### 18-100 Introduction to Electrical and Computer Engineering

Lecture 04 Semiconductors, Diodes, and Light Emitting Diodes (LEDs)



Are you here?

Let us know and win prizes.



## **Course Syllabus**

**18-100:** *Introduction to Electrical and Computer Engineering* 

### **Spring 2025**

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Office Hours: Monday, 2-4pm or by appointment

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13-Jan

15-Jan

20-Jan

22-Jan

29-Jan

3-Feb

5-Feb

10-Feb

12-Feb

17-Feb

19-Feb

24-Feb

26-Feb

3-Mar

5-Mar

4

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27-Jan M

## Carnegie Mellon

L06: Professional Identity, Professional Responsibility, and Ethics

L01: Intro, Physics, EM, Leveling Students

Martin Luther King Celebration (No Lecture)

L07: Capacitors, RC Time Constants, RC Circuits

L04: Semiconductors, Diodes, LEDs

L08: Inductors, RL Time Constants, 555

L09: Binary, Logic Gates, Boolean Logic

L10: Latches, Registers, RAM, Flip-Flops

L05: MOSFETs to Simple Gates

L02: Circuits Basics

Exam 1

L11: Computers

L12: Op Amps SPRING BREAK

SPRING BREAK

L03: Equivalent Circuits

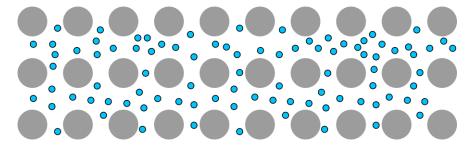
### Objectives of this Lecture

- Semiconductors
- Diodes
- Light Emitting Diodes (LEDs)

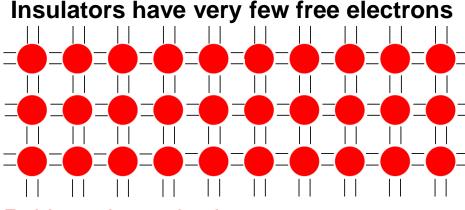
#### Conductors vs. Insulators

- Material conductivity is a material electrical property
- More free electrons, more current can flow

#### **Conductors have many free electrons**



Gold, copper, aluminum, salt water...

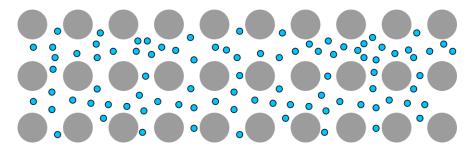


Rubber, glass, plastic, rust...

### Conductors vs. Insulators vs. Semiconductors

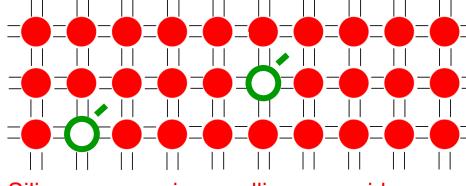
- Material conductivity is a material electrical property
- More free electrons, more current can flow

#### **Conductors have many free electrons**



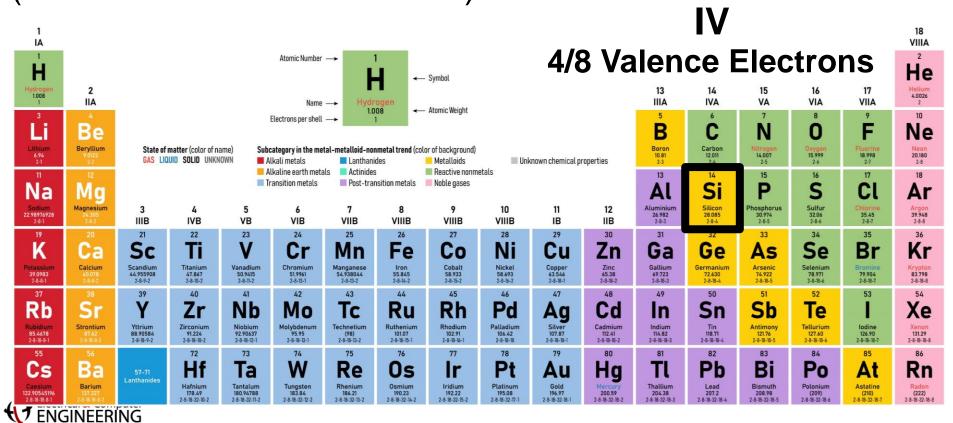
Gold, copper, aluminum, salt water...

#### Semiconductors have a few free electrons



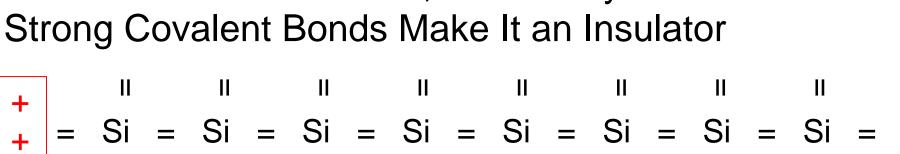
Silicon, germanium, gallium arsenide...

# Start with a Block of Pure, Electrically Neutral Silicon (Or Another Semiconductor) Column



### Start with a Block of Pure, Electrically Neutral Silicon:

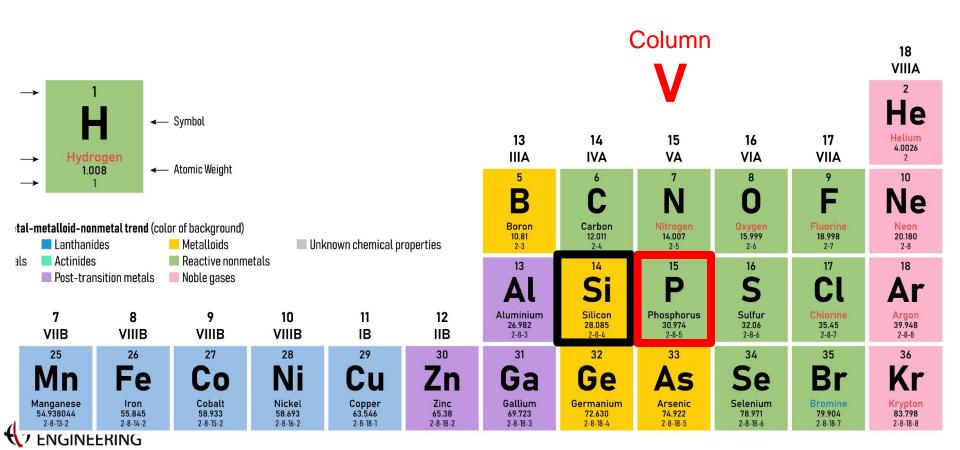
### Start with a Block of Pure, Electrically Neutral Silicon: Strong Covalent Bonds Make It an Insulator



= Si = Si = Si =

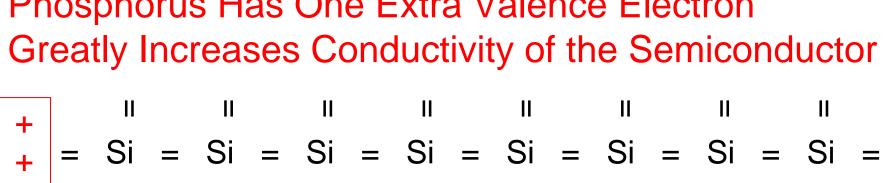
= Si = Si = Si =

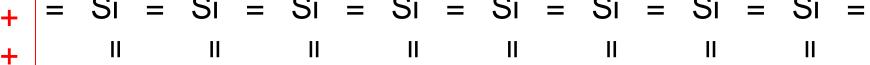
### Phosphorus Has One Extra Valence Electron (5/8)

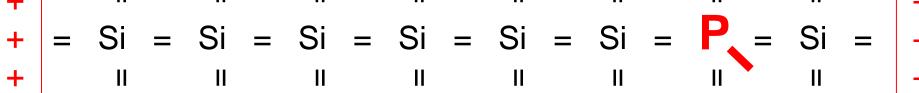


### Phosphorus Has One Extra Valence Electron

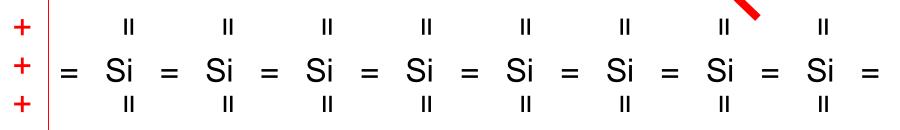
# Phosphorus Has One Extra Valence Electron



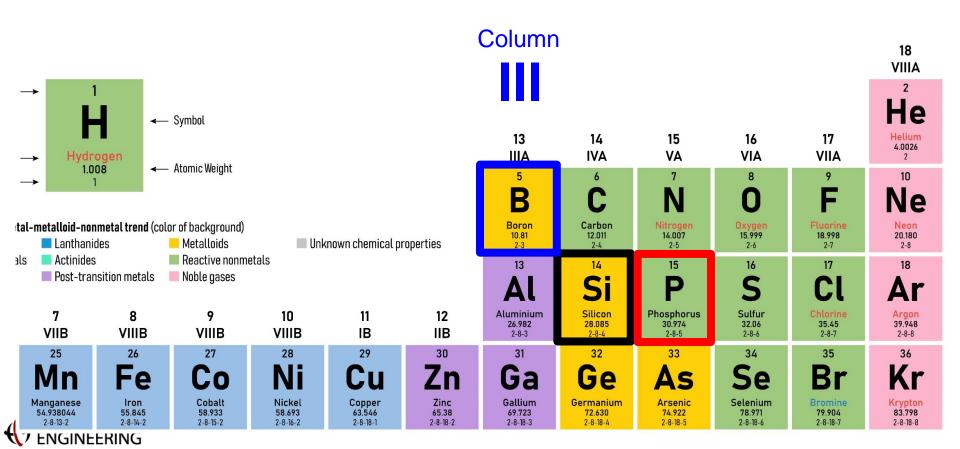




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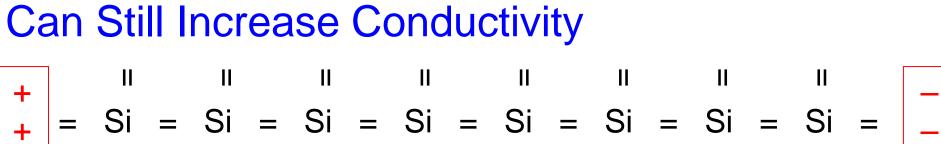
### Boron Has One Fewer Valence Electron (3/8)

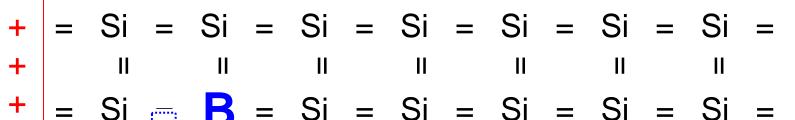


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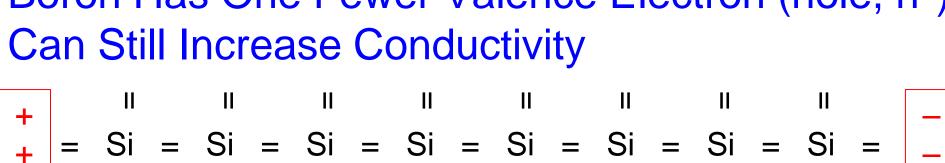








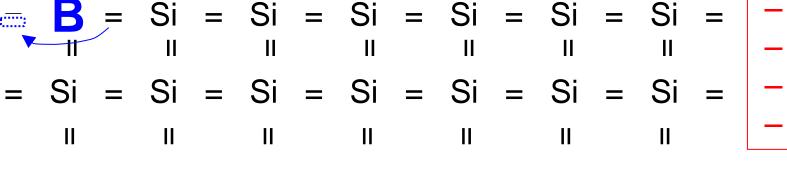
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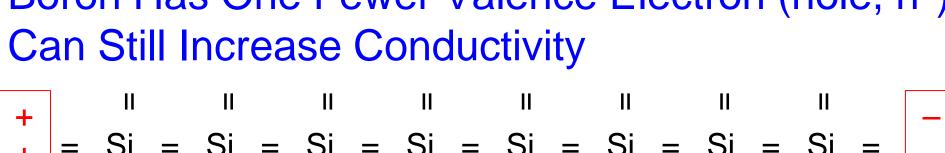


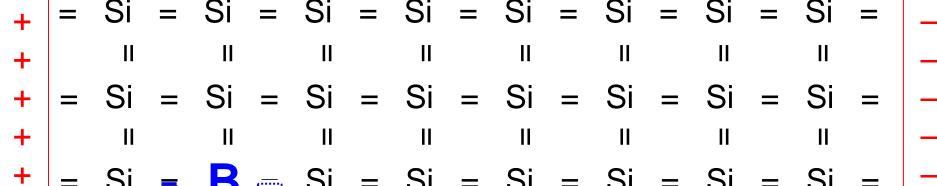
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$$= Si = Si = Si = Si$$



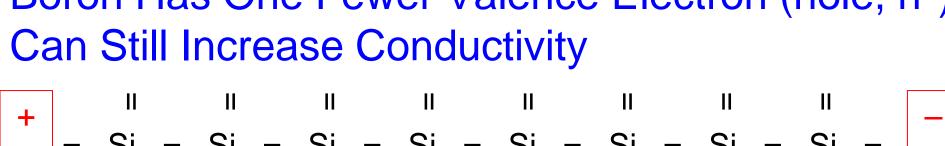


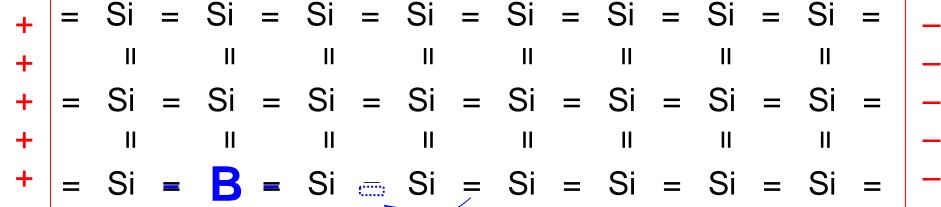




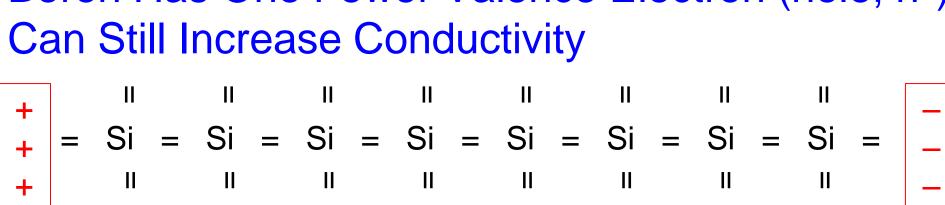
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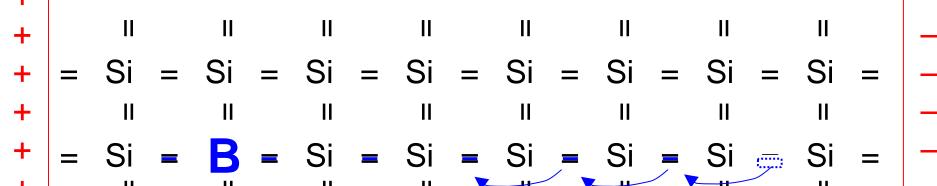
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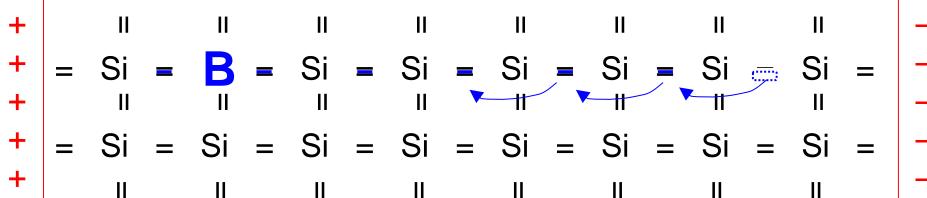




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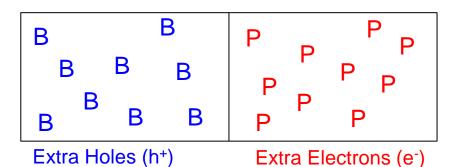






# Add a Small Amount of Boron (extra h<sup>+</sup>) and Phosphorus (extra e<sup>-</sup>) to Separate Areas

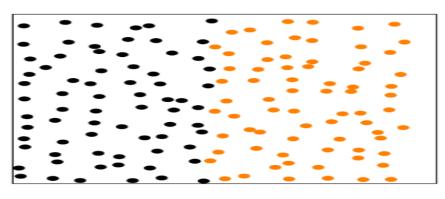
Fewer Electrons
P-Type Silicon

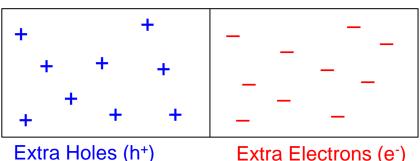


N-Type Silicon



### Extra (e<sup>-</sup>) and Missing (h<sup>+</sup>) Electrons Are Free to Diffuse (Randomly Drift Around)

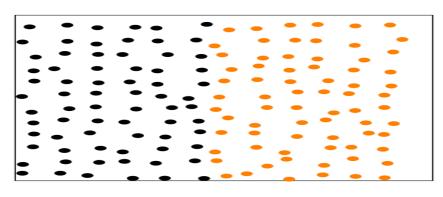


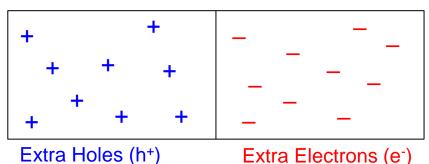


**Fewer Electrons** P-Type Silicon N-Type Silicon

Extra Electrons (e<sup>-</sup>)

### Extra (e<sup>-</sup>) and Missing (h<sup>+</sup>) Electrons Are Free to Diffuse (Randomly Drift Around)



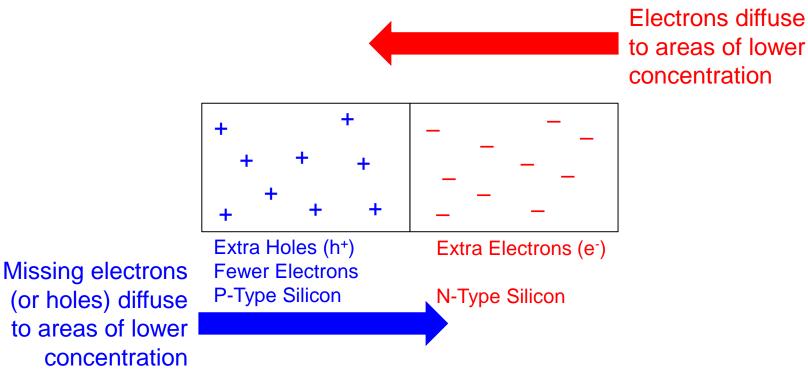


**Fewer Electrons** 

P-Type Silicon

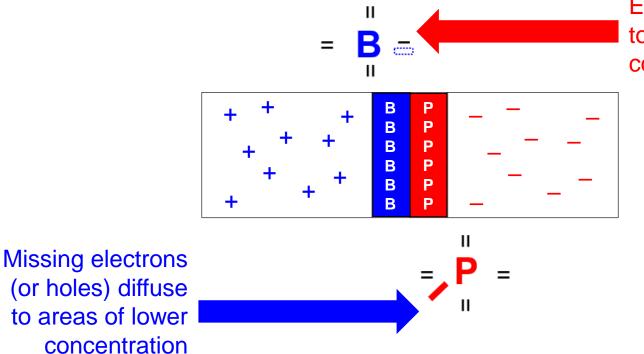
N-Type Silicon

### Extra (e<sup>-</sup>) and Missing (h<sup>+</sup>) Electrons Are Free to Diffuse (Randomly Drift Around)





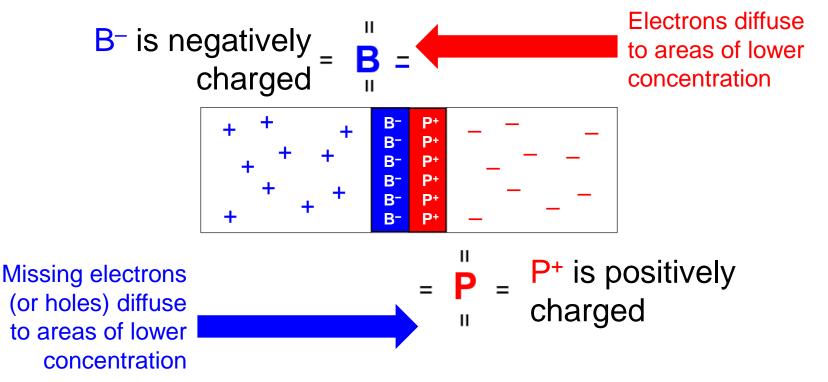
# P Nucleus Has One Additional Positive ChargeB Nucleus Has One Less Positive Charge



Electrons diffuse to areas of lower concentration

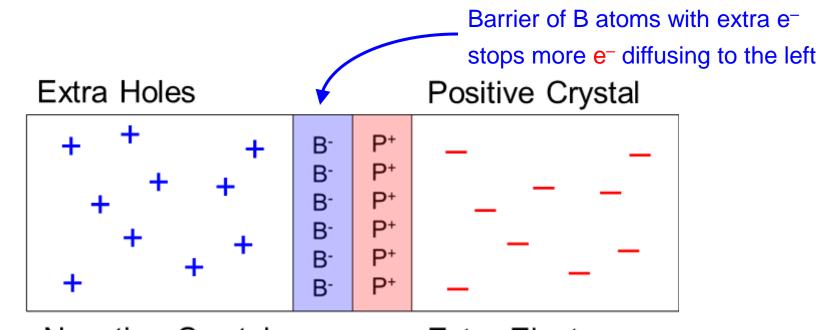
Electrical & Computer ENGINEERING

# P Nucleus Has One Additional Positive ChargeB Nucleus Has One Less Positive Charge





### Charged Barrier (~0.7V) Prevents More Diffusion

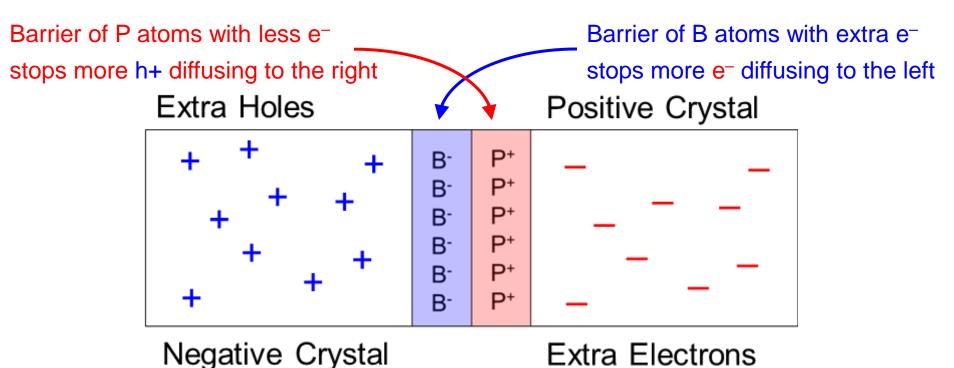


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Negative Crystal P-Type Silicon

Extra Electrons N-Type Silicon

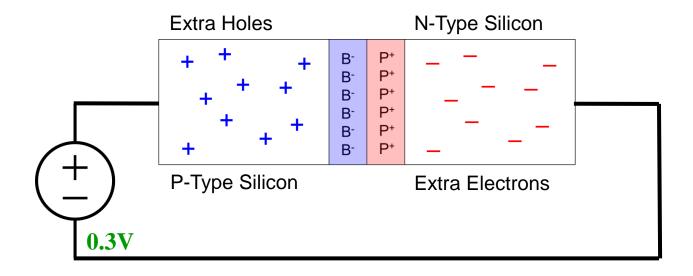
## Charged Barrier (~0.7V) Prevents More Diffusion



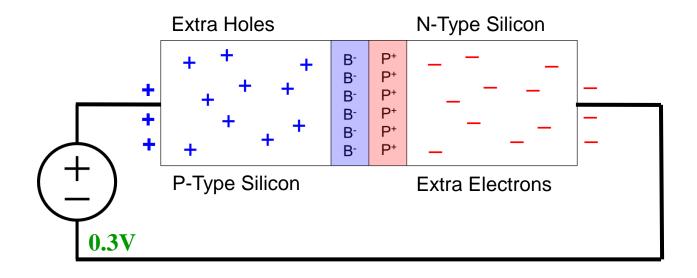
Electrical & Computer ENGINEERING

P-Type Silicon

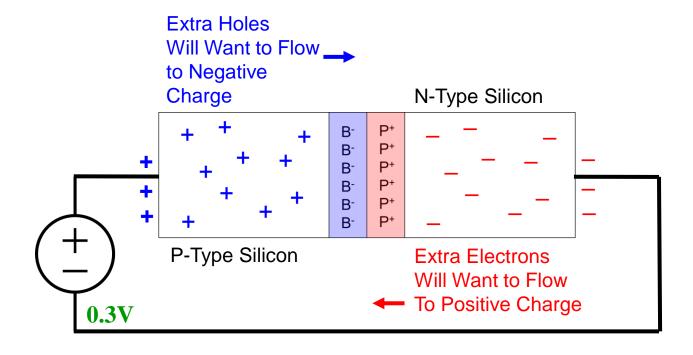
N-Type Silicon



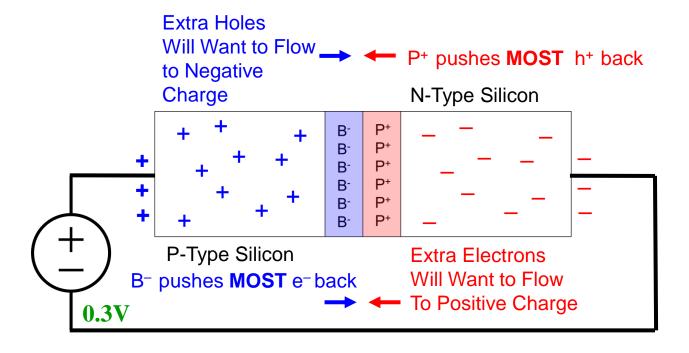






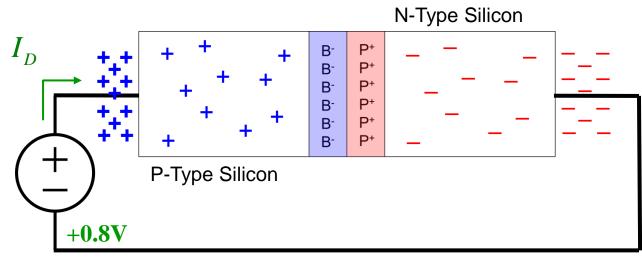








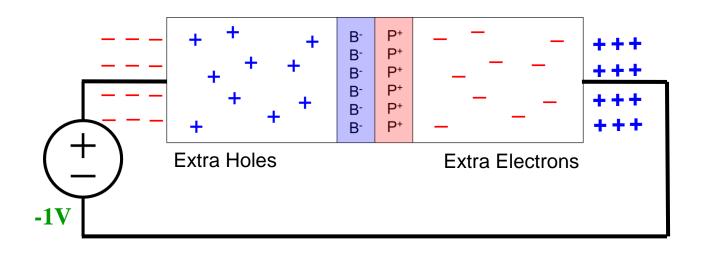
# Larger Positive Voltage (+0.7V) Overcomes B<sup>-</sup> / P<sup>+</sup> Barrier



Lots of current can flow

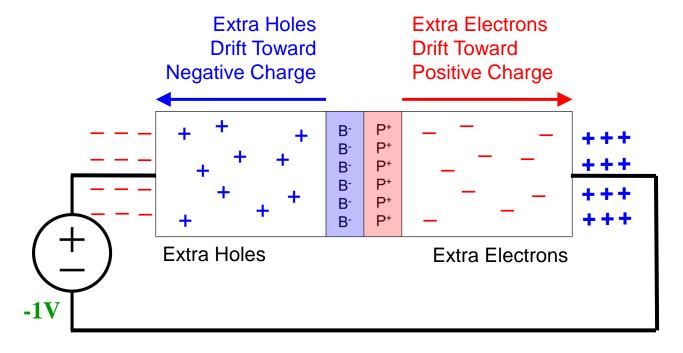


### Apply a Negative Diode Voltage (-1V) Almost No Diode Current Flows



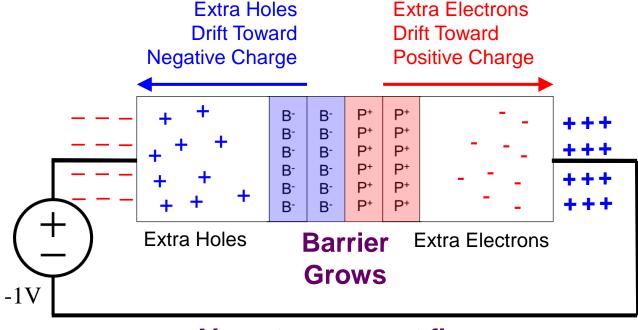


## Apply a Negative Diode Voltage (-1V) Almost No Diode Current Flows



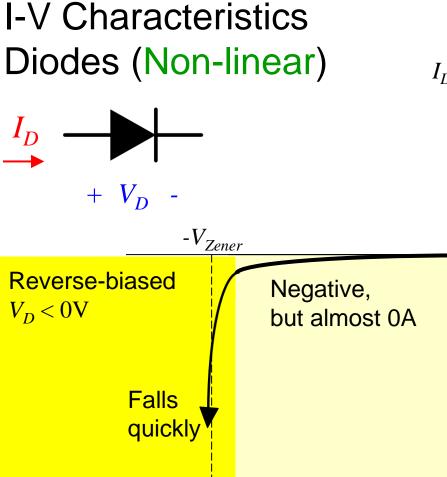


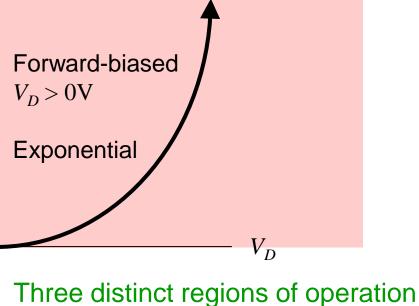
## Apply a Negative Diode Voltage (-1V) Almost No Diode Current Flows



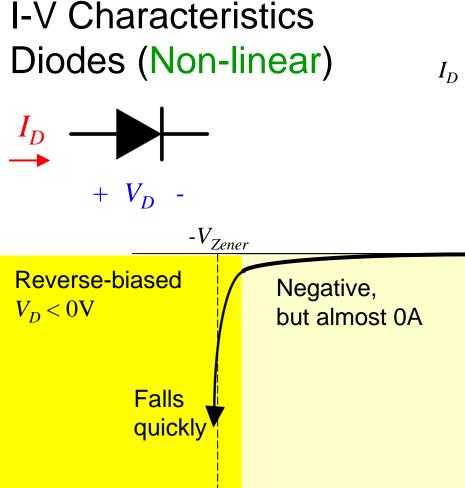
Almost no current flows

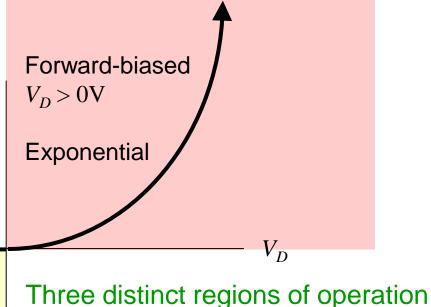






hree distinct regions of operation

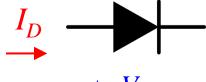




Diodes are relatively complicated, so we use **models** (**approximations**) to make our work easier

### Knee Model 18-100

 $I_D = 0$ A for  $V_D \le V_{KNEE}$ 

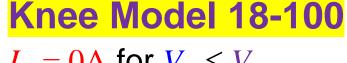


+  $V_D$  - "Reverse Bias"  $(V_D < 0 \text{V})$ 

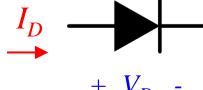
"Forward Bias" Region  $(V_D > 0V)$ 

**Three Rules:** 





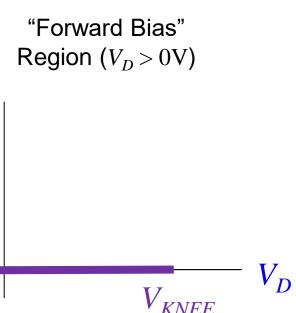
 $I_D = 0$ A for  $V_D \le V_{KNEE}$ 

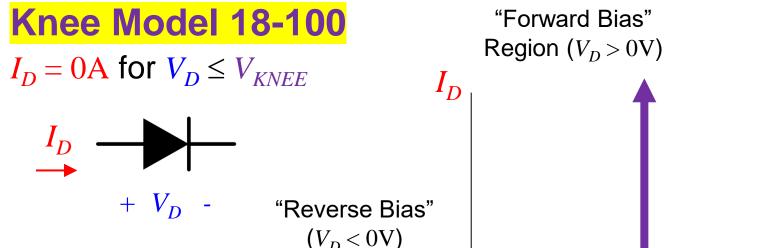


"Reverse Bias"  $(V_D < 0V)$ 

**Three Rules:** 

• If  $V_D < V_{KNFE}$ ,  $I_D = 0$ A





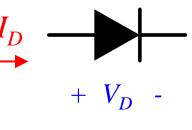
#### **Three Rules:**

- If  $V_D < V_{KNEE}$ ,  $I_D = 0$ A
- If  $V_D = V_{KNEE}$ ,  $I_D \ge 0$ A

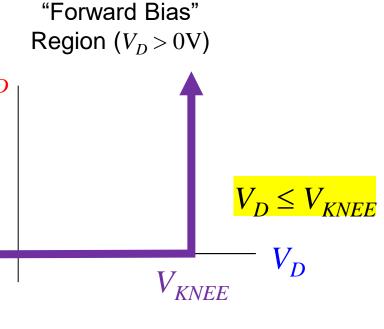


### Knee Model 18-100

 $I_D = 0$ A for  $V_D \le V_{KNEE}$ 



"Reverse Bias"  $(V_D < 0 \text{V})$ 



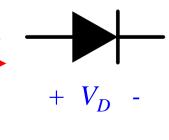
#### **Three Rules:**

- If  $V_D < V_{KNEE}$ ,  $I_D = 0$ A
- If  $V_D = V_{KNEE}$ ,  $I_D \ge 0$ A
- $V_D \le V_{KNEE}$



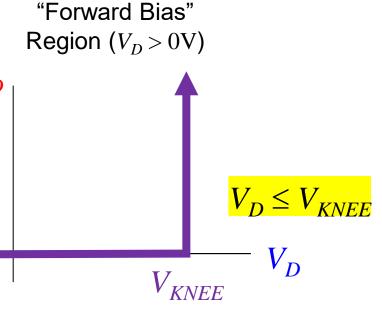
### Knee Model 18-100

 $I_D = 0$ A for  $V_D \le V_{KNEE}$ 



KIVEE

"Reverse Bias"  $(V_D < 0 \text{V})$ 



#### **Three Rules:**

- If  $V_D < V_{KNEE}$ ,  $I_D = 0$ A
- If  $V_D = V_{KNEE}$ ,  $I_D \ge 0$ A
- $V_D \leq V_{KNEE}$ ,  $I_D \leq V_{KNEE}$

~0.7V for silicon diodes

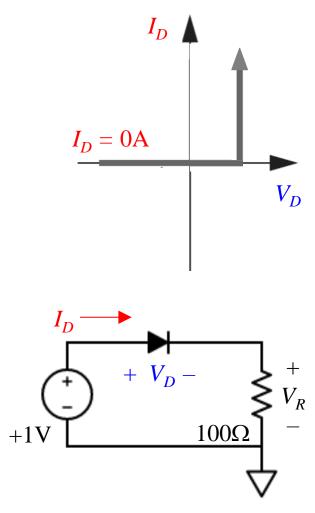
~2V for red LEDs

~2.5V for green LEDs

~3V for blue LEDs



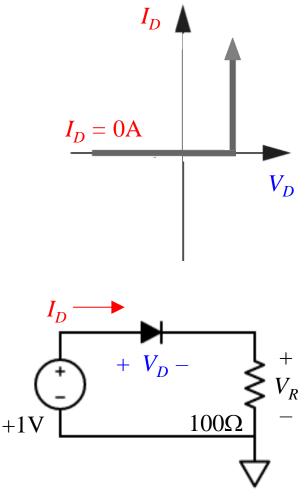
$$(V_{KNEE}=0.7V)$$



$$(V_{KNEE} = 0.7V)$$

KVL is always true. It does not depend upon the diode being on.

$$+1V = V_D + V_R$$

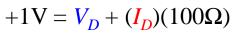


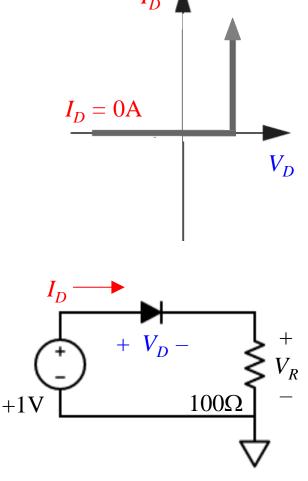
$$(V_{KNEE} = 0.7V)$$

KVL is always true. It does not depend upon the diode being on.

$$+1V = V_D + V_R$$

$$+1V = V_2 + (I_2)(1000)$$





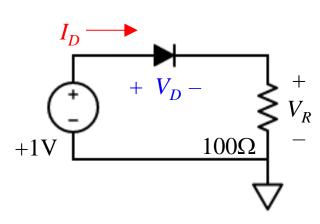
$$(V_{KNEE} = 0.7V)$$

KVL is always true. It does not depend upon the diode being on.

$$+1V = \frac{V_D}{V_D} + V_R$$

$$+1V = V_D + (I_D)(100\Omega)$$

Assume diode is on:  $V_D = V_{KNEE}$ 



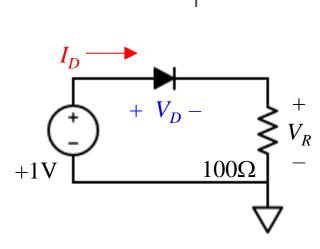


$$(V_{KNEE}=0.7V)$$

KVL is always true. It does not depend upon

$$+1V = V_D + V_R$$
 Assume diode is on:  $V_D = V_{KNEE}$ 

$$+1V = V_D + (I_D)(100\Omega) = 0.7V + (I_D)(100\Omega)$$



$$(V_{KNEE} = 0.7V)$$

KVL is always true. It does not depend upon the diode being on.

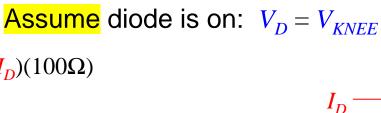
 $+1V = V_{D} + V_{R}$ 

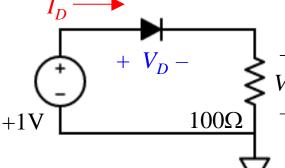
$$I_D =$$

+1V =











$$(V_{KNEE} = 0.7V)$$

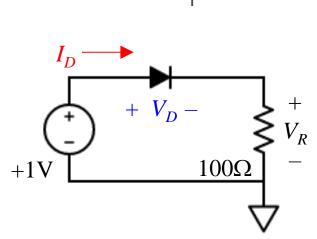
KVL is always true. It does not depend upon

$$+1V = V_D + V_R$$
 Assume diode is on:  $V_D = V_{KNEE}$ 
 $+1V = 0.7V + (I_D)(100\Omega)$ 

$$(100\Omega)$$

$$=0.7V + (I_D)(100\Omega)$$

$$I_D = (1V - 0.7V)/100\Omega = 3mA$$





$$(V_{KNEE} = 0.7V)$$

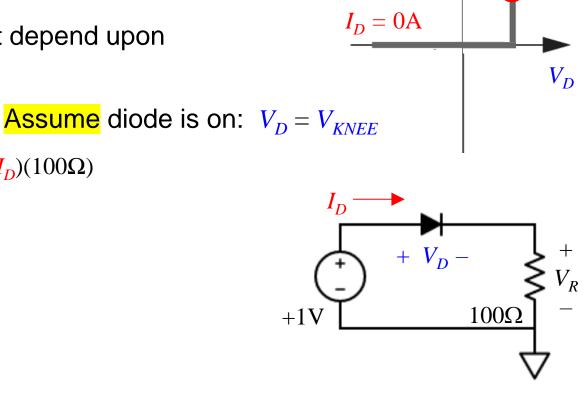
KVL is always true. It does not depend upon the diode being on.

$$+1V = V_D + V_R$$
 Assume

$$+1V = V_D + (I_D)(100\Omega) = 0.7V + (I_D)(100\Omega)$$

$$I_D = \left(1V - 0.7V\right) / 100\Omega = 3mA$$

**Check assumption:** 





$$(V_{KNEE} = 0.7V)$$

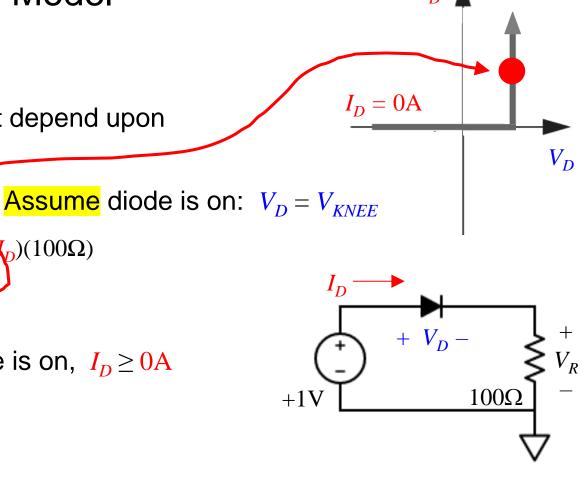
KVL is always true. It does not depend upon the diode being on.

$$+1V = V_D + V_R$$

$$+1V = V_D + (I_D)(100\Omega) = 0.7V + (V_D)(100\Omega)$$

 $I_D = (1V - 0.7V)/100\Omega = 3mA$ 

Check assumption: If diode is on,  $I_D \ge 0$ A



$$(V_{KNEE} = 0.7V)$$

KVL is always true. It does not depend upon the diode being on.

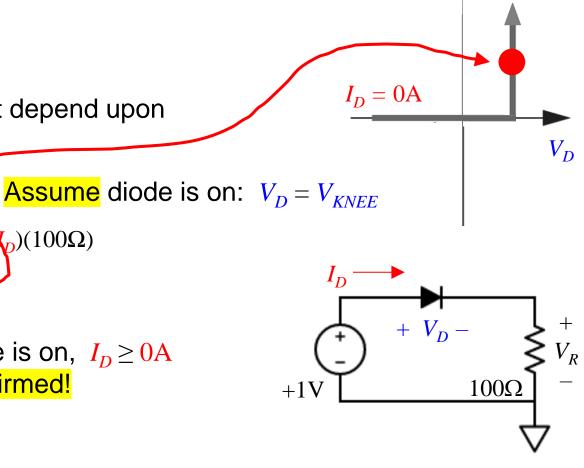
$$+1V = V_D + V_R$$

 $+1V = V_D + (I_D)(100\Omega) = 0.7V + (V_D)(100\Omega)$ 

 $I_D = (1V - 0.7V)/100\Omega = 3mA$ 

Check assumption: If diode is on, 
$$I_D \ge 0$$
A

 $3mA \ge 0A$ , assumption confirmed!



(approximation)  $(V_{KNFF}=0.7V)$ 

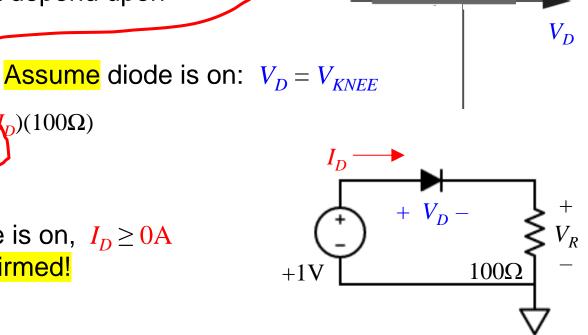
KVL is always true. It does not depend upon the diode being on.

$$+1V = V_D + V_R$$

 $+1V = V_D + (I_D)(100\Omega) = 0.7V + (V_D)(100\Omega)$ 

$$I_D = (1V - 0.7V)/100\Omega = 3mA$$

Check assumption: If diode is on,  $I_D \ge 0$ A  $3mA \ge 0A$ , assumption confirmed!



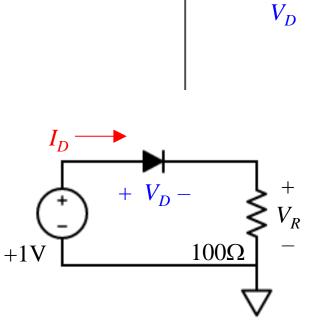
# Using the Diode Knee Model $(V_{KNEE} = 0.7V)$ (appro

(approximation)

KVL is always true. It does not depend upon the diode being on.

$$+1V = V_D + V_R$$

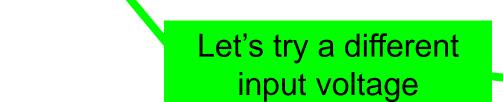
Let's try a different input voltage

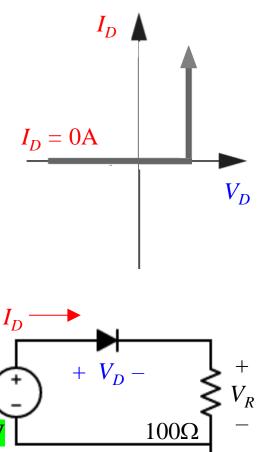


### Using the Diode Knee Model $(V_{KNEE} = 0.7V)$

(approximation)

KVL is always true. It does not depend upon the diode being on.



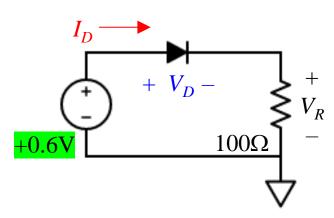


 $+0.6V = V_D + (I_D)(100\Omega)$ 

$$(V_{KNEE} = 0.7V)$$
 (approximation)

KVL is always true. It does not depend upon

Assume diode is on:  $V_D = V_{KNEE}$  $+0.6V = V_D + (I_D)(100\Omega)$ 





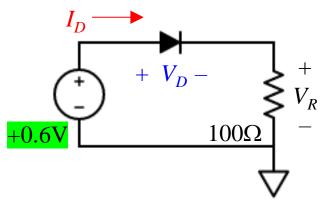
$$(V_{KNEE} = 0.7V)$$
 (approximation)

KVL is always true. It does not depend upon the diode being on.

$$\frac{+0.6\text{V}}{100} = V_D + (I_D)(100\Omega)$$

$$+0.6V = 0.7V + (I_D)(100\Omega)$$

Assume diode is on:  $V_D = V_{KNEE}$ 





### Using the Diode Knee Model $(V_{KNEE} = 0.7V)$

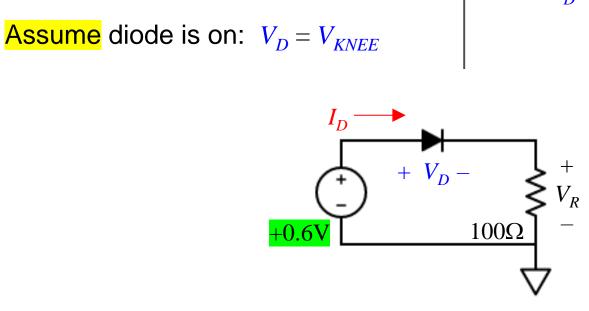
(approximation)

KVL is always true. It does not depend upon the diode being on.

$$+0.6\mathbf{V} = V_D + (I_D)(100\Omega)$$

 $+0.6V = 0.7V + (I_D)(100\Omega)$ 

 $I_D =$ 





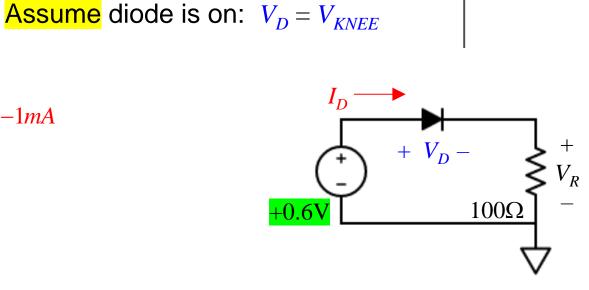
$$(V_{KNEE} = 0.7V)$$
 (approximation)

KVL is always true. It does not depend upon the diode being on.

$$\frac{+0.6V}{+0.6V} = V_D + (I_D)(100\Omega)$$

$$+0.6V = 0.7V + (I_D)(100\Omega)$$

$$I_D = (0.6V - 0.7V)/100\Omega = -1mA$$



### Using the Diode Knee Model $(V_{KNEE} = 0.7V)$

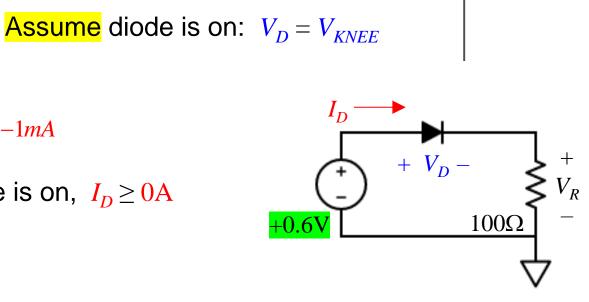
KVL is always true. It does not depend upon the diode being on.

$$+0.6\mathbf{V} = V_D + (I_D)(100\Omega)$$

 $+0.6V = 0.7V + (I_D)(100\Omega)$ 

$$I_D = (0.6V - 0.7V)/100\Omega = -1mA$$

Check assumption: If diode is on,  $I_D \ge 0$ A





### Using the Diode Knee Model $(V_{KNEE} = 0.7V)$

(approximation)

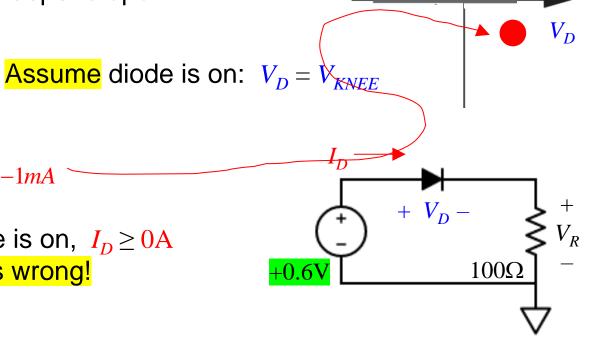
KVL is always true. It does not depend upon the diode being on.

$$+0.6V = V_D + (I_D)(100\Omega)$$

 $+0.6V = 0.7V + (I_D)(100\Omega)$ 

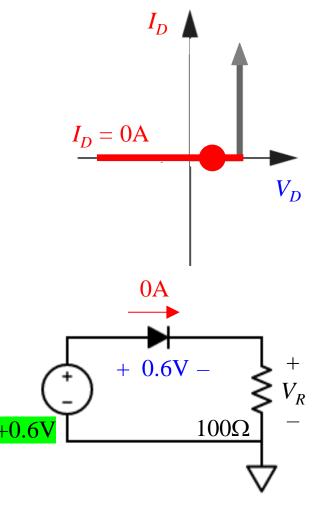
$$I_D = (0.6V - 0.7V)/100\Omega = -1mA$$

Check assumption: If diode is on,  $I_D \ge 0$ A -1mA ≥ 0A, assumption was wrong!



$$(V_{KNEE}=0.7V)$$

KVL is always true. It does not depend upon the diode being on.

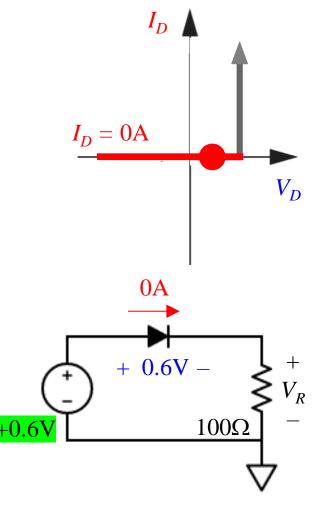




$$(V_{KNEE}=0.7V)$$

KVL is always true. It does not depend upon the diode being on.

$$+0.6V = V_D + (I_D)(100\Omega)$$

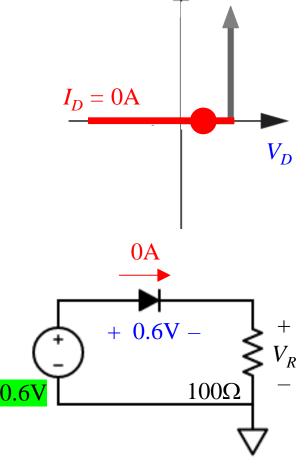


$$(V_{KNEE}=0.7V)$$

KVL is always true. It does not depend upon the diode being on.

$$\frac{+0.6V}{} = V_D + (I_D)(100\Omega)$$

$$+0.6V = V_D + (0A)(100\Omega)$$



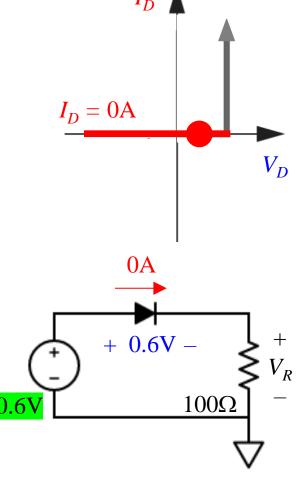
$$(V_{KNEE} = 0.7V)$$

KVL is always true. It does not depend upon the diode being on.

$$\frac{+0.6V}{} = V_D + (I_D)(100\Omega)$$

$$+0.6V = V_D + (0A)(100\Omega)$$

$$V_D =$$





$$(V_{KNEE}=0.7V)$$

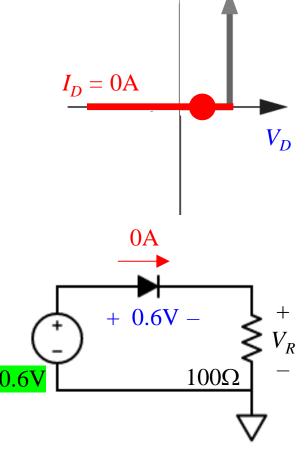
KVL is always true. It does not depend upon the diode being on.

$$+0.6V = V_D + (I_D)(100\Omega)$$

Diode is off: 
$$I_D = 0$$
A

$$+0.6V = V_D + (0A)(100\Omega)$$

$$V_D = \frac{+0.6\text{V}}{-(0\text{A})(100\Omega)} = +0.6\text{V}$$





$$(V_{KNEE}=0.7V)$$

KVL is always true. It does not depend upon the diode being on.

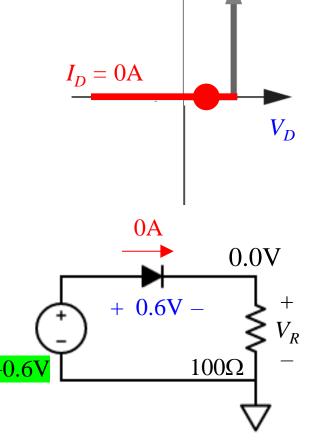
$$+0.6\mathbf{V} = V_D + (I_D)(100\Omega)$$

Diode is off: 
$$I_D = 0$$
A

$$+0.6V = V_D + (0A)(100\Omega)$$

$$V_D = \frac{+0.6\text{V}}{-(0\text{A})(100\Omega)} = +0.6\text{V}$$

$$V_R = \frac{0.6 \text{V}}{0.6 \text{V}} - 0.6 \text{V} = 0 \text{V} = (\frac{0 \text{A}}{0.00})(100 \Omega)$$





$$(V_{KNEE}=0.7V)$$

KVL is always true. It does not depend upon the diode being on.

$$+0.6\mathbf{V} = \mathbf{V_D} + (\mathbf{I_D})(100\Omega)$$

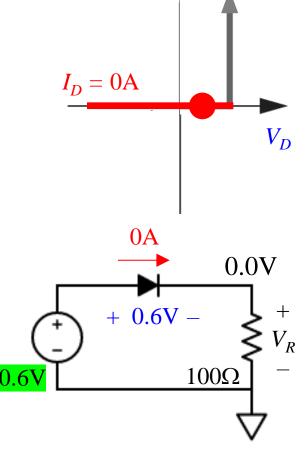
Diode is off:  $I_D = 0A$ 

$$+0.6V = V_D + (0A)(100\Omega)$$

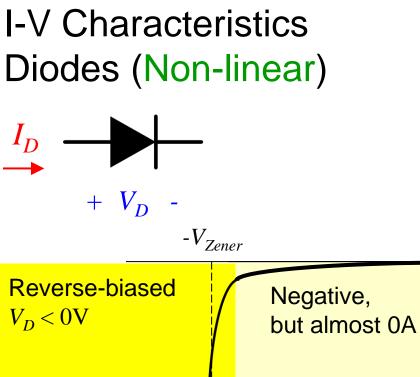
$$V_D = +0.6V - (0A)(100\Omega) = +0.6V$$

$$V_R = 0.6V - 0.6V = 0V = (0A)(100\Omega)$$

#### Diode is off: $I_D = 0$ A, and $V_D = 0.6$ V < $V_{KNEE}$

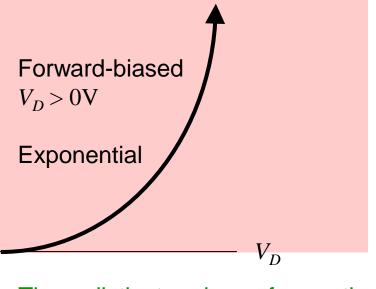






Falls

quickly



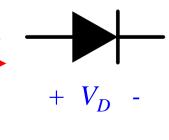
Three distinct regions of operation

Diodes are relatively complicated,
so we use **models** (**approximations**)

to make our work easier

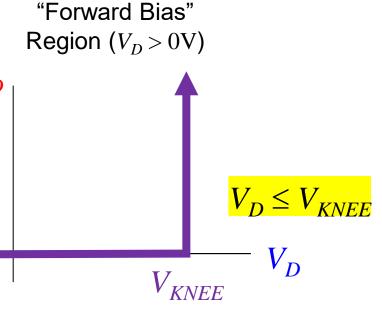
### Knee Model 18-100

 $I_D = 0$ A for  $V_D \le V_{KNEE}$ 



KIVEE

"Reverse Bias"  $(V_D < 0 \text{V})$ 



#### **Three Rules:**

- If  $V_D < V_{KNEE}$ ,  $I_D = 0$ A
- If  $V_D = V_{KNEE}$ ,  $I_D \ge 0$ A
- $V_D \leq V_{KNEE}$ ,  $I_D \leq V_{KNEE}$

~0.7V for silicon diodes

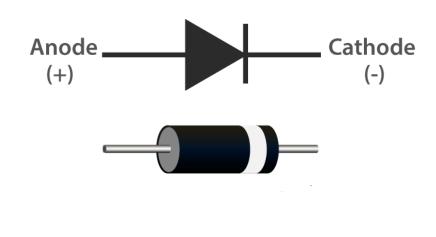
~2V for red LEDs

~2.5V for green LEDs

~3V for blue LEDs



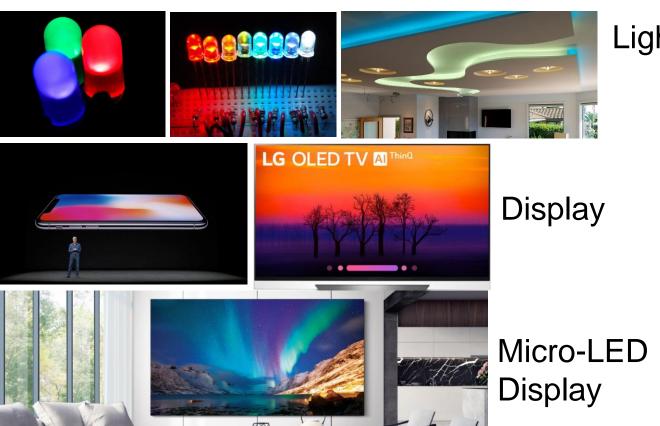
#### Diodes IRL (In Real Life)



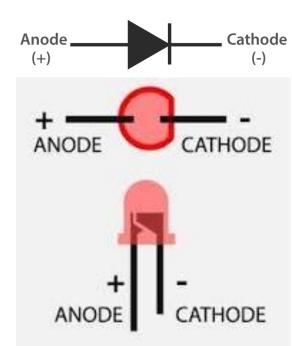




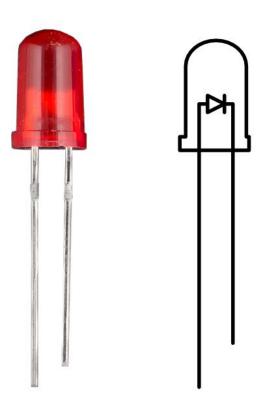
### Light Emitting Diodes (LEDs)

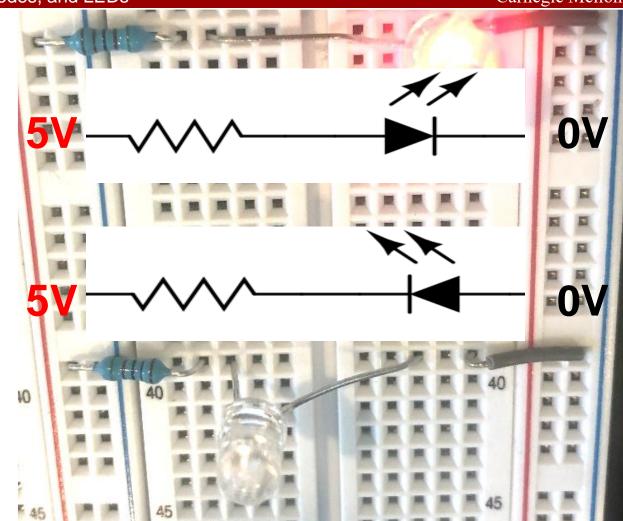


Lighting



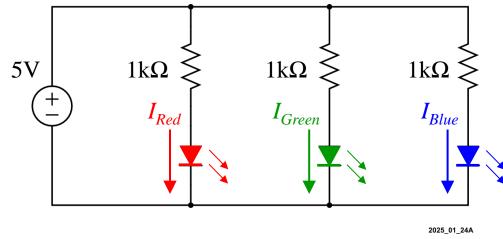
## Wiring Diodes

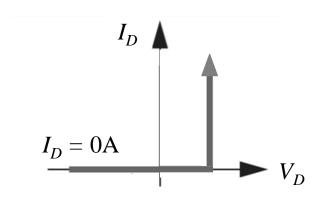




Red  $(V_{KNEE} = 2V)$ Green  $(V_{KNEE} = 2.5V)$  & Blue  $(V_{KNEE} = 3V)$ 

Blue  $(V_{KNEE} = 3V)$ LEDs



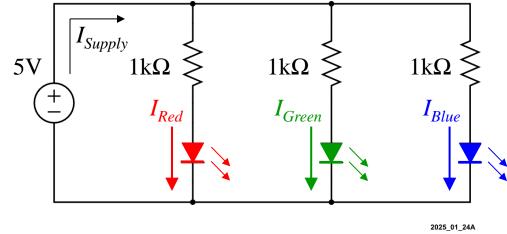


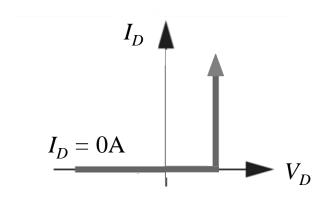
Red  $(V_{KNEE} = 2V)$ 

Green  $(V_{KNEE} = 2.5V)$  &

Blue ( $V_{KNEE} = 3V$ )

LEDs: Find  $I_{Supply}$ 



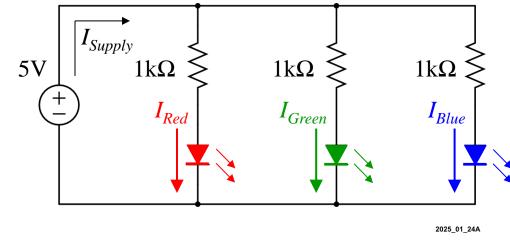


Red  $(V_{KNEE} = 2V)$ 

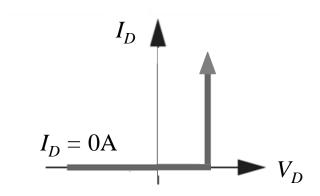
Green  $(V_{KNEE} = 2.5V)$  &

Blue  $(V_{KNEE} = 3V)$ 

LEDs: Find  $I_{Supply}$ 





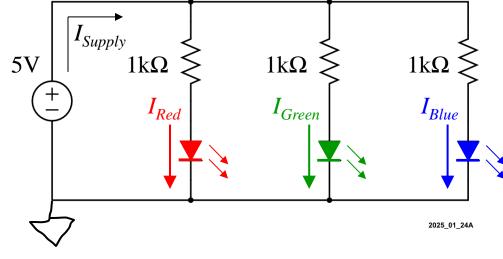


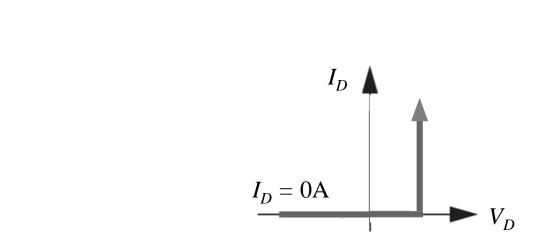
Red  $(V_{KNEE} = 2V)$ Green  $(V_{KNEE} = 2)$ 

Green  $(V_{KNEE} = 2.5V)$  &

Blue  $(V_{KNEE} = 3V)$ 

LEDs: Find  $I_{Supply}$ 

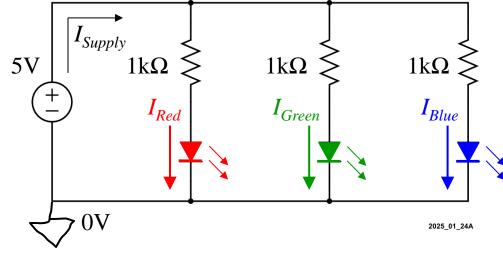


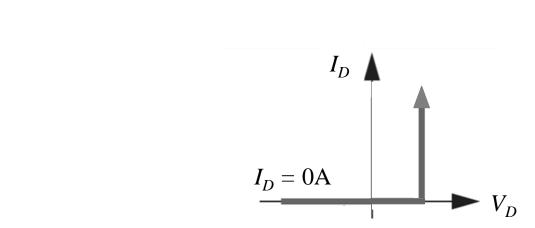




Red  $(V_{KNEE} = 2V)$ Green  $(V_{KNEE} = 2.5V)$  & Blue  $(V_{KNEE} = 3V)$ 

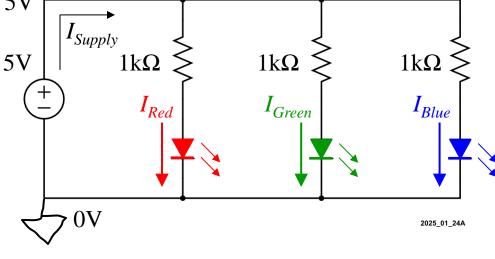
LEDs: Find  $I_{Supply}$ 

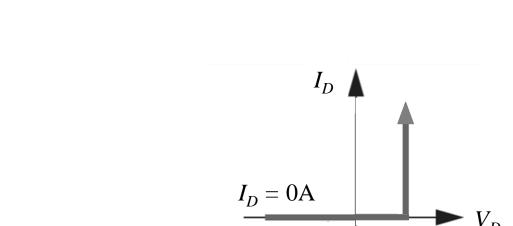




Red  $(V_{KNEE} = 2V)$ Green  $(V_{KNEE} = 2.5V)$  & Blue  $(V_{KNEE} = 3V)$ 

LEDs: Find  $I_{Supply}$ 



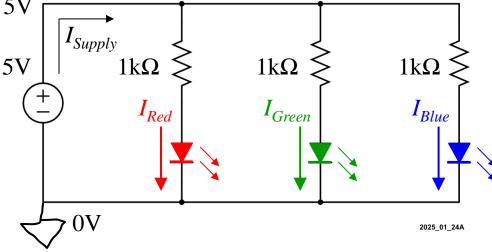


Green ( $V_{KNEE} = 2.5V$ ) & Blue ( $V_{KNEE} = 3V$ )

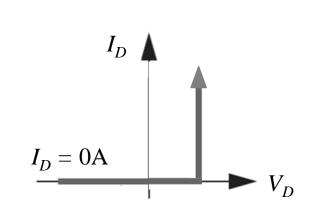
LEDs: Find  $I_{Supply}$ 

Assume On  $(V_D = V_{KNEE})$ 

KVL is always true:  $5V = I_{Red}(1k\Omega) + 2V$ 







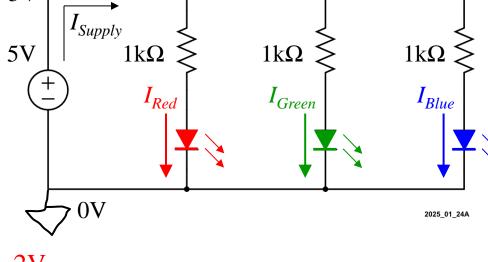


LEDs: Find  $I_{Supply}$ 

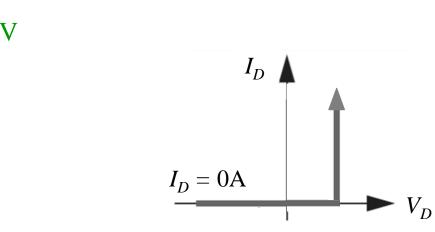
Assume On  $(V_D = V_{KNEE})$ 



KVL is always true:  $5V = I_{Red}(1k\Omega) + 2V$  $5V = I_{Green}(1k\Omega) + 2.5V$ 







 $1k\Omega$ 

2025 01 24A

Green  $(V_{KNEE} = 2.5V)$  &

Blue  $(V_{KNEE} = 3V)$ 

LEDs: Find  $I_{Supply}$ 

Assume On  $(V_D = V_{KNEE})$ 

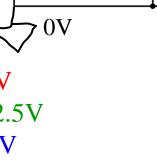
KVL is always true:

 $5V = I_{Red}(1k\Omega) + 2V$  $5V = I_{Green}(1k\Omega) + 2.5V$ 

 $5V = I_{Blue}(1k\Omega) + 3V$ 

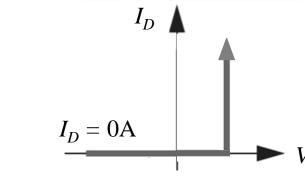


5V

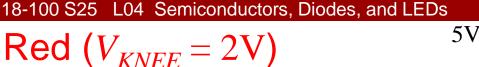


 $1k\Omega$ 

 $I_{Red}$ 



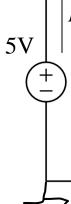
 $1k\Omega$ 





Carnegie Mellon

 $1k\Omega$ 

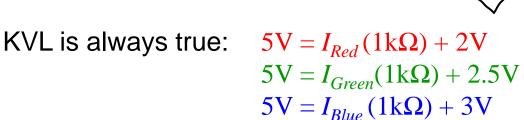


 $1k\Omega$  $1k\Omega$  $I_{Red}$ 

Assume On 
$$(V_D = V_{KNEE})$$

Blue  $(V_{KNEE} = 3V)$ 

LEDs: Find  $I_{Supply}$ 



Green  $(V_{KNEE} = 2.5V)$  &

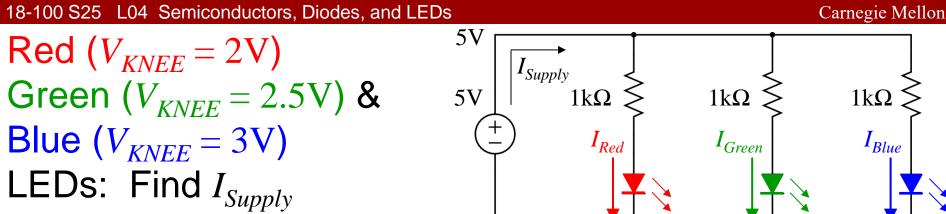
 $I_{Rod} = 3.0 \text{mA}$  $I_{Green} = 2.5 \text{mA}$  $I_{Blue} = 2.0 \text{mA}$ 

**Assumption** Confirmed  $(I_D=0A)$ 

2025 01 24A



 $I_D = 0A$ 



Assume On  $(V_D = V_{KNEE})$ 

KVL is always true:

$$I_{SE}$$

$$5V = I_{Red} (1k\Omega) + 2V$$

$$5V = I_{Green} (1k\Omega) + 2.5$$

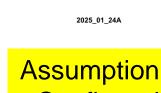
$$5V = I_{Blue} (1k\Omega) + 3V$$

$$I_R$$
.5V  $I_G$ 

$$I_{Red} = 3.0 \text{mA}$$
 $I_{Green} = 2.5 \text{mA}$ 

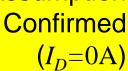


 $I_D = 0A$ 



$$5V = I_{Green}(1k\Omega) + 2.5V$$
  $I_{Green} = 2.5mA$   
 $5V = I_{Blue}(1k\Omega) + 3V$   $I_{Blue} = 2.0mA$ 



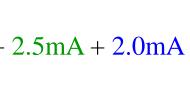






= 7.5 mA





Light

## Light Emitting Diode (LED)

Converts electrical energy to photon energy

$$E_{Photon} \approx (e^{-})(V_{KNEE})$$

$$V_{KNEE,RED\,LED} \approx 2V$$

$$E_{Photon} \approx (1.60x10^{-19}C)(2V) = 3.20x10^{-19}J$$

 $f = \frac{c}{2}$ 

Longer

Anode

leg

 $E_{Photon} = hf$ 

$$E_{Photon} = \frac{hc}{2} \qquad 3.20x10^{-19} J = \frac{\left(6.63x10^{-34} J \cdot s\right)\left(3.00x10^{-8} m / s\right)}{2}$$

$$(3.00x10^{-8} m/s)$$

diode

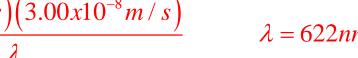
Epoxy

case -

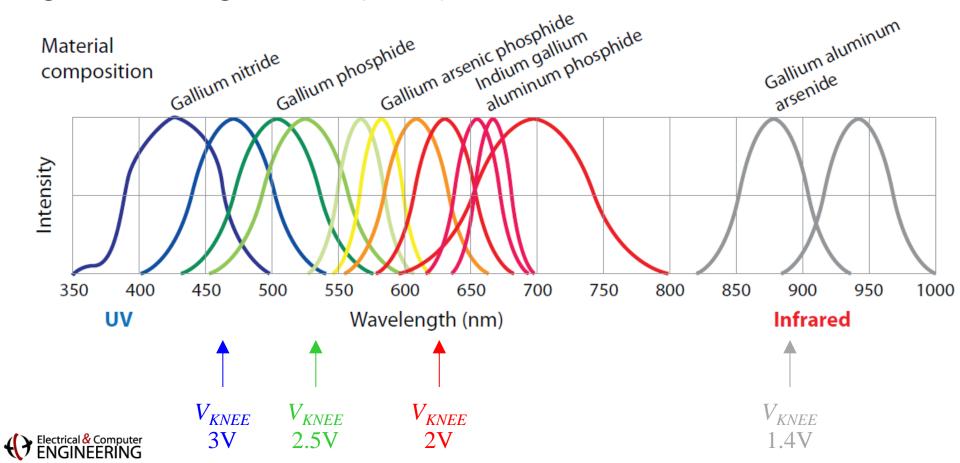
Lens

Light-emitting semiconductor

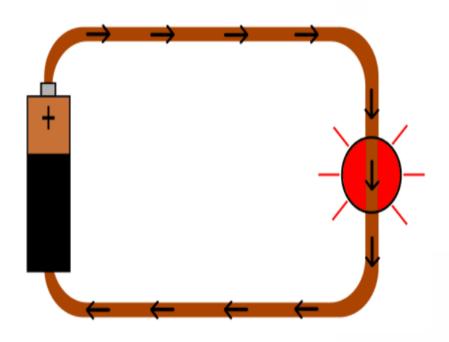


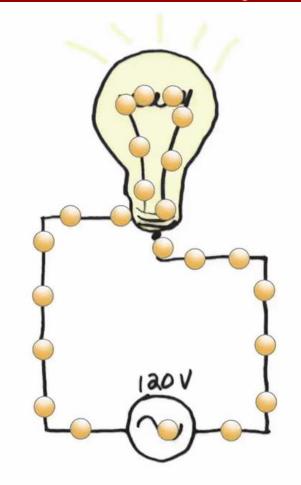


### Light Emitting Diode (LED)



### DC vs. AC Power Systems

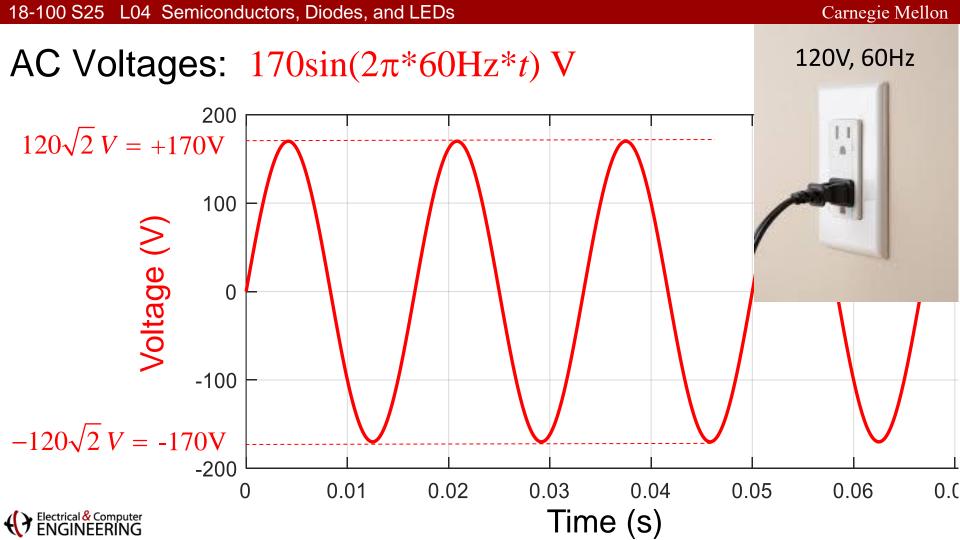




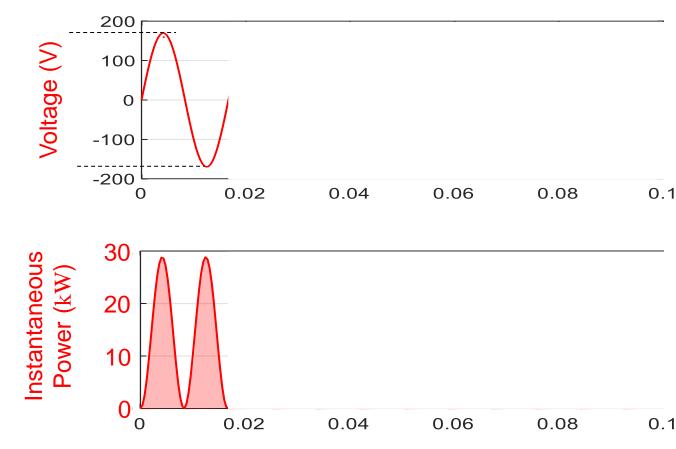


## AC Voltages:



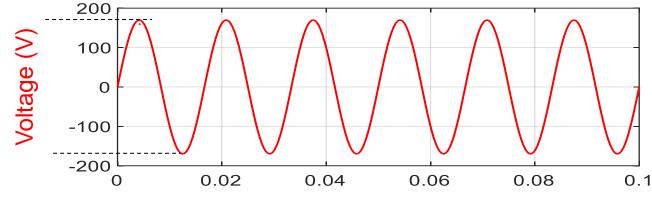


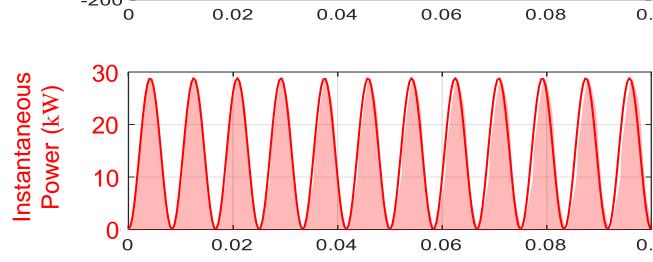
$$P(t) = \frac{V(t)}{R}$$



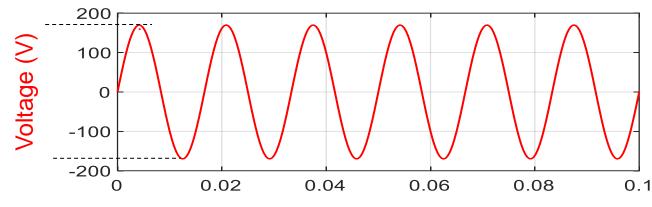


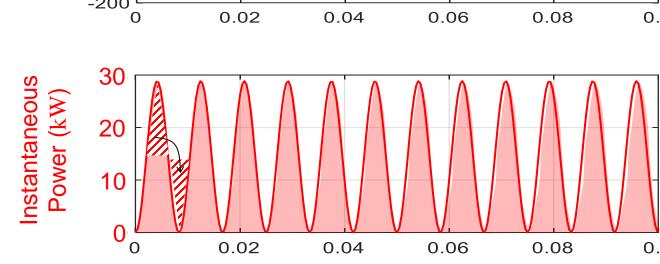
$$P(t) = \frac{V^2(t)}{R}$$



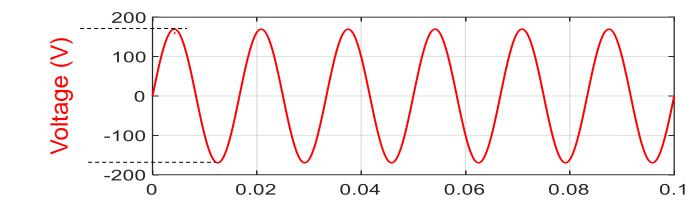


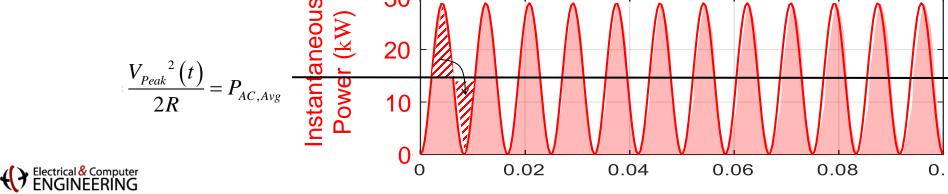
$$P(t) = \frac{V^2(t)}{R}$$



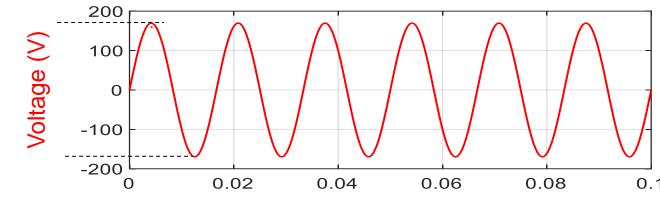


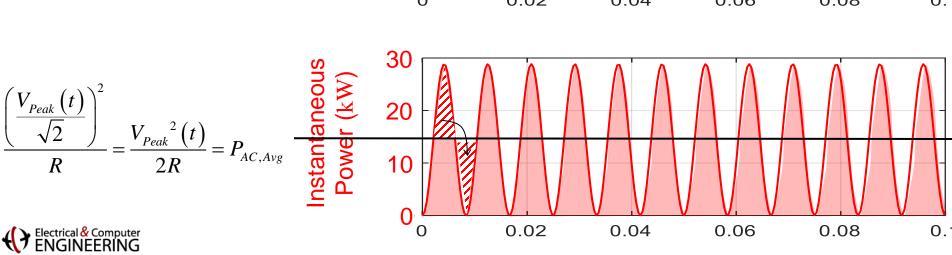
$$P(t) = \frac{V^2(t)}{R}$$





$$P(t) = \frac{V^2(t)}{R}$$





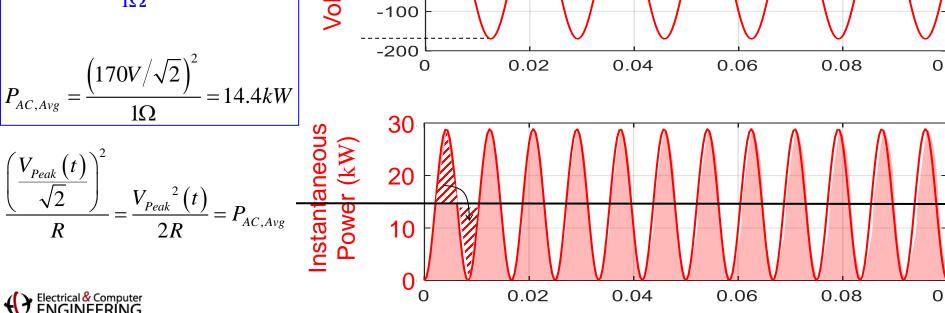
$$P(t) = \frac{V^{2}(t)}{R}$$

$$P_{DC,Avg} = \frac{(120V_{DC})^{2}}{1\Omega} = 14.4kW$$

$$P_{AC,Avg} = \frac{(170V/\sqrt{2})^{2}}{100} = 14.4kW$$

$$P_{AC,Avg} = \frac{1}{1}\Omega$$

$$P_{AC,Avg} = \frac{\left(170V/\sqrt{2}\right)^2}{1}\Omega = 14.4kW$$



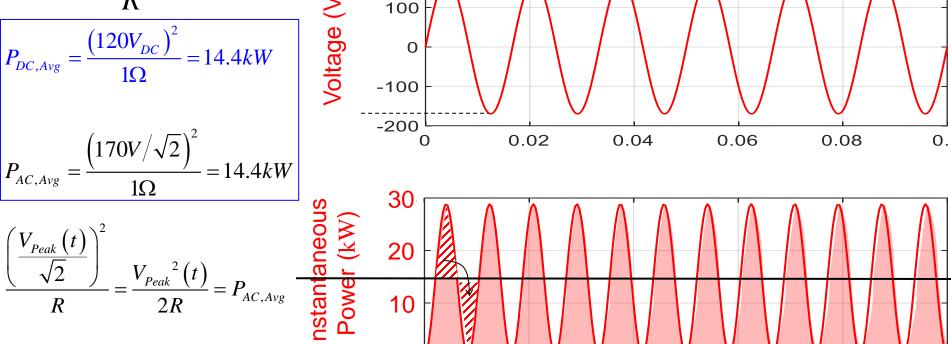


$$P(t) = \frac{V^{2}(t)}{R}$$

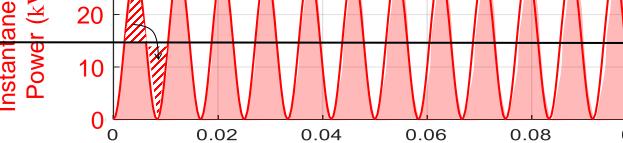
$$P_{DC,Avg} = \frac{(120V_{DC})^{2}}{1\Omega} = 14.4kW$$

$$P_{AC,Avg} = \frac{(170V/\sqrt{2})^{2}}{1} = 14.4kW$$

$$P_{AC,Avg} = \frac{(170V/\sqrt{2})^{2}}{1} = 14.4kW$$



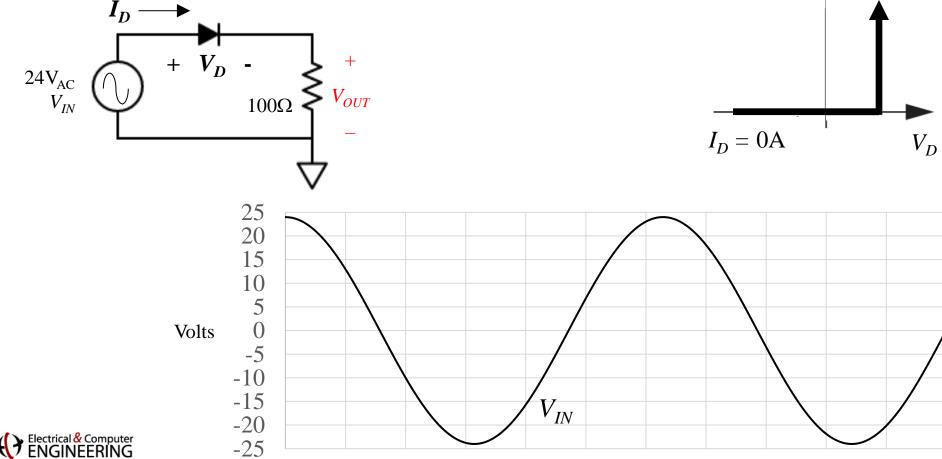




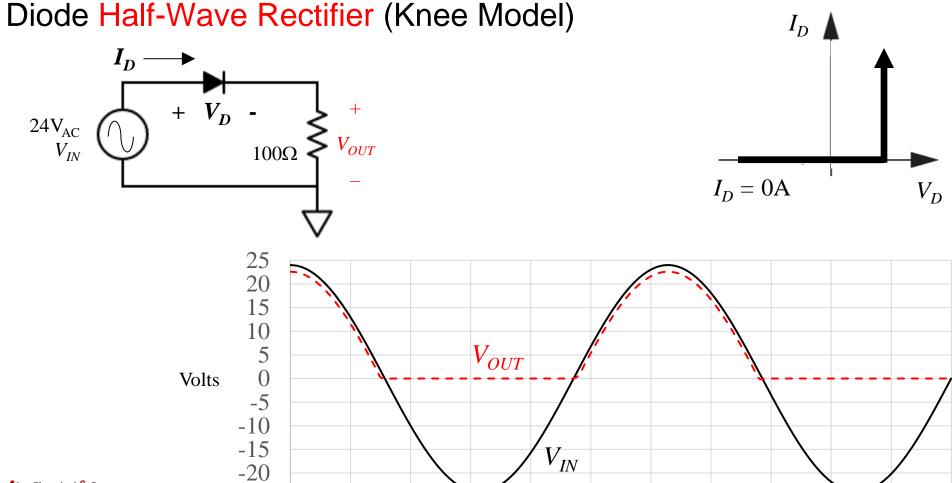
#### How Do We Convert AC Power to DC?



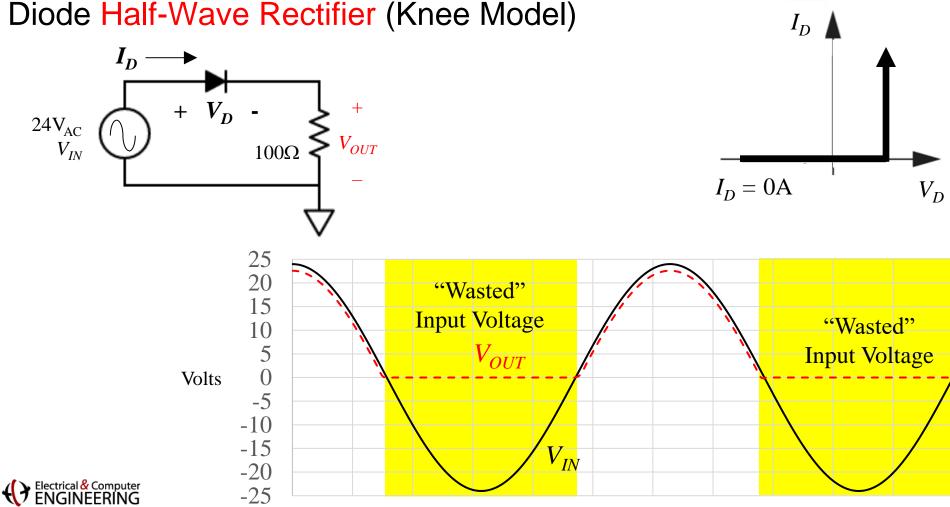


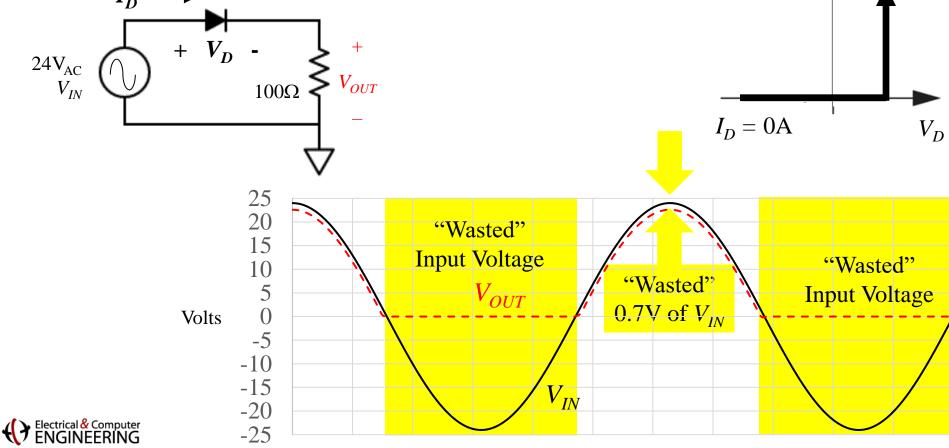


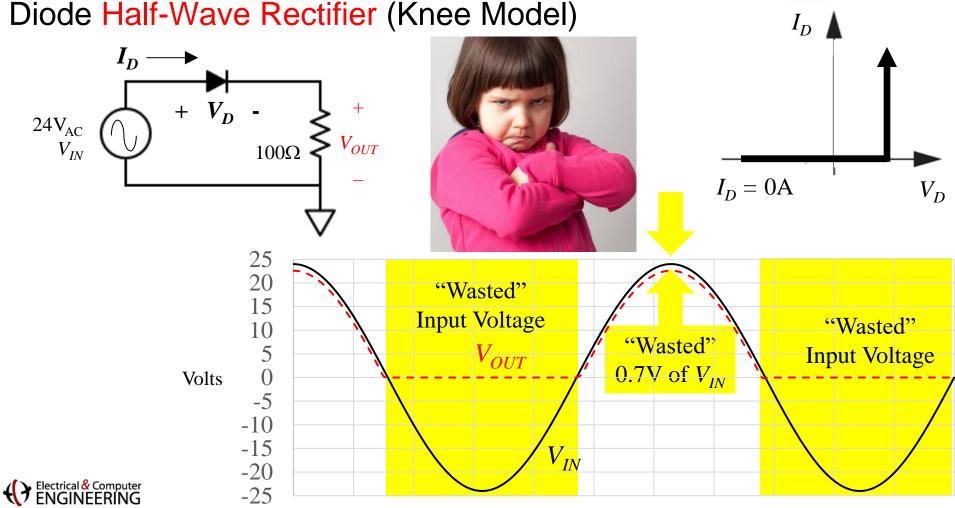
-25



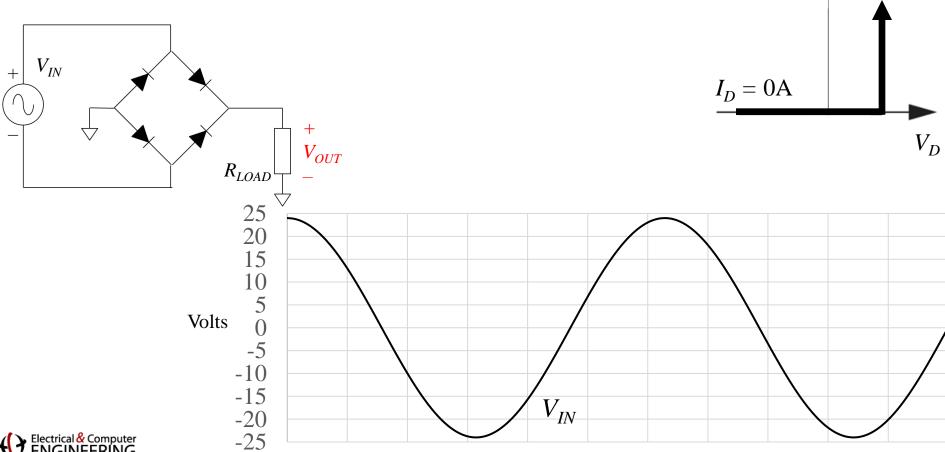
-25



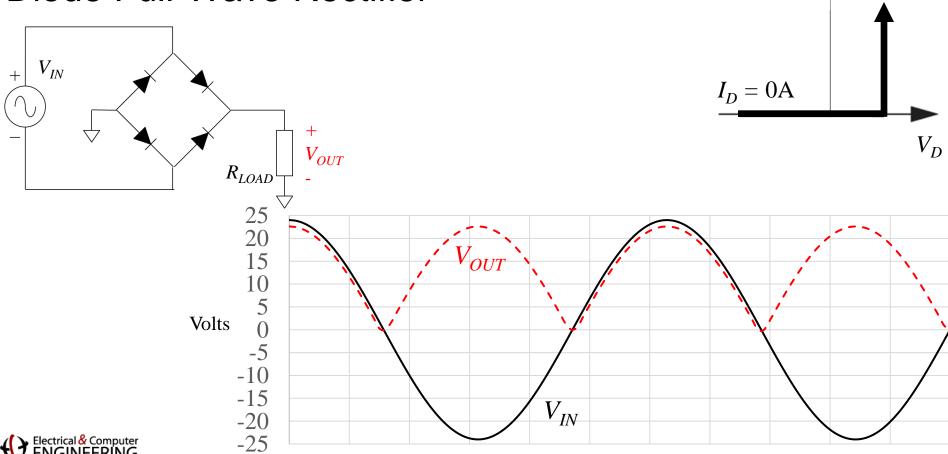




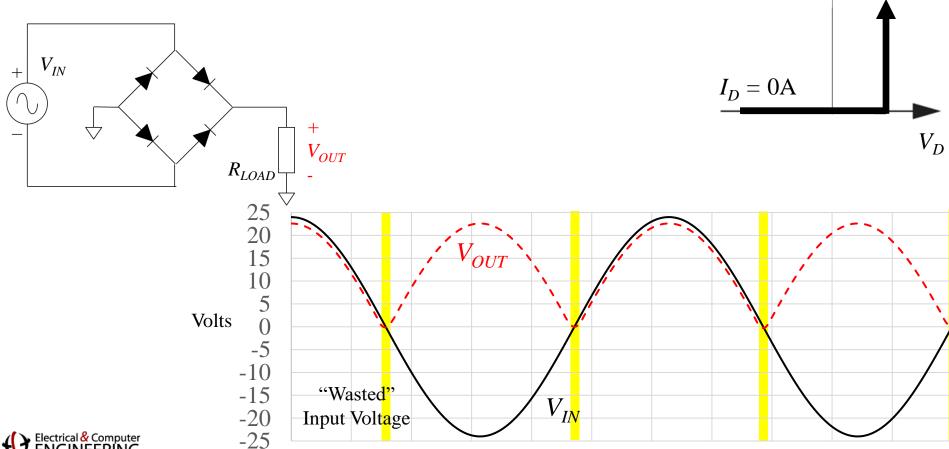


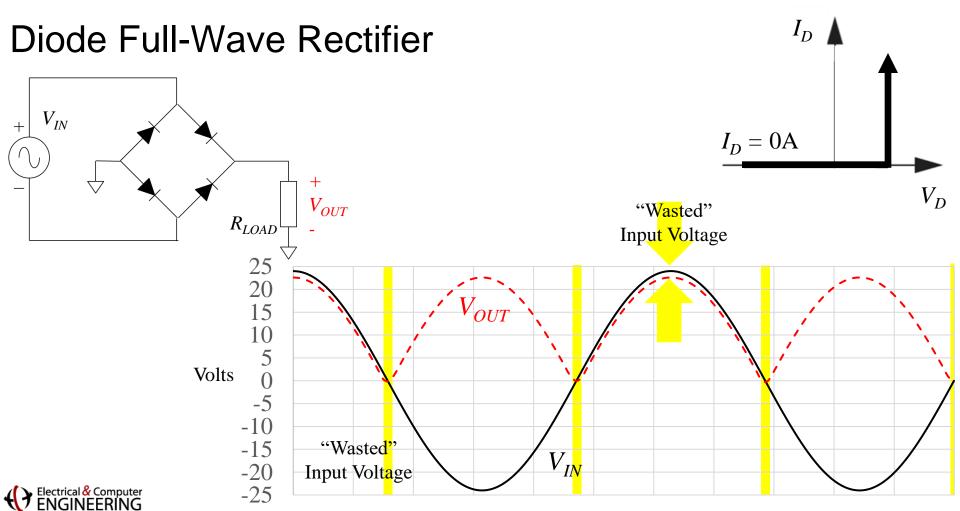


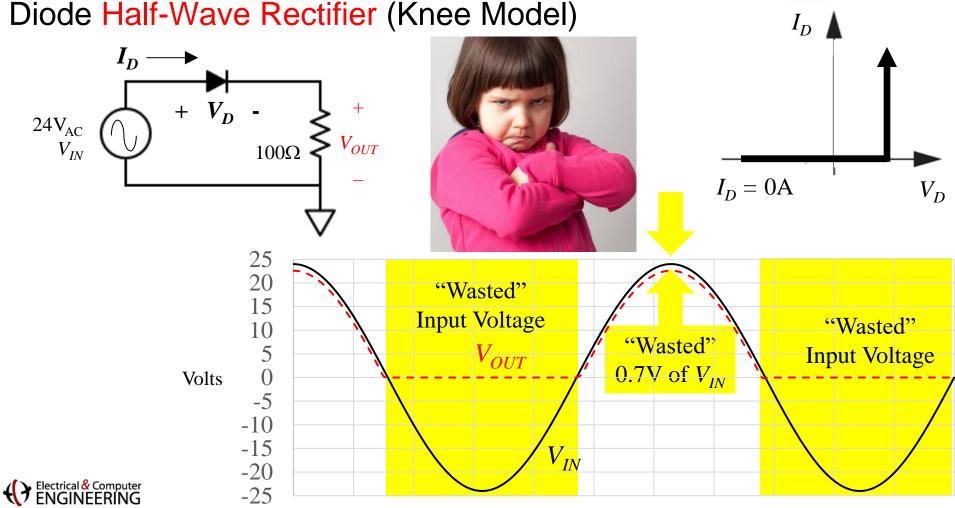


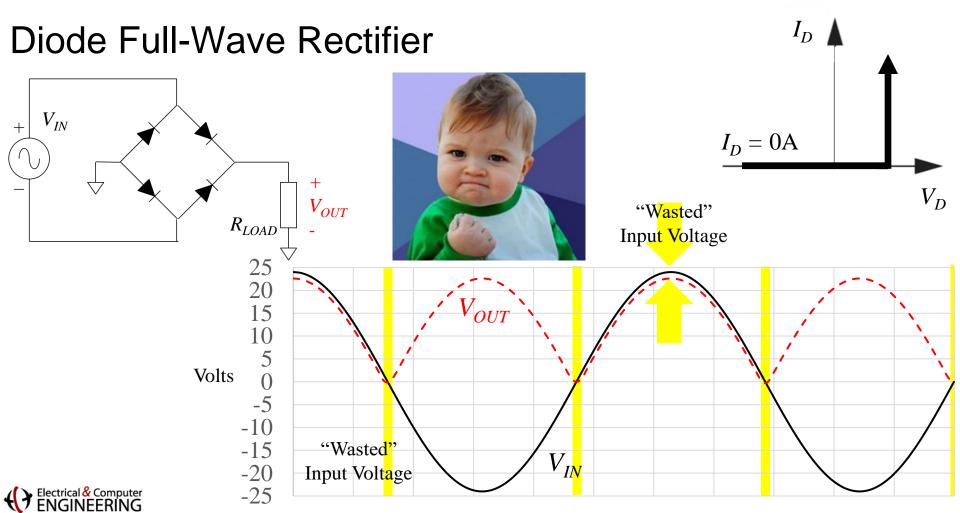


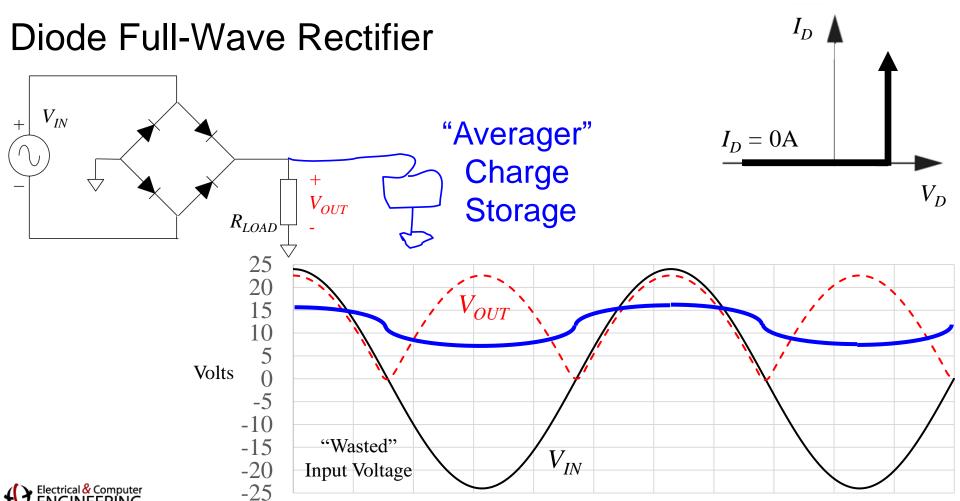


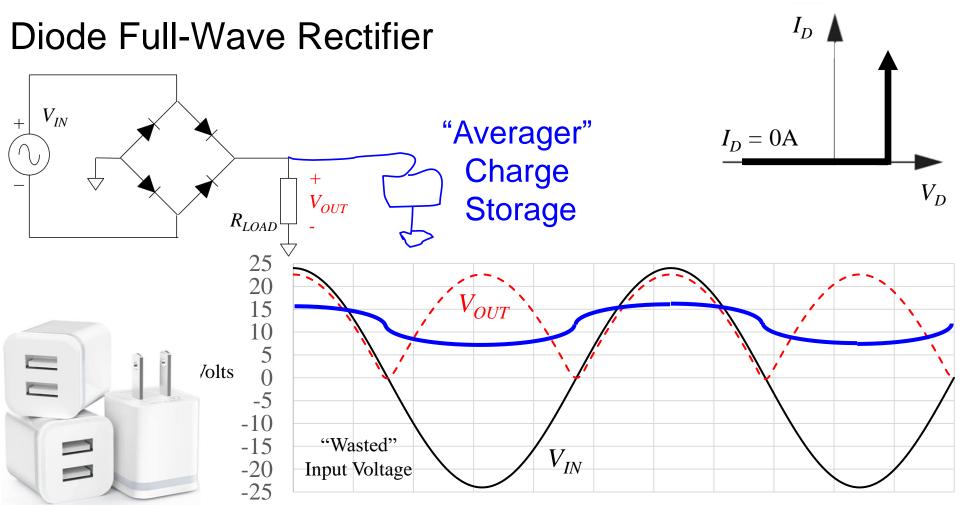






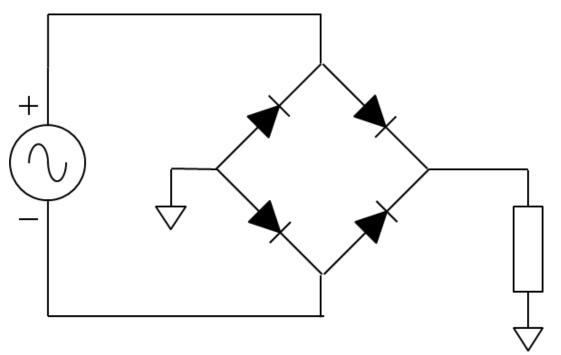


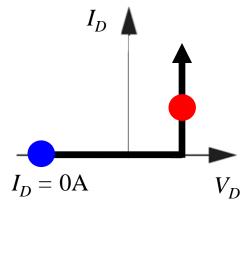




#### Diode Full-Wave Rectifier

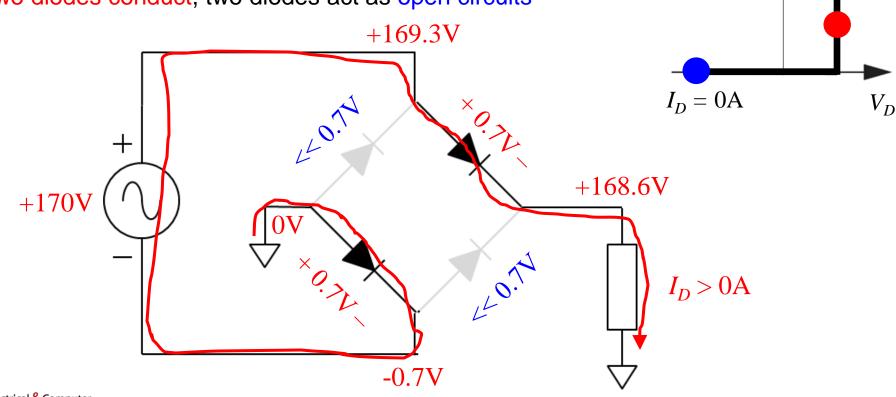
• Two diodes conduct, two diodes act as open circuits





#### Diode Full-Wave Rectifier

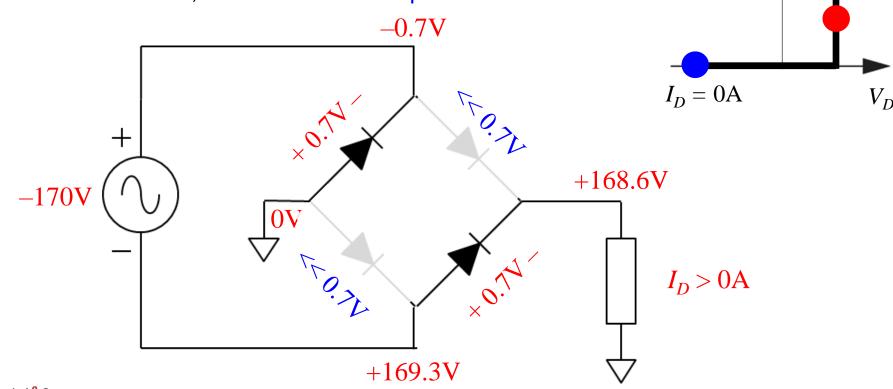
Two diodes conduct, two diodes act as open circuits





### Diode Full-Wave Rectifier

Two diodes conduct, two diodes act as open circuits





#### What Do You Need to Do Next?

- 1. Take the **Lecture 4 Quiz** on canvas!
- 2. Check out Piazza and Gradescope

