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Project 3

EE568

1)Introduction

2)

2.1)

In this part, magnetic loading of the machine with the parameters given in Table 1 will be examined.

|  |  |
| --- | --- |
| **Parameters** | **Value** |
| Number of phases | 3 |
| Number of poles | 4 |
| Motor axial length (mm) | 100 |
| Air-gap clearance (mm) | 1 |
| Magnet to pole pitch ratio | 0.8 |
| Magnet type | NdFeB (N42) |
| Rotor diameter (mm) | 100 |
| Magnet thickness (mm) | 4 |
| Remanent flux of the magnet (Br) | 1.28 |
| Relevant coercivity of the magnet (µr) | 1.05 |

Table 1: Machine parameters

By using the equivalent magnetic circuit given in Figure 1 is used to find magnetic field in the air gap,

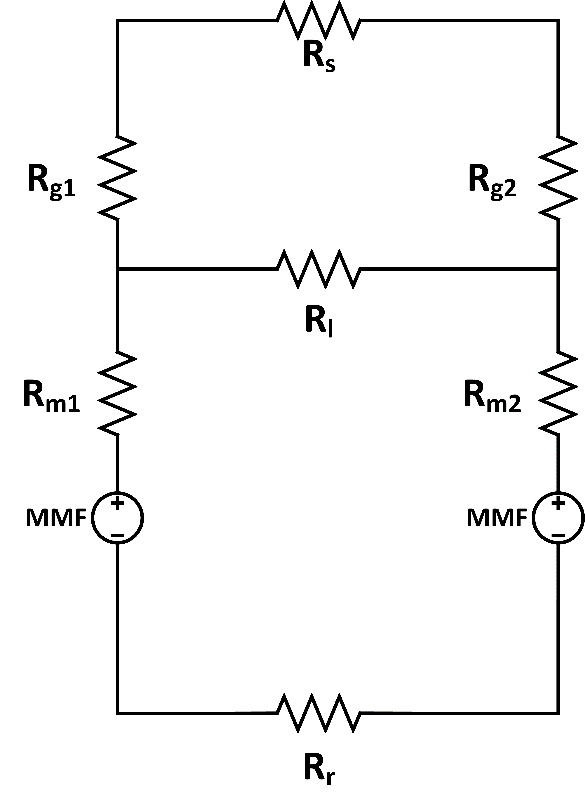


Figure 1: Equivalent magnetic circuit of the machine

Where Rs, Rr, Rl, Rg and Rm are reluctances of stator, rotor, leakage, air-gap and magnets, respectively. In this case, Rs, Rr and Rl are ignored. As a further step, MMF and reluctances of air-gap and magnets are calculated. For this purpose, area of magnet and airgap should be calculated initially.

=0.0063 m2 (1)

Then, by using general reluctance equation, reluctances can be found easily as follows.

(2)

(3)

Finally, MMF is calculated as follows:

(4)

Then, by using equivalent magnetic circuit of the machine and variables that are calculated above, magnetic flux density of the machine can be calculated as follows:

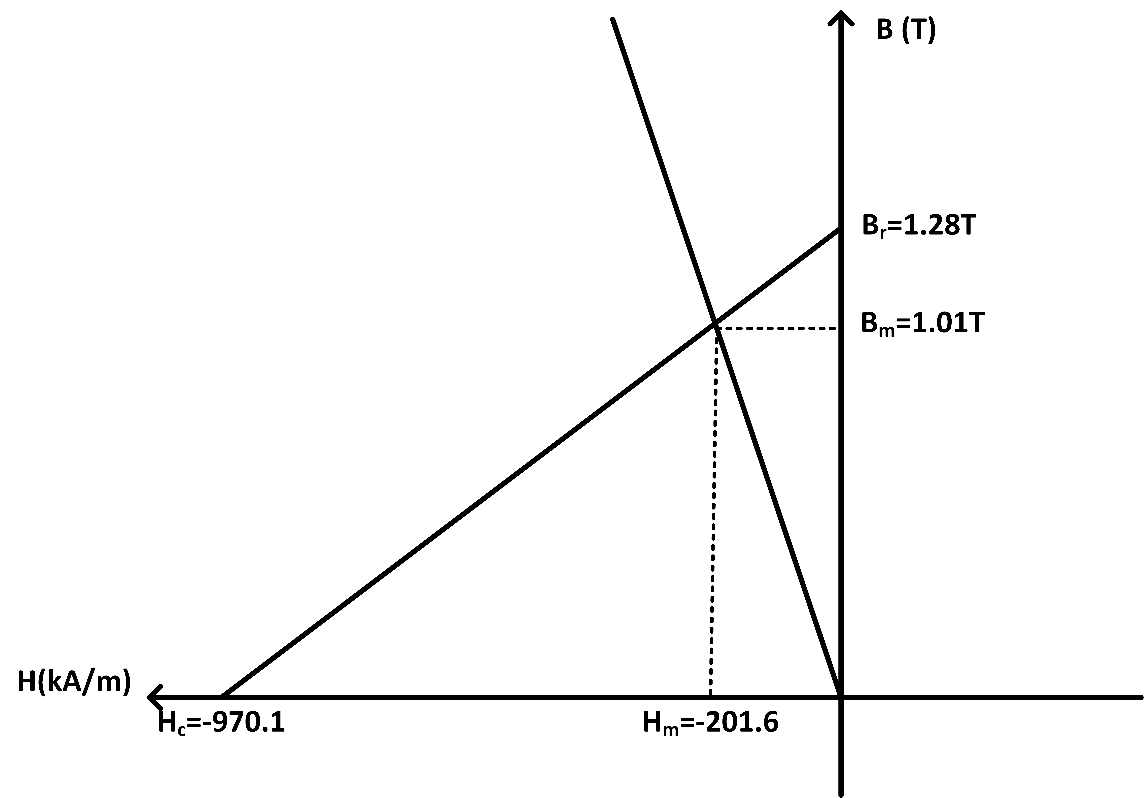


Figure 2: Load line and operating point on the B-H curve

2.2)

Magnetic loading of the machine can be calculated as follows:

(5)

2.3)

In this part, FEA validation of above parts is performed. FEA draw of the machine is given in Figure 2 and results are given in Figure 3.

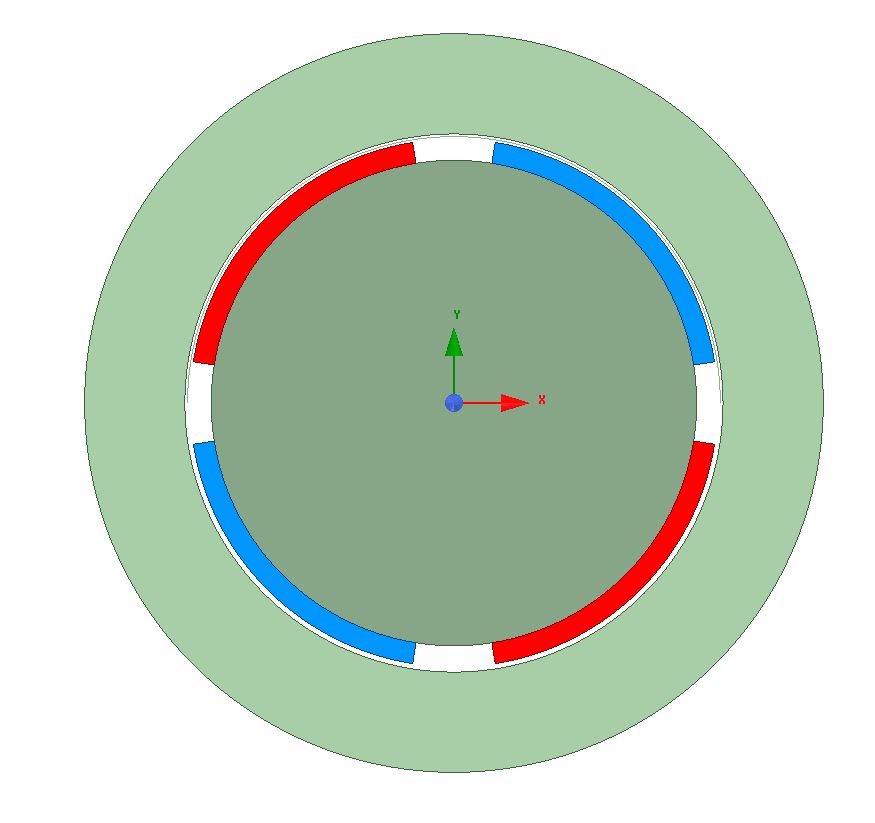


Figure 2: 2D FEA draw of the machine

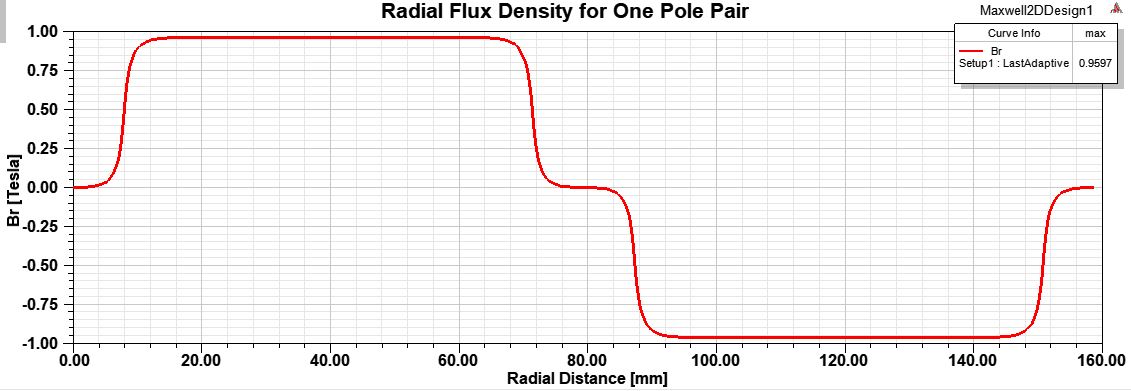


Figure 3: 2D FEA results of air gap flux density at r=(Ri+air-gap/2)

Analytical results and numerical results are close to each other but they are not equal to each other. While analytical calculations are performed, leakage flux can not be modelled and taken into consideration. However, numerical results includes leakage flux and this result is slightly smaller than analytical result.

3)

3.1)

In this part, slot number of the machine is chosen. In this case, q is taken two and the corresponding slot number is 24.

3.2)

In this part, wire diameter should be chosen. For this, the restriction is maximum current density (J) in the coil and it is 5 A/mm2. Also, coil current (I) for this machine is 2.5 Ampere. Then, minimum coil area can be calculated as follows:

=0.5 mm2 (6)

So, the wire diameter is chosen larger than that value in order to make sure that maximum current density in the coil is smaller than 5 A/mm2. If frequency is known and larger areas are acceptable, it can be discussed later. Then, AWG20 cable is chosen with 0.518 mm2  coil area.

3.3)

In this part, slot height, turn numbers in a slot and back core thickness are calculated. Firstly, slot ratio should be defined. Slot ratio is the ratio of diameter of inner part of slot to diameter of outer side of the slot (Di/Do). If it is chosen smaller, corresponding slot height is higher. Generally, it is chosen between 0.5 and 1. In this study, it is chosen as 0.7. Since Di is 102 mm, Do and slot height hs can be calculated easily as follows :

145.7 mm (7)

(8)

Moreover, turn number for each slot should be calculated. For this, slot area should be calculated. Firstly, the ratio of slot width to teeth width is chosen as 1 in this study. Then, width of a slot can be calculated as follows (rectangular teeth is chosen):

(9)

Then, fill factor is taken 0.6 for round wires and turn numbers can be calculated as follows:

(10)

Finally, back core thickness can be calculated by using the following equation (which is presented in the class) where kstacking is the stacking factor of the machine and it is taken as 0.95 in this study and yoke flux density Byoke is taken 0.85 Tesla according to stator material:

(11)

3.4)

In order to calculated electrical loading, the formula given below is used (It is presented in the class):

(12)

Usual values of electrical loading for PMSM is presented in the class as 35-65 kA/m. The value that is found above is in this range. Therefore, it can be said that chosen parameters are logical by now.

3.5)

Average tangential stress of the machine can be found by using the equation given below where cosφ is taken 1 for PMSM:

(13)

Then, corresponding total force can be calculated as follows where is rotor surface area:

(14)

3.6)

In order to calculate power output of the machine, electrical radial speed of the machine and torque output should be known. Firstly, torque output of the machine can be calculated as follows:

(15)

Then, rotor speed pf the machine is 1500 rpm (mechanically). It can be converted to radial speed by multiplying with 2\*π/60 and is obtained as 157.08 rad/sec. Then power output of the machine can be calculated as follows:

(16)

4)

4.1)

In this part, the machine outer diameter is fixed to 160 mm and it is optimized in order to obtain maximum torque output. For this, slot ratio is called again which is D=(Di/Do). Then the relationship between back core thickness (hst) and Di should be determined. For rectangular teeth shape, slot are is proportional to (1-D2)/D and rotor volume is proportional to D2. Then, output torque is proportional to ((1-D2)/D)\*D2=(1-D2)\*D. So, the optimum D is 0.58 as calculated in class. Relationship between Di and Do can be shown as follows:

(17)

Furthermore, magnet thickness and air-gap clearance is same with the values considered in first question. Thus, magnetic loading of the machine does not change ( ). Then, magnet area can be calculated by using the equation . Maximum stator flux density is considered as 0.9 Tesla again and is taking 0.95 again. Then, back core thickness of the machine can be calculated as follows:

(18)

Then, we can calculate Di as follows:

(19)

Finally, Di can be found as 64.77 mm, Do can be found 111.66 mm and hst can be found 24.17 mm.

4.1.1) Magnetic loading

Magnetic loading of the machine does not change and it is equal to 813.37 mT.

4.1.2) Number of slots

Number of slots is chosen 24 again for the same reasons given above.

4.1.3) AWG cable

Applied current and maximum current density are taken as taken in previous parts. Therefore, chosen cable is taken same and it is AWG20 with the area 0.518 mm2.

4.1.4) Slot height, Number of coils per slot and Back core thickness

Di and Do are calculated above and corresponding slot height is calculated as 23.45 mm. Width of slot can be calculated as follows:

(20)

(20)

In order to calculate number of coils per slot can be calculated as follows where fill factor is taken 0.5:

(21)

Finally, back core thickness is calculated above and is found as 24.17 mm.

4.1.5) Electrical loading

Electrical loading of the machine can be calculated as follows:

(22)

For PMSM, electrical loading is in the range 35-65 kA/m and this value is in the range.

4.1.6) Average tangential stress and Total force

Average tangential force of the previous machine is calculated above and for this machine it can be calculated as follows:

(23)

Moreover, total force can be calculated as follows:

(24)

4.1.7) Power output of the machine

In order to calculate power output, torque output of the machine should be calculated as follows:

(25)

Corresponding output power can be calculated as follows:

(16)

4.1.8) FEA Results

4.2) Replacing NdFeB with Ferrite Magnet