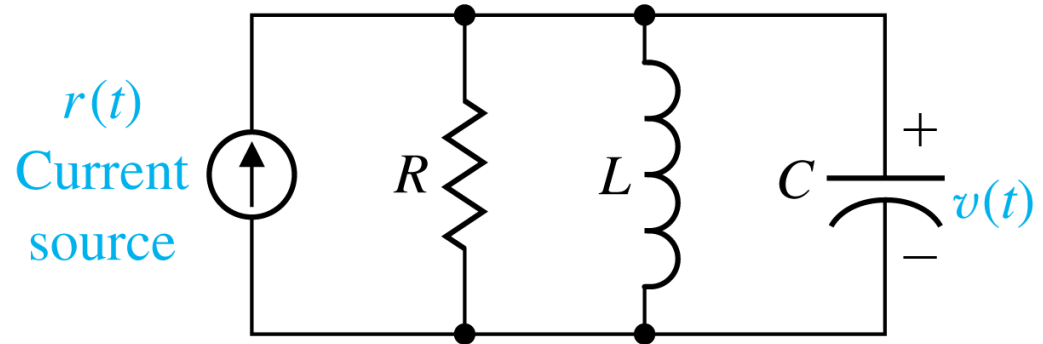
Spring-mass-damper와 비교

$$M \frac{dv(t)}{dt} + bv(t) + k \int_0^t v(t) = r(t)$$

Analogous variables: $v(t)$ – velocity vs voltage

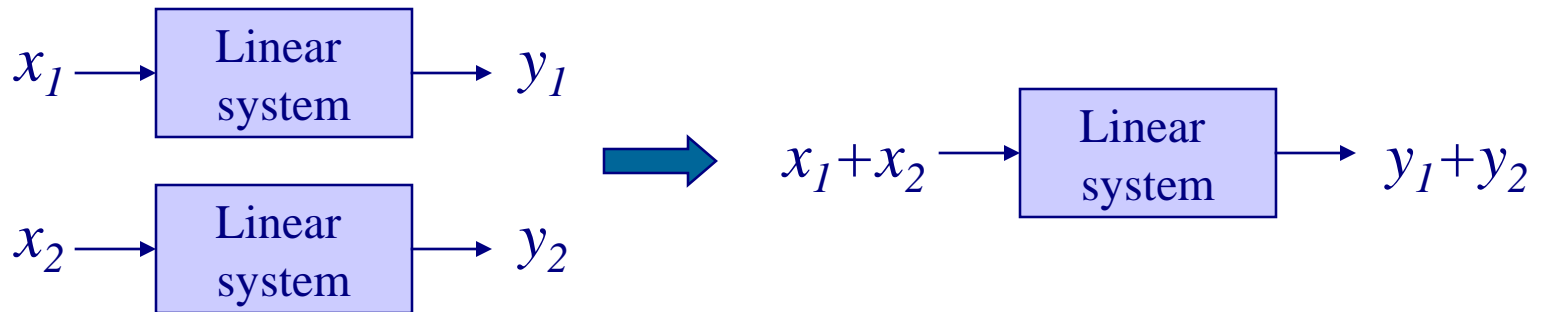
$$v(t) = K_2 e^{-\alpha_2 t} \cos(\beta_2 t + \theta_2)$$

(underdamped)

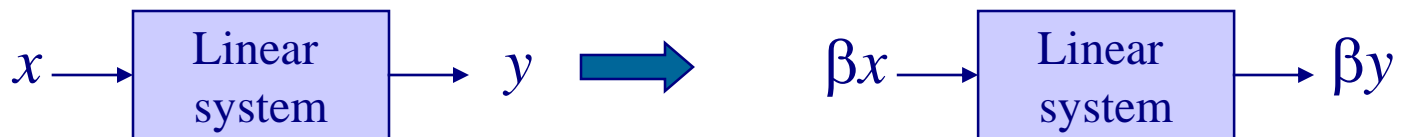


Linear approximations of physical systems

- *Linear* in terms of the system excitation and response
- A linear system satisfies the properties of
 - superposition and



- homogeneity.



Linear approximations of physical systems

- Linearization

- The relationship of the two variables is given as

$$y(t) = g(x(t))$$

- A Taylor series expansion about the normal operating point x_0

$$y = g(x) = g(x_0) + \left. \frac{dg}{dx} \right|_{x=x_0} \frac{(x-x_0)}{1!} + \left. \frac{d^2g}{dx^2} \right|_{x=x_0} \frac{(x-x_0)^2}{2!} + \dots$$

- The slope at the operating point is a good approximation to the curve over a small range of $(x-x_0)$.

$$y = g(x_0) + \left. \frac{dg}{dx} \right|_{x=x_0} (x-x_0) = y_0 + m(x-x_0)$$

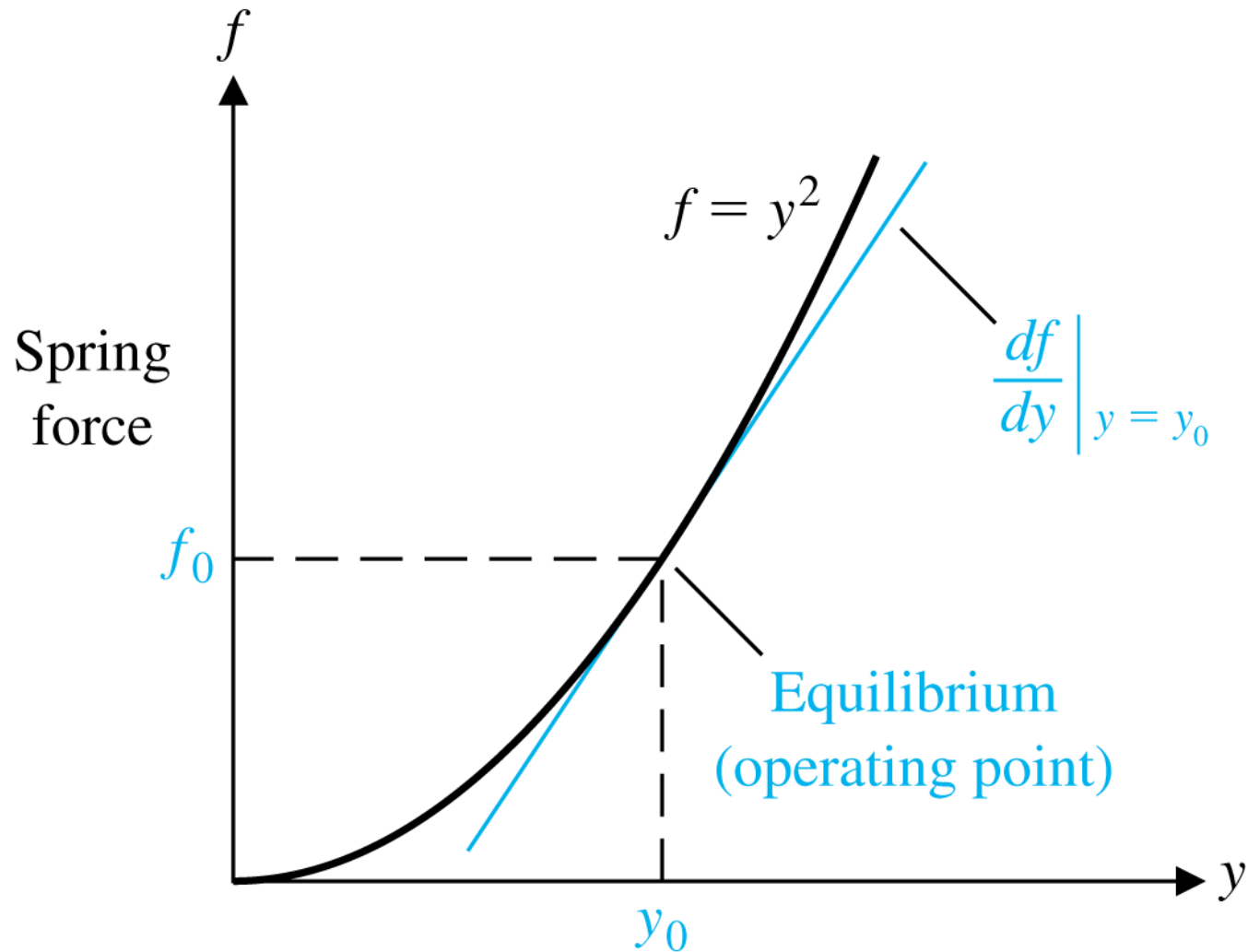


$$y - y_0 = m(x - x_0)$$

$$\Delta y = m \Delta x$$

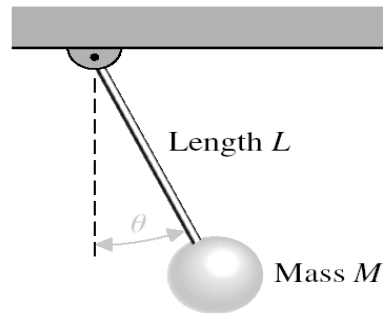
Linear equation

Linear approximations of physical systems

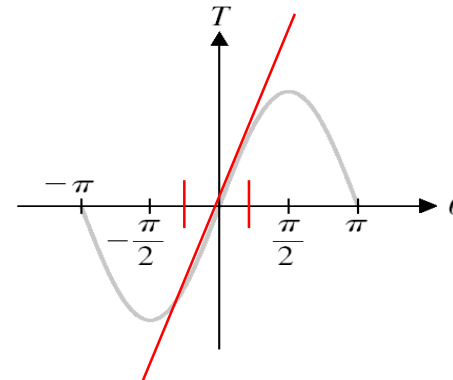


Linear approximations of physical systems

- Pendulum oscillator



(a)



(b)

Newton's 2nd law

$$\tau = MgL \sin \theta$$



$$\tau = I\alpha = ML^2\alpha \longrightarrow \frac{dw}{dt} = \frac{g}{L} \sin \theta$$

Linearization at operating point(0°)

$$\sin \theta \approx \sin(0^\circ) + \cos(0^\circ) (\theta - 0^\circ) + \dots$$



$$\frac{d^2\theta}{dt^2} = \frac{g}{L} \theta$$

$$\left(-\frac{\pi}{4} \leq \theta \leq \frac{\pi}{4}\right)$$

The transfer function of linear systems

Transfer function of a linear system:

The ratio of the Laplace transform of the output variable to the Laplace transform of the input variable, with all initial conditions assumed to be zero.



$$G(s) = \frac{Y(s)}{U(s)}$$

$$Y(s) = G(s)U(s)$$

The transfer function of linear systems

The dynamic system represented by the differential equation

$$\begin{aligned} & \frac{d^n y(t)}{dt^n} + a_{n-1} \frac{d^{n-1} y(t)}{dt^{n-1}} + \dots + a_1 \frac{dy(t)}{dt} + a_0 y(t) \\ &= b_m \frac{d^m u(t)}{dt^m} + b_{m-1} \frac{d^{m-1} u(t)}{dt^{m-1}} + \dots + b_1 \frac{du(t)}{dt} + b_0 u(t) \end{aligned}$$

$$\begin{aligned} & (s^n + a_{n-1}s^{n-1} + \dots + a_1s + a_0)Y(s) \\ &= (b_ms^m + b_{m-1}s^{m-1} + \dots + b_1s + b_0)U(s) \end{aligned}$$

$$G(s) = \frac{Y(s)}{U(s)} = \frac{b_ms^m + b_{m-1}s^{m-1} + \dots + b_1s + b_0}{s^n + a_{n-1}s^{n-1} + \dots + a_1s + a_0}$$

The transfer function of linear systems

■ Second order differential equation example



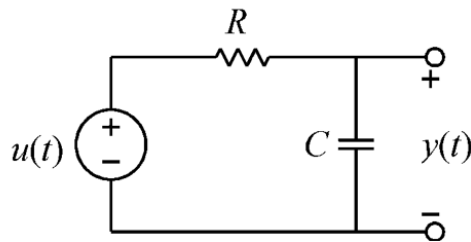
$$a_2\ddot{y}(t) + a_1\dot{y}(t) + a_0y(t) = r(t)$$

$$Y(s) = \frac{1}{a_2s^2 + a_1s + a_0} R(s)$$

$$\Rightarrow G(s) = \frac{Y(s)}{R(s)} = \frac{1}{a_2s^2 + a_1s + a_0}$$

The transfer function of linear systems

■ RC circuit example



$$RC \frac{dy(t)}{dt} + y(t) = u(t)$$

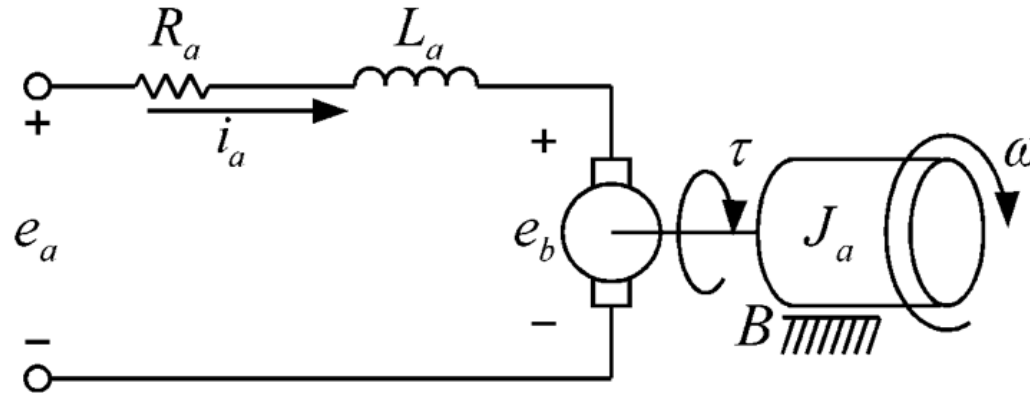
$$RC(sY(s) - y(0)) + Y(s) = U(s)$$

$$Y(s) = \frac{1}{RCs + 1} (U(s) + y(0))$$

$$G(s) = \frac{1}{RCs + 1}$$

The transfer function of linear systems

■ DC servo motor example



$$e_a = R_a i_a + L_a \frac{di_a}{dt} + e_b = R_a i_a + L_a \frac{di_a}{dt} + K_b \frac{d\theta}{dt}$$

$$\tau = K_t i_a = J_a \frac{d^2\theta}{dt^2} + B \frac{d\theta}{dt}$$

$$e_b = K_b \frac{d\theta}{dt} = K_b \omega$$



$$E_a(s) = R_a I_a(s) + L_a s I_a(s) + K_b s \Theta(s)$$

$$\frac{\Theta(s)}{E_a(s)} = \frac{K_t}{(J_a s^2 + B s)(L_a s + R_a) + K_t K_b s}$$

The transfer function of linear systems

■ Solution of a differential equation

$$\frac{d^2 y}{dt^2} + 4 \frac{dy}{dt} + 3y = 2r(t) \quad \text{with initial conditions of } y(0) = 1, \frac{dy}{dt}(0) = 0, \text{ and } r(t) = 1, t \geq 0$$

Taking the Laplace transform:

$$[s^2 Y(s) - \boxed{sy(0)}] + 4[sY(s) - \boxed{y(0)}] + 3Y(s) = 2\boxed{R(s)}$$

$$\Rightarrow Y(s) = \frac{\boxed{=1}}{(s+4)} + \frac{2}{s(s^2 + 4s + 3)} \quad \boxed{=1} \quad \boxed{=1/s}$$

By the partial fraction expansion

$$Y(s) = \left[\frac{3/2}{(s+1)} + \frac{-1/2}{(s+3)} \right] + \left[\frac{-1}{(s+1)} + \frac{1/3}{(s+3)} \right] + \frac{2/3}{s}$$

Hence the response is

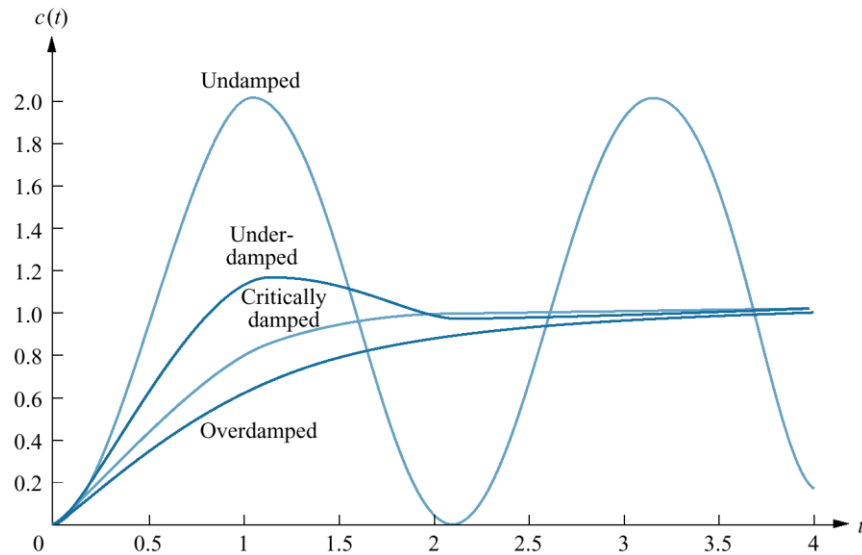
$$y(t) = \left[\frac{3}{2} e^{-t} - \frac{1}{2} e^{-3t} \right] + \left[-e^{-t} + \frac{1}{3} e^{-3t} \right] + \frac{2}{3}$$

the steady state response is

$$\lim_{t \rightarrow \infty} y(t) = \frac{2}{3}$$

The Laplace transform (2nd order system)

- Overdamped response (b)
- Underdamped response (c)
- Undamped response (d)
- Critically damped response (e)



System	Pole-zero Plot	Response
$(a) \quad R(s) = \frac{1}{s} \rightarrow \boxed{\frac{G(s)}{s^2 + as + b}} \rightarrow C(s)$ <p style="text-align: center;">General</p>		
$(b) \quad R(s) = \frac{1}{s} \rightarrow \boxed{\frac{9}{s^2 + 9s + 9}} \rightarrow C(s)$ <p style="text-align: center;">Overdamped</p>		$c(t) = 1 + 0.171e^{-7.854t} - 1.171e^{-1.146t}$
$(c) \quad R(s) = \frac{1}{s} \rightarrow \boxed{\frac{9}{s^2 + 2s + 9}} \rightarrow C(s)$ <p style="text-align: center;">Underdamped</p>		$c(t) = 1 - e^{-t}(\cos\sqrt{8}t + \frac{\sqrt{8}}{8}\sin\sqrt{8}t) = 1 - 1.06e^{-t}\cos(\sqrt{8}t - 19.47^\circ)$
$(d) \quad R(s) = \frac{1}{s} \rightarrow \boxed{\frac{9}{s^2 + 9}} \rightarrow C(s)$ <p style="text-align: center;">Undamped</p>		$c(t) = 1 - \cos 3t$
$(e) \quad R(s) = \frac{1}{s} \rightarrow \boxed{\frac{9}{s^2 + 6s + 9}} \rightarrow C(s)$ <p style="text-align: center;">Critically damped</p>		$c(t) = 1 - 3te^{-3t} - e^{-3t}$

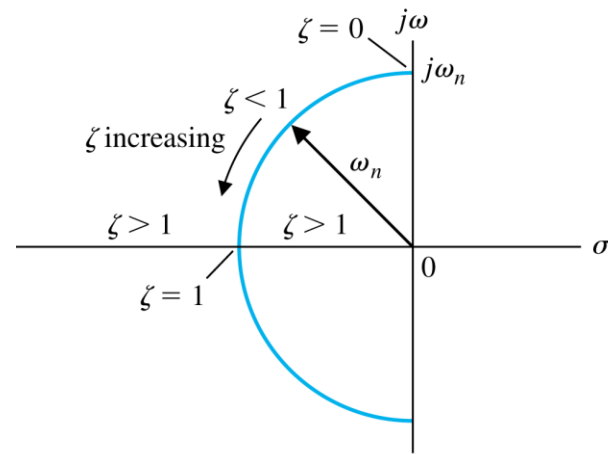
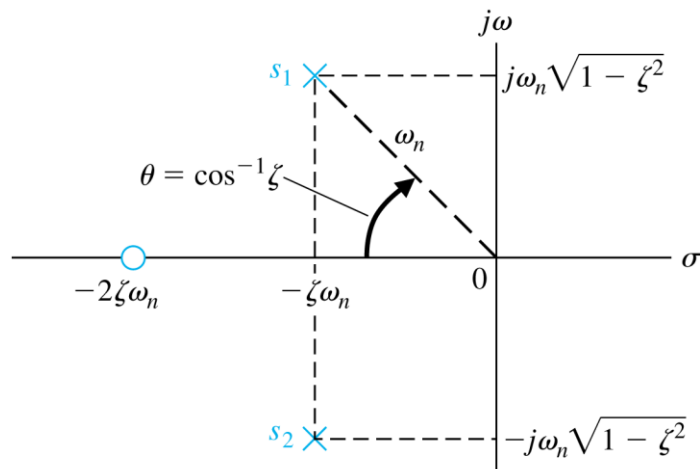
The Laplace transform (2nd order system)

- The general Second-order System
 - Natural frequency(ω_n): the frequency of oscillation of the system without damping.
 - Damping ratio(ζ): $\zeta = \frac{\text{Exponential decay frequency}}{\text{Natural frequency (rad/sec)}}$

General second-order transfer function
$$G(s) = \frac{\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2}$$

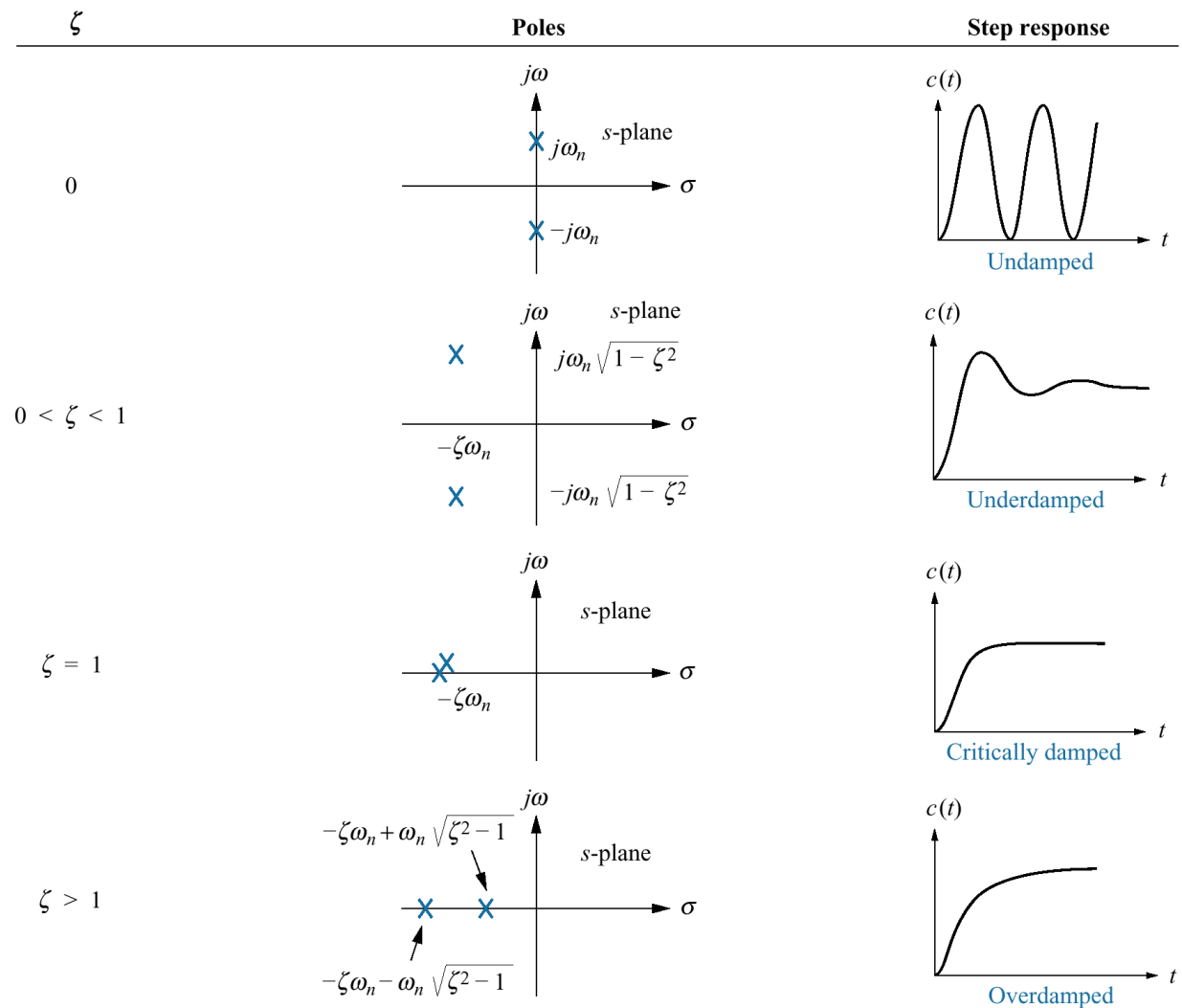
The poles of the transfer function:

$$s_{1,2} = -\zeta\omega_n \pm j\omega_n\sqrt{1-\zeta^2}$$



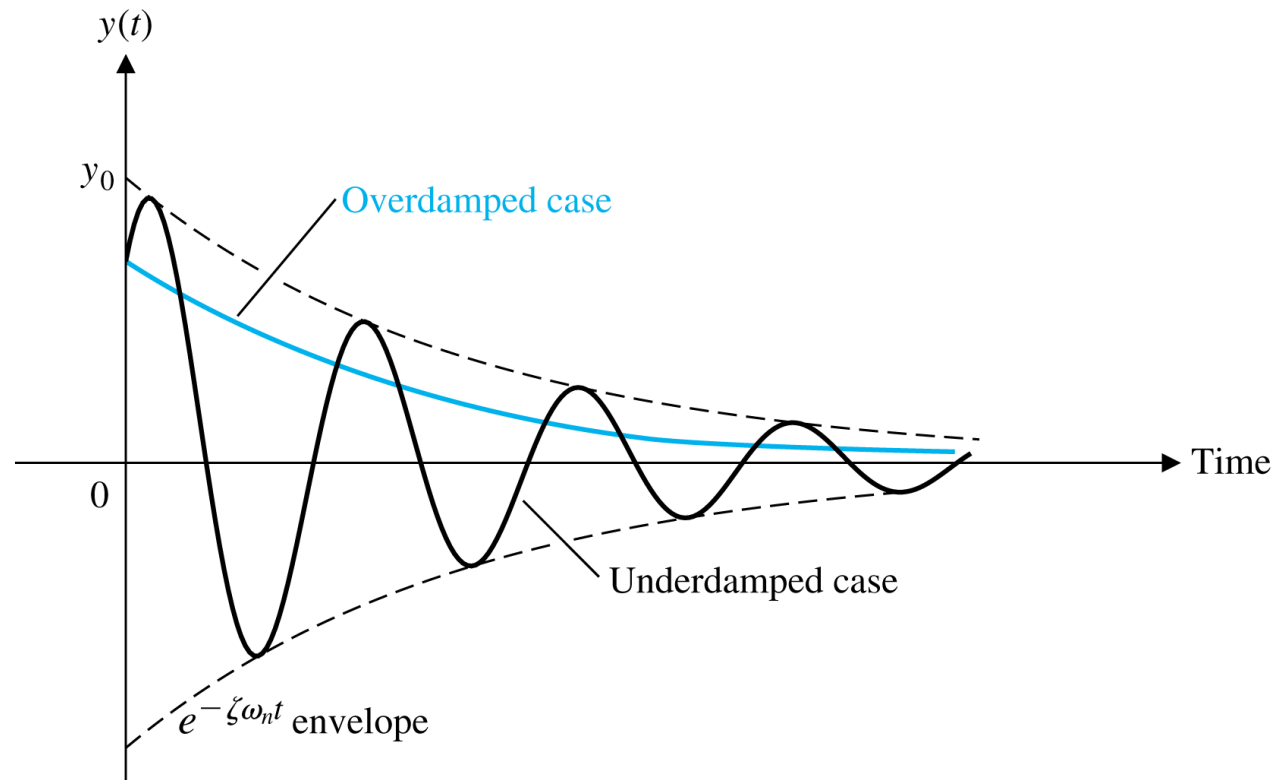
The Laplace transform (2nd order system)

Second-order response
as a function of damping
ratio



The Laplace transform (2nd order system)

Response of the spring-mass-damper system



State variable and state vector

A system is represented in **state space** by the following equations:

$$\dot{x} = Ax + Bu$$

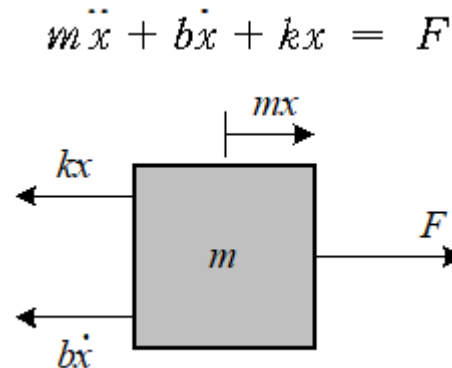
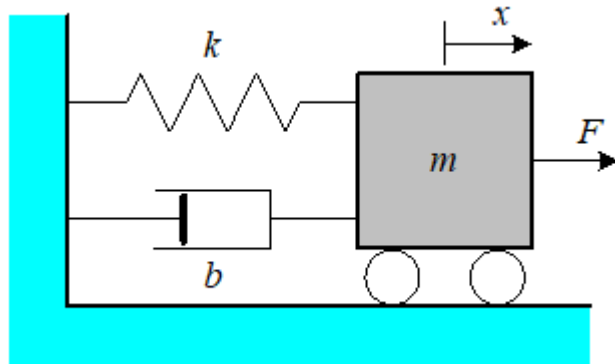
$$y = Cx + Du$$

State variable: The smallest set of linearly independent system variables such that the values of the members of the set at time t_0 along with known forcing functions completely determine the value of all system variables for all $t \geq t_0$

State vector: A vector whose elements are the state variables.

State variable and state vector

■ Mass-spring-damper system



$$m\ddot{x} + b\dot{x} + kx = F$$

$$\begin{aligned} x_1(t) &= x(t) & : \text{position} \\ x_2(t) &= \dot{x}(t) & : \text{velocity} \end{aligned}$$

$$\begin{aligned} \dot{x}_1(t) &= \dot{x}(t) = x_2(t) \\ \dot{x}_2(t) &= \ddot{x}(t) = -\frac{k}{m}x_1 - \frac{b}{m}x_2 + \frac{1}{m}F \end{aligned}$$

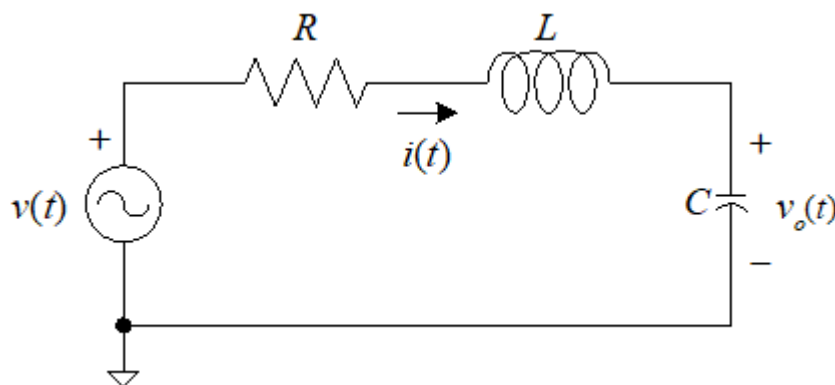
⇒

$$\begin{bmatrix} \dot{x}_1(t) \\ \dot{x}_2(t) \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -\frac{k}{m} & -\frac{b}{m} \end{bmatrix} \begin{bmatrix} x_1(t) \\ x_2(t) \end{bmatrix} + \begin{bmatrix} 0 \\ \frac{1}{m} \end{bmatrix} F$$

$$\begin{aligned} \text{State variables} &= [x(t) \quad v(t)] \\ \text{Input} &= u(t) = F \end{aligned}$$

State variable and state vector

■ RLC circuit system



$$v(t) = R i(t) + L \frac{d}{dt} i(t) + v_o(t)$$

$$i(t) = C \frac{d}{dt} v_o(t)$$



$$\begin{aligned} \dot{x}(t) &= \begin{bmatrix} 0 & \frac{1}{C} \\ -\frac{1}{L} & -\frac{R}{L} \end{bmatrix} x(t) + \begin{bmatrix} 0 \\ \frac{1}{L} \end{bmatrix} u(t) \\ y(t) &= [1 \quad 0] x(t) \end{aligned}$$

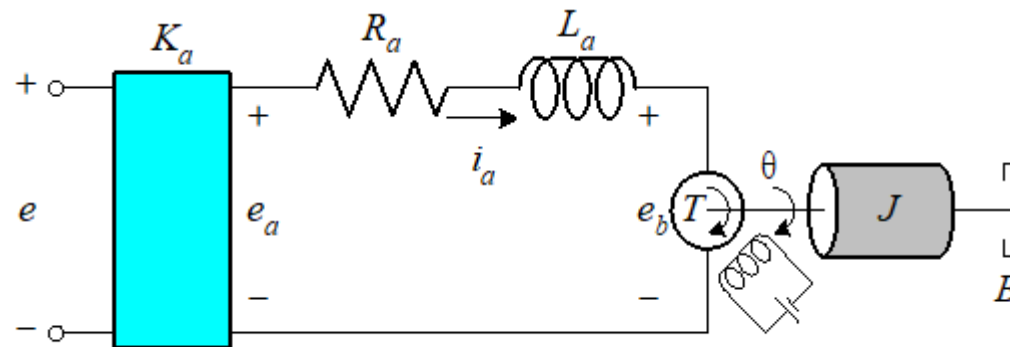
State variables = $[v_o(t) \quad i(t)]$

Input = $u(t) = v(t)$

Output = $y(t) = v_o(t)$

State variable and state vector

■ DC servo motor



$$\begin{aligned}
 e_a &= K_a e = R_a i_a + L_a \frac{di_a}{dt} + e_b \\
 e_b &= K_b \omega = K_b \frac{d\theta}{dt}
 \end{aligned}
 \quad \longrightarrow \quad
 \begin{aligned}
 \frac{d}{dt} \begin{bmatrix} i_a \\ \dot{\theta} \\ \theta \end{bmatrix} &= \begin{bmatrix} -R_a/L_a & -K_b/L_a & 0 \\ K_t/J & -B/J & 0 \\ 0 & 1 & 0 \end{bmatrix} \begin{bmatrix} i_a \\ \dot{\theta} \\ \theta \end{bmatrix} + \begin{bmatrix} K_a/L_a \\ 0 \\ 0 \end{bmatrix} e \\
 y &= [0 \ 0 \ 1] \begin{bmatrix} i_a \\ \dot{\theta} \\ \theta \end{bmatrix}
 \end{aligned}$$

State variables = $[i_a \quad \dot{\theta} \quad \theta]$

Input = $u(t) = e$

Output = $y(t) = \theta$

Derivation of transfer function from S.E.

$$\begin{aligned}\dot{x}(t) &= Ax(t) + Bu(t) \\ y(t) &= Cx(t) + Du(t)\end{aligned}$$



Laplace transformation

$$\begin{aligned}sX(s) - x(0) &= AX(s) + BU(s) \\ Y(s) &= CX(s) + DU(s)\end{aligned}$$



Transfer function is ratio
of input $U(s)$ and $Y(s)$
with $x(0) = 0$

$$\begin{aligned}(sI - A)X(s) &= BU(s) \\ X(s) &= (sI - A)^{-1}BU(s) \\ Y(s) &= [C(sI - A)^{-1}B + D]U(s) \\ \Rightarrow G(s) &= \frac{Y(s)}{U(s)} = C(sI - A)^{-1}B + D\end{aligned}$$

Derivation of transfer function from S.E.

■ S.E \Rightarrow Transfer Function

$$\dot{x}(t) = \begin{bmatrix} -1 & -2 \\ 1 & 0 \end{bmatrix} x(t) + \begin{bmatrix} 1 \\ 1 \end{bmatrix} u(t)$$

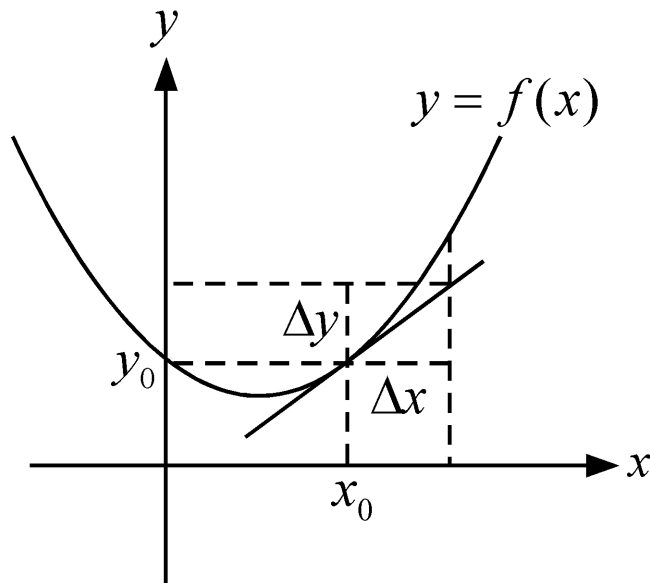
$$y(t) = [2 \ 1] x(t) + 3u(t)$$

$$A = \begin{bmatrix} -1 & -2 \\ 1 & 0 \end{bmatrix}, \quad B = \begin{bmatrix} 1 \\ 1 \end{bmatrix}, \quad C = [2 \ 1], \quad D = 3$$

$$\begin{aligned} \Rightarrow G(s) &= C(sI - A)^{-1}B + D \\ &= [2 \ 1] \begin{bmatrix} s+1 & 2 \\ -1 & s \end{bmatrix}^{-1} \begin{bmatrix} 1 \\ 1 \end{bmatrix} + 3 \\ &= \frac{1}{s^2 + s + 2} [2 \ 1] \begin{bmatrix} s & -2 \\ 1 & s+1 \end{bmatrix} \begin{bmatrix} 1 \\ 1 \end{bmatrix} + 3 \\ &= \frac{3s-2}{s^2 + s + 2} + 3 \end{aligned}$$

Linearization

$$y = f(x)$$



$$\Delta y = \left(\left. \frac{df}{dx} \right|_{x=x_0} \right) \cdot \Delta x = K \cdot \Delta x$$

$$y_0 = f(x_0)$$

Linearization

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \vdots \\ \dot{x}_n \end{bmatrix} = \begin{bmatrix} f_1(x_1, x_2, \dots, x_n, u) \\ f_2(x_1, x_2, \dots, x_n, u) \\ \vdots \\ f_n(x_1, x_2, \dots, x_n, u) \end{bmatrix}$$

Nonlinear dynamic eq.

$$(x_{10}, x_{20}, \dots, u_0)$$

Operating point

$$\dot{x}_{i0} = f_i(x_{10}, x_{20}, \dots, u_0), \quad i = 1, 2, \dots, n$$

$$x_i = x_{i0} + \Delta x_i, \quad i = 1, 2, \dots, n$$

$$u = u_0 + \Delta u$$

Linearization

Step 1) Suppose

If the input u changes slightly by δu in the vicinity of the equilibrium point, state x and output y change finely by δx and δy .

Step 2) Taylor series expansion at (x_0, u_0, y_0)

$$\begin{aligned}\frac{d}{dt} [x_0 + \delta x(t)] &= f(x_0 + \delta x, u_0 + \delta u) \\ &= f(x_0, u_0) + \frac{\partial}{\partial x} f(x_0, u_0) \delta x(t) + \frac{\partial}{\partial u} f(x_0, u_0) \delta u(t) + O(\delta x, \delta u) \\ &\approx f(x_0, u_0) + \frac{\partial}{\partial x} f(x_0, u_0) \delta x(t) + \frac{\partial}{\partial u} f(x_0, u_0) \delta u(t) \\ y_0 + \delta y(t) &\approx g(x_0, u_0) + \frac{\partial}{\partial x} g(x_0, u_0) \delta x(t) + \frac{\partial}{\partial u} g(x_0, u_0) \delta u(t)\end{aligned}$$

Linearization

$$\begin{aligned}\dot{x}_i &= \dot{x}_{i0} + \Delta \dot{x}_i = f_i(x_1, x_2, \dots, x_n, u) \\ &\approx f_i(x_{10}, x_{20}, \dots, u_0) + \left(\frac{\partial f_i}{\partial x_1} \bigg|_{x_1=x_{10}, x_2=x_{20}, \dots, x_n=x_{n0}, u=u_0} \right) \cdot \Delta x_1 \\ &\quad + \left(\frac{\partial f_i}{\partial x_2} \bigg|_{x_1=x_{10}, x_2=x_{20}, \dots, x_n=x_{n0}, u=u_0} \right) \cdot \Delta x_2 \\ &\quad \vdots \\ &\quad + \left(\frac{\partial f_i}{\partial x_n} \bigg|_{x_1=x_{10}, x_2=x_{20}, \dots, x_n=x_{n0}, u=u_0} \right) \cdot \Delta x_n \\ &\quad + \left(\frac{\partial f_i}{\partial u} \bigg|_{x_1=x_{10}, x_2=x_{20}, \dots, x_n=x_{n0}, u=u_0} \right) \cdot \Delta u, \quad i = 1, 2, \dots, n\end{aligned}$$

Linearization

$$\begin{bmatrix} \Delta \dot{x}_1 \\ \Delta \dot{x}_2 \\ \vdots \\ \Delta \dot{x}_n \end{bmatrix} = \begin{bmatrix} a_{11} & a_{12} & \cdots & a_{1n} \\ a_{21} & a_{22} & \cdots & a_{2n} \\ \vdots & \vdots & & \vdots \\ a_{n1} & a_{n2} & \cdots & a_{nn} \end{bmatrix} \begin{bmatrix} \Delta x_1 \\ \Delta x_2 \\ \vdots \\ \Delta x_n \end{bmatrix} + \begin{bmatrix} b_1 \\ b_2 \\ \vdots \\ b_n \end{bmatrix} \Delta u$$

$$a_{ij} = \left. \frac{\partial f_i}{\partial x_j} \right|_{x_1=x_{10}, x_2=x_{20}, \dots, x_n=x_{n0}, u=u_0}, b_i = \left. \frac{\partial f_i}{\partial u} \right|_{x_1=x_{10}, x_2=x_{20}, \dots, x_n=x_{n0}, u=u_0}$$

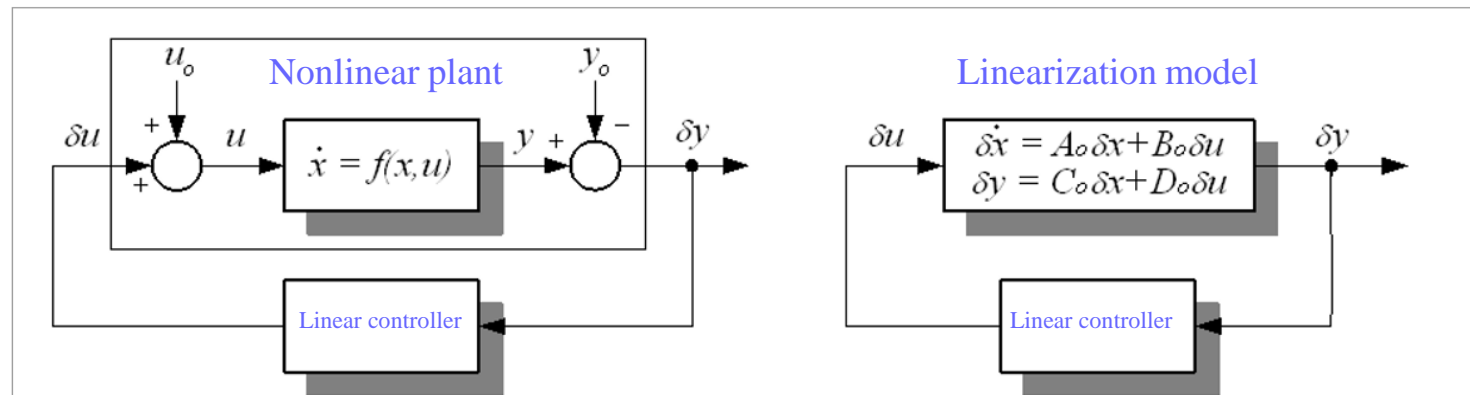
Linearization

Step 3) Linearization model

$$\begin{aligned}\delta \dot{x}(t) &\approx A_0 \delta x(t) + B_0 \delta u(t) \\ \delta y(t) &\approx C_0 \delta x(t) + D_0 \delta u(t)\end{aligned}$$

$$\begin{aligned}A_0 &= \frac{\partial}{\partial x} f(x_0, u_0), & B_0 &= \frac{\partial}{\partial u} f(x_0, u_0) \\ C_0 &= \frac{\partial}{\partial x} g(x_0, u_0), & D_0 &= \frac{\partial}{\partial u} g(x_0, u_0)\end{aligned}$$

$$\delta u = u - u_0, \quad \delta x = x - x_0, \quad \delta y = y - y_0$$



Linearization

■ Nonlinear system operating point and linearization

$$\begin{aligned}\dot{x}(t) &= -x^2(t) - u^2(t) + 1 \\ y(t) &= x(t)u(t)\end{aligned}$$

1) Operating point

$$f(x_0, u_0) = -x_0^2 - u_0^2 + 1 = 0$$

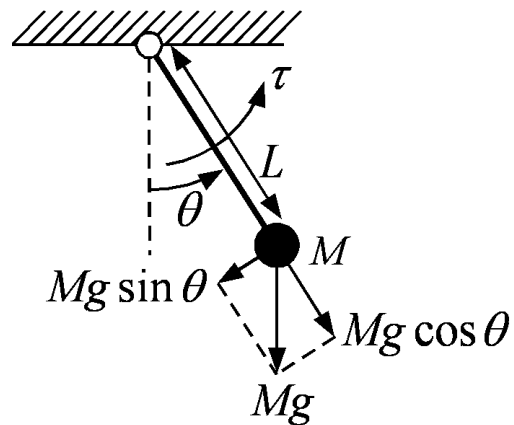
2) Taylor series

$$\begin{aligned}\delta \dot{x}(t) &\approx A_0 \delta x(t) + B_0 \delta u(t) \\ \delta y(t) &\approx C_0 \delta x(t) + D_0 \delta u(t)\end{aligned}$$

$$A_0 = \frac{\partial f}{\partial x}(1, 0) = -2, \quad B_0 = \frac{\partial f}{\partial u}(1, 0) = 0$$

$$C_0 = \frac{\partial g}{\partial x}(1, 0) = 0, \quad D_0 = \frac{\partial g}{\partial u}(1, 0) = 1$$

Ex 1



$$\tau - LMg \sin \theta = ML^2 \frac{d^2 \theta}{dt^2}$$

$$x_1 = \theta, \quad x_2 = \dot{\theta}, \quad u = \tau$$

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} f_1(x_1, x_2, u) \\ f_2(x_1, x_2, u) \end{bmatrix} = \begin{bmatrix} x_2 \\ -\frac{g}{L} \sin x_1 + \frac{1}{ML^2} u \end{bmatrix}$$

Ex 1

$$\left. \frac{\partial f_1}{\partial x_1} \right|_{x_1=0, x_2=0, u=0} = 0,$$

$$\left. \frac{\partial f_1}{\partial x_2} \right|_{x_1=0, x_2=0, u=0} = 1,$$

$$\left. \frac{\partial f_2}{\partial x_1} \right|_{x_1=0, x_2=0, u=0} = -\frac{g}{L} \cos x_1 \Big|_{x_1=0, x_2=0, u=0} = -\frac{g}{L},$$

$$\left. \frac{\partial f_2}{\partial x_2} \right|_{x_1=0, x_2=0, u=0} = 0$$

$$\left. \frac{\partial f_1}{\partial u} \right|_{x_1=0, x_2=0, u=0} = 0,$$

$$\left. \frac{\partial f_2}{\partial u} \right|_{x_1=0, x_2=0, u=0} = \frac{1}{ML^2}$$

Ex 1

$$\begin{bmatrix} \Delta \dot{x}_1 \\ \Delta \dot{x}_2 \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -\frac{g}{L} & 0 \end{bmatrix} \begin{bmatrix} \Delta x_1 \\ \Delta x_2 \end{bmatrix} + \begin{bmatrix} 0 \\ \frac{1}{ML^2} \end{bmatrix} \Delta u$$

$$s\Delta X_1(s) = \Delta X_2(s)$$

$$s\Delta X_2(s) = -\frac{g}{L}\Delta X_1(s) + \frac{1}{ML^2}\Delta U(s)$$

$$\frac{\Delta X_1(s)}{\Delta U(s)} = \frac{1}{ML^2} \frac{1}{s^2 + (g/L)}$$
