



Dynamics of Open Chains

CS 6341 Robotics

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Robot Dynamics

- Dynamic equations (equations of motion)

$$M(\theta) \in \mathbb{R}^{n \times n}$$

Mass matrix

$$h(\theta, \dot{\theta}) \in \mathbb{R}^n$$

Centripetal, Coriolis, gravity, friction

$$\tau = M(\theta)\ddot{\theta} + h(\theta, \dot{\theta})$$

$$\tau \in \mathbb{R}^n$$

Joint forces and torques

$$\theta \in \mathbb{R}^n$$

Joint variables

This equation can be very complex

Robot Dynamics

- Forward dynamics

- Given robot state $(\theta, \dot{\theta})$ and the joint forces and torques \mathcal{T}
- Determine the robot's acceleration $\ddot{\theta}$

$$\ddot{\theta} = M^{-1}(\theta) (\tau - h(\theta, \dot{\theta}))$$

Simulation

- Inverse dynamics

- Given robot state $(\theta, \dot{\theta})$ and a desired acceleration $\ddot{\theta}$ (from motion planning)
- Find the joint forces and torques \mathcal{T}

$$\tau = M(\theta) \ddot{\theta} + h(\theta, \dot{\theta})$$

Control

Robot Dynamics

- How to find this equation for a robot manipulator?

$$\tau = M(\theta)\ddot{\theta} + h(\theta, \dot{\theta})$$

Last Lecture: Dynamics of a Single Rigid Body

- Body twist $\mathcal{V}_b = (\omega_b, v_b)$

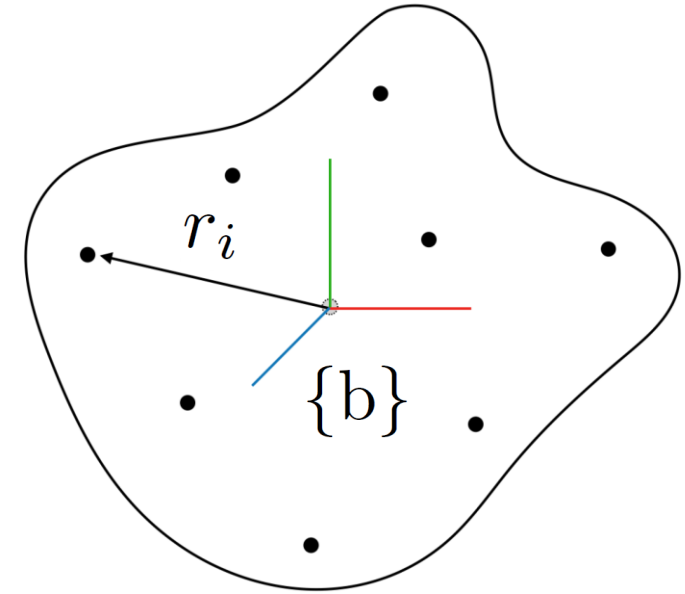
- Linear dynamics

$$f_b = \mathbf{m}(\dot{v}_b + [\omega_b]v_b)$$

- Rotational dynamics

$$m_b = \mathcal{I}_b \dot{\omega}_b + [\omega_b] \mathcal{I}_b \omega_b$$

$$\mathcal{I}_b = - \sum_i \mathbf{m}_i [r_i]^2 \in \mathbb{R}^{3 \times 3}$$



Twist-Wrench Formulation

- Linear dynamics $f_b = \mathbf{m}(\dot{v}_b + [\omega_b]v_b)$
- Rotation dynamics $m_b = \mathcal{I}_b\dot{\omega}_b + [\omega_b]\mathcal{I}_b\omega_b$

$$\begin{bmatrix} m_b \\ f_b \end{bmatrix} = \begin{bmatrix} \mathcal{I}_b & 0 \\ 0 & \mathbf{m}I \end{bmatrix} \begin{bmatrix} \dot{\omega}_b \\ \dot{v}_b \end{bmatrix} + \begin{bmatrix} [\omega_b] & 0 \\ 0 & [\omega_b] \end{bmatrix} \begin{bmatrix} \mathcal{I}_b & 0 \\ 0 & \mathbf{m}I \end{bmatrix} \begin{bmatrix} \omega_b \\ v_b \end{bmatrix}$$

Body wrench

Spatial inertia matrix

Spatial momentum

Body twist

$$\mathcal{F}_b = \begin{bmatrix} m_b \\ f_b \end{bmatrix}$$

$$\mathcal{G}_b = \begin{bmatrix} \mathcal{I}_b & 0 \\ 0 & \mathbf{m}I \end{bmatrix}$$

$$\mathcal{G}_b \in \mathbb{R}^{6 \times 6}$$

$$\mathcal{P}_b = \begin{bmatrix} \mathcal{I}_b\omega_b \\ \mathbf{m}v_b \end{bmatrix}$$

$$= \begin{bmatrix} \mathcal{I}_b & 0 \\ 0 & \mathbf{m}I \end{bmatrix} \begin{bmatrix} \omega_b \\ v_b \end{bmatrix} = \mathcal{G}_b \mathcal{V}_b$$

$$\mathcal{P}_b \in \mathbb{R}^6$$

$$\mathcal{V}_b = \begin{bmatrix} \omega_b \\ v_b \end{bmatrix}$$

Twist-Wrench Formulation

$$\mathcal{F}_b = \mathcal{G}_b \dot{\mathcal{V}}_b - \begin{bmatrix} [\omega_b] & 0 \\ 0 & [\omega_b] \end{bmatrix} \mathcal{G}_b \mathcal{V}_b$$

We can show that (see Lynch & Park 8.2.2)

Lie bracket of twist

$$\begin{aligned} \mathcal{F}_b &= \mathcal{G}_b \dot{\mathcal{V}}_b - \text{ad}_{\mathcal{V}_b}^T(\mathcal{P}_b) \\ &= \mathcal{G}_b \dot{\mathcal{V}}_b - [\text{ad}_{\mathcal{V}_b}]^T \mathcal{G}_b \mathcal{V}_b \end{aligned}$$

$$[\text{ad}_{\mathcal{V}_b}] = \begin{bmatrix} [\omega_b] & 0 \\ [v_b] & [\omega_b] \end{bmatrix}$$

$$\tau = M(\theta)\ddot{\theta} + h(\theta, \dot{\theta})$$

Dynamics of a Single Rigid Body

- Inverse dynamics

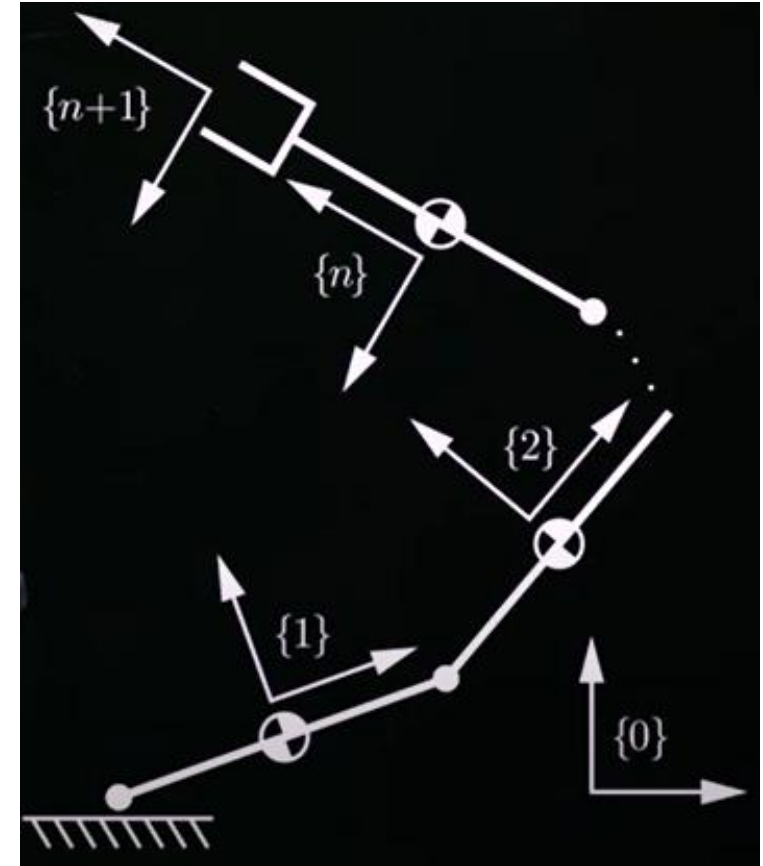
$$\mathcal{F}_b = \mathcal{G}_b \dot{\mathcal{V}}_b - [\text{ad}_{\mathcal{V}_b}]^T \mathcal{G}_b \mathcal{V}_b$$

- Forward dynamics

$$\dot{\mathcal{V}}_b = \mathcal{G}_b^{-1} (\mathcal{F}_b + [\text{ad}_{\mathcal{V}_b}]^T \mathcal{G}_b \mathcal{V}_b)$$

Inverse Dynamics of Open Chains

- N-link open chain
- A body-fixed reference frame $\{i\}$ is attached to the center of mass of each link i
- Base frame $\{0\}$, end-effector frame $\{n+1\}$ (fixed in $\{n\}$)

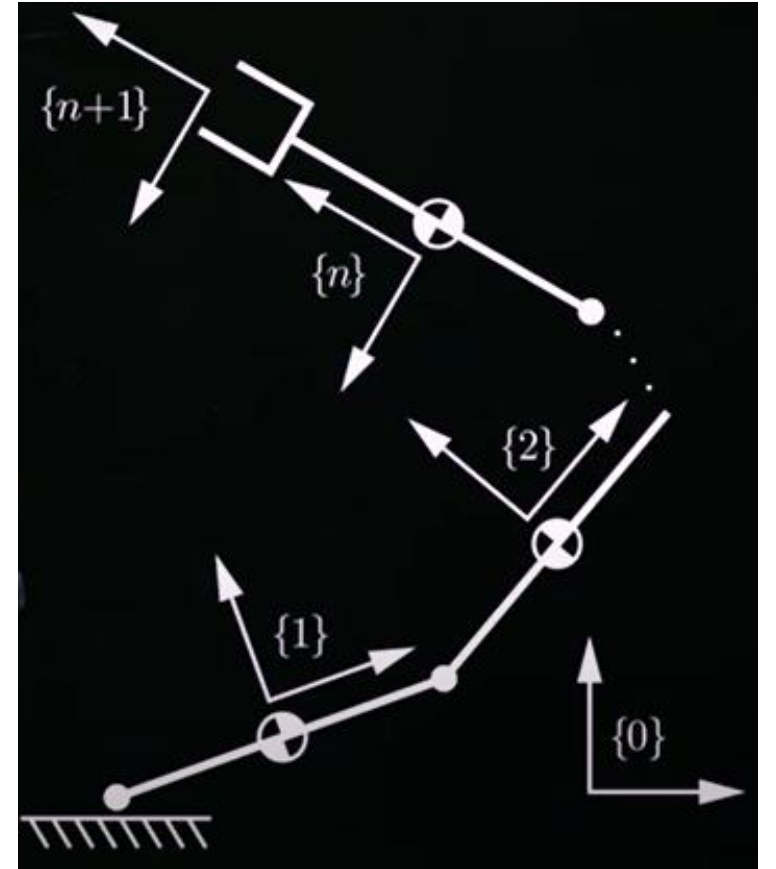


Inverse Dynamics of Open Chains

- At home position (all joints are zeros)
 - Configuration of frame $\{j\}$ in $\{i\}$ $M_{i,j} \in SE(3)$
 - Configuration of $\{i\}$ in base frame $\{0\}$ $M_i = M_{0,i}$

$$M_{i-1,i} = M_{i-1}^{-1} M_i$$

$$M_{i,i-1} = M_i^{-1} M_{i-1}$$

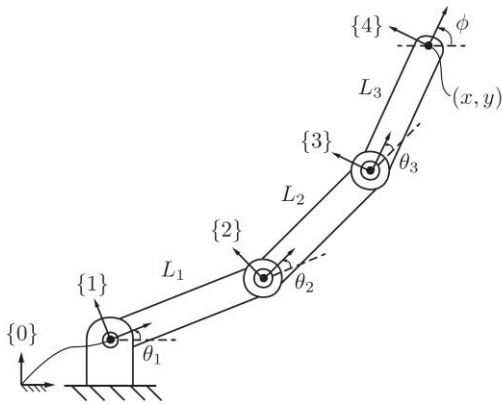


Inverse Dynamics of Open Chains

- Screw axis for joint i in link frame $\{i\}$ \mathcal{A}_i , in space frame $\{0\}$ \mathcal{S}_i

$$\mathcal{A}_i = \text{Ad}_{M_i^{-1}}(\mathcal{S}_i)$$

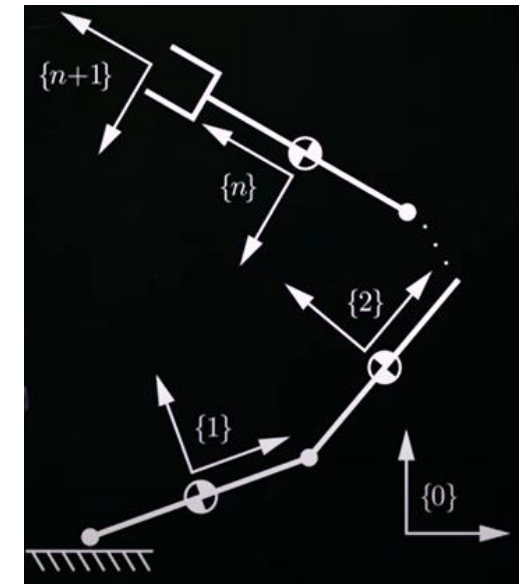
- Recall screw axis



$$\mathcal{S}_a = [\text{Ad}_{T_{ab}}] \mathcal{S}_b$$

$$\mathcal{S}_3 = \begin{bmatrix} \omega_3 \\ v_3 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 1 \\ 0 \\ -(L_1 + L_2) \\ 0 \end{bmatrix}$$

$$[\text{Ad}_T] = \begin{bmatrix} R & 0 \\ [p]R & R \end{bmatrix} \in \mathbb{R}^{6 \times 6}$$



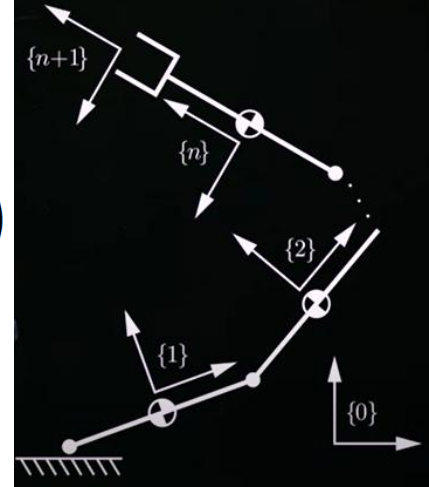
Inverse Dynamics of Open Chains

- Screw axis for joint i in link frame $\{i\}$ \mathcal{A}_i , in space frame $\{0\}$ \mathcal{S}_i
- The configuration of $\{j\}$ in $\{i\}$ with joint variables $T_{i,j} \in SE(3)$

$$T_{i-1,i}(\theta_i)$$

$$T_{i,i-1}(\theta_i) = T_{i-1,i}^{-1}(\theta_i)$$

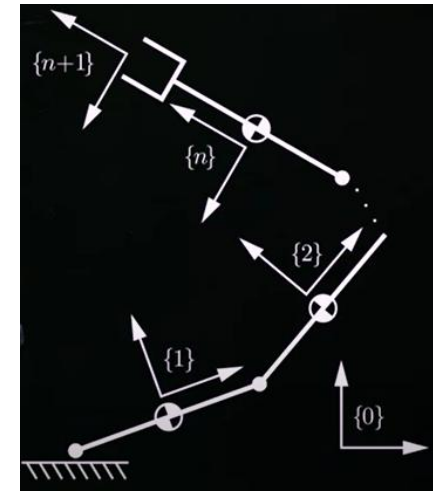
$$T_{i-1,i}(\theta_i) = M_{i-1,i} e^{[\mathcal{A}_i]\theta_i} \quad T_{i,i-1}(\theta_i) = e^{-[\mathcal{A}_i]\theta_i} M_{i,i-1}$$



- Twist of link frame $\{i\}$ expressed in $\{i\}$ $\mathcal{V}_i = (\omega_i, v_i)$
- Wrench transmitted through joint i to link frame $\{i\}$ expressed in $\{i\}$

$$\mathcal{F}_i = (m_i, f_i)$$

Inverse Dynamics of Open Chains



- Spatial inertia matrix of link i $\mathcal{G}_i \in \mathbb{R}^{6 \times 6}$ $\mathcal{G}_i = \begin{bmatrix} \mathcal{I}_i & 0 \\ 0 & m_i I \end{bmatrix}$

- Recursively calculate the twist and acceleration, moving from the base to the tip

$$\mathcal{V}_i = \underset{\substack{\uparrow \\ \text{Twist from joint } i}}{\mathcal{A}_i \dot{\theta}_i} + [\text{Ad}_{T_{i,i-1}}] \underset{\substack{\uparrow \\ \text{Twist from previous link } i-1}}{\mathcal{V}_{i-1}} \quad (\text{Velocity for link } i)$$

$$\dot{\mathcal{V}}_i = \mathcal{A}_i \ddot{\theta}_i + [\text{Ad}_{T_{i,i-1}}] \dot{\mathcal{V}}_{i-1} + \frac{d}{dt} ([\text{Ad}_{T_{i,i-1}}]) \mathcal{V}_{i-1}$$

See Lynch & Park for derivation

$$\dot{\mathcal{V}}_i = \mathcal{A}_i \ddot{\theta}_i + [\text{Ad}_{T_{i,i-1}}] \dot{\mathcal{V}}_{i-1} + [\text{ad}_{\mathcal{V}_i}] \mathcal{A}_i \dot{\theta}_i \quad [\text{ad}_{\mathcal{V}}] = \begin{bmatrix} [\omega] & 0 \\ [v] & [\omega] \end{bmatrix} \in \mathbb{R}^{6 \times 6}$$

Inverse Dynamics of Open Chains

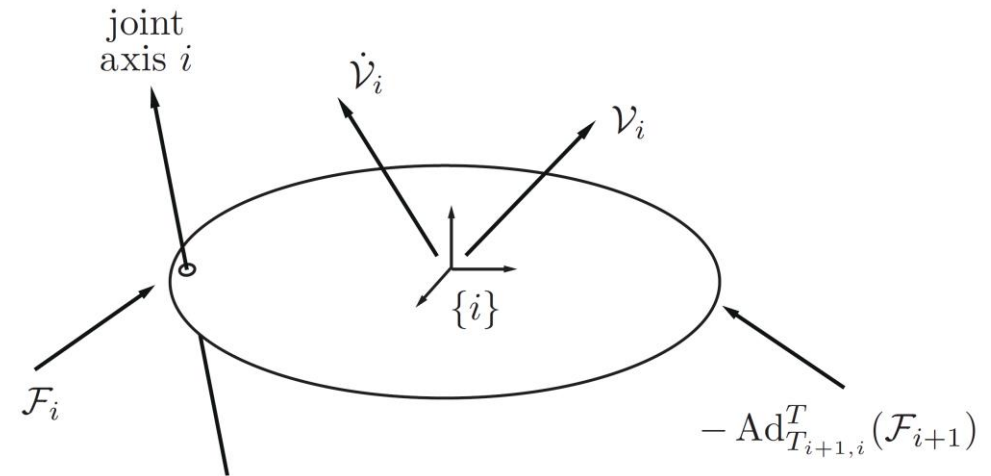
- Accelerations from base to tip

$$\mathcal{F}_b = [\text{Ad}_{T_{ab}}]^T \mathcal{F}_a$$

$$\dot{\mathcal{V}}_i = \mathcal{A}_i \ddot{\theta}_i + [\text{Ad}_{T_{i,i-1}}] \dot{\mathcal{V}}_{i-1} + [\text{ad}_{\mathcal{V}_i}] \mathcal{A}_i \dot{\theta}_i$$

- Recall rigid body dynamic equations

$$\begin{aligned} \mathcal{F}_b &= \mathcal{G}_b \dot{\mathcal{V}}_b - \text{ad}_{\mathcal{V}_b}^T (\mathcal{P}_b) \\ &= \mathcal{G}_b \dot{\mathcal{V}}_b - [\text{ad}_{\mathcal{V}_b}]^T \mathcal{G}_b \mathcal{V}_b \end{aligned}$$



- Wrench on link i from joint i and joint i+1

$$\mathcal{G}_i \dot{\mathcal{V}}_i - \text{ad}_{\mathcal{V}_i}^T (\mathcal{G}_i \mathcal{V}_i) = \mathcal{F}_i - \text{Ad}_{T_{i+1,i}}^T (\mathcal{F}_{i+1})$$

Inverse Dynamics

- Solve the wrench from tip to base \mathcal{F}_i
- Force or torque at the joint in the direction of the joint's screw axis

$$\tau_i \dot{\theta}_i = \mathcal{F}_i^T \mathcal{A}_i \dot{\theta}_i$$

Principle of conservation of power

$$\tau_i = \mathcal{F}_i^T \mathcal{A}_i$$

Power = force × velocity

- Newton-Euler Inverse Dynamics Algorithm

Newton-Euler Inverse Dynamics Algorithm

Given $\theta, \dot{\theta}, \ddot{\theta}$ Compute \mathcal{T}

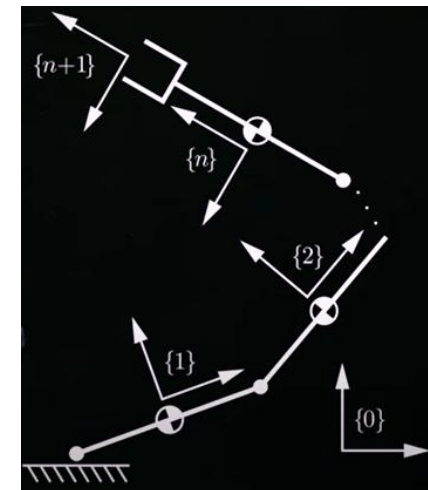
Forward iterations Given $\theta, \dot{\theta}, \ddot{\theta}$, for $i = 1$ to n do

$$\begin{aligned}\mathcal{V}_0 &= (0, 0) & T_{i,i-1} &= e^{-[\mathcal{A}_i]\theta_i} M_{i,i-1}, \\ \dot{\mathcal{V}}_0 &= (0, -g) & \mathcal{V}_i &= \text{Ad}_{T_{i,i-1}}(\mathcal{V}_{i-1}) + \mathcal{A}_i \dot{\theta}_i, \\ & & \dot{\mathcal{V}}_i &= \text{Ad}_{T_{i,i-1}}(\dot{\mathcal{V}}_{i-1}) + \text{ad}_{\mathcal{V}_i}(\mathcal{A}_i) \dot{\theta}_i + \mathcal{A}_i \ddot{\theta}_i.\end{aligned}$$

Backward iterations For $i = n$ to 1 do

$$\begin{aligned}\mathcal{F}_{n+1} &= \mathcal{F}_{\text{tip}} \\ &= (m_{\text{tip}}, f_{\text{tip}}) \\ \mathcal{F}_i &= \text{Ad}_{T_{i+1,i}}^T(\mathcal{F}_{i+1}) + \mathcal{G}_i \dot{\mathcal{V}}_i - \text{ad}_{\mathcal{V}_i}^T(\mathcal{G}_i \mathcal{V}_i), \\ \tau_i &= \mathcal{F}_i^T \mathcal{A}_i.\end{aligned}$$

The wrench applied to the environment by the end-effector



Statics of Open Chains

- Principle of conservation of power

power at the joints = (power to move the robot) + (power at the end-effector)

- Considering the robot to be at static equilibrium (no power to move robot)

$$\tau^T \dot{\theta} = \mathcal{F}_b^T \mathcal{V}_b \quad \text{power at the end-effector}$$

$$\mathcal{V}_b = J_b(\theta) \dot{\theta}$$

$$\tau = J_b^T(\theta) \mathcal{F}_b$$

Statics of Open Chains

- If an external wrench $-\mathcal{F}$ is applied to the end-effector when the robot is at equilibrium, joint torque to keep the robot at equilibrium

$$\tau = J^T(\theta)\mathcal{F}$$

- Equations of motion with external wrench on the end-effector

$$\tau - J^T(\theta)\mathcal{F}_{\text{tip}} = M(\theta)\ddot{\theta} + h(\theta, \dot{\theta})$$

Forward Dynamics of Open Chains

- Forward dynamics $M(\theta)\ddot{\theta} = \tau(t) - h(\theta, \dot{\theta}) - J^T(\theta)\mathcal{F}_{\text{tip}}$
 - Given $\theta, \dot{\theta}, \tau, \mathcal{F}_{\text{tip}}$ Solve $\ddot{\theta}$
- $h(\theta, \dot{\theta})$ can be computed by the inverse dynamics algorithm with $\ddot{\theta} = 0$ and $\mathcal{F}_{\text{tip}} = 0$
- We can solve

$$M\ddot{\theta} = b, \text{ for } \ddot{\theta}$$

$$b = \tau(t) - h(\theta, \dot{\theta}) - J^T(\theta)\mathcal{F}_{\text{tip}}$$

Forward Dynamics of Open Chains

- Simulate the motion of a robot

$$\ddot{\theta} = \textit{ForwardDynamics}(\theta, \dot{\theta}, \tau, \mathcal{F}_{\text{tip}})$$

First-order differential equations

$$\begin{aligned} q_1 &= \theta, \quad q_2 = \dot{\theta} & \dot{q}_1 &= q_2, \\ & & \dot{q}_2 &= \textit{ForwardDynamics}(q_1, q_2, \tau, \mathcal{F}_{\text{tip}}) \end{aligned}$$

First-order Euler iteration

$$\begin{aligned} q_1(t + \delta t) &= q_1(t) + q_2(t)\delta t, \\ q_2(t + \delta t) &= q_2(t) + \textit{ForwardDynamics}(q_1, q_2, \tau, \mathcal{F}_{\text{tip}})\delta t \end{aligned}$$

Initial values $q_1(0) = \theta(0)$ and $q_2(0) = \dot{\theta}(0)$

Summary

- Robot Dynamics
- Newton-Euler Inverse Dynamics Algorithm
- Forward Dynamics of Open Chains

Further Reading

- Sections 3.4, 4.3 and Chapter 8 in Kevin M. Lynch and Frank C. Park. Modern Robotics: Mechanics, Planning, and Control. 1st Edition, 2017.